

Individual Demonstration

Basic open loop Converter:

Components:

Ideal Condition:

Turn ratio $N_1:N_2 = 7:4$

$$V_o = \frac{N_2}{N_1} dV_s$$

Duty cycle = 0.4

$L = 32.85\mu H$

$$L = \frac{VTA}{\Delta i_L}$$

$C = 234.375\mu F$

$$C = \frac{ITA}{\Delta V_o}$$

Ripple:

$$\Delta V_o = 0.01 (R_{load} = 8.53\Omega)$$

$$\Delta V_o = 0.01 (R_{load} = 1.28\Omega)$$

Real condition:

Turn ratio $N_1:N_2 = 9:9$

Magnetic Inductance:

$$L_{mag} = 210.6\mu H$$

Duty cycle = 0.27

$L = 42.5\mu H$

C (Output) = $300\mu F$ ESR = 0.05467Ω (0.164Ω for each)

AC Input = $230 \times \sqrt{2} = 325.269 V$

AC Series Resistance = 0.1Ω

AC Series Inductance = $0.001\mu H$

C (Input) = $2mF$ ESR = 0.022Ω (0.044Ω for each)

Rectifier Diode: $V_f = 1.2V, R_{on} = 0.51\Omega$

Diode: $V_f = 1.9V, R_{on} = 0.041\Omega$

MOSFET: $R_{on} = 0.11\Omega$

Ripple:

$$\Delta V_o = 0.09597 (R_{load} = 8.53\Omega)$$

$$\Delta V_o = 0.08477 (R_{load} = 1.28\Omega)$$

Main Transformer (9:9):

$$N = \frac{VTA (Worst)}{\Delta B A_{core}}$$

$$N = \frac{37 \times 0.45 \times 10 \times 10^{-6}}{200 \times 10^{-3} \times 97.1 \times 10^{-3}} = 8.573635$$

$$N = 9$$

$$L_{mag} = A_L N^2 = 2600 \times 10^{-9} \times 9^2$$

$$L_{mag} = 210.6 \mu H$$

$$\hat{i}_{mag} = \frac{V_s dT}{L_{mag}} = 0.49245 A$$

Area of copper required:

$$A_{turn} = \frac{i_{RMS}}{J} = \frac{2.68479}{5 \times 10^6} = 0.53664 \mu m^2$$

$$A_{cu} = N \frac{i_{RMS}}{J} = 4.833 \mu m^2$$

$$A_{turn} = \frac{\pi d^2}{4}$$

$$K_{fill} = \frac{A_{cu}}{A_w} = 0.0396$$

Skin depth:

$$\delta = \sqrt{\frac{2\rho}{2\pi f \mu_r \mu_0}} = 0.2062 mm$$

Effective Area for one wire of (Wire 26 AWG)

$$Effective Area = 0.2^2 \times \pi \times 10^{-6}$$

Number of wires required:

$$number\ of\ wires = \frac{0.53664 \times 10^{-6}}{0.2^2 \times \pi \times 10^{-6}} = 4.27044 \approx 5$$

\therefore Five wires are required

Loss:

$$R_{DC} = \frac{\rho l_{winding}}{A_{turn}} = \frac{1.77 \times 10^{-8} \times 2 \times 9 \times (11.1 + 25.6) \times 10^{-3}}{0.53664 \times 10^{-6}}$$

$$R_{DC} = 0.0209 \Omega$$

$$R_{AC} = \frac{\rho l}{A_{eff}} = 0.0158 \Omega$$

$$R_{AC} < 2 \times R_{DC}$$

Inductor:

Air gap = 0.5mm

Number of turns:

$$N = \sqrt{\frac{gL}{\mu_0 A}} = \sqrt{\frac{0.5 \times 10^{-3} \times 42.5 \times 10^{-6}}{4\pi \times 10^{-7} \times 97.1 \times 10^{-6}}} = 13.1967 \approx 14$$

$$N = 14$$

Peak Flux Density:

$$\hat{B} = \sqrt{\frac{\mu_0 L}{gA}} \hat{i} = \sqrt{\frac{4\pi \times 10^{-7} \times 42.5 \times 10^{-6}}{0.5 \times 10^{-3} \times 97.1 \times 10^{-6}}} \times 6.41246 = 212.68 \text{mT}$$

$$B_{\text{hat}} < B_{\text{sat}} (400 \text{mT})$$

Area of copper required:

$$A_{\text{turn}} = \frac{i_{\text{RMS}}}{J} = \frac{5.16309}{5 \times 10^6} = 1.032618 \mu\text{m}^2$$

$$A_{\text{cu}} = N \frac{i_{\text{RMS}}}{J} = 14.456652 \mu\text{m}^2$$

$$A_{\text{turn}} = \frac{\pi d^2}{4}$$

$$K_{\text{fill}} = \frac{A_{\text{cu}}}{A_{\text{w}}} = 0.11849$$

Skin depth:

$$\delta = \sqrt{\frac{2\rho}{2\pi f \mu_r \mu_0}} = 0.2062 \text{mm}$$

Effective Area for one wire of (Wire 26 AWG)

$$\text{Effective Area} = 0.2^2 \times \pi \times 10^{-6}$$

Number of wires required:

$$\text{number of wires} = \frac{1.032618 \times 10^{-6}}{0.2^2 \times \pi \times 10^{-6}} = 8.2173 \approx 9$$

∴ Nine wires are required

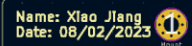
Loss:

$$R_{\text{DC}} = \frac{\rho l_{\text{winding}}}{A_{\text{turn}}} = \frac{1.77 \times 10^{-8} \times 60.5 \times 14 \times 10^{-3}}{0.53664 \times 10^{-6}}$$

$$R_{\text{DC}} = 0.0145 \Omega$$

$$R_{AC} < 2 \times R_{DC}$$

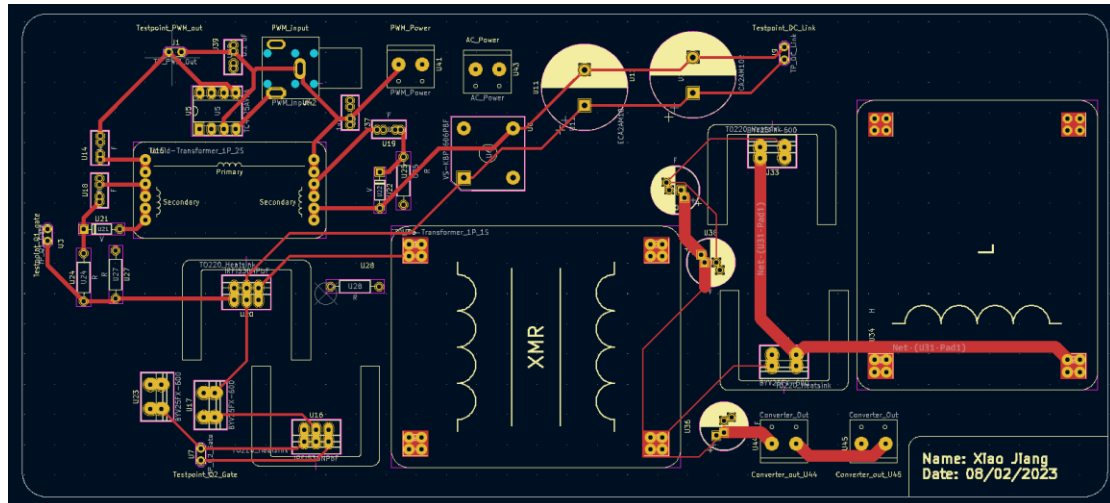
Front:



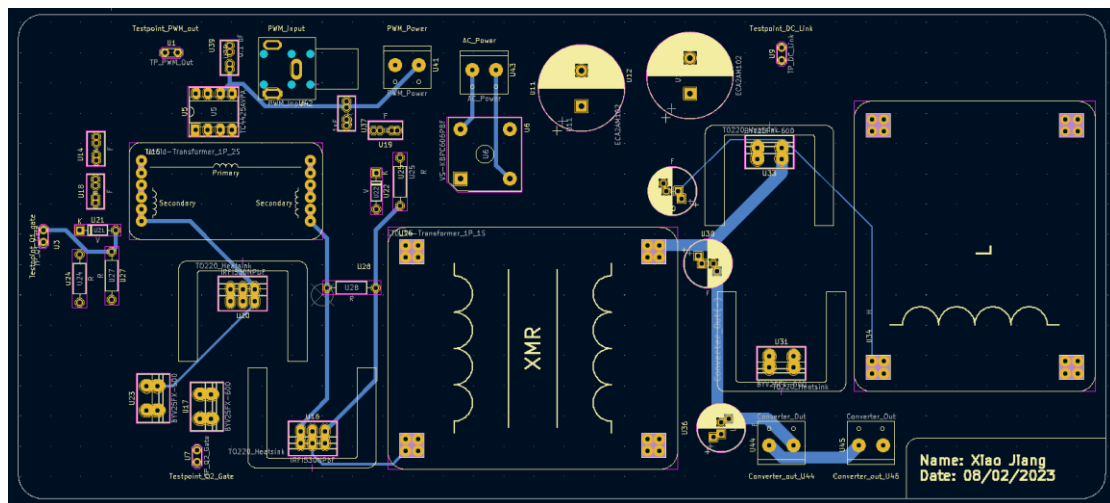
Name: Xiao Jiang
Date: 08/02/2023

Modified:

Front:



Back:



Control and Closed Loop:

Calculation code:

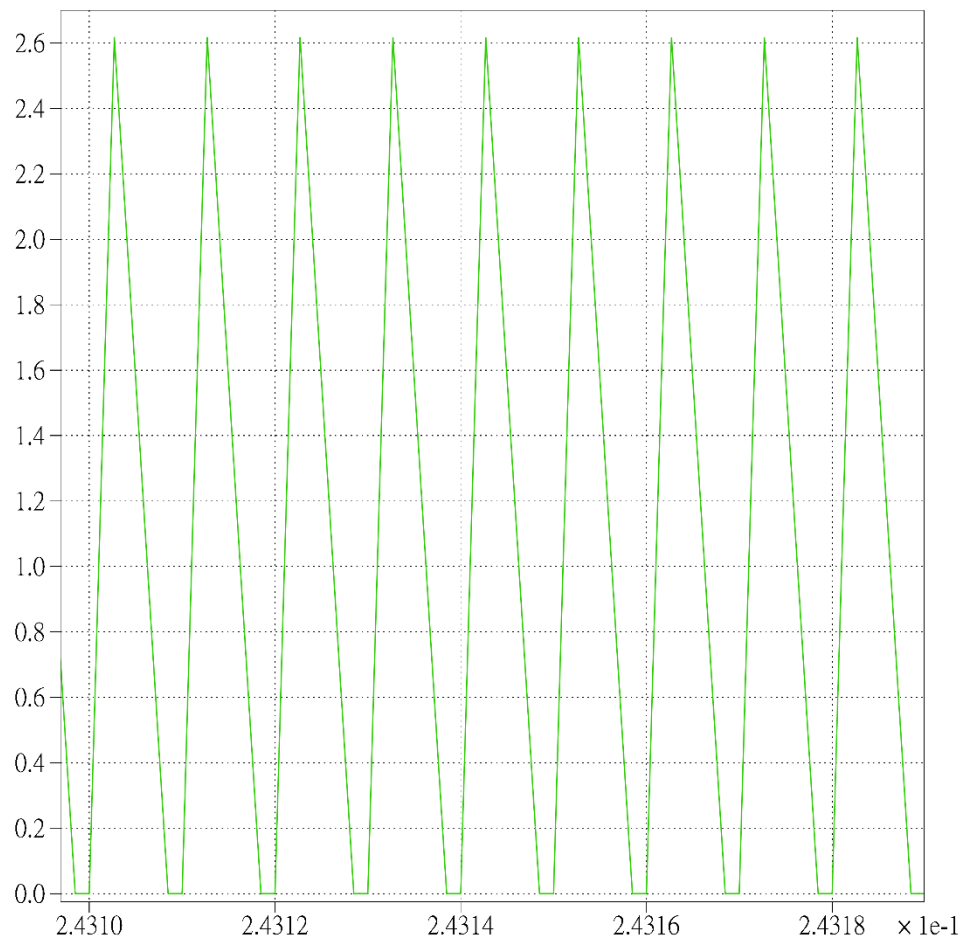
Type1:

```
% Parameters
Rc = 0.05477;
Rload_thres = 8.53;
L = 42.5e-6;
C = 300e-6;
Wc = 1/(10*sqrt(L*C));
n = 1; % Transformer turns ratio
Ra1 = 22000; % Amplifier Potential Divider 1
Ra2 = 10000;
a = Ra2/(Ra1+Ra2); % Amplifier Potential Divider Ratio
Vin = 39.5; % Max Voltage Input (AC)
dmax = 0.45; % PWM
Kpwm = dmax/(3.8-0.5);
Kmisc = n*a*Vin*Kpwm;
% Transfer function for filter circuit
Gf = tf([Rc*C 1], [L*C (L/Rload_thres)+C*Rc 1])
% bode(Gf)
% margin(Gf)
% Magnitude of Gc at wc
%Gfjwc = (Rc*C*Wc*i+1)/(-1*L*C*(Wc)^2+((L/Rload_thres)+C*Rc)*Wc*i+1);
[mag, phase]=bode(Gf,Wc);
G = 1/Kmisc*abs(mag);
A = G*Wc;
Gc = tf([A], [1 0])
Gloop = Gc*Gf*Kmisc;
margin(Gloop);
R1=12000;
C1=1/(A*R1)
```

