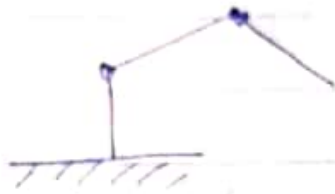


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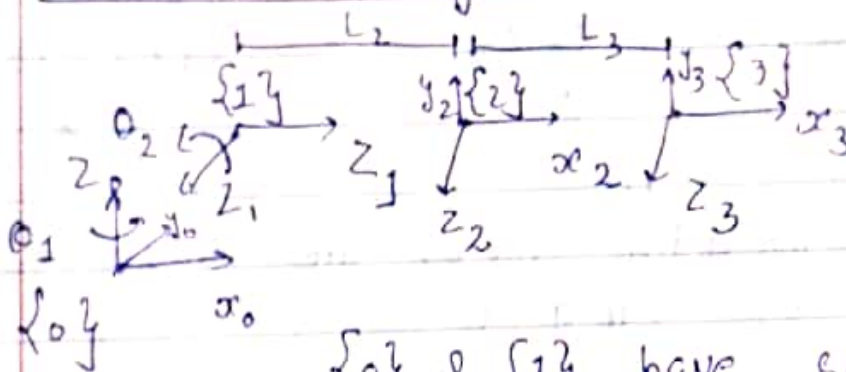
## Robotics - Assignment 2

A1



Each link has its com at centre.

### DH Frame Assignment



{0} & {1} have same origin

| Link i | $a_i$ | $\alpha_i$ | $d_i$ | $\theta_i$ | $q_i$ | $\cos \alpha_i$ | $\sin \alpha_i$ |
|--------|-------|------------|-------|------------|-------|-----------------|-----------------|
| 1      | 0     | $90^\circ$ | 0     | $\theta_1$ | $q_1$ | 0               | 1               |
| 2      | $L_2$ | 0          | 0     | $\theta_2$ | $q_2$ | 1               | 0               |
| 3      | $L_3$ | 0          | 0     | $\theta_3$ | $q_3$ | 1               | 0               |

$$\rightarrow {}^0T_1 = \begin{bmatrix} c_1 & 0 & s_1 & 0 \\ s_1 & 0 & -c_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^1T_2 = \begin{bmatrix} c_2 & -s_2 & 0 & L_2 c_2 \\ s_2 & c_2 & 0 & L_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^2T_3 = \begin{bmatrix} c_3 & -s_3 & 0 & L_3 c_3 \\ s_3 & c_3 & 0 & L_3 s_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \Rightarrow {}^0T_2 = \begin{bmatrix} c_1 c_2 & -c_1 s_2 & s_1 & L_2 c_1 c_2 \\ s_1 c_2 & -s_1 s_2 & -c_1 & L_2 s_1 c_2 \\ s_2 & c_2 & 0 & L_2 s_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

(2)

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finally,  ${}^0T_3 = {}^0T_1 {}^1T_2 {}^2T_3$

$$\Rightarrow \begin{bmatrix} c_1 c(\theta_2 + \theta_3) & -c_1 s(\theta_2 + \theta_3) & s_1 & c_1 [L_3 c_{23} + L_2 c_2] \\ s_1 c(\theta_2 + \theta_3) & -s_1 s(\theta_2 + \theta_3) & -c_1 & s_1 [L_3 c_{23} + L_2 c_2] \\ s(\theta_2 + \theta_3) & c(\theta_2 + \theta_3) & 0 & L_3 s_{23} + L_2 s_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

→ Now, for interactive forces, we have :-

$$F_{0,1} - F_{1,2} + m_1 g = 0$$

$$F_{1,2} - F_{2,3} + m_2 g = 0$$

$$F_{2,3} - F_{3,4} + m_3 g = 0$$

(\*) ⇒ Now, for simplification, we assume  $L_2 = L_3 = a$  and  $m_1 = m_2 = m$ .

