



Department of Electronic & Telecommunication Engineering,
University of Moratuwa, Sri Lanka.

Pick and Place Robot Arm

Design Documentation

V 2.0

Discussion Group C
Group 8

Group Members:

210179R Gammune D.J.T.

Submitted in partial fulfillment of the requirements for the module
EN2160 - Electronic Design Realization

2024/03/26

Contents

1	General	2
1.1	Marketing Needs	2
1.2	Existing Product Analysis	2
1.3	User Profile	2
1.4	Market Segment	2
1.5	User Survey	2
1.6	Specifications	2
2	Electronics Design	2
2.1	Conceptual Block Diagram	2
2.2	Sub-Assembly Design	2
2.3	Component Selection	2
2.3.1	Motor Driver: A4988	2
2.3.2	Stepper Motor: NEMA17 and ST-PM35-15-11C	2
2.4	Circuit Testing	2
2.5	Design Problems and Solutions	2
2.6	Layout Information	2
2.7	Final Circuit Diagrams	2
2.8	Industry Standards	3
3	Industrial (Mechanical) Design	3
3.1	Design of Mechanical Sub-assemblies	3
3.2	Specifications	3
3.3	Selection Criteria for Various Parts	3
3.4	Rough Sketches	3
3.4.1	Horizontal and Vertical Conveyor Systems	3
3.4.2	T8 Screw Rod:	3
3.4.3	3D Printed Parts	3
3.4.4	Mechanical Gripper Mechanism	4
3.5	PCB Dimensions Finalized	4
3.6	Reasons for Selection and Non-selection	4
3.7	Standards Used	4
3.8	Finish	5
3.9	Material Used	5
3.10	Final Drawings	5
4	Mechanical Design	5
4.1	Design of Mechanical Sub-assemblies	5
4.2	Specifications	5
4.3	Selection Criteria for Various Parts	5
5	Software Details	5
5.1	Structure Diagram	5
5.2	Flowchart	5
5.3	Rough Work	5
6	Data Sheets	7
6.1	NEMA17 Stepper Motor	7
6.2	ST-PM35-15-11C Stepper Motor	8
6.3	A4988 Stepper Motor Driver	9

1 General

1.1 Marketing Needs

The inspiration for an automated system to assemble electronic components such as rivets, washers, and transistors onto cylindrical heat sinks for a 3-phase H-bridge system using industrial-grade motors stemmed from discussions with Professor Jayasinghe.

1.2 Existing Product Analysis

Solutions from industry leaders like ABB, KUKA, FANUC, and Yaskawa Motoman were analyzed through YouTube videos, product brochures, and academic papers. Key features such as multi-axis motion control, gripper customization, and integrated vision systems were highlighted.

1.3 User Profile

The target users for the product are manufacturers and industrial facilities involved in electronics assembly and production.

1.4 Market Segment

The market segment for the product is the industrial automation and electronics manufacturing sector.

1.5 User Survey

1.6 Specifications

Throughout the device creation process, tasks documentation will be seamlessly integrated.

2 Electronics Design

2.1 Conceptual Block Diagram

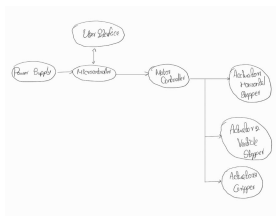


Figure 1: Electronic Block Diagram

2.2 Sub-Assembly Design

The system includes electronic sub-assemblies such as motor drivers, microcontrollers, and control circuits.

2.3 Component Selection

Components like stepper motors, linear rails, and gripper mechanisms were selected based on criteria such as payload capacity, accuracy, speed, and reach.

2.3.1 Motor Driver: A4988

The motor driver receives control signals from the controller interface and translates them into appropriate power outputs for the stepper motor. It plays a crucial role in controlling the speed and direction of the horizontal conveyor system.

2.3.2 Stepper Motor: NEMA17 and ST-PM35-15-11C

The stepper motor is responsible for converting electrical signals from the motor driver into rotational motion. The rotation of the stepper motor drives the T8 screw rod, enabling precise horizontal movement.



Figure 2: NEMA17 Stepper Motor

2.4 Circuit Testing

Throughout the device creation process, tasks documentation will be seamlessly integrated.

2.5 Design Problems and Solutions

Throughout the device creation process, tasks documentation will be seamlessly integrated.

2.6 Layout Information

Information such as component lists, instructions, and guidelines were added based on the conceptual designs

2.7 Final Circuit Diagrams

Throughout the device creation process, tasks documentation will be seamlessly integrated.

2.8 Industry Standards

Relevant industry standards for electronics and robotics were followed.

3 Industrial (Mechanical) Design

3.1 Design of Mechanical Sub-assemblies

The mechanical design includes a modular robot arm design, customized grippers for components, and a user-friendly programming interface. Safety measures like emergency stop systems and intuitive controls were prioritized. The design also considers the development of a slider system for efficient movement and stacking.

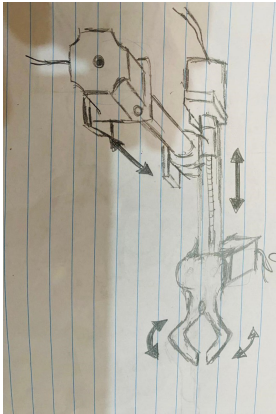


Figure 3: Mechanical Concept Design

3.2 Specifications

3.3 Selection Criteria for Various Parts

The selection of parts for the mechanical sub-assemblies is based on several criteria to ensure optimal performance and reliability of the system. Factors considered during part selection may include functionality, compatibility, durability, cost-effectiveness, availability, manufacturability, safety standards compliance, and material suitability.

3.4 Rough Sketches

3.4.1 Horizontal and Vertical Conveyor Systems

The horizontal conveyor system serves as the foundation for the linear movement of the robotic arm along the x-axis.

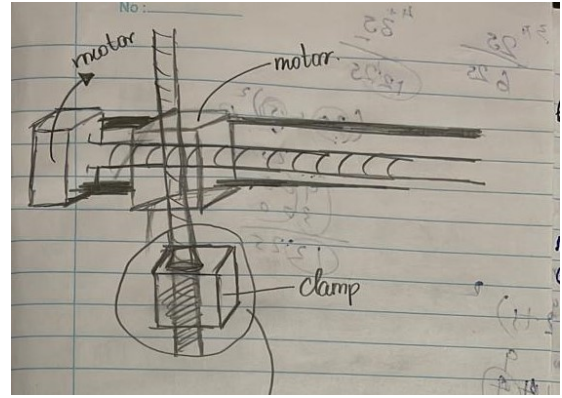


Figure 4: Proposed Device sketch

It comprises:

3.4.2 T8 Screw Rod:

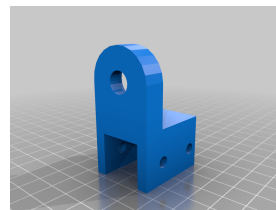
A horizontally oriented T8 screw rod is responsible for the linear motion along the x-axis. It is connected to a stepper motor, which drives the rotation of the screw rod.



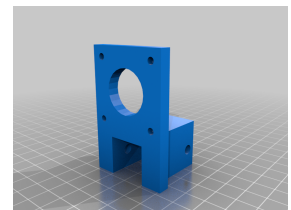
Figure 5: T8 Screw Rod

3.4.3 3D Printed Parts

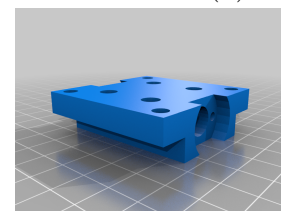
The connecting parts of the device will be created using 3D printing with 100% fill as it needs to be hard.



(a) Connector 1



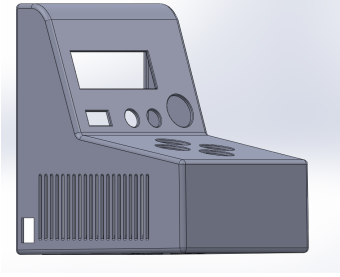
(b) Connector 2



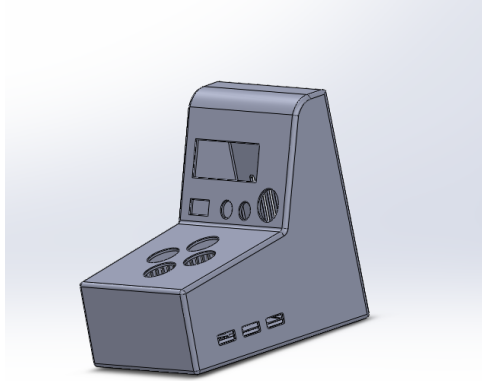
(c) Base Plate

Figure 6: 3D Printing Concepts

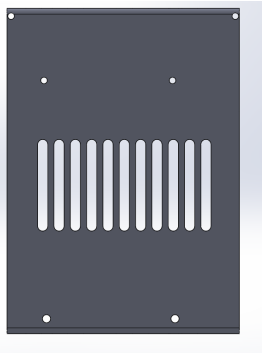
The for the enclosure we are using 3D printing to create the enclosure.



(a) Front View of the Enclosure



(b) Assembly of the Enclosure



(c) Closing Pad of the Enclosure

Figure 7: Enclosure Views

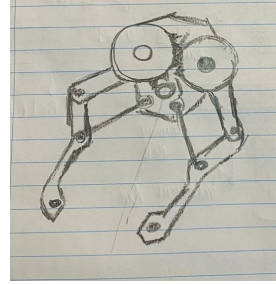
To create these plastic enclosures, 3D printing materials such as Nylon PA12 or Nylon PA11 are planned to be used.

3.4.4 Mechanical Gripper Mechanism

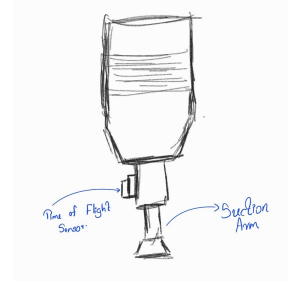
The gripper mechanism is connected to the vertical conveyor system and is responsible for picking up and placing H-Bridge components. It includes:

- **Gripper Module:** The gripper module is designed to securely hold and release electronic components during the pick and place operation. It is attached to the vertical conveyor system to enable controlled vertical movement.

