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Hw2

Problem 1

$$\underline{x} = \begin{pmatrix} 1 \\ 2 \\ 3 \end{pmatrix}, \quad \underline{\sigma}(\underline{x}) = \begin{bmatrix} 1 & 0 & 2y \\ 0 & 1 & 4x \\ 2y & 4x & 1 \end{bmatrix} \text{ ksi} = \begin{bmatrix} 1 & 0 & 4 \\ 0 & 1 & 4 \\ 4 & 4 & 1 \end{bmatrix} \text{ ksi}$$

plane we study $x+y+z = 6 \text{ in}$, $\underline{n} = \frac{1}{\sqrt{3}} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$

$$a) \underline{T}(\underline{n}) = \underline{\sigma} \underline{n} = \frac{1}{\sqrt{3}} \begin{bmatrix} 1 & 0 & 4 \\ 0 & 1 & 4 \\ 4 & 4 & 1 \end{bmatrix} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \frac{1}{\sqrt{3}} \begin{pmatrix} 5 \\ 5 \\ 9 \end{pmatrix} \text{ ksi}$$

$$b) \underline{T}_n(\underline{n}) = \underline{n}^T \underline{T} \underline{n} = \left(\frac{1}{\sqrt{3}} \right)^3 \begin{bmatrix} 1 & 1 & 1 \end{bmatrix} \begin{pmatrix} 5 \\ 5 \\ 9 \end{pmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \end{bmatrix} \begin{pmatrix} 5 \\ 5 \\ 9 \end{pmatrix} = \frac{1}{3} \begin{pmatrix} 19 \end{pmatrix} = \frac{19}{3} \text{ ksi}$$

$$\underline{T} = \underline{T}_n + \underline{T}_t, \quad \underline{T}_t = \underline{T} - \underline{T}_n = \frac{1}{3} \begin{pmatrix} 5 \\ 5 \\ 9 \end{pmatrix} - \frac{19}{3} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \approx 3.66 \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \text{ ksi}$$

$$c) = \begin{pmatrix} (5)3^{-\frac{1}{2}} & -(19)3^{-\frac{3}{2}} \\ (5)3^{-\frac{1}{2}} & -(19)3^{-\frac{3}{2}} \\ (9)3^{-\frac{1}{2}} & -(19)3^{-\frac{3}{2}} \end{pmatrix} \text{ ksi} \approx \begin{pmatrix} -0.77 \\ -0.77 \\ 1.54 \end{pmatrix} \text{ ksi}$$

$$|\underline{\sigma} - \lambda \underline{1}| = 0 = \begin{vmatrix} 1-\lambda & 0 & 4 \\ 0 & 1-\lambda & 4 \\ 4 & 4 & 1-\lambda \end{vmatrix} = -\lambda^3 + 3\lambda^2 + 24\lambda - 31$$

from the cubic equation, $\lambda_1 = 1 + 4\sqrt{2}$
 $\lambda_2 = 1$
 $\lambda_3 = 1 - 4\sqrt{2}$

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$$(\underline{\sigma} - \lambda \underline{1}) \underline{s} = 0$$

$$4z - x\lambda + x = 0$$

$$4z - y\lambda + y = 0$$

$$4x + 4y - z\lambda + z = 0$$

Plugging in

gives

$$\sigma_1 = 1 + 4\sqrt{2} \text{ ksi} \quad s_1 = \frac{1}{2} \begin{pmatrix} 1 \\ 1 \\ \sqrt{2} \end{pmatrix} \text{ in}$$

$$\sigma_2 = 1 \text{ ksi} \quad s_2 = \frac{\sqrt{2}}{2} \begin{pmatrix} -1 \\ 1 \\ 0 \end{pmatrix} \text{ in}$$

$$\sigma_3 = 1 - 4\sqrt{2} \text{ ksi} \quad s_3 = \frac{1}{2} \begin{pmatrix} -1 \\ -1 \\ \sqrt{2} \end{pmatrix} \text{ in}$$