So, we have  ${}^{i-1}r_i = {}^i r_{i+1} - {}^0R_i (-{}^i\sigma_j)$

$$* (-F_{i,i+2}) - {}^0R_{i-1} ({}^{i-1}\sigma_i + {}^i\sigma_j) \\ * F_{i-1,i}$$

→ Now finding all ' $\sigma$ ' vectors,

$${}^3\sigma_3 = {}^2\sigma_2 = \begin{bmatrix} -a/2 \\ 0 \\ 0 \end{bmatrix}; {}^1r_1 = \begin{bmatrix} 0 \\ -a/2 \\ 0 \end{bmatrix}$$

(3)

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$${}^2\mathbf{r}_3 = \begin{bmatrix} a c_3 \\ a s_3 \\ 0 \end{bmatrix}$$

$${}^0\mathbf{r}_1 = \begin{bmatrix} 0 \\ 0 \\ a \end{bmatrix}$$

$${}^1\mathbf{r}_2 = \begin{bmatrix} a c_2 \\ a s_2 \\ 0 \end{bmatrix}$$

$$\Rightarrow \mathbf{F}_{3,P} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \text{ kgf} \quad \mathbf{r}_{3,m} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

All wot  $\{0\}$ .

$$\mathbf{F}_{23} = \mathbf{F}_{3P} - m_3 \mathbf{g} \Rightarrow \mathbf{g} = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$$

$$\text{So, } \mathbf{F}_{23} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ -mg \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ m \end{bmatrix} \text{ kg force}$$

$$\text{Similarly, } \mathbf{F}_{12} = \mathbf{F}_{23} - m \mathbf{g} = \begin{bmatrix} 1 \\ 0 \\ 2m \end{bmatrix} \text{ kg}$$

$$\& \mathbf{F}_{01} = \mathbf{F}_{12} - m \mathbf{g} = \begin{bmatrix} 1 \\ 0 \\ 3m \end{bmatrix} \text{ kg}$$



(4)

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(\*) Now, taking home position simplification,  
 $q_i = 0 \quad \forall i$

So,  $I_{34}$  becomes  $\begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$

Also,  $I_{23} = I_{34} - {}^0R_3 \begin{bmatrix} -3r_3 & -f_{31} \end{bmatrix} - {}^0R_2 ({}^2r_3 + {}^3r_3) f_{23}$

$$\Rightarrow I_{23} = \begin{bmatrix} 1 \\ 0 \\ am/2 \end{bmatrix} \text{ kg-cm} \quad \underline{\text{Ans}}$$

Similarly  $I_{12} = \begin{bmatrix} 1 \\ 0 \\ am \end{bmatrix} \text{ kg-cm} \quad \underline{\text{Ans}}$

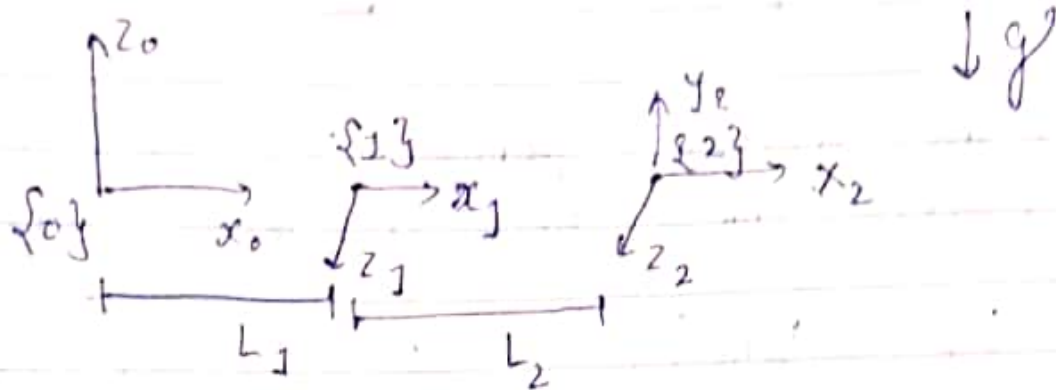
$$\text{d } I_{01} = \begin{bmatrix} \frac{5am}{2} + 1 \\ -a/2 \\ am - a/2 \end{bmatrix} \text{ kg-cm} \quad \underline{\text{Ans}}$$