- **Actuation System:** The actuation system within the gripper module allows controlled opening and closing of the gripper, ensuring a secure hold on the components during transportation.



(a) Mechanical Gripper Concept



(b) Pneumatic Suction Gripper Concept

Figure 8: Gripper Concepts

3.5 PCB Dimensions Finalized

The dimensions of the PCB is finalized to 77.34mm in length and 66.42mm in width.

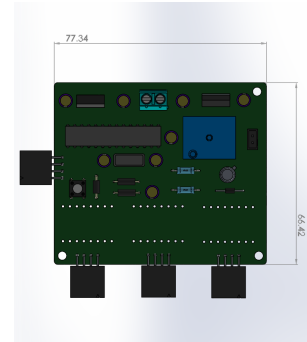


Figure 9: PCB with Dimensions

3.6 Reasons for Selection and Non-selection

Reasons for the selection and non-selection of mechanical parts include factors such as performance, cost, availability, compatibility, manufacturability, and adherence to design specifications. Any changes made to the original design concept will also be recorded.

3.7 Standards Used

Relevant industry standards for mechanical design and fabrication will be followed to ensure compliance with safety, quality, and regulatory requirements. Standards may include ISO, ANSI, ASTM, and specific industry guidelines for robotics and automation.

3.8 Finish

The finish of mechanical components is determined based on functional requirements, aesthetic considerations, and environmental factors. Common finishes include paint, powder coating, anodizing, plating, and surface treatments to enhance durability and appearance.

3.9 Material Used

Materials for mechanical components are selected based on their mechanical properties, compatibility with environmental conditions, manufacturability, and cost-effectiveness. Common materials include metals (e.g., aluminum, steel), plastics, composites, and alloys.

3.10 Final Drawings

4 Mechanical Design

4.1 Design of Mechanical Sub-assemblies

The mechanical design of the system as a whole involves the creation and integration of various sub-assemblies such as the robot arm, gripper mechanism, sliding system, and any other mechanical components necessary for the functioning of the system. Each sub-assembly will be designed to fulfill specific functions within the system, such as precise movement, component manipulation, and overall structural stability.

4.2 Specifications

Specifications for the mechanical sub-assemblies outline the desired characteristics and performance parameters that each component should meet. This includes factors such as dimensions, material properties, load-bearing capacity, precision, and compatibility with other system components. For example, specifications for the robot arm may include its length, payload capacity, range of motion, and speed, while specifications for the gripper mechanism may include its gripping force, opening/closing mechanism, and adaptability to different component shapes and sizes.

4.3 Selection Criteria for Various Parts

The selection of parts for the mechanical sub-assemblies is based on several criteria to ensure optimal performance and reliability of the system. Factors considered during part selection may include:

- **Functionality:** Parts should fulfill their intended functions within the system, such as providing movement, support, or gripping capabilities.
- **Compatibility:** Parts should be compatible with other components in terms of size, shape, mounting interfaces, and operational requirements.
- **Durability and Reliability:** Parts should be durable enough to withstand the operational stresses and environmental conditions they will be exposed to during use. They should also have a proven track record of reliability to minimize maintenance and downtime.
- **Cost-effectiveness:** Parts should be cost-effective in terms of initial procurement costs as well as long-term maintenance and replacement expenses.
- **Availability:** Parts should be readily available from reliable suppliers to ensure timely procurement and maintenance support.
- **Manufacturability:** Parts should be manufacturable using appropriate techniques and technologies, considering factors such as production lead times, scalability, and ease of assembly.
- **Safety:** Parts should meet safety standards and regulations to ensure the safety of operators and other personnel interacting with the system.

By adhering to these selection criteria, the mechanical design team can choose the most suitable parts and components to construct the mechanical sub-assemblies, thereby contributing to the overall functionality, efficiency, and longevity of the system.

5 Software Details

5.1 Structure Diagram

5.2 Flowchart

5.3 Rough Work

References

- [1] NEMA17 Datasheet https://components101.com/sites/default/files/component_datasheet/NEMA17.pdf
- [2] ST-PM35-15-11C Stepper Datasheet <https://cdn.sparkfun.com/datasheets/Robotics/ST-PM35-15-11C.pdf>

[3] A4988 Stepper Motor Driver Datasheet <https://www.alldatasheet.com/datasheet-pdf/pdf/338780/ALLEGRO/A4988.html>

6 Data Sheets

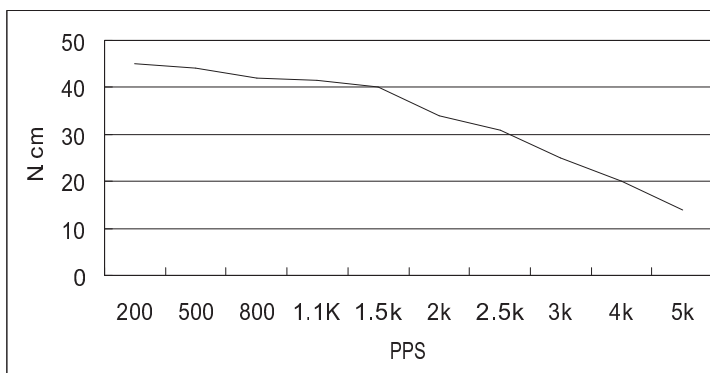
6.1 NEMA17 Stepper Motor

HIGH TORQUE HYBRID STEPPING MOTOR SPECIFICATIONS

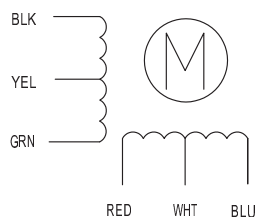
General specifications		Electrical specifications	
Step Angle (°)	1.8	Rated Voltage (V)	4
Temperature Rise (°C)	80 Max (rated current, 2 phase on)	Rated Current (A)	1.2
Ambient temperature (°C)	-20~+50	Resistance Per Phase ($\pm 10\%$)	3.3 (25°C)
Number of Phase	2	Inductance Per Phase ($\pm 20\%$ mH)	2.8
Insulation Resistance	100M Ω , Min (500VDC)	Holding Torque (Kg.cm)	3.17
Insulation Class	Class B	Detent Torque (g.cm)	200
Max.radial force (N)	28 (20mm from the flange)	Rotor Inertia (g.cm ²)	68
Max.axial force (N)	10	Weight (Kg)	0.365

● Pull out torque curve:

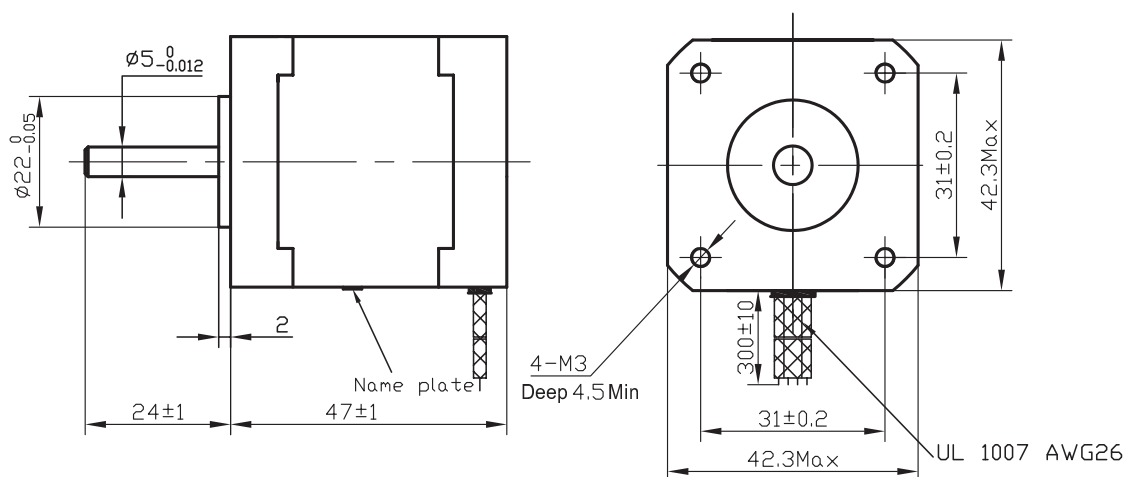
VOLTAGE: 24VDC, CONSTANT CURRENT: 1.2A, HALF STEP



● Wiring Diagram:



● Dimensions: (unit=mm)



					SY42STH47-1206A	TECHNICAL CONDITIONS
	REV	REVISIONS	DESCRIPTION	BY	DATE	
	DRAW	任飞飞	2010.06.29			060047000
	CHECK					
	APPROVE					
CHANGZHOU SONGYANG MACHINERY & ELECTRONICS NEW TECHNIC INSTITUTE						

