

# EE102B Signal Processing and Linear Systems II

## Solutions to Lab One 2012-2013 Spring Quarter

1. (15 points) *Derivation of the Fourier Coefficients for the periodic pulse of Problem 1.4 and a full-wave rectified sine wave.*

(a) The periodic pulse of Problem 1.4 :

$$\begin{aligned}a_k &= \frac{1}{T} \int_{-T/2}^{T/2} x(t) e^{-j \frac{2\pi}{T} kt} dt \\&= \frac{1}{8} \int_{-4}^4 x(t) e^{-j \frac{\pi}{4} kt} dt \\&= \frac{1}{8} \int_{-1}^1 x(t) e^{-j \frac{\pi}{4} kt} dt\end{aligned}$$

(i) When  $k = 0$ ,

$$a_k = \frac{20 \cdot 2}{8} = 5$$

(ii) When  $k \neq 0$ ,

$$a_k = \frac{5}{2} \left[ \frac{1}{-j \frac{\pi}{4} k} e^{-j \frac{\pi}{4} kt} \right]_{-1}^1 = \frac{20 \sin(\frac{\pi}{4} k)}{\pi k}$$

(b) A full-wave rectified sine wave :

$$\begin{aligned}
a_k &= \frac{1}{T} \int_{-T/2}^{T/2} x(t) e^{-j \frac{2\pi}{T} kt} dt \\
&= 120 \int_{-\frac{1}{240}}^{\frac{1}{240}} |120\sqrt{2} \sin(120\pi t)| e^{-j240\pi kt} dt \\
&= 120 \int_0^{\frac{1}{120}} 120\sqrt{2} \sin(120\pi t) e^{-j240\pi kt} dt \\
&= 120^2 \sqrt{2} \int_0^{\frac{1}{120}} \frac{1}{j2} (e^{j120\pi t} - e^{-j120\pi t}) e^{-j240\pi kt} dt \\
&= \frac{120^2 \sqrt{2}}{j2} \left[ \frac{e^{-j120\pi(2k-1)t}}{-j120\pi(2k-1)} - \frac{e^{-j120\pi(2k+1)t}}{-j120\pi(2k+1)} \right]_0^{\frac{1}{120}} \\
&= \frac{60\sqrt{2}}{\pi(4k^2-1)} \left[ (2k+1)e^{-j120\pi(2k-1)t} - (2k-1)e^{-j120\pi(2k+1)t} \right]_0^{\frac{1}{120}} \\
&= \frac{60\sqrt{2}}{\pi(4k^2-1)} \left[ (2k+1)e^{-j(2k-1)\pi} - (2k-1)e^{-j(2k+1)\pi} - (2k+1) + (2k-1) \right] \\
&= \frac{60\sqrt{2}}{\pi(4k^2-1)} [(2k+1) \cdot (-1) - (2k-1) \cdot (-1) - 2] \\
&= \frac{60\sqrt{2}}{\pi(4k^2-1)} [-4] \\
&= \frac{240\sqrt{2}}{\pi(1-4k^2)}
\end{aligned}$$