\* The general form of  $I_{01}$  comes as :-

$$\begin{bmatrix} 1 + L_2 m_3 c_2 s_{1/2} - L_3 m_3 s_1 (2c_{23} - c_2) + \frac{L_1 m_{33}}{2} - \frac{L_2 s_1 \sigma_2 m_3}{2} \\ \frac{L_1}{2} - \frac{L_3 s_{23}}{2} - \frac{L_2 s_2}{2} + \frac{L_3 s_2}{2} + \frac{L_2 c_1 \sigma_2 m_{33}}{2} + \frac{L_3 s_3 c_1 \sigma_1}{2} \\ -\frac{L_1}{2} - \frac{s_1}{2} [L_2 - L_3 c_{23}] - \frac{s_1 L_2}{2} + \frac{L_3 c_2 s_1}{2} \end{bmatrix}$$

5

A22 i) Lagrange-Euler Approach.



D-H params

| i | $a_i$ | $\alpha_i$ | $d_i$ | $\theta_i$ | $\dot{\theta}_i$ | $C\theta_i$ | $S\theta_i$ |
|---|-------|------------|-------|------------|------------------|-------------|-------------|
| 1 | $L_1$ | $90^\circ$ | 0     | $\theta_1$ | $\dot{\theta}_1$ | $C_1$       | $S_1$       |
| 2 | $L_2$ | 0          | 0     | $\theta_2$ | $\dot{\theta}_2$ | $C_2$       | $S_2$       |

$$\Rightarrow {}^0T_1 = \begin{bmatrix} C_1 & 0 & S_1 & L_1 \\ S_1 & 0 & -C_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^1T_2 = \begin{bmatrix} C_2 & -S_2 & 0 & L_2 C_2 \\ S_2 & C_2 & 0 & L_2 S_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0T_2 = \begin{bmatrix} C_1 S_2 & -C_1 S_2 & S_1 & L_2 C_1 C_2 + L_1 C_1 \\ S_1 S_2 & -S_1 S_2 & -C_1 & L_2 S_1 C_2 + L_1 S_1 \\ S_2 & C_2 & 0 & L_2 S_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

6

$$a_1 = a_2 = \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad \text{Since, } \{i\} \text{ \& } \{j\} \text{ are R.}$$

→ The Inertial frames  $I_1$  &  $I_2$  for 2 slender links with COM at centre are:-

$$I_1 = \begin{bmatrix} \frac{1}{3} m_1 L_1^2 & 0 & 0 & -\frac{1}{2} m_1 L_1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ -\frac{1}{2} m_1 L_1 & 0 & 0 & m_1 \end{bmatrix} \quad \begin{array}{l} I_{xx} = 0 \\ I_{xy} = I_{yz} = I_{xz} = 0 \\ I_{yy} = m_1 L_1^2 / 3 \\ I_{zz} = m_1 L_1^2 / 3 \end{array}$$

$$I_2 = \begin{bmatrix} \frac{1}{3} m_2 L_2^2 & 0 & 0 & -\frac{1}{2} m_2 L_2 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ -\frac{1}{2} m_2 L_2 & 0 & 0 & m_2 \end{bmatrix} \quad \begin{array}{l} I_{xx} = 0 \\ I_{xy} = I_{yz} = I_{xz} = 0 \\ I_{yy} = m_2 L_2^2 / 3 \\ I_{zz} = m_2 L_2^2 / 3 \end{array}$$

$$\rightarrow d_{11} = \partial^0 I_1 / \partial \theta_1 = \begin{bmatrix} -s_1 & 0 & c_1 & -L_1 s_1 \\ c_1 & 0 & s_1 & L_1 c_1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$d_{12} = \frac{\partial^0 I_1}{\partial \theta_2} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$d_{21} = \frac{\partial^0 I_2}{\partial \theta_1} = \begin{bmatrix} s_1 c_2 - s_1 s_2 & c_1 & -L_2 s_1 c_2 - L_1 s_1 \\ c_1 c_2 - s_1 s_2 & s_1 & L_2 c_1 c_2 + L_1 c_1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$



(7)