Figure 10: NEMA17 Datasheet

6.2 ST-PM35-15-11C Stepper Motor

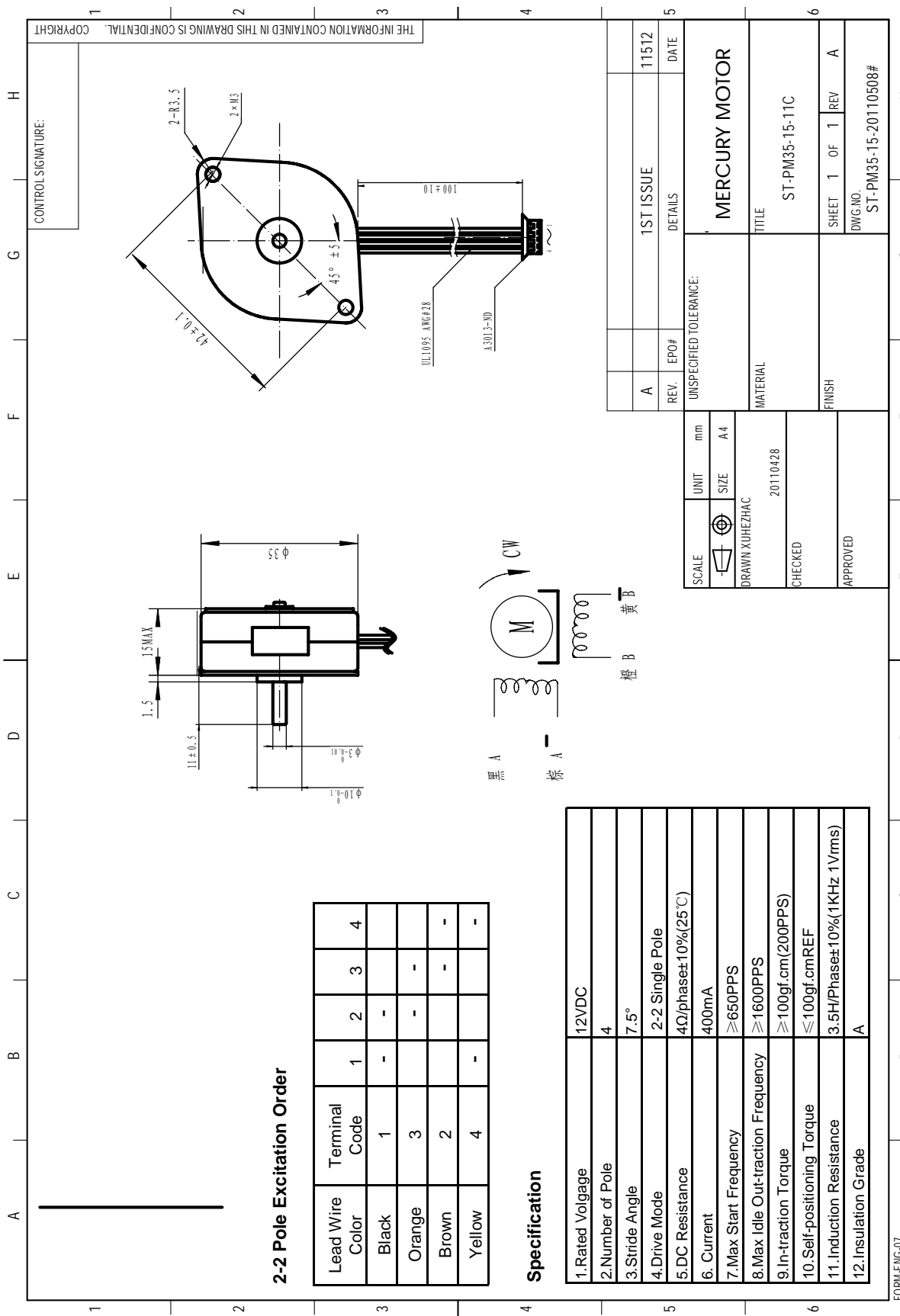


Figure 11: ST-PM35-15-11C Datasheet

6.3 A4988 Stepper Motor Driver



A4988

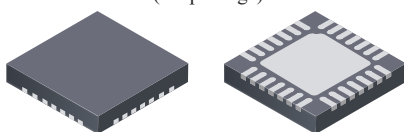
DMOS Microstepping Driver with Translator and Overcurrent Protection

FEATURES AND BENEFITS

- Low $R_{ds(on)}$ outputs
- Automatic current decay mode detection/selection
- Mixed and slow current decay modes
- Synchronous rectification for low power dissipation
- Internal UVLO
- Crossover-current protection
- 3.3 and 5 V compatible logic supply
- Thermal shutdown circuitry
- Short-to-ground protection
- Shorted load protection
- Five selectable step modes: full, $1/2$, $1/4$, $1/8$, and $1/16$

PACKAGE:

28-contact QFN
with exposed thermal pad
5 mm × 5 mm × 0.90 mm
(ET package)



Not to scale

DESCRIPTION

The A4988 is a complete microstepping motor driver with built-in translator for easy operation. It is designed to operate bipolar stepper motors in full-, half-, quarter-, eighth-, and sixteenth-step modes, with an output drive capacity of up to 35 V and ± 2 A. The A4988 includes a fixed off-time current regulator which has the ability to operate in slow or mixed decay modes.

The translator is the key to the easy implementation of the A4988. Simply inputting one pulse on the STEP input drives the motor one microstep. There are no phase sequence tables, high-frequency control lines, or complex interfaces to program. The A4988 interface is an ideal fit for applications where a complex microprocessor is unavailable or is overburdened.

During stepping operation, the chopping control in the A4988 automatically selects the current decay mode: slow or mixed. In mixed decay mode, the device is set initially to a fast decay for a proportion of the fixed off-time, then to a slow decay for the remainder of the off-time. Mixed decay current control results in reduced audible motor noise, increased step accuracy, and reduced power dissipation.

Continued on the next page...

TYPICAL APPLICATION DIAGRAM

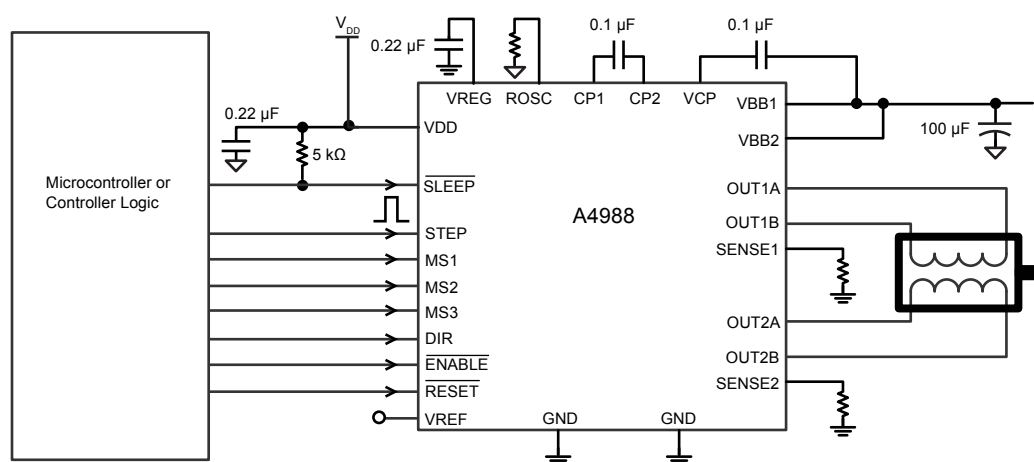


Figure 12: A4988 Datasheet

A4988

DMOS Microstepping Driver with Translator and Overcurrent Protection

DESCRIPTION (continued)

Internal synchronous rectification control circuitry is provided to improve power dissipation during PWM operation. Internal circuit protection includes: thermal shutdown with hysteresis, undervoltage lockout (UVLO), and crossover-current protection. Special power-on sequencing is not required.

The A4988 is supplied in a surface-mount QFN package (ET), 5 mm × 5 mm, with a nominal overall package height of 0.90 mm and an exposed pad for enhanced thermal dissipation. It is lead (Pb) free (suffix -T), with 100% matte-tin-plated leadframes.

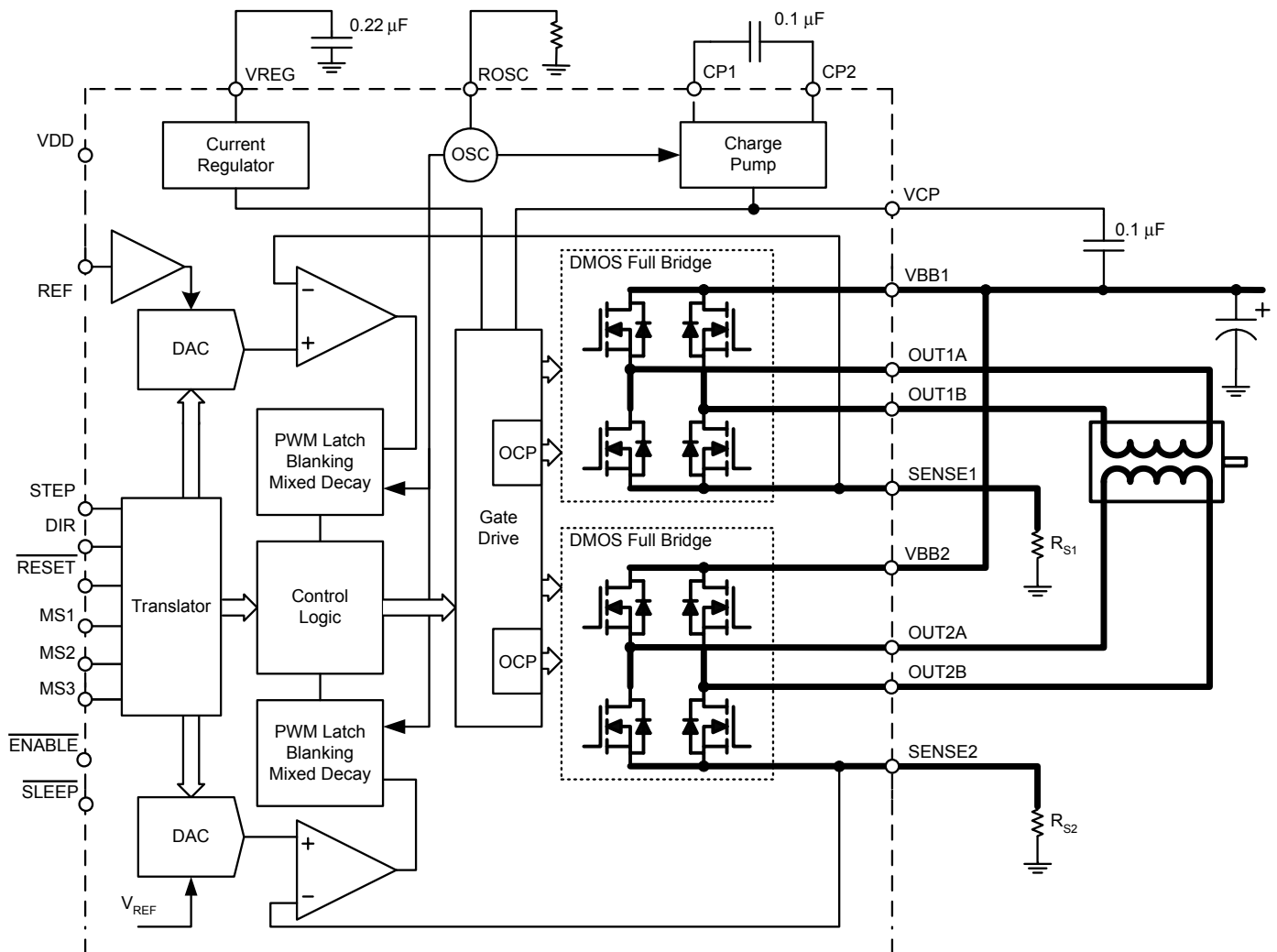
SELECTION GUIDE

Part Number	Package	Packing
A4988SETTR-T	28-contact QFN with exposed thermal pad	1500 pieces per 7-in. reel