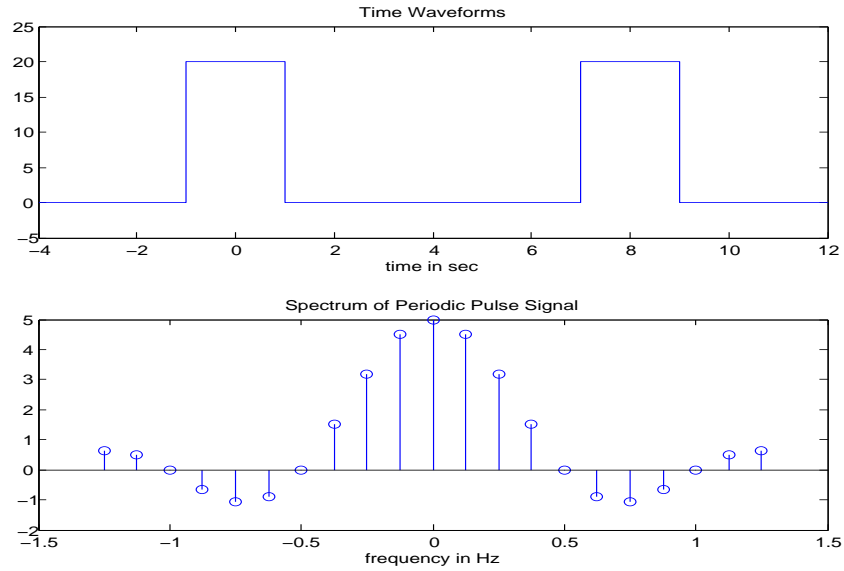
2. (20 points) *Implement your M-file, syn\_Fourier().*

```
function      xx = syn_fourier(tt, ak, fk)
%SYN_FOURIER  Function to synthesize a sum of complex
%             exponentials over the time range given by tt
%  usage:
%      xx = syn_fourier(tt, ak, fk)
%      tt = vector of times, for the time axis
%      ak = vector of complex Fourier coefficients
%      fk = vector of frequencies
%           (usually contains both negative and positive freqs)
%      xx = vector of synthesized waveform values
%
%  Note: fk and ak must be the same length.
%        ak(1) corresponds to frequency fk(1),
%        ak(2) corresponds to frequency fk(2), etc.
%
% Note: the output might have a tiny imaginary part even if it
%       is supposed to be purely real.  If so, take the real part.
%
xx = exp( tt(:)*(2i*pi*fk(:)') ) * ak(:);
%set imaginary part to zero if it is small
if( max(abs(imag(xx)))<1e-6 ), xx = real(xx); end
```

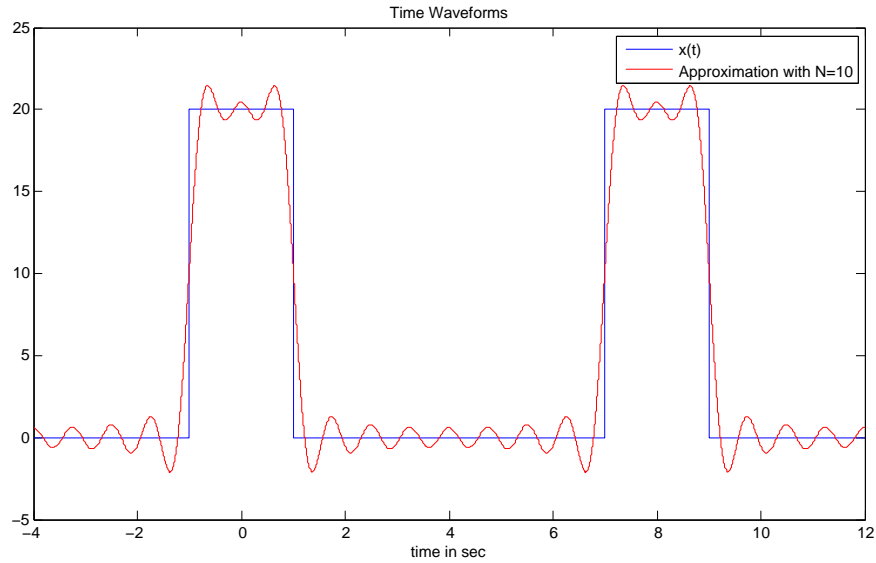
3. (50 points) *Experiments and Annotated Plots.*

(a) 3.3 Synthesis of the Periodic Pulse Signal of Problem 1.4

(i) The periodic pulse signal and its Fourier coefficients.



(ii) Fourier Synthesis with  $N=10$ .



