

# Computer Exercise 4

## EL2520 Control Theory and Practice

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### Minimum phase case

#### Dynamic decoupling

The dynamic decoupling in exercise 3.2.1 is

$$W(s) = \begin{bmatrix} 1 & -\frac{0.01476}{s + 0.0213} \\ -\frac{0.01336}{s + 0.02572} & 1 \end{bmatrix}$$

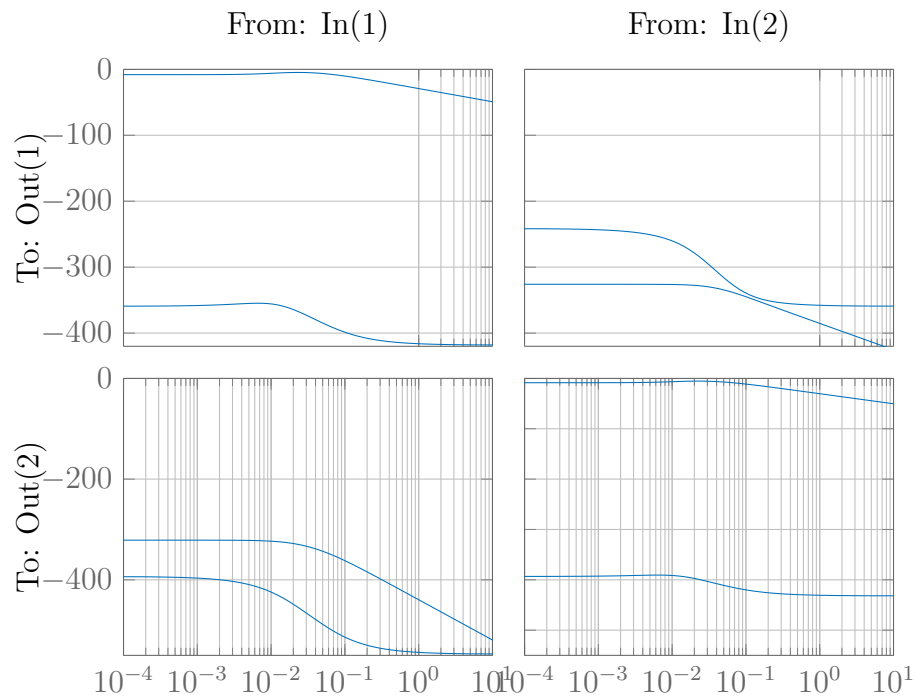


Figure 1: Bode diagram of  $\tilde{G}(s)$  derived in exercise 3.2.1

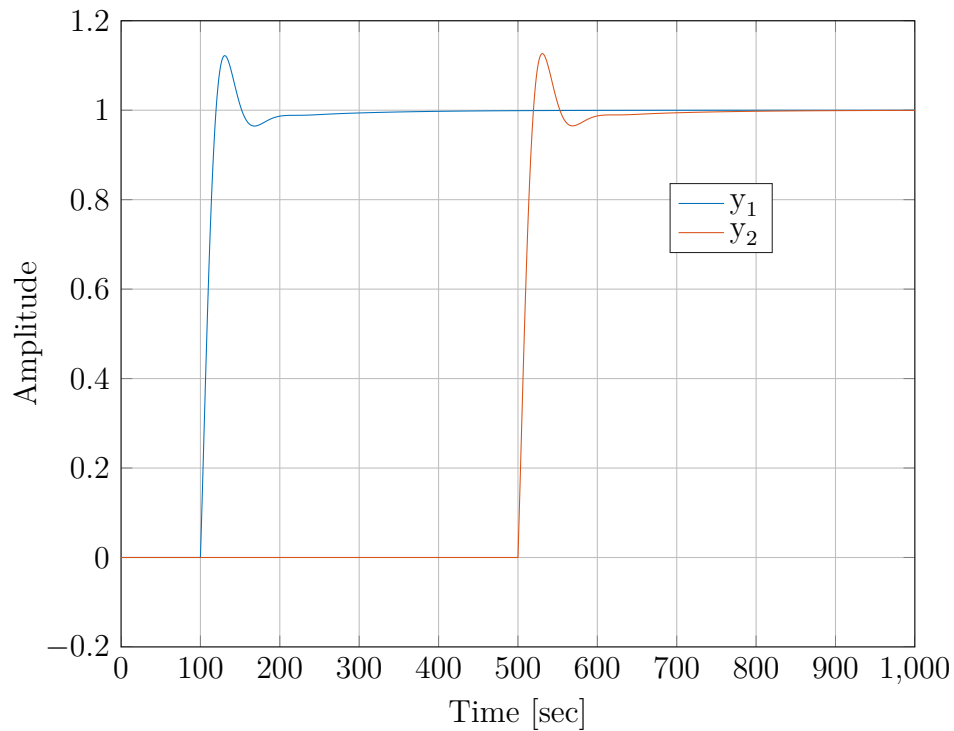


Figure 2: Simulink plots from exercise 3.2.4

In this case, inputs  $u_1, u_2$  should be paired to outputs  $y_1$  and  $y_2$  respectively. Figure 1 shows that input  $u_2$  is severely attenuated with respect to output  $y_1$ ; exactly the same happens with respect to input  $u_1$  and output  $y_2$ . The controller is thus successful.