ABSOLUTE MAXIMUM RATINGS

Characteristic	Symbol	Notes	Rating	Units
Load Supply Voltage	V_{BB}		35	V
Output Current	I_{OUT}		±2	A
Logic Input Voltage	V_{IN}		-0.3 to 5.5	V
Logic Supply Voltage	V_{DD}		-0.3 to 5.5	V
Motor Outputs Voltage			-2.0 to 37	V
Sense Voltage	V_{SENSE}		-0.5 to 0.5	V
Reference Voltage	V_{REF}		5.5	V
Operating Ambient Temperature	T_A	Range S	-20 to 85	°C
Maximum Junction	$T_J(max)$		150	°C
Storage Temperature	T_{stg}		-55 to 150	°C

Functional Block Diagram



ELECTRICAL CHARACTERISTICS [1]: Valid at $T_A = 25^\circ\text{C}$, $V_{BB} = 35\text{ V}$ (unless otherwise noted)

Characteristics	Symbol	Test Conditions	Min.	Typ. [2]	Max.	Units
OUTPUT DRIVERS						
Load Supply Voltage Range	V _{BB}	Operating	8	–	35	V
		During Sleep Mode	0	–	35	V
Logic Supply Voltage Range	V _{DD}	Operating	3	–	5.5	V
Output On-Resistance	R _{ds(on)}	Source driver, I _{OUT} = –1.5 A	–	320	430	mΩ
		Sink driver, I _{OUT} = 1.5 A	–	320	430	mΩ
Body Diode Forward Voltage	V _F	Source diode, I _F = –1.5 A	–	–	1.2	V
		Sink diode, I _F = 1.5 A	–	–	1.2	V
Motor Supply Current	I _{BB}	f _{PWM} < 50 kHz	–	–	4	mA
		Operating, outputs disabled	–	–	2	mA
		Sleep Mode	–	–	10	μA
Logic Supply Current	I _{DD}	f _{PWM} < 50 kHz	–	–	8	mA
		Outputs off	–	–	5	mA
		Sleep Mode	–	–	10	μA
CONTROL LOGIC						
Logic Input Voltage	V _{IN(1)}		V _{DD} × 0.7	–	–	V
	V _{IN(0)}		–	–	V _{DD} × 0.3	V
Logic Input Current	I _{IN(1)}	V _{IN} = V _{DD} × 0.7	–20	<1.0	20	μA
	I _{IN(0)}	V _{IN} = V _{DD} × 0.3	–20	<1.0	20	μA
Microstep Select	R _{MS1}	MS1 pin	–	100	–	kΩ
	R _{MS2}	MS2 pin	–	50	–	kΩ
	R _{MS3}	MS3 pin	–	100	–	kΩ
Logic Input Hysteresis	V _{HYS(IN)}	As a % of V _{DD}	5	11	19	%
Blank Time	t _{BLANK}		0.7	1	1.3	μs
Fixed Off-Time	t _{OFF}	OSC = VDD or GND	20	30	40	μs
		R _{OSC} = 25 kΩ	23	30	37	μs
Reference Input Voltage Range	V _{REF}		0	–	4	V
Reference Input Current	I _{REF}		–3	0	3	μA
Current Trip-Level Error [3]	err _I	V _{REF} = 2 V, %I _{TripMAX} = 38.27%	–	–	±15	%
		V _{REF} = 2 V, %I _{TripMAX} = 70.71%	–	–	±5	%
		V _{REF} = 2 V, %I _{TripMAX} = 100.00%	–	–	±5	%
Crossover Dead Time	t _{DT}		100	475	800	ns
PROTECTION						
Overcurrent Protection Threshold [4]	I _{OCPST}		2.1	–	–	A
Thermal Shutdown Temperature	T _{TSD}		–	165	–	°C
Thermal Shutdown Hysteresis	T _{TSDHYS}		–	15	–	°C
VDD Undervoltage Lockout	V _{DDUVLO}	V _{DD} rising	2.7	2.8	2.9	V
VDD Undervoltage Hysteresis	V _{DDUVLOHYS}		–	90	–	mV

[1] For input and output current specifications, negative current is defined as coming out of (sourcing) the specified device pin.

[2] Typical data are for initial design estimations only, and assume optimum manufacturing and application conditions. Performance may vary for individual units, within the specified maximum and minimum limits.

[3] $V_{ERR} = [(V_{REF}/8) - V_{SENSE}] / (V_{REF}/8)$.[4] Overcurrent protection (OCP) is tested at $T_A = 25^\circ\text{C}$ in a restricted range and guaranteed by characterization.

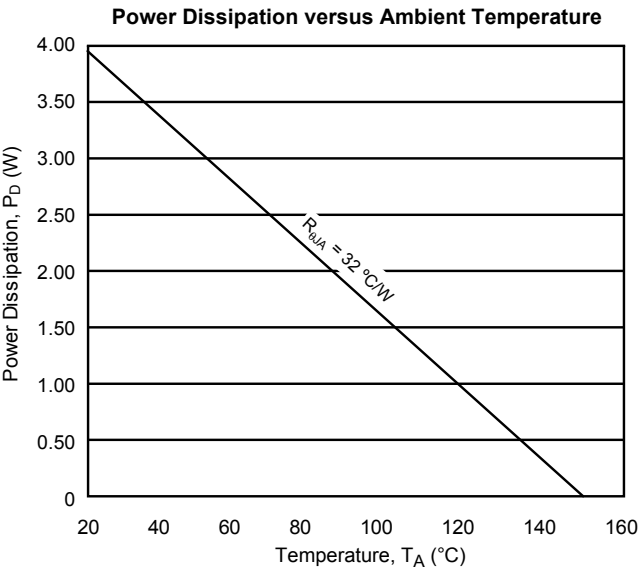
A4988

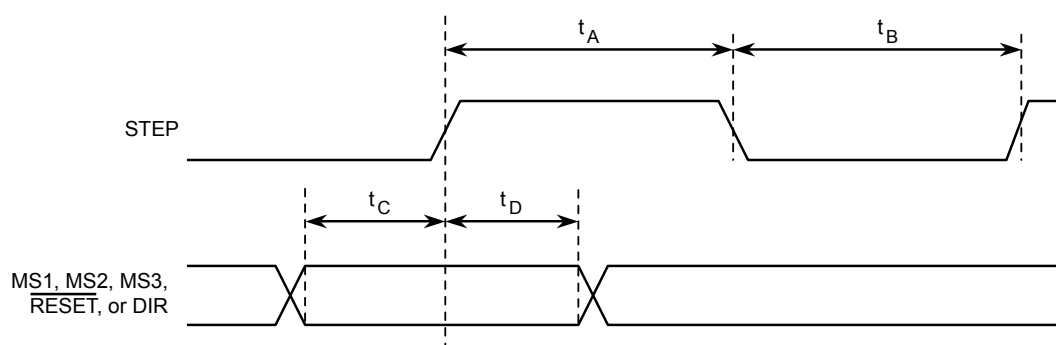
DMOS Microstepping Driver
with Translator and Overcurrent Protection

THERMAL CHARACTERISTICS

Characteristic	Symbol	Test Conditions*	Value	Units
Package Thermal Resistance	$R_{\theta JA}$	Four-layer PCB, based on JEDEC standard	32	°C/W

*Additional thermal information available on Allegro website.





Time Duration	Symbol	Typ.	Unit
STEP minimum, HIGH pulse width	t_A	1	μs
STEP minimum, LOW pulse width	t_B	1	μs
Setup time, input change to STEP	t_C	200	ns
Hold time, input change to STEP	t_D	200	ns

Figure 1: Logic Interface Timing Diagram

Table 1: Microstepping Resolution Truth Table

MS1	MS2	MS3	Microstep Resolution	Excitation Mode
L	L	L	Full Step	2 Phase
H	L	L	Half Step	1-2 Phase
L	H	L	Quarter Step	W1-2 Phase
H	H	L	Eighth Step	2W1-2 Phase
H	H	H	Sixteenth Step	4W1-2 Phase

FUNCTIONAL DESCRIPTION

Device Operation. The A4988 is a complete microstepping motor driver with a built-in translator for easy operation with minimal control lines. It is designed to operate bipolar stepper motors in full-, half-, quarter-, eighth, and sixteenth-step modes. The currents in each of the two output full-bridges and all of the N-channel DMOS FETs are regulated with fixed off-time PWM (pulse-width modulated) control circuitry. At each step, the current for each full-bridge is set by the value of its external current-sense resistor (R_{S1} and R_{S2}), a reference voltage (V_{REF}), and the output voltage of its DAC (which in turn is controlled by the output of the translator).