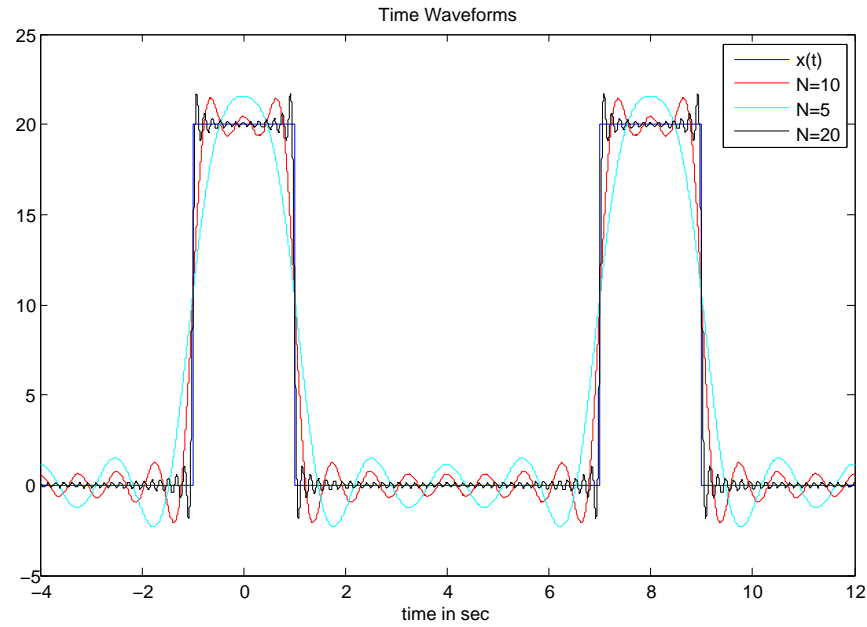
(iii) What is the equivalent ideal low-pass filter's cutoff frequency?

The filtered signal must have the  $f_{-10}$  and  $f_{10}$  components, and should not have any components for  $|k| > 10$ .

$$\therefore \frac{1}{8} \cdot 10 \text{ (Hz)} < f_{cutoff} < \frac{1}{8} \cdot 11 \text{ (Hz)}$$

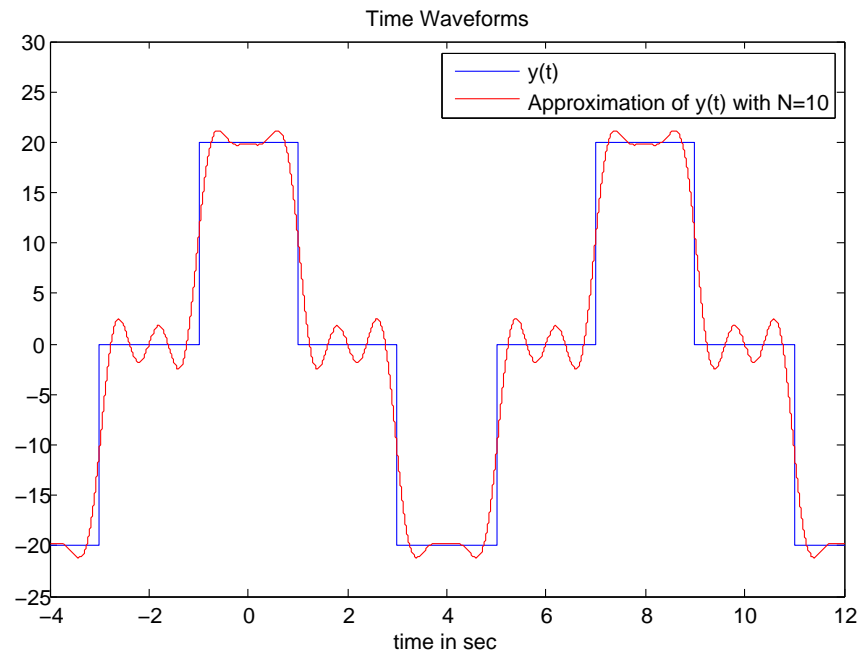
The answer is Not unique.

(iv) Add two more examples,  $N > 10$  and  $N < 10$ , and report what you observe.