Figure 2 exhibits the step responses of the closed-loop system. It is evident that the output signal  $y_2$ , seen here with red colour, is not in the least influenced by the preceding step input  $u_1$ . Output  $y_1$  exhibits the same behaviour with respect to the step input  $u_2$ . The output signals are now decoupled.

## Glover-MacFarlane robust loop-shaping

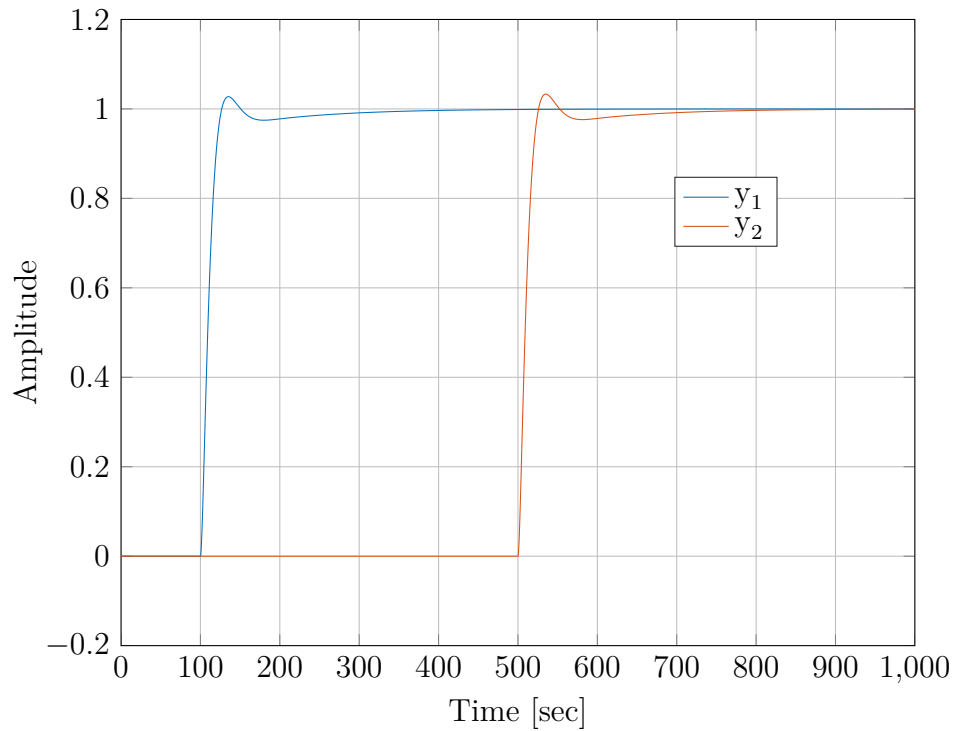


Figure 3: Simulink plots from exercise 3.3.4

Figure 3 illustrates the step responses of the closed-loop system after shaping the open loop using the Glover-McFarlane method. Both this and the nominal design method result in successful decoupling, however the Glover-McFarlane method takes provision towards robustness. In this case, comparing the latter method to the former, we can see that it results in lower overshoot, but with the usual (although small) increase in rise and settling times.