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$$d_{22} = \frac{\partial^2 T_2}{\partial \dot{\theta}_2^2} = \begin{bmatrix} -c_1 s_2 & -c_1 c_2 & 0 & -L_2 c_1 s_2 \\ -s_1 s_2 & -s_1 c_2 & 0 & -L_2 s_1 s_2 \\ c_2 & -s_2 & 0 & L_2 c_2 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\Rightarrow M_{ij} = \sum_{p=1}^n T_p \left[ d_{pi} I_p d_{pj} \right]$$

$$\Rightarrow M_{11} = T_1 (d_{11} I_1 d_{11}) + T_2 (d_{21} I_2 d_{21})$$

$$= m_1 L_1^2 / 3 + m_2 L_2^2 + m_2 L_1 L_2 c_2 + 2m_2 L_2^2 c_2 / 3$$

$$\Rightarrow M_{22} = T_2 (d_{22} I_2 d_{22})$$

$$= m_2 L_2^2 / 3$$

$$\Rightarrow M_{21} = M_{12} = T_2 (d_{22} I_2 d_{21})$$

$$= 0$$

$\Rightarrow$  The coriolis & centrifugal force coefficient can be calculated as

$$h_{ijk} = \sum_{p=1}^n T_p \left[ \frac{\partial (d_{pk})}{\partial \dot{q}_{ic}} I_p d_{pi} \right]$$

{ here  $n = 2$  }

8

$$\Rightarrow h_{111} = h_{222} = 0 \quad \left\{ T_2 \left\{ \frac{\partial d_{11}}{\partial \theta_1} I_2 d_{21} \right\} \right\}$$

$$h_{122} = 0$$

$$h_{211} = T_2 \left\{ \frac{\partial d_{11}}{\partial \theta_1} I_2 d_{21} \right\} = \frac{m_2 L_2 S_2}{6} (3L_1 + 2L_2)$$

$$h_{221} = h_{212} = T_2 \left( \frac{\partial d_{21}}{\partial \theta_1} I_2 d_{21} \right)$$

$$= \frac{m_2 L_2 S_2}{6} [3L_1 + 3L_2 C_2]$$

$$h_{121} = h_{112} = 0$$

$$\Rightarrow H_i = \sum_{j=1}^n \sum_{k=1}^n h_{ijk} \dot{\theta}_j \dot{\theta}_k$$

$$H_1 = 0$$

$$H_2 = h_{211} \dot{\theta}_1^2 + h_{212} \dot{\theta}_1 \dot{\theta}_2 + h_{221} \dot{\theta}_1 \dot{\theta}_2 + h_{222} \dot{\theta}_2^2$$

$$\Rightarrow {}^1 \dot{\bar{x}}_1 = {}^2 \dot{\bar{x}}_2 = \begin{bmatrix} -\frac{L_1}{2} & 0 & 0 & 1 \end{bmatrix}' = \begin{bmatrix} -\frac{L_2}{2} & 0 & 0 & 1 \end{bmatrix}'$$

Gravity is in  $-z_0$  direction.

$$g = \begin{bmatrix} 0 & 0 & -g & 0 \end{bmatrix}$$

$$F_{g1} = \begin{bmatrix} m_1 g d_{11} {}^1 \bar{x}_1 + m_2 g d_{21} {}^2 \bar{x}_2 \\ = 0 \end{bmatrix}$$



Now, Jacobian using principle of virtual work to find joint torques of payload.

$$J = \begin{bmatrix} -L_2 S_1 C_2 - L_1 S_1 & -L_2 C_1 S_2 \\ L_2 C_1 C_2 + L_1 C_1 & -L_2 S_1 S_2 \\ 0 & L_2 C_2 \\ 0 & S_1 \\ 0 & -C_1 \\ 1 & 0 \end{bmatrix}$$

$$\delta f_{ext} = \begin{bmatrix} 0 & 0 & -W & 0 & 0 & 0 \end{bmatrix}'$$

$$T_{ext} = J(q)' \cdot f_{ext} = \begin{bmatrix} 0 & -L_2 C_2 W \end{bmatrix}'$$