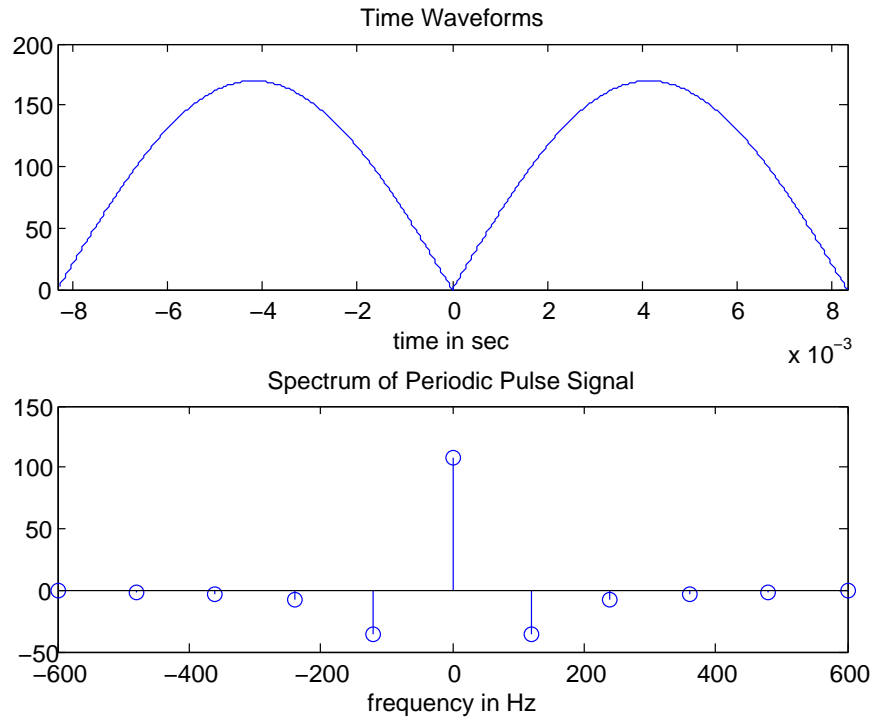
In the  $N > 10$  case, we can observe the Gibbs phenomenon.

(v) Approximate the periodic output of the LTI system,  $h(t) = \delta(t) - \delta(t - 4)$ .

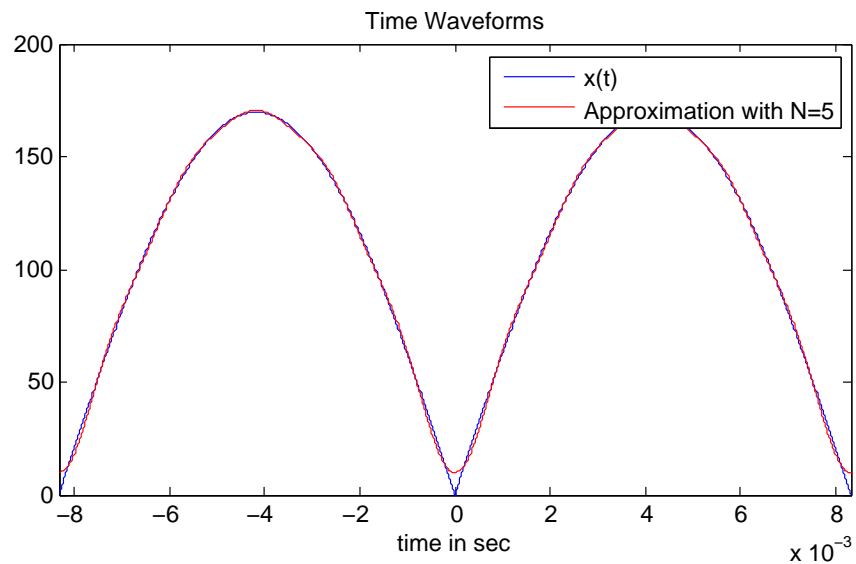


## (b) 3.4 Synthesis of a Full-Wave Rectified Sine Wave

(i) The periodic pulse signal and its Fourier coefficients.



(ii) Fourier Synthesis with  $N=5$ .



(iii) We want to make the output signal of a low-pass filter a constant DC value of the input signal. What is the equivalent ideal low-pass filter's cutoff frequency?

The filtered signal must have the  $f_0$  components, and should not have

any components for  $|k| > 0$ .

