

Energy transfer in ITG/KBM system

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1 Appendix: equation for the evolution of zonal flow

define flux average as

$$\langle f \rangle = \frac{\int \int f d\theta d\zeta}{\int \int d\theta d\zeta} \quad (1)$$

and the flux-averaged derivation term of vorticity is written as:

$$\begin{aligned} \frac{\partial}{\partial t} \langle \nabla_{\perp}^2 \phi \rangle &= \frac{\partial}{\partial t} \langle \frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial \phi}{\partial r}) \rangle \\ &= \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial}{\partial t} \langle \frac{\partial \phi}{\partial r} \rangle \\ &= \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial}{\partial t} (v_E) \end{aligned} \quad (2)$$

the other flux-averaged term can be written as

$$- \langle [\phi, \Omega] \rangle = \frac{1}{r} \langle \frac{\partial \phi}{\partial \theta} \frac{\partial \Omega}{\partial r} - \frac{\partial \phi}{\partial r} \frac{\partial \Omega}{\partial \theta} \rangle \quad (3)$$

$$\langle \frac{\partial \phi}{\partial \theta} \frac{\partial \Omega}{\partial r} \rangle = \int \frac{\partial \phi}{\partial \theta} \frac{\partial \Omega}{\partial r} d\theta = \int \frac{\partial}{\partial r} (\frac{\partial \phi}{\partial \theta} \Omega) d\theta - \int \frac{\partial^2 \phi}{\partial r \partial \theta} \Omega d\theta \quad (4)$$

$$\langle \frac{\partial \phi}{\partial r} \frac{\partial \Omega}{\partial \theta} \rangle = \int \frac{\partial \phi}{\partial r} \frac{\partial \Omega}{\partial \theta} d\theta = [\Omega \frac{\partial \phi}{\partial r}]_0^{2\pi} - \int \frac{\partial^2 \phi}{\partial r \partial \theta} \Omega d\theta = - \int \frac{\partial^2 \phi}{\partial r \partial \theta} \Omega d\theta \quad (5)$$

then:

$$\begin{aligned} - \langle [\phi, \Omega] \rangle &= \frac{1}{r} \frac{\partial}{\partial r} \langle \Omega \frac{\partial \phi}{\partial \theta} \rangle \\ &= \frac{1}{r} \frac{\partial}{\partial r} \langle \phi \frac{\partial \Omega}{\partial \theta} \rangle \end{aligned} \quad (6)$$

and we can convert it to the form like Reynolds stress as follows:

$$\begin{aligned} \int \frac{\partial \phi}{\partial \theta} \nabla_{\perp}^2 \phi d\theta &= \int \frac{\partial \phi}{\partial \theta} \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \phi}{\partial r} d\theta + \int \frac{\partial \phi}{\partial \theta} \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2} d\theta \\ &= \int \frac{\partial \phi}{\partial \theta} \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \phi}{\partial r} d\theta + \frac{1}{2r^2} \int \frac{\partial}{\partial \theta} (\frac{\partial \phi}{\partial \theta})^2 d\theta \\ &= \int \frac{\partial \phi}{\partial \theta} \frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \phi}{\partial r} d\theta + \int \frac{1}{r} (r \frac{\partial \phi}{\partial r} \frac{\partial^2 \phi}{\partial r \partial \theta}) d\theta \\ &= \int \frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial \phi}{\partial r} \frac{\partial \phi}{\partial \theta}) d\theta \\ &= \frac{1}{r} \frac{\partial}{\partial r} \langle r \frac{\partial \phi}{\partial r} \frac{\partial \phi}{\partial \theta} \rangle \\ &= - \frac{1}{r} \frac{\partial}{\partial r} r^2 \langle v_{\theta} v_r \rangle \end{aligned} \quad (7)$$

and we can deduce the maxwell stress in a similiar way:

$$\begin{aligned}
-\frac{\beta}{n_{eq}} < [A, j] > &= \frac{\beta}{n_{eq}} < [A, \nabla_{\perp}^2 A] > \\
&= \frac{\beta}{n_{eq}} \frac{1}{r} \frac{\partial}{\partial r} < j \frac{\partial A}{\partial \theta} > \\
&= \frac{\beta}{n_{eq}} \frac{1}{r} \frac{\partial}{\partial r} < A \frac{\partial j}{\partial \theta} > \\
&= \frac{\beta}{n_{eq}} \frac{1}{r} \frac{\partial}{\partial r} r^2 < B_{\theta} B_r >
\end{aligned} \tag{8}$$

as for curvature terms,

$$\begin{aligned}
- < \omega_d \cdot f > &= -2\epsilon < [r \cos \theta, f] > \\
&= 2\epsilon < \frac{1}{r} \left(\frac{\partial(r \cos \theta)}{\partial \theta} \frac{\partial f}{\partial r} - \frac{\partial(r \cos \theta)}{\partial r} \frac{\partial f}{\partial \theta} \right) > \\
&= \frac{2\epsilon}{r} (- < r \sin \theta \frac{\partial f}{\partial r} > - < \cos \theta \frac{\partial f}{\partial \theta} >) \\
&= \frac{2\epsilon}{r} (- < r \sin \theta \frac{\partial f}{\partial r} > - < f \sin \theta >) \\
&= -2\epsilon < \left(\frac{\partial f}{\partial r} + \frac{f}{r} \right) \sin \theta > \\
&= -2\epsilon \frac{1}{r} \frac{\partial}{\partial r} r < f \sin \theta >
\end{aligned} \tag{9}$$

Here,

$$f = T_i + \frac{T_{eq}}{n_{eq}} n + \frac{p_e}{n_{eq}} = \frac{p}{n_{eq}} \tag{10}$$

then,

$$- < \omega \cdot \frac{p}{n_{eq}} > = -\frac{2\epsilon}{n_{eq}} \frac{1}{r} \frac{\partial}{\partial r} r < p \sin \theta > \tag{11}$$

so the evolution of zonal flow in the limit of collisionless situation is as follows,

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial}{\partial t} (v_E) = -\frac{1}{r} \frac{\partial}{\partial r} \frac{1}{r} \frac{\partial}{\partial r} r^2 < v_{\theta} v_r > + \frac{1}{r} \frac{\partial}{\partial r} \frac{\beta}{n_{eq}} \frac{1}{r} \frac{\partial}{\partial r} r^2 < B_{\theta} B_r > - \frac{2\epsilon}{n_{eq}} \frac{1}{r} \frac{\partial}{\partial r} r < p \sin \theta > \tag{12}$$

eliminate the commom part, we get,

$$\frac{\partial}{\partial t} < v_E > = -\frac{1}{r^2} \frac{\partial}{\partial r} r^2 < v_{\theta} v_r > + \frac{\beta}{n_{eq}} \frac{1}{r^2} \frac{\partial}{\partial r} r^2 < B_{\theta} B_r > - \frac{2\epsilon}{n_{eq}} < p \sin \theta > \tag{13}$$

and in the code, we use the alternative expression,

$$\frac{\partial}{\partial t} < v_E > = \frac{1}{r} < \phi \frac{\partial \Omega}{\partial \theta} > + \frac{\beta}{n_{eq}} \frac{1}{r} < A \frac{\partial A}{\partial \theta} > - \frac{2\epsilon}{n_{eq}} < p \sin \theta > \tag{14}$$

when we use the Fourier expansion,

$$\frac{\partial}{\partial t} < v_E > = \sum_{m1+m2=0} \phi_{m1} \Omega_{\theta, m2} + \sum_{m1+m2=0} A_{m1} j_{\theta, m2} - \frac{i\epsilon}{n_{eq}} (p_{1,0} - p_{-1,0}) \tag{15}$$

$$< p \sin \theta > = \frac{i}{2} (p_{1,0} - p_{-1,0}) \tag{16}$$

2 Appendix: equation for the evolution of $\langle p \sin \theta \rangle$

we can deduce the evolution of p with the derivative equation of n and T ,

$$\frac{\partial}{\partial t} p = R_Q + R_F + R_C + R_{NL} + R_{LD} + R_S \quad (17)$$