## Non-minimum phase case

### Dynamic decoupling

The dynamic decoupling in exercise 3.2.1 is

$$W(s) = \begin{bmatrix} \frac{0.2}{s + 0.2} & \frac{-1.615s - 0.1386}{s + 0.2} \\ \frac{-1.143s - 0.1039}{s + 0.2} & \frac{0.2}{s + 0.2} \end{bmatrix}$$

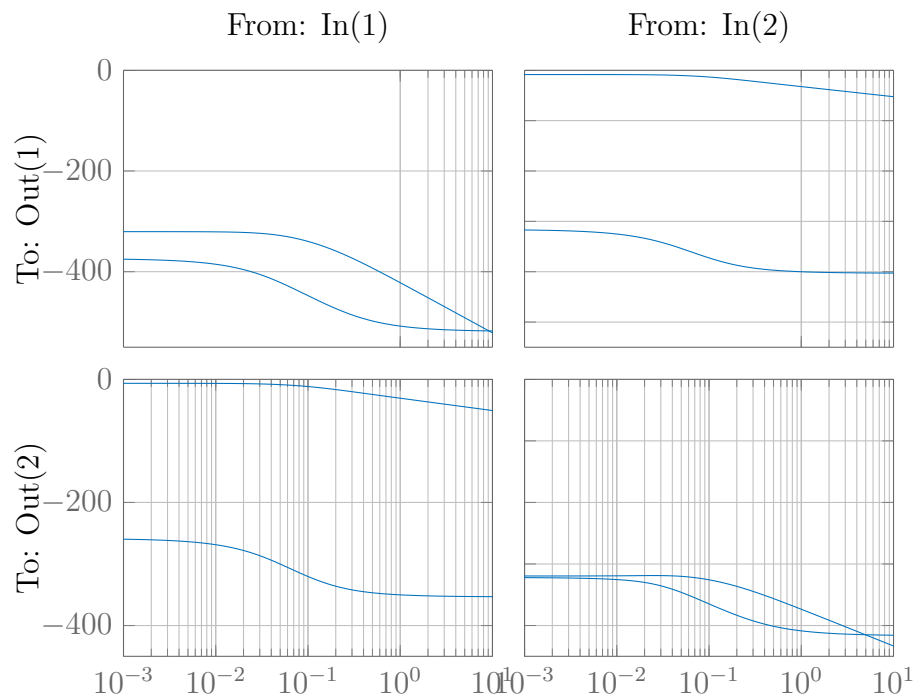


Figure 4: Bode diagram of  $\tilde{G}(s)$  derived in exercise 3.2.1

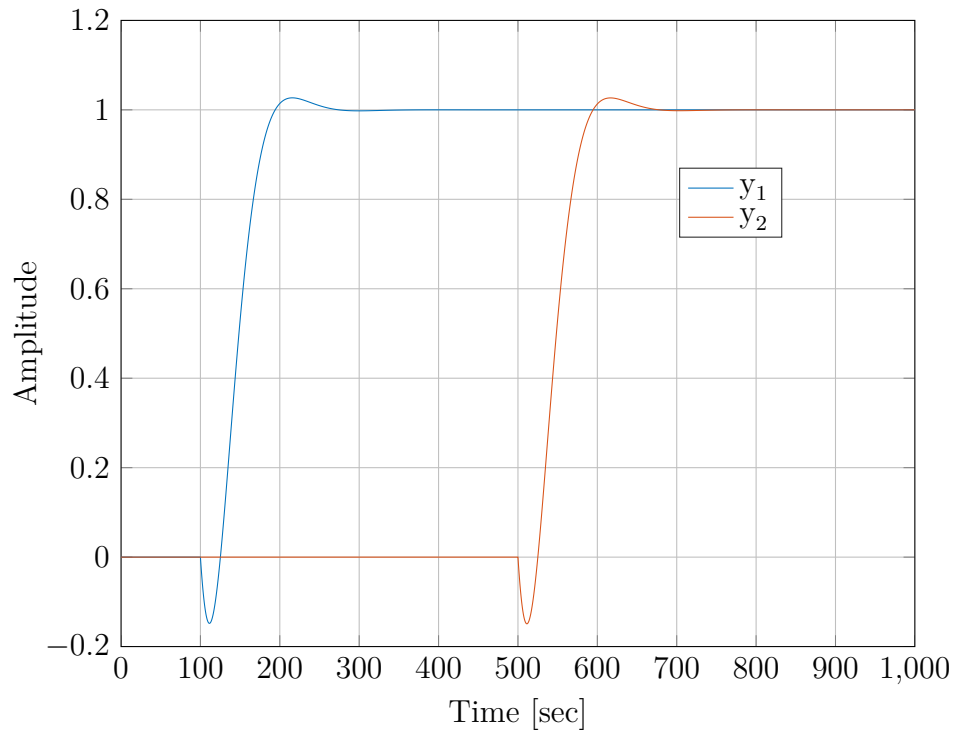


Figure 5: Simulink plots from exercise 3.2.4

In this case, inputs  $u_1, u_2$  should be paired to outputs  $y_2$  and  $y_1$  respectively. Figure 4 shows that input  $u_2$  is severely attenuated with respect to output  $y_2$ ; exactly the same happens with respect to input  $u_2$  and output  $y_1$ . The controller is thus successful.