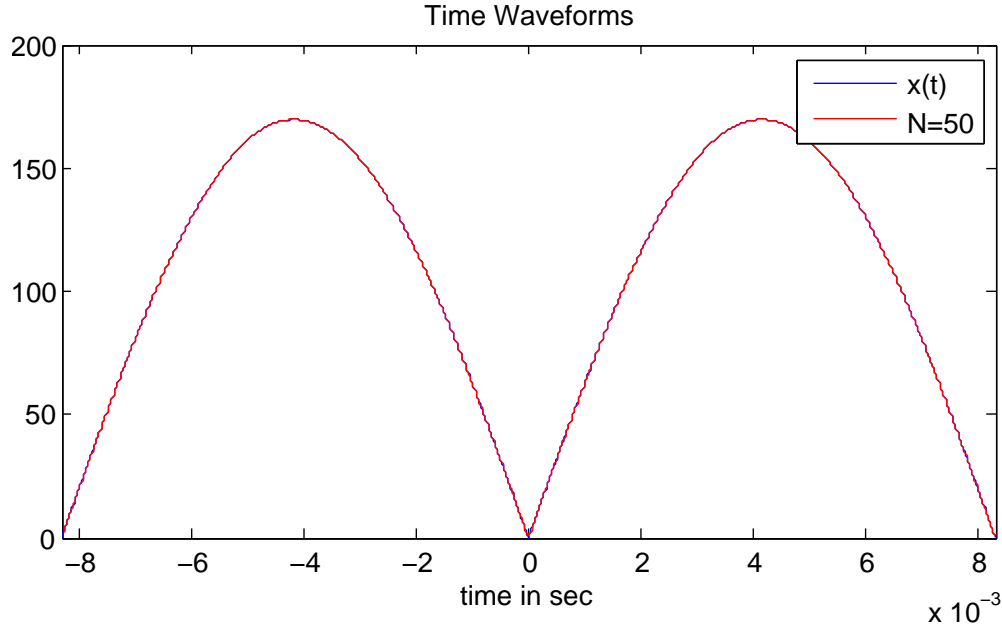
$$\frac{1}{1/120} \cdot 0 \text{ (Hz)} < f_{cutoff} < \frac{1}{1/120} \cdot 1 \text{ (Hz)}$$

$$\therefore 0 \text{ (Hz)} < f_{cutoff} < 120 \text{ (Hz)}$$

The answer is Not unique and the constant output of the low-pass filter is 108.04 which is the  $a_0$  coefficient value.

(iv) Increase N and report what you observe.

Here we chose N=50.



Even though the N value is large enough and the difference between the original the synthesized signals is negligible, we can still find relatively high error around the sharp zero-touching regions of the original signal. The reason is that the Fourier synthesis is basically a sum of continuous/differentiable functions. Since the components are all continuous/differentiable, so the summation is. Unless we choose  $N = \infty$ , we will still see the 'relatively' high errors around those regions.

(v) Approximate the periodic output of the LTI system,  $h(t) = \alpha e^{-\alpha t} u(t)$ .

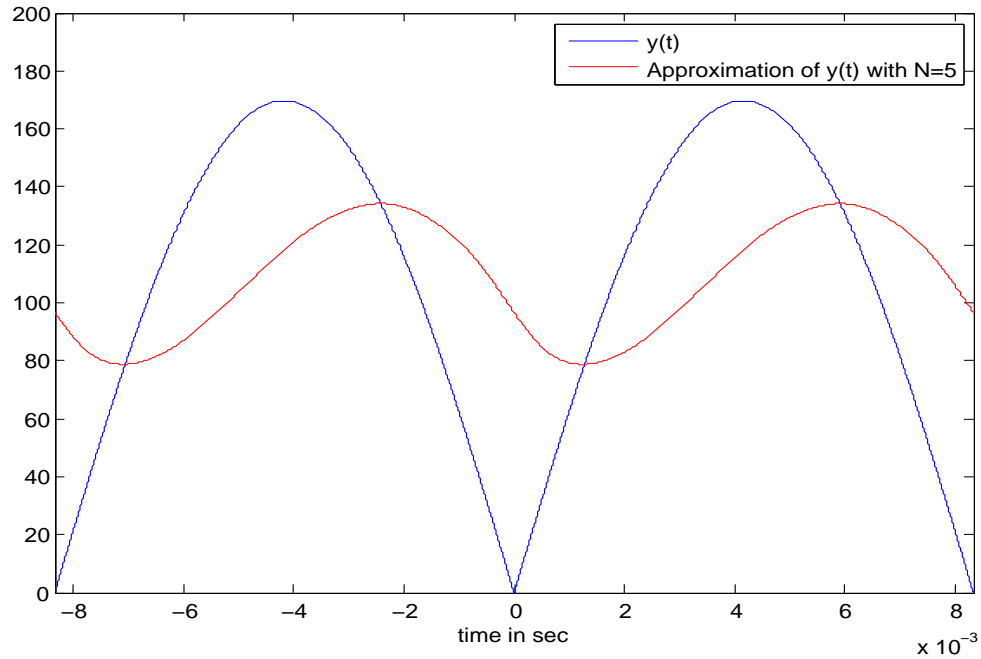
The output of the filter for the  $2N + 1$  terms approximation is