Type 3:

```
%%
% Parameters
Rc = 0.05477;
Rload_thres = 8.53;
L = 42.5e-6;
C = 1410e-6;
Wc = 7*1/sqrt(L*C)
n = 1; % Transformer turns ratio
Ra1 = 22000; % Amplifier Potential Divider 1
Ra2 = 10000;
a = Ra2/(Ra1+Ra2); % Amplifier Potential Divider Ratio
Vin = 50; % Max Voltage Input (AC)
dmax = 0.45; % PWM
Kpwm = dmax/(3.8-0.5);
Kmisc = n*a*Vin*Kpwm;
% Transfer function for filter circuit
Gf = tf([Rc*C 1], [L*C (L/Rload_thres)+C*Rc 1])
% bode(Gf)
% margin(Gf)
% Magnitude of Gc at wc
%Gfjwc = (Rc*C*Wc*i+1)/(-1*L*C*(Wc)^2+((L/Rload_thres)+C*Rc)*Wc*i+1);
[mag,phase]=bode(Gf,Wc)
%margin(Gf);
phaseMargin=60;
boost=phaseMargin-180+90-phase;
k=(tand((boost/4)+45))^2;
R1=2200;
G=1/(Kmisc*mag);
A=G*Wc/k;
C2=1/(R1*Wc*G);
C1=C2*(k-1);
R2=sqrt(k)/(Wc*C1);

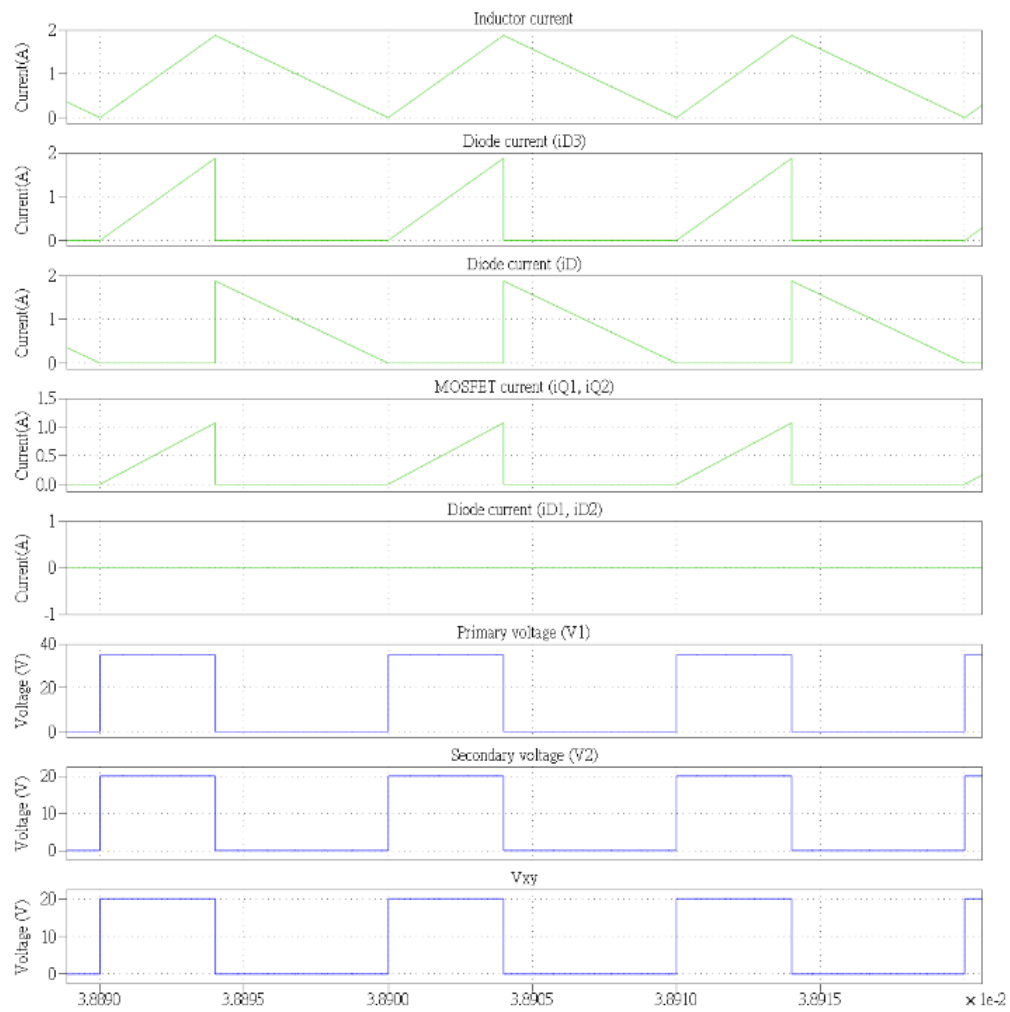
R3=R1/(k-1);
C3=1/(R3*Wc*sqrt(k));
Wz1=1/(C1*R2);
Wp1=(C1+C2)/(C2*C1*R2);
Wz2=1/(C3*(R1+R3));
Wp2=1/(C3*R3);
Ga=tf([A], [1 0]);
Gb=tf([1/Wz1 1], [1/Wp1 1]);
Gc=Ga*Gb*Gb;
Gloop=Gc*Gf*Kmisc;
margin(Gloop);
```