$$\sigma_n = \frac{1}{3} \text{tr} \underline{\sigma} = 1 \text{ ksi}$$

$$\underline{\sigma}_{dev} = \underline{\sigma} - \sigma_n \underline{1}$$

$$\begin{bmatrix} 0 & 0 & 4 \\ 0 & 0 & 4 \\ 4 & 4 & 0 \end{bmatrix} \text{ ksi}$$

$$\sigma_e = \left(\frac{3}{2} \sum_{\alpha=\beta}^3 \sum_{\alpha=\beta}^3 (\sigma_{dev \alpha \beta})^2 \right)^{1/2} = \sqrt{\frac{3}{2} (4)(4^2)} = \sqrt{96} \text{ ksi}$$

$$\sigma_y = 15.6 \text{ ksi}, \quad F = 1.5$$

tresca, yield if $F \tau_{max} \geq \frac{\sigma_y}{2}$

$$\tau_{max} = \frac{1}{2} (\sigma_1 - \sigma_3) = 4\sqrt{2}$$

$$F \tau_{max} = 6\sqrt{2} \approx 8.4853 \text{ ksi}$$

$$\frac{\sigma_y}{2} = 7.8$$

So tresca predicts yielding

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Von mises yield if $\sigma_e \geq \sigma_y$

$$\sigma_e \approx 9.798 \text{ ksi}$$

So von mises predicts there will not be yield

Problem 2 - see matlab

housecleaning

```
clear all
close all
clc

% sympref('FloatingPointOutput',true)
% sympref('FloatingPointOutput',false)
addpath('C:\joshFunctionsMatlab\')
```

Problem 2

```
clear

% Torque
syms T
assume(1<T)

% givens
p = 100/1000; % ksi
r = 25;
t = .1;
A = pi*r^2;

% stress state
sigHoop = p*r/t;
sigAxial = p*r/(2*t);
tau = T/(2*t*A);

sig0 = [[sigAxial,tau,0];[tau,sigHoop,0];[0,0,0]];

% stress state in principle reference frame
[S,sig0] = eig(sig0);
temp = [sig0(1,1),sig0(2,2),sig0(3,3)];
[temp,I] = sort(temp,'descend');
sig0 = [[temp(1),0,0];[0,temp(2),0];[0,0,temp(3)]];

S = [S(:,I(1)),S(:,I(2)),S(:,I(3))];
clear temp I

% hydrostatic, deviatoric, max shear, effective stress
sig_h = (1/3)*trace(sig0);
sig_dev = sig0 - sig_h*eye(3);

sig_e = ((3/2)*sum(sum(sig_dev.^2)))^(1/2);
tau_max = (1/2)*(sig0(1,1)-sig0(3,3));

% solve for T
sig_y = 30; % ksi
eqn1 = tau_max == sig_y/2;
eqn2 = sig_e == sig_y;
```

```

sol1 = solve(eqn1,T);
sol2 = solve(eqn2,T);

temp = [sig0(1,1),sig0(2,2),sig0(3,3)];
disp('The principle stresses are in ksi are: ')
disp(temp')
disp('While using the tresca yeild criterion, T can be as high as
'+string(sol1)+' = '+string(vpa(sol1,5))+' kip-in.')
disp('While using the von mises yeild criterion, T can be as high as
'+string(sol2)+' = '+string(vpa(sol2,5))+' kip-in.')
disp('We can conclude that tresca yeild condition is more conservative than
von mises yeild condition because ')

```

The principle stresses are in ksi are:

$$\frac{(9375\pi + (16T^2 + 9765625\pi^2)^{1/2})}{(500\pi)}$$

$$\frac{(9375\pi - (16T^2 + 9765625\pi^2)^{1/2})}{(500\pi)}$$
0

While using the tresca yeild criterion, T can be as high as

$$(625 \cdot 14^{1/2} \pi) / 2 = 3673.4 \text{ kip-in.}$$
While using the von mises yeild criterion, T can be as high as

$$(625 \cdot 23^{1/2} \pi) / 2 = 4708.3 \text{ kip-in.}$$
We can conclude that tresca yeild condition is more conservative than von
mises yeild condition because the yield torque is lower for the tresca critirion than
The von mises

Published with MATLAB® R2022a