At power-on or reset, the translator sets the DACs and the phase current polarity to the initial Home state (shown in Figures 9 through 13), and the current regulator to Mixed decay mode for both phases. When a step command signal occurs on the STEP input, the translator automatically sequences the DACs to the next level and current polarity. (See Table 2 for the current-level sequence.) The microstep resolution is set by the combined effect of the MSx inputs, as shown in Table 1.

When stepping, if the new output levels of the DACs are lower than their previous output levels, then the decay mode for the active full-bridge is set to Mixed. If the new output levels of the DACs are higher than or equal to their previous levels, then the decay mode for the active full-bridge is set to Slow. This automatic current decay selection improves microstepping performance by reducing the distortion of the current waveform that results from the back EMF of the motor.

Microstep Select (MSx). The microstep resolution is set by the voltage on logic inputs MSx, as shown in Table 1. The MS1 and MS3 pins have a 100 k Ω pull-down resistance, and the MS2 pin has a 50 k Ω pull-down resistance. When changing the step mode, the change does not take effect until the next STEP rising edge.

If the step mode is changed without a translator reset, and absolute position must be maintained, it is important to change the step mode at a step position that is common to both step modes in order to avoid missing steps. When the device is powered down, or reset due to TSD or an overcurrent event, the translator is set to the home position which is by default common to all step modes.

Mixed Decay Operation. The bridge operates in Mixed decay mode, at power-on and reset, and during normal running according to the ROSC configuration and the step sequence, as shown in Figures 9 through 13. During Mixed decay mode, when the trip point is reached, the A4988 initially goes into a fast decay interval for 31.25% of the off-time, t_{OFF} . After that, it switches to slow decay for the remainder of t_{OFF} . A timing diagram for this feature appears on the next page.

Typically, mixed decay is only necessary when the current in the winding is going from a higher value to a lower value as determined by the state of the translator. For most loads, automatically selected mixed decay is convenient because it minimizes ripple when the current is rising and prevents missed steps when the current is falling. For some applications where microstepping at very low speeds is necessary, the lack of back EMF in the winding causes the current to increase in the load quickly, resulting in missed steps. This is shown in Figure 2. By pulling the ROSC pin to ground, mixed decay is set to be active 100% of the time, for both rising and falling currents, and prevents missed steps as shown in Figure 3. If this is not an issue, it is recommended that automatically selected mixed decay be used, because it will produce reduced ripple currents. Refer to the Fixed Off-Time section for details.

Low Current Microstepping. Intended for applications where the minimum on-time prevents the output current from regulating to the programmed current level at low current steps. To prevent this, the device can be set to operate in Mixed decay mode on both rising and falling portions of the current waveform. This feature is implemented by shorting the ROSC pin to ground. In this state, the off-time is internally set to 30 μ s.

Reset Input ($\overline{\text{RESET}}$). The $\overline{\text{RESET}}$ input sets the translator to a predefined Home state (shown in Figures 9 through 13), and turns off all of the FET outputs. All STEP inputs are ignored until the $\overline{\text{RESET}}$ input is set to high.

Step Input (STEP). A low-to-high transition on the STEP input sequences the translator and advances the motor one increment. The translator controls the input to the DACs and the direc-

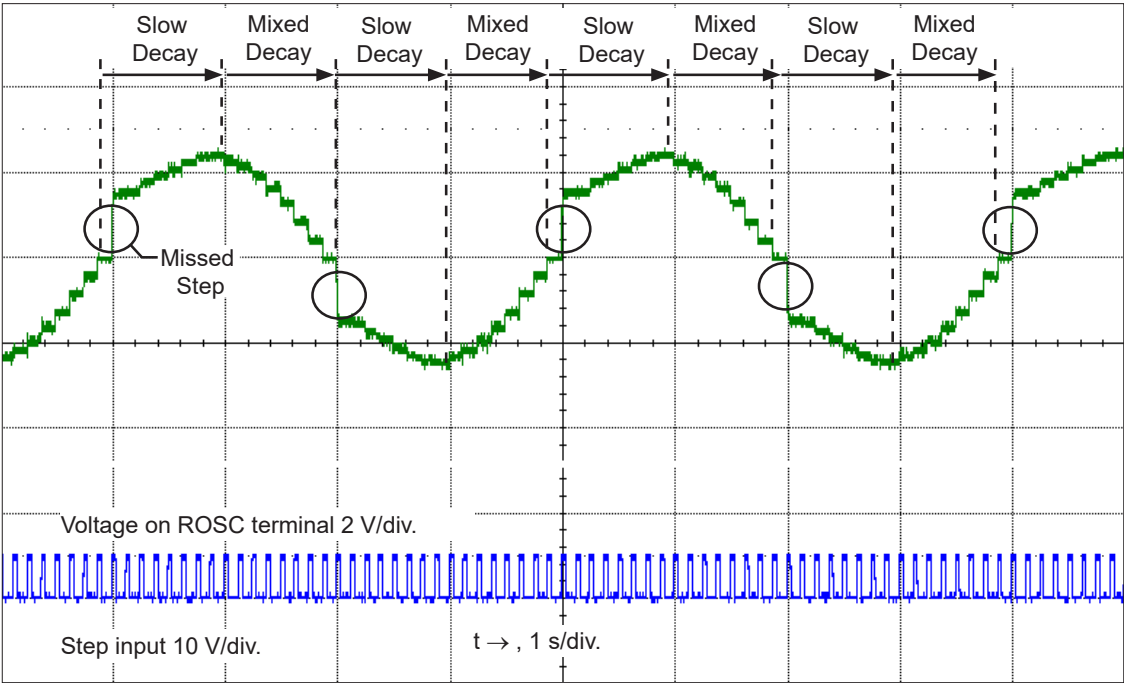


Figure 2: Missed Steps in Low-Speed Microstepping

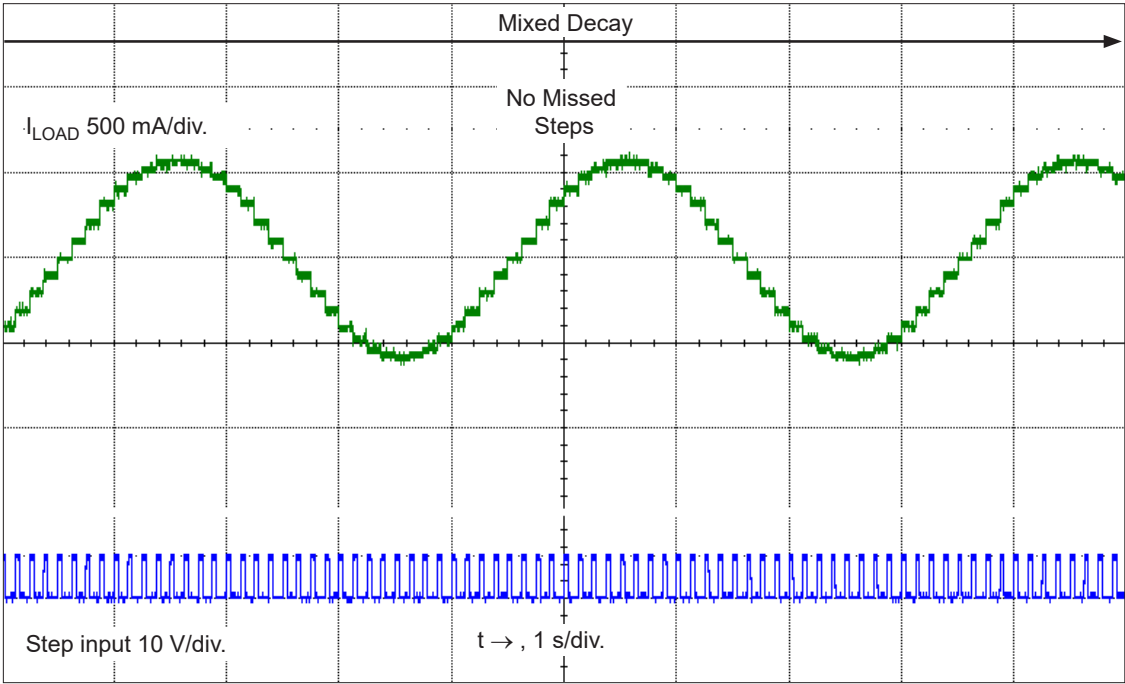


Figure 3: Continuous Stepping Using Automatically-Selected Mixed Stepping (ROSC pin grounded)

tion of current flow in each winding. The size of the increment is determined by the combined state of the MSx inputs.

Direction Input (DIR). This determines the direction of rotation of the motor. Changes to this input do not take effect until the next STEP rising edge.

Internal PWM Current Control. Each full-bridge is controlled by a fixed off-time PWM current control circuit that limits the load current to a desired value, I_{TRIP} . Initially, a diagonal pair of source and sink FET outputs are enabled and current flows through the motor winding and the current sense resistor, R_{Sx} . When the voltage across R_{Sx} equals the DAC output voltage, the current sense comparator resets the PWM latch. The latch then turns off the appropriate source driver and initiates a fixed off-time decay mode

The maximum value of current limiting is set by the selection of R_{Sx} and the voltage at the VREF pin. The transconductance function is approximated by the maximum value of current limiting, $I_{TripMAX}$ (A), which is set by

$$I_{TripMAX} = V_{REF} / (8 \times R_S)$$

where R_S is the resistance of the sense resistor (Ω) and V_{REF} is the input voltage on the REF pin (V).

The DAC output reduces the V_{REF} output to the current sense comparator in precise steps, such that

$$I_{trip} = (\%I_{TripMAX} / 100) \times I_{TripMAX}$$

(See Table 2 for $\%I_{TripMAX}$ at each step.)

It is critical that the maximum rating (0.5 V) on the SENSE1 and SENSE2 pins is not exceeded.