where,

$$\begin{aligned} R_Q &= a[(1+\tau)T_{eq}\frac{\partial n_{eq}}{\partial r} + n_{eq}\frac{\partial T_{eq}}{\partial r}]\nabla_\theta \phi + (1+\tau)\beta T_{eq}\frac{\partial j_0}{\partial r}\nabla_\theta A \\ R_F &= -(\Gamma+\tau)n_{eq}T_{eq}\nabla_\parallel v + (1+\tau)T_{eq}\nabla_\parallel j \\ R_C &= \omega_d((\Gamma+\tau)n_{eq}T_{eq}\phi) + \omega_d((2\Gamma-1)n_{eq}T_{eq}T) + \omega_d((\Gamma-1)-\tau(\tau+1))T_{eq}^2 n \\ R_{NL} &= -(1+\tau)T_{eq}[\phi, n] - n_{eq}[\phi, T] + (\Gamma+\tau)n_{eq}T_{eq}\beta[A, v] - (1+\tau)T_{eq}\beta[A, j] \\ R_{LD} &= -(\Gamma-1)\sqrt{\frac{8T_{eq}}{\pi}}n_{eq}|\nabla_\parallel|T \\ R_S &= (1+\tau)T_{eq}D_n\nabla_\perp^2 n + n_{eq}D_T\nabla_\perp^2 T \end{aligned} \quad (18)$$

with,

$$\begin{aligned} \langle \nabla_\theta f \sin \theta \rangle &= \int \frac{1}{r} \frac{\partial f}{\partial \theta} \sin \theta d\theta \\ &= -\frac{1}{r} \langle f \cos \theta \rangle \end{aligned} \quad (19)$$

$$\begin{aligned} \langle \nabla_\parallel f \sin \theta \rangle &= \int \frac{a}{R} (f_\theta/q + f_\zeta) \sin \theta d\theta d\zeta \\ &\approx -\frac{\epsilon}{q} \langle f \cos \theta \rangle \end{aligned} \quad (20)$$

$$\begin{aligned} \langle (\omega_d \cdot f) \sin \theta \rangle &= 2\epsilon \langle [r \cos \theta, f] \sin \theta \rangle \\ &= \frac{2\epsilon}{r} (\langle \frac{\partial f}{\partial \theta} \cos \theta \sin \theta \rangle - \langle r \frac{\partial f}{\partial r} \sin^2 \theta \rangle) \\ &= \epsilon (\langle \frac{\partial f}{\partial r} \rangle - \langle (\frac{2f}{r} + \frac{\partial f}{\partial r}) \cos 2\theta \rangle) \end{aligned} \quad (21)$$

we can convert the terms form to,

$$\begin{aligned} \langle R_Q \sin \theta \rangle &= a[(1+\tau)T_{eq}\frac{\partial n_{eq}}{\partial r} + n_{eq}\frac{\partial T_{eq}}{\partial r}] \langle \phi \cos \theta \rangle + (1+\tau)\beta T_{eq}\frac{\partial j_0}{\partial r} \langle A \cos \theta \rangle \\ \langle R_F \sin \theta \rangle &= (\Gamma+\tau)n_{eq}T_{eq}\frac{\epsilon}{q} \langle v \cos \theta \rangle - (1+\tau)T_{eq}\frac{\epsilon}{q} \langle j \cos \theta \rangle \\ \langle R_C \sin \theta \rangle &= \epsilon(\Gamma+\tau)p_{eq} \langle v_\theta \rangle + \epsilon(2\Gamma-1)p_{eq} \langle \frac{\partial T}{\partial r} \rangle + \epsilon((\Gamma-1)-\tau(\tau+1))T_{eq}^2 \langle \frac{\partial n}{\partial r} \rangle \\ \langle R_{LD} \sin \theta \rangle &= -(\Gamma-1)\sqrt{\frac{8T_{eq}}{\pi}}n_{eq}\frac{\epsilon}{q} \langle T \sin \theta \rangle \end{aligned} \quad (22)$$