$$\Rightarrow \begin{bmatrix} T_1 \\ T_2 \end{bmatrix} = \begin{bmatrix} \frac{m_1 L_1^2}{3} + m_2 L_2^2 + m_2 L_1 L_2 C_2 + \frac{2}{3} m_2 L_2^2 C_2 & 0 \\ 0 & m_2 L_2^2 / 3 \end{bmatrix} \begin{bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{bmatrix}$$

$$+ \begin{bmatrix} 0 \\ m_2 g L_2 \frac{L_2}{2} \end{bmatrix} + \begin{bmatrix} 0 \\ -W L_2 C_2 \end{bmatrix}$$

$$+ \begin{bmatrix} 0 \\ \frac{m_2 L_2 S_2}{6} (3L_1 + 2L_2 C_2) (\dot{\theta}_1^2 + 2\dot{\theta}_1 \dot{\theta}_2) \end{bmatrix}$$

{ Using EOM }

(10)

## ii) Newton - Euler Method.

Assuming initial conditions.

$${}^0V_0 = {}^0\omega_0 = {}^0\dot{\omega}_0 = 0 = [0 \ 0 \ 0]^T$$

The transformation & inertial matrix remain same as in previous part.

→ Forward iteration  $i = 1$

$${}^1\omega_1 = {}^1R_0 \cdot [{}^0\omega_0 + \hat{Z}_0 \dot{\theta}_1] = [0 \ 1 \ 0]^T \dot{\theta}_1$$

$${}^1\dot{\omega}_1 = \frac{d}{dt}({}^1R_0 {}^1V_1) = {}^1R_0 {}^0\dot{V}_0 + {}^1\omega_1 \times {}^1R_0 {}^0\dot{V}_1 + {}^1\dot{\omega}_1 \times [{}^1\omega_1 (-{}^1R_0 {}^0D_1)]$$

$$= [-L_1 \dot{\theta}_1^2 \quad g \quad -L_1 \ddot{\theta}_1]^T$$

$${}^1\dot{V}_1 = [-L_1 \dot{\theta}_1^2 / 2 \quad g \quad -L_1 / 2 \ddot{\theta}_1]^T$$

→ Iteration  $i = 2$  :

$${}^2\omega_2 = {}^2R_1 [{}^1\omega_1 + \hat{Z}_1 \dot{\theta}_2] = [s_2 \dot{\theta}_1 \quad c_2 \dot{\theta}_1 \quad \dot{\theta}_2]^T$$

$${}^2\dot{\omega}_2 = {}^2R_1 [{}^1\dot{\omega}_1 + \hat{Z}_1 \ddot{\theta}_2 + {}^2\omega_1 \hat{Z}_1 \dot{\theta}_2]$$

$$= \begin{bmatrix} c_2 \dot{\theta}_1 \dot{\theta}_2 + s_2 \ddot{\theta}_1 \\ -s_2 \dot{\theta}_1 \dot{\theta}_2 + c_2 \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{bmatrix}$$

$${}^2V_2 = {}^2R_1 {}^1\dot{V}_1 + {}^2\omega_2 ({}^2R_0 D_2) + {}^2\omega_2 ({}^2\omega_2 {}^2R_0 D_2)$$

$$= \begin{bmatrix} -L_1 \ddot{\theta}_1^2 c_2 - L_2 \ddot{\theta}_1^2 - L_2 \dot{\theta}_1^2 + g s_2 \\ L_2 \ddot{\theta}_2 + L_1 \ddot{\theta}_1^2 s_2 + s_2 c_2 L_2 \dot{\theta}_1^2 + g c_2 \\ -L_1 \ddot{\theta}_1 - L_2 c_2 \ddot{\theta}_1 + 2 s_2 L_2 \dot{\theta}_1 \dot{\theta}_2 \end{bmatrix}$$

$${}^2\dot{V}_2 = \begin{bmatrix} 0 & -L_2/2 \ddot{\theta}_1 & L_2/2 c_2 \dot{\theta}_1 \end{bmatrix}^T$$