Fixed Off-Time. The internal PWM current control circuitry uses a one-shot circuit to control the duration of time that the DMOS FETs remain off. The off-time, t_{OFF} , is determined by the ROSC terminal. The ROSC terminal has three settings:

- ROSC tied to VDD — off-time internally set to 30 μ s; decay mode is automatic Mixed, except when in full-step where decay mode is set to Slow.
- ROSC tied directly to ground — off-time internally set to 30 μ s; current decay is set to Mixed for both increasing and decreasing currents for all step modes.

- ROSC through a resistor to ground — off-time is determined by the following formula; the decay mode is automatic Mixed for all step modes except full-step which is set to Slow.

$$t_{OFF} \approx R_{OSC} / 825$$

where t_{OFF} is in μ s.

Blanking. This function blanks the output of the current sense comparators when the outputs are switched by the internal current control circuitry. The comparator outputs are blanked to prevent false overcurrent detection due to reverse recovery currents of the clamp diodes, and switching transients related to the capacitance of the load. The blank time, t_{BLANK} (μ s), is approximately

$$t_{BLANK} \approx 1 \mu s$$

Shorted Load and Short-to-Ground Protection.

If the motor leads are shorted together, or if one of the leads is shorted to ground, the driver will protect itself by sensing the overcurrent event and disabling the driver that is shorted, protecting the device from damage. In the case of a short-to-ground, the device will remain disabled (latched) until the \overline{SLEEP} input goes high or V_{DD} power is removed. A short-to-ground overcurrent event is shown in Figure 4.

When the two outputs are shorted together, the current path is through the sense resistor. After the blanking time ($\approx 1 \mu$ s) expires, the sense resistor voltage is exceeding its trip value, due to the overcurrent condition that exists. This causes the driver to go into a fixed off-time cycle. After the fixed off-time expires, the driver turns on again and the process repeats. In this condition, the driver is completely protected against overcurrent events, but the short is repetitive with a period equal to the fixed off-time of the driver. This condition is shown in Figure 5.

During a shorted load event, it is normal to observe both a positive and negative current spike as shown in Figure 3, due to the direction change implemented by the Mixed decay feature. This is shown in Figure 6. In both instances, the overcurrent circuitry is protecting the driver and prevents damage to the device.

Charge Pump (CP1 and CP2). The charge pump is used to generate a gate supply greater than that of V_{BB} for driving the source-side FET gates. A 0.1 μ F ceramic capacitor should be connected between CP1 and CP2. In addition, a 0.1 μ F ceramic capacitor is required between VCP and VBB, to act as a reservoir for operating the high-side FET gates.

Capacitor values should be Class 2 dielectric $\pm 15\%$ maximum, or tolerance R, according to EIA (Electronic Industries Alliance) specifications.

V_{REG} (VREG). This internally generated voltage is used to operate the sink-side FET outputs. The nominal output voltage of the VREG terminal is 7 V. The VREG pin must be decoupled with a 0.22 μ F ceramic capacitor to ground. V_{REG} is internally monitored. In the case of a fault condition, the FET outputs of the A4988 are disabled.

Capacitor values should be Class 2 dielectric $\pm 15\%$ maximum, or tolerance R, according to EIA (Electronic Industries Alliance) specifications.

Enable Input ($\overline{\text{ENABLE}}$). This input turns on or off all of the FET outputs. When set to a logic high, the outputs are disabled. When set to a logic low, the internal control enables the outputs as required. The translator inputs STEP, DIR, and MSx, as well as the internal sequencing logic, all remain active, independent of the $\overline{\text{ENABLE}}$ input state.

Shutdown. In the event of a fault, overtemperature (excess T_J) or an undervoltage (on VCP), the FET outputs of the A4988 are disabled until the fault condition is removed. At power-on, the UVLO (undervoltage lockout) circuit disables the FET outputs and resets the translator to the Home state.

Sleep Mode ($\overline{\text{SLEEP}}$). To minimize power consumption when the motor is not in use, this input disables much of the internal circuitry including the output FETs, current regulator, and charge pump. A logic low on the $\overline{\text{SLEEP}}$ pin puts the A4988 into Sleep mode. A logic high allows normal operation, as well as startup (at which time the A4988 drives the motor to the Home microstep position). When emerging from Sleep mode, in order to allow the charge pump to stabilize, provide a delay of 1 ms before issuing a Step command.

Mixed Decay Operation. The bridge operates in Mixed decay mode, depending on the step sequence, as shown in Figures 9 through 13. As the trip point is reached, the A4988 initially goes into a fast decay interval for 31.25% of the off-time, t_{OFF} . After that, it switches to slow decay for the remainder of t_{OFF} . A timing diagram for this feature appears in Figure 7.

Synchronous Rectification. When a PWM-off cycle is triggered by an internal fixed-off time cycle, load current recirculates according to the decay mode selected by the control logic. This synchronous rectification feature turns on the appropriate FETs during current decay, and effectively shorts out the body diodes with the low FET $R_{\text{ds(on)}}$. This reduces power dissipation significantly, and can eliminate the need for external Schottky diodes in many applications. Synchronous rectification turns off when the load current approaches zero (0 A), preventing reversal of the load current.

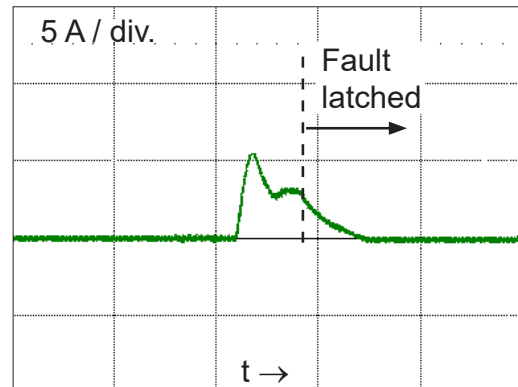


Figure 4: Short-to-Ground Event

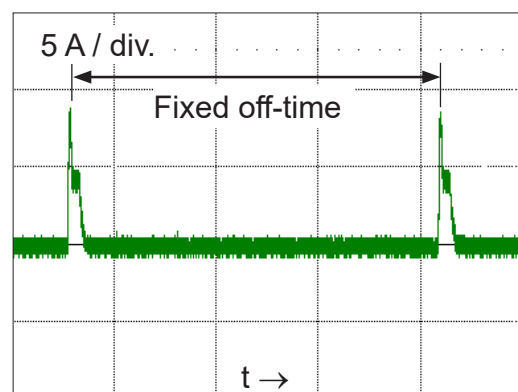


Figure 5: Shorted Load (OUTxA → OUTxB) in Slow Decay Mode

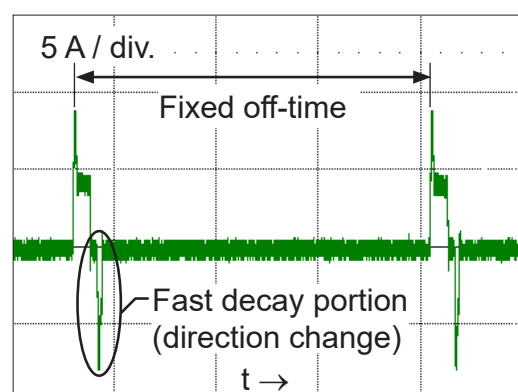


Figure 6: Shorted Load (OUTxA → OUTxB) in Mixed Decay Mode

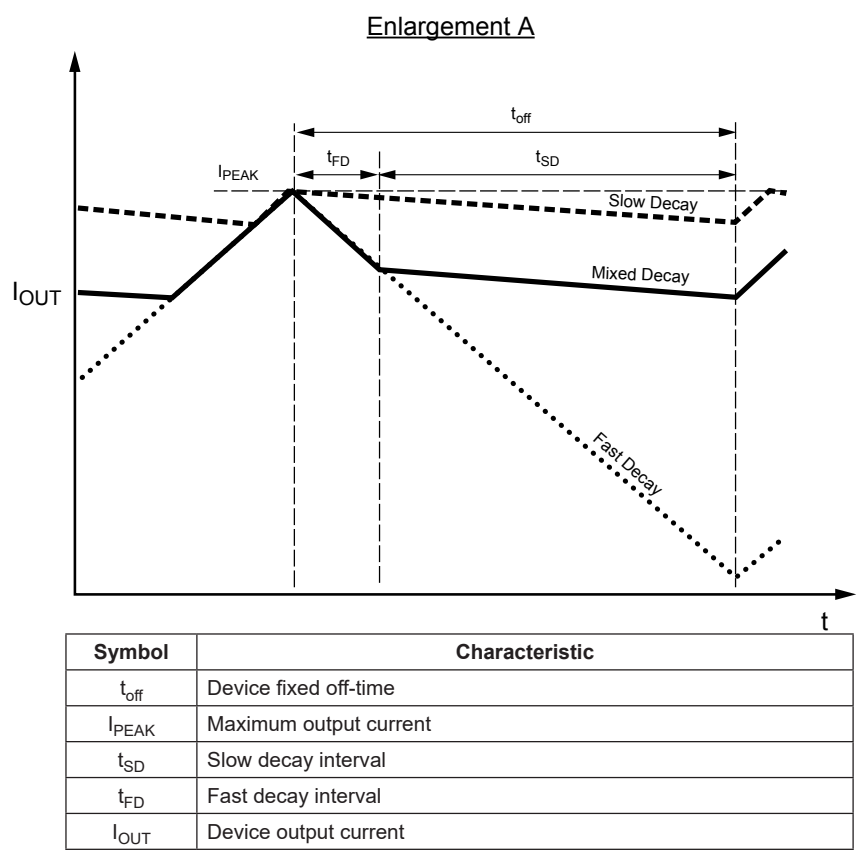
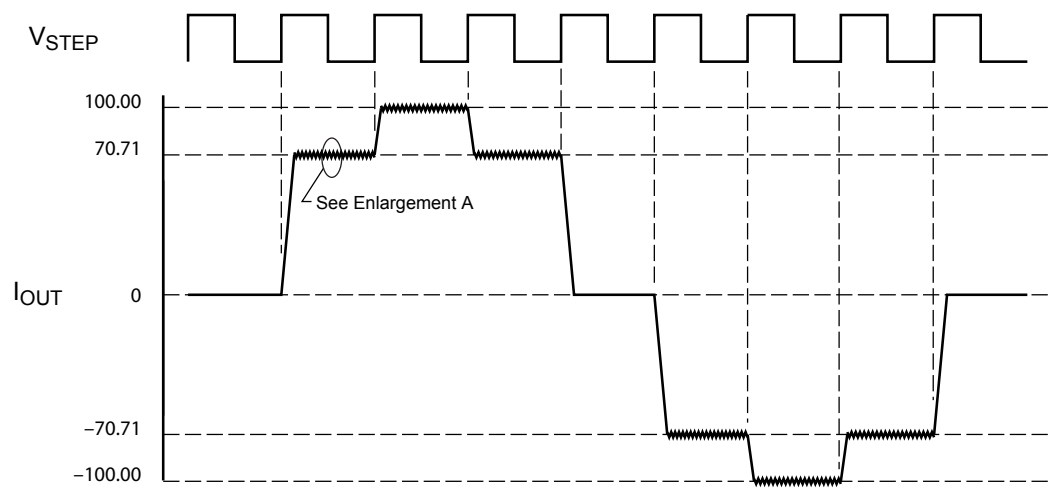