Figure 5 exhibits the step responses of the closed-loop system. It is evident that the output signal  $y_2$ , seen here with red colour, is not in the least influenced by the preceding step input  $u_2$ . Output  $y_2$  exhibits the same behaviour with respect to the step input  $u_1$ . The output signals are now decoupled.

## Glover-MacFarlane robust loop-shaping

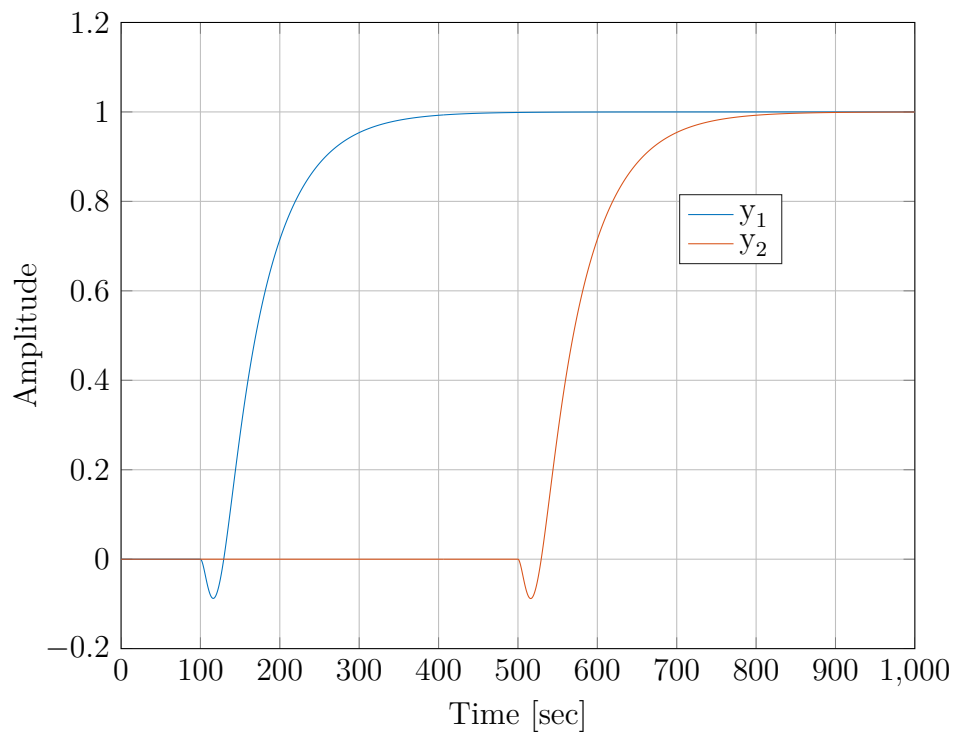


Figure 6: Simulink plots from exercise 3.3.4

Figure 6 illustrates the step responses of the closed-loop system after shaping the open loop using the Glover-McFarlane method. Both this and the nominal design method result in successful decoupling, however the Glover-McFarlane method takes provision towards robustness. In this case, comparing the latter method to the former, we can see that it results in no overshoot at all, but with a somewhat major increase in rise and settling times.