> Backward iterations  $i=2$

Payload  $w \Rightarrow {}^3F_3 = \begin{bmatrix} 0 & -w & 0 \end{bmatrix}^T$

$${}^2F_2 = \ddot{m}_2 = {}^2\dot{V}_2 = m_2 \begin{bmatrix} -L_1 \ddot{\theta}_1^2 c_2 - \frac{L_2}{2} L_2 \dot{\theta}_1^2 + g s_2 \\ \frac{L_2}{2} \ddot{\theta}_2 + L_1 \ddot{\theta}_1^2 s_2 + \frac{L_2}{2} c_2 s_2 \dot{\theta}_1^2 + g c_2 \\ -L_1 \ddot{\theta}_1 - \frac{L_2 c_2 \ddot{\theta}_1}{2} + L_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \end{bmatrix}$$

$${}^2N_2 = \begin{bmatrix} c_2 \dot{\theta}_1 \ddot{\theta}_2 + s_2 \ddot{\theta}_1 \\ s_2 \dot{\theta}_1 \ddot{\theta}_2 \\ -c_2 s_2 \dot{\theta}_1^2 \end{bmatrix} \left\{ \begin{array}{l} I_2 {}^2\omega_2 \\ + 2\omega_2 I_2 {}^2\omega_2 \end{array} \right\}$$

$${}^2F_2 = {}^2F_2 + {}^2R_3 {}^3F_3 \quad {}^2R_3 = [I]_{3 \times 3}$$

$$= \begin{bmatrix} m_2 \left( -L_1 \ddot{\theta}_1^2 c_2 - \frac{L_2}{2} c_2 \dot{\theta}_1^2 - \frac{L_2}{2} \ddot{\theta}_2^2 + g s_2 \right) \\ -w + m_2 \left( \frac{L_2}{2} \ddot{\theta}_2 + L_1 \ddot{\theta}_1^2 s_2 + \frac{L_2}{2} c_2 s_2 \dot{\theta}_1^2 + g c_2 \right) \\ m_2 \left( -L_1 \ddot{\theta}_1 - \frac{L_2 c_2 \ddot{\theta}_1}{2} + L_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \right) \end{bmatrix}$$



(12)

$${}^2\mathcal{L}_2 = {}^2R_3 {}^2m_3 + {}^2R_0 {}^1D_2 + {}^2R_3 {}^3F_3 +$$

$$\left( {}^2R_0 {}^1D_2 + {}^2R_0 {}^2\bar{s}_2 \right) + {}^1F_2 {}^2N_2$$

$$= \begin{bmatrix} -\omega L_2 S_{12} \\ 0 \\ +\omega L_2 C_1 \end{bmatrix} + \frac{L_2}{2} \begin{bmatrix} 2C_1 - C_{12} \\ 2S_1 + S_{12} \\ -2S_{12} + S_1 \end{bmatrix} \times A$$

$$o) {}^1F_i = m_i \ddot{v}_i \quad \{ i=1 \}$$

$$m_1 = \left[ -\frac{L_1}{2} \ddot{\theta}_1^2 \quad g \quad -\frac{L_1}{2} \ddot{\theta}_1' \right]$$

$${}^1N_i = [0 \ 0]$$

$${}^1F_1 = {}^1F_1 + {}^1R_2 {}^2F_2$$

$$\mathcal{L}_1 = {}^1N_1 + {}^1R_0 \hat{z}_0 \quad \text{and}$$

$$\mathcal{L}_2 = {}^2N_2 + {}^2R_1 \hat{z}_0 \quad \{ \text{simplifying} \}$$

$$\begin{bmatrix} \mathcal{L}_1 \\ \mathcal{L}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ -\omega L_2 C_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{2} m_2 g L_2 C_2 \end{bmatrix} + \begin{bmatrix} -\frac{1}{3} m_2 L_2 S_1, (2L_2 C_2 - 1) L_1 \ddot{\theta}_1, \ddot{\theta}_2 \\ 0 \end{bmatrix}$$

$$+ \begin{bmatrix} \frac{1}{3} m_1 L_1^2 + \frac{1}{3} m_2 L_2^2 C_2^2 + m_2 L_1 L_2 C_2 + m_2 L_1^2 & 0 \\ 0 & \frac{1}{3} m_2 L_2^2 \end{bmatrix} \begin{bmatrix} \ddot{\theta}_1' \\ \ddot{\theta}_2' \end{bmatrix}$$