Figure 7: Current Decay Modes Timing Chart

APPLICATION LAYOUT

Layout. The printed circuit board should use a heavy ground-plane. For optimum electrical and thermal performance, the A4988 must be soldered directly onto the board. Pins 3 and 18 are internally fused, which provides a path for enhanced thermal dissipation. These pins should be soldered directly to an exposed surface on the PCB that connects to thermal vias are used to transfer heat to other layers of the PCB.

In order to minimize the effects of ground bounce and offset issues, it is important to have a low-impedance single-point ground, known as a *star ground*, located very close to the device. By making the connection between the pad and the ground plane directly under the A4988, that area becomes an ideal location for a star ground point. A low-impedance ground will prevent ground bounce during high-current operation and ensure that the supply voltage remains stable at the input terminal.

The two input capacitors should be placed in parallel, and as close to the device supply pins as possible. The ceramic capacitor (CIN1) should be closer to the pins than the bulk capacitor (CIN2). This is necessary because the ceramic capacitor will be responsible for delivering the high-frequency current components. The sense resistors, RSx, should have a very low-impedance path to ground, because they must carry a large current while supporting very accurate voltage measurements by the current sense comparators. Long ground traces will cause additional voltage drops, adversely affecting the ability of the comparators to accurately measure the current in the windings. The SENSEx pins have very short traces to the RSx resistors and very thick, low-impedance traces directly to the star ground under the device. If possible, there should be no other components on the sense circuits.

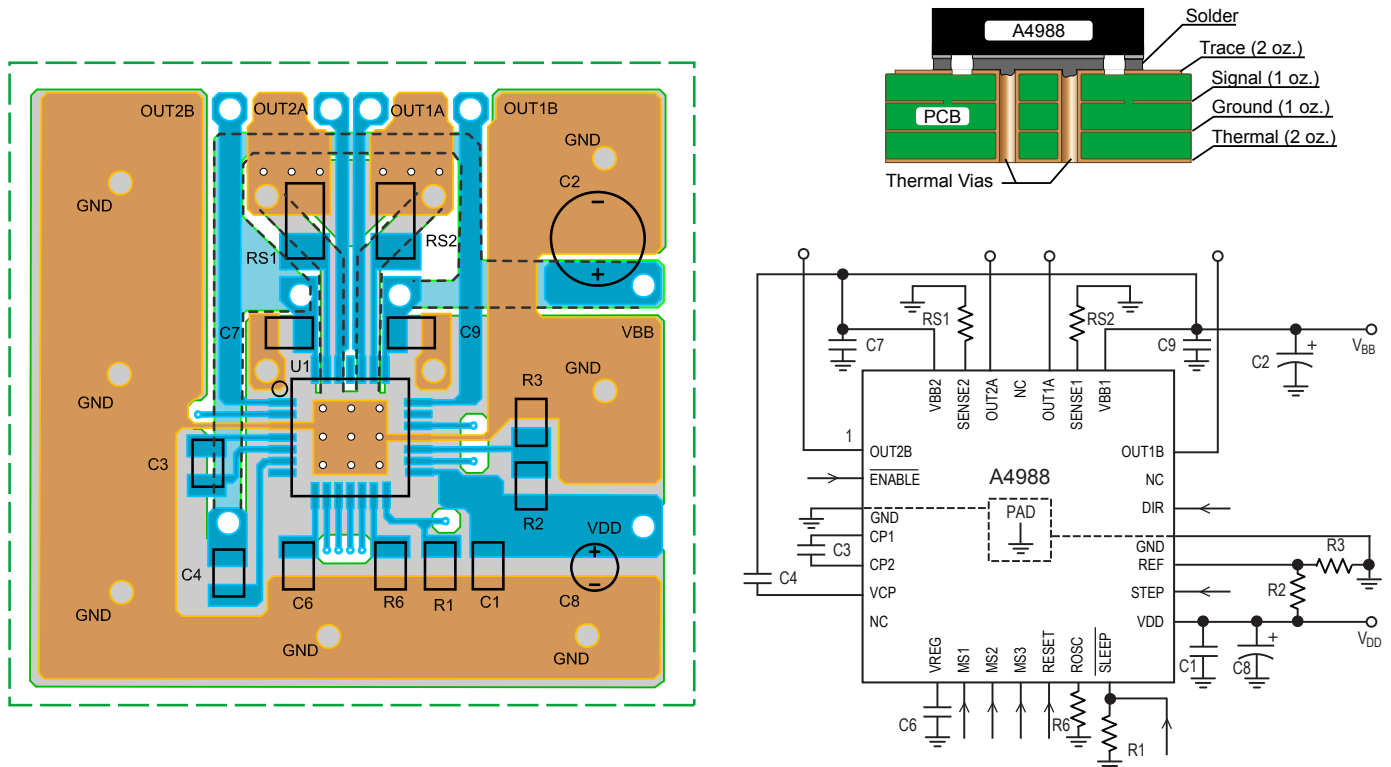
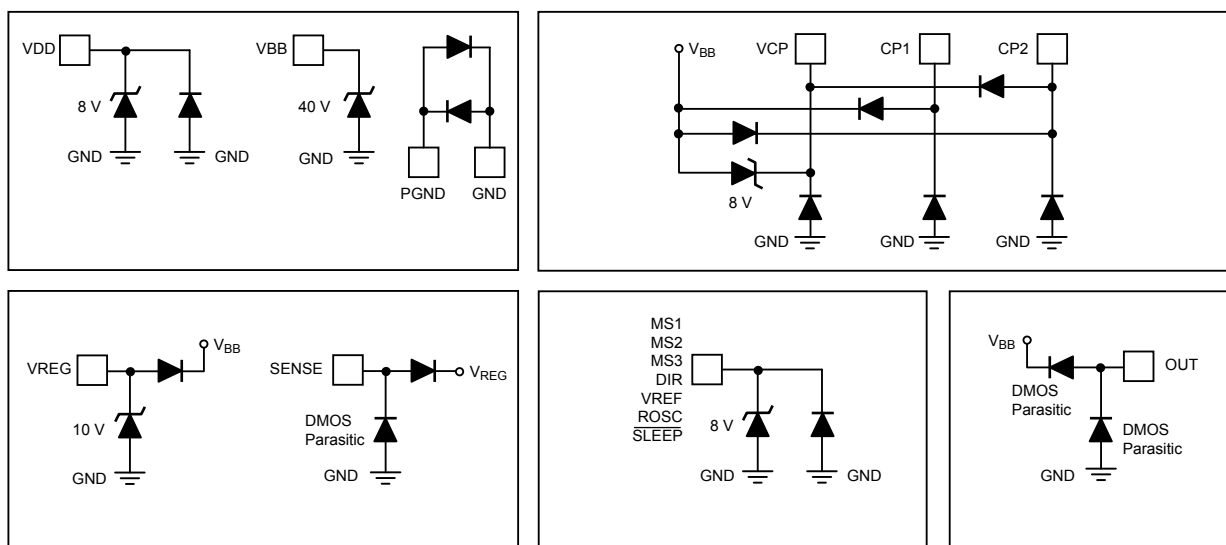
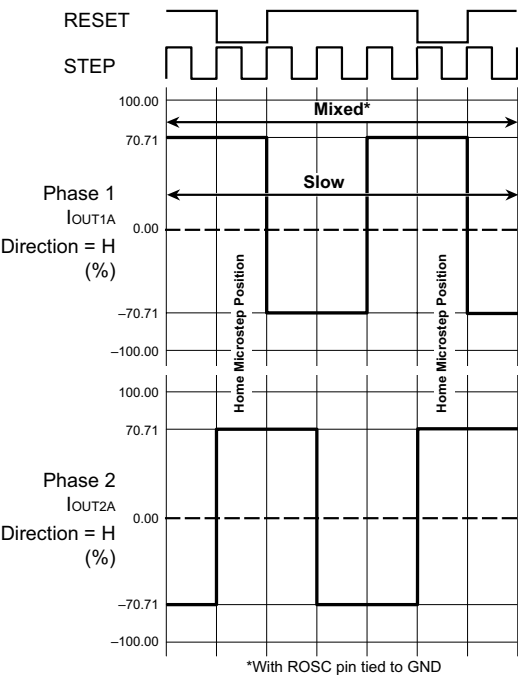