$$y(t) = \sum_{k=-N}^N b_k e^{j\omega_0 k t} \quad \text{where} \quad b_k = a_k H(j\omega_0 k)$$

$$\omega_0 = \frac{2\pi}{T}$$

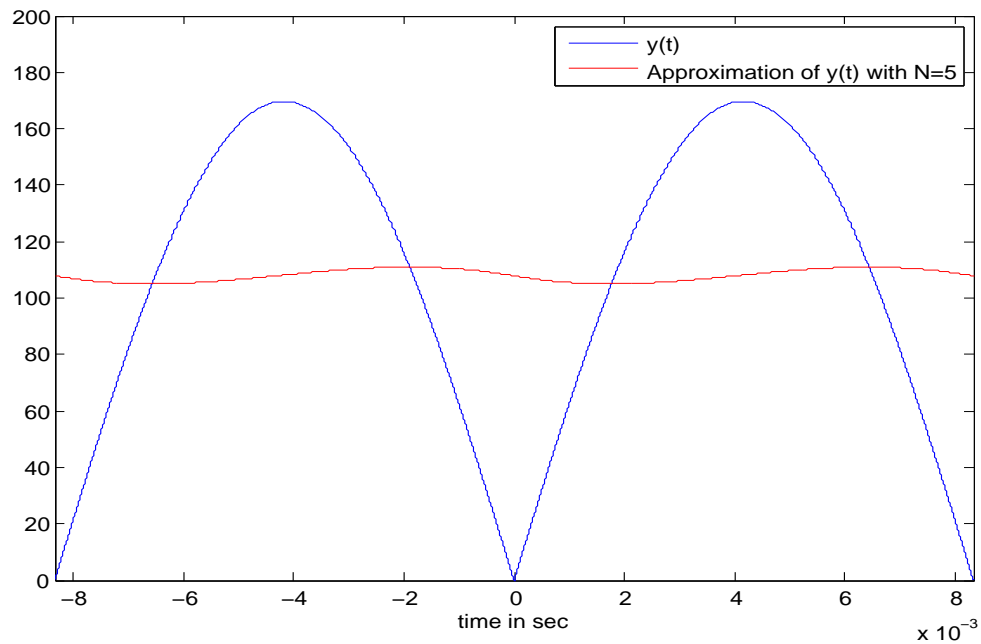
$$H(j\omega) = \frac{\alpha}{\alpha + j\omega}$$

We have 2 figures below. The top one is when  $\alpha = 100\pi$  which is quite a large number. Large N implies a fast decay in  $h(t)$ . Reminding that what



a low-pass filter does is basically to add many consecutive samples, fast decaying  $h(t)$  roughly corresponds to a weighted sum of a small number of samples. This is why the filtered signal follows the original signal and doesn't look like a DC component.

When we decrease the  $\alpha$  to  $10\pi$ , we can observe the bottom one.