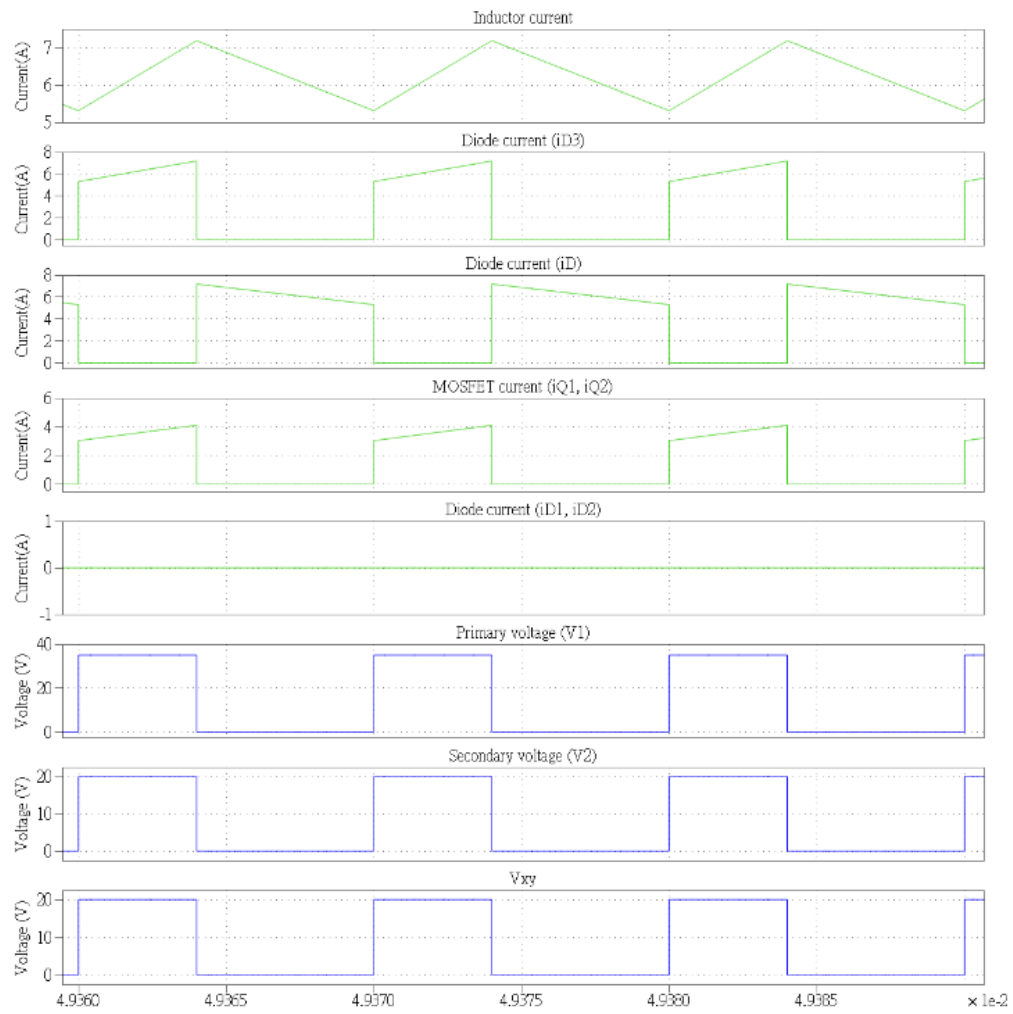
Waveform:

Ideal:

Threshold:

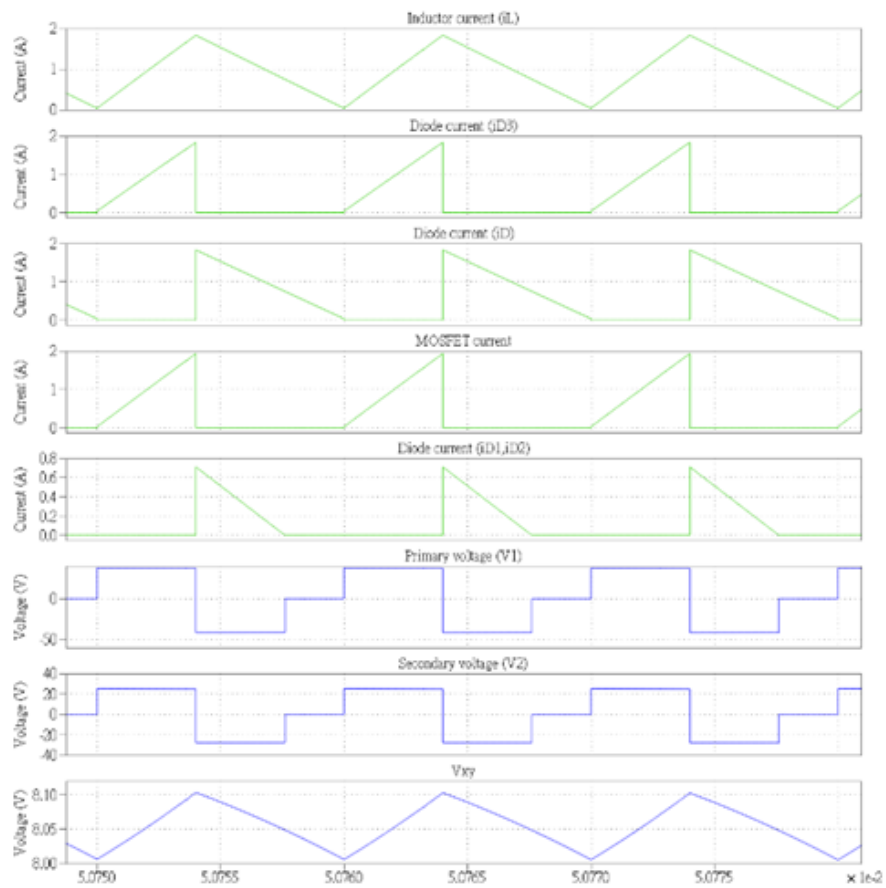


Rated:

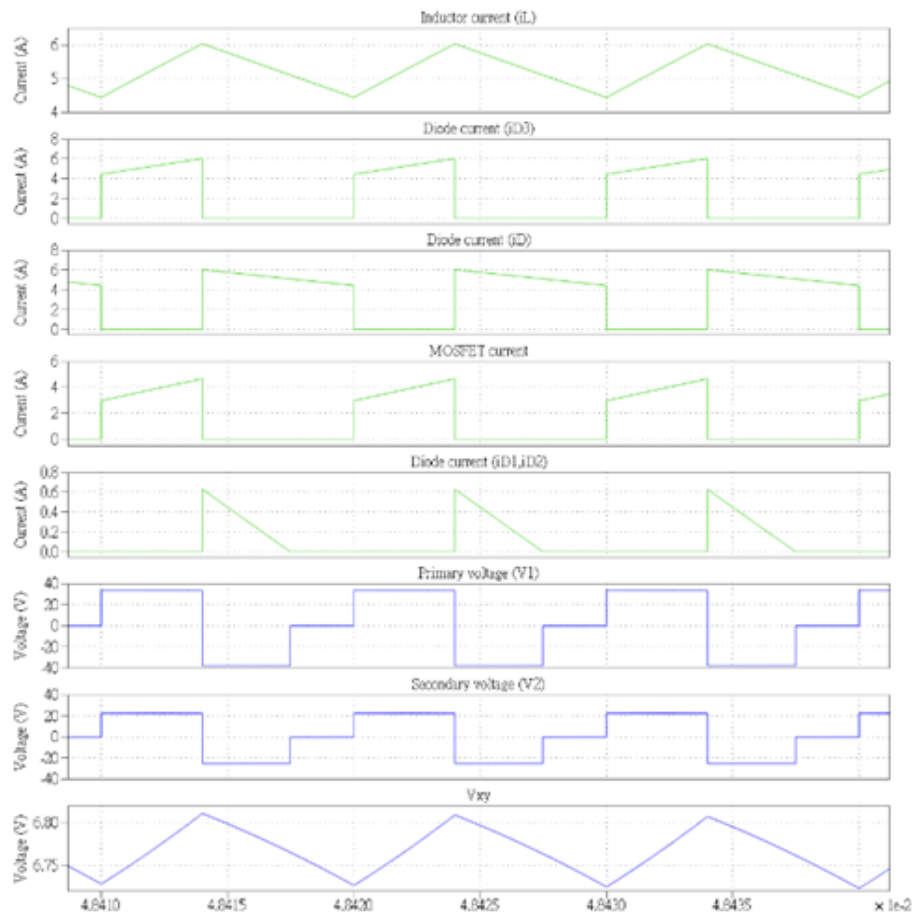


Real:

Threshold:



Rated:



Imag:

Calaulated:0.49245