In this case, the filtered signal more looks like a DC component (i.e. less

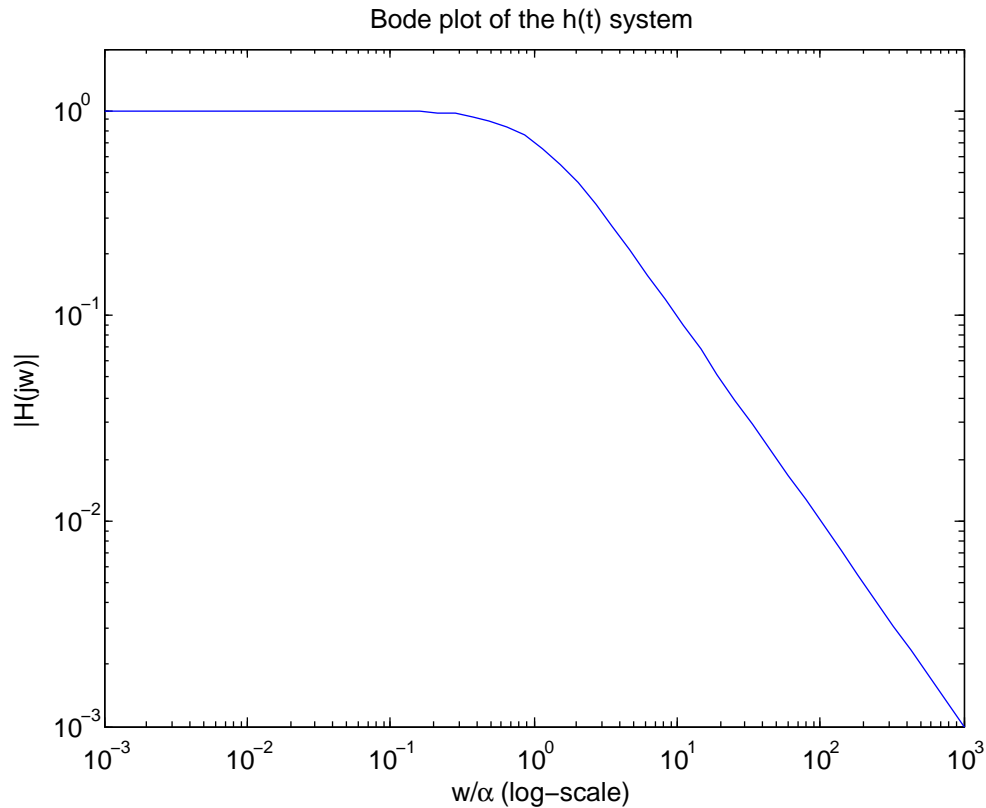


ripple), and we can say the filter does a good job as a low-pass filter.

4. (15 points) *Formula for the peak-to-peak ripple remaining in the filtered output of the full-wave rectified sine wave.*

$$h(t) = \alpha e^{-\alpha t} u(t) \leftrightarrow H(j\omega) = \frac{\alpha}{\alpha + j\omega}$$

The below is a Bode plot of the  $h(t)$  system. As you can see, it is a simple RC low-pass filter. The cutoff frequency of the filter is  $\omega_{cutoff} = \alpha$ . Since the



problem's assumption says to only consider the fundamental frequency, i.e. higher frequencies are negligible for the value of  $\alpha$  to be used. To analyze the out ripple's peak-to-peak value, let's start from the corresponding output signal component

at the fundamental frequency,  $w_0 = \frac{2\pi}{T} = 240\pi$ .

$$\begin{aligned}
(\text{output signal component at } w_0) &= a_1 H(jw_0) e^{jw_0 t} + a_{-1} H(-jw_0) e^{-jw_0 t} \\
&= a_1 [H(jw_0) e^{jw_0 t} + H(-jw_0) e^{-jw_0 t}] \\
&= a_1 \left[ \frac{\alpha}{\alpha + jw_0} e^{jw_0 t} + \frac{\alpha}{\alpha - jw_0} e^{-jw_0 t} \right] \\
&= a_1 \alpha \left[ \frac{(\alpha - jw_0) e^{jw_0 t} + (\alpha + jw_0) e^{-jw_0 t}}{(\alpha + jw_0)(\alpha - jw_0)} \right] \\
&= a_1 \alpha \left[ \frac{2\alpha \cos(w_0 t) + 2\alpha \sin(w_0 t)}{\alpha^2 + w_0^2} \right] \\
&= \frac{2a_1 \alpha \sqrt{\alpha^2 + w_0^2} \sin(w_0 + \phi)}{\alpha^2 + w_0^2} \\
&= \frac{2a_1 \alpha \sin(w_0 + \phi)}{\sqrt{\alpha^2 + w_0^2}}
\end{aligned}$$

$$\therefore (\text{peak-to-peak ripple size}) = \frac{4|a_1 \alpha|}{\sqrt{\alpha^2 + w_0^2}} \approx \frac{144|\alpha|}{\sqrt{\alpha^2 + (240\pi)^2}}$$

Here is a comparison between the theoretical and experimental peak-to-peak ripple values for various  $\alpha$  values.

$\alpha$	$2.4\pi$	$24\pi$	$240\pi$	$2400\pi$	$24000\pi$
<b>Experimental value</b>	<b>1.43</b>	<b>14.21</b>	<b>104.50</b>	<b>159.07</b>	<b>160.74</b>
<b>Theoretical value</b>	<b>1.44</b>	<b>14.32</b>	<b>101.82</b>	<b>143.29</b>	<b>144.00</b>

We can find that the above theoretical analysis works well.