Figure 8: Typical Application and Circuit Layout

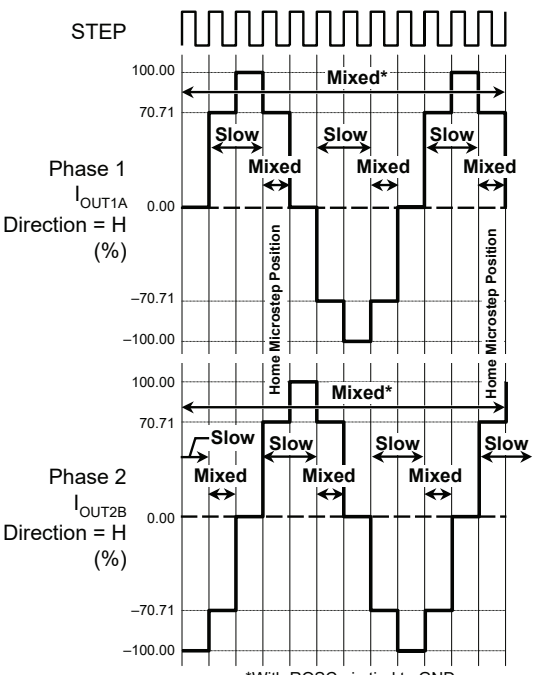
PIN CIRCUIT DIAGRAMS





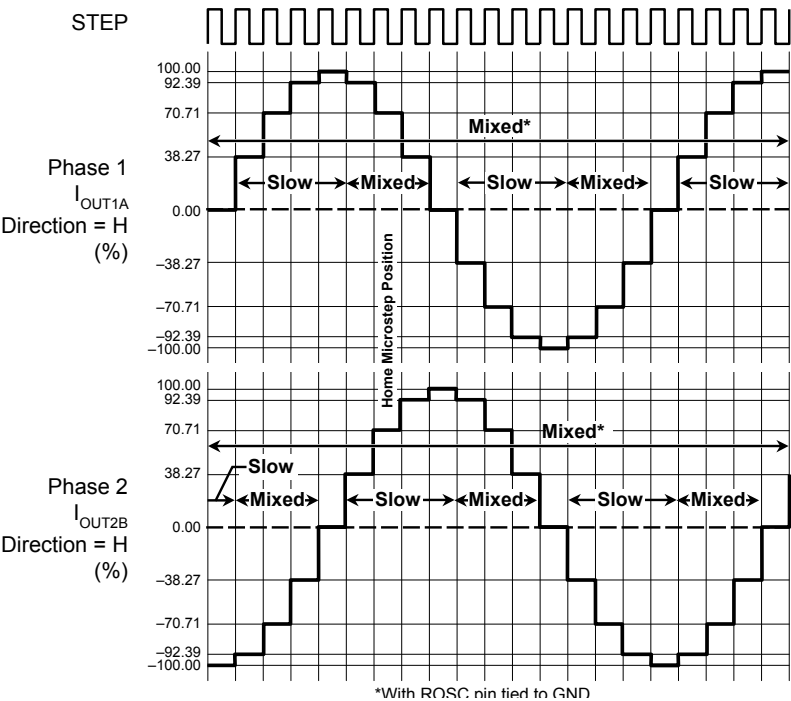
DIR= H

Figure 9: Decay Mode for Full-Step Increments



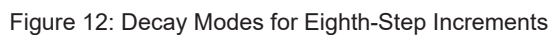
DIR= H

Figure 10: Decay Modes for Half-Step Increments



DIR= H

Figure 11: Decay Modes for Quarter-Step Increments



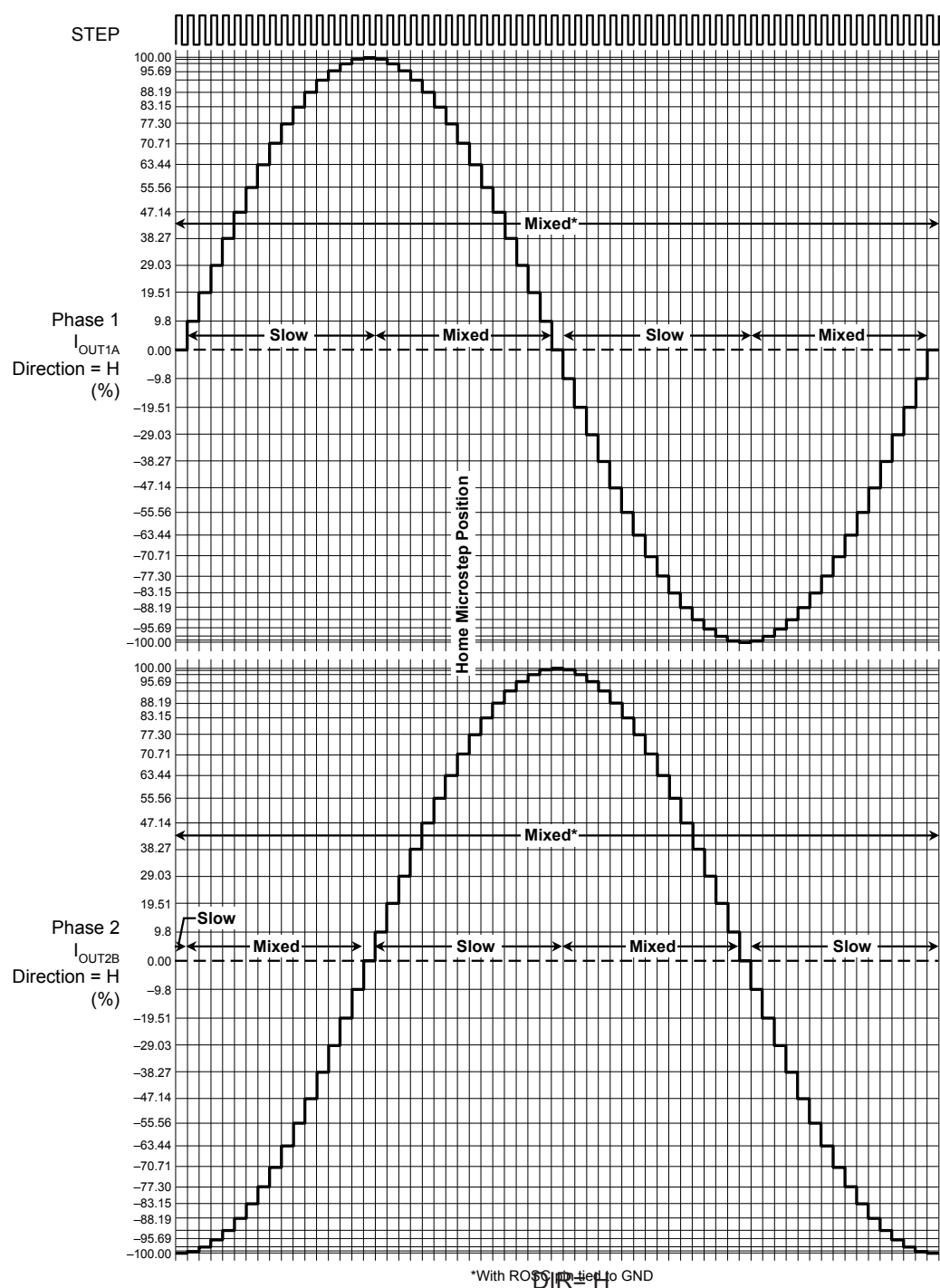


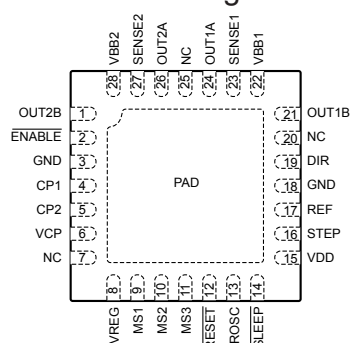
Figure 13: Decay Modes for Sixteenth-Step Increments

Table 2: Step Sequencing Settings

Home microstep position at Step Angle 45°; DIR = H

Full Step #	Half Step #	1/4 Step #	1/8 Step #	1/16 Step #	Phase 1 Current [% I _{tripMax}] (%)	Phase 2 Current [% I _{tripMax}] (%)	Step Angle (°)	Full Step #	Half Step #	1/4 Step #	1/8 Step #	1/16 Step #	Phase 1 Current [% I _{tripMax}] (%)	Phase 2 Current [% I _{tripMax}] (%)	Step Angle (°)
	1	1	1	1	100.00	0.00	0.0		5	9	17	33	-100.00	0.00	180.0
				2	99.52	9.80	5.6					34	-99.52	-9.80	185.6
			2	3	98.08	19.51	11.3				18	35	-98.08	-19.51	191.3
				4	95.69	29.03	16.9					36	-95.69	-29.03	196.9
		2	3	5	92.39	38.27	22.5			10	19	37	-92.39	-38.27	202.5
				6	88.19	47.14	28.1					38	-88.19	-47.14	208.1
			4	7	83.15	55.56	33.8				20	39	-83.15	-55.56	213.8
				8	77.30	63.44	39.4					40	-77.30	-63.44	219.4
1	2	3	5	9	70.71	70.71	45.0	3	6	11	21	41	-70.71	-70.71	225.0
				10	63.44	77.30	50.6					42	-63.44	-77.30	230.6
			6	11	55.56	83.15	56.3				22	43	-55.56	-83.15	236.3
				12	47.14	88.19	61.9					44	-47.14	-88.19	241.9
		4	7	13	38.27	92.39	67.5			12	23	45	-38.27	-92.39	247.5
				14	29.03	95.69	73.1					46	-29.03	-95.69	253.1
			8	15	19.51	98.08	78.8				24	47	-19.51	-98.08	258.8
				16	9.80	99.52	84.4					48	-9.80	-99.52	264.4
	3	5	9	17	0.00	100.00	90.0		7	13	25	49	0.00	-100.00	270.0
				18	-9.80	99.52	95.6					50	9.80	-99.52	275.6
			10	19	-19.51	98.08	101.3				26	51	19.51	-98.08	281.3
				20	-29.03	95.69	106.9					52	29.03	-95.69	286.9
		6	11	21	-38.27	92.39	112.5			14	27	53	38.27	-92.39	292.5
				22	-47.14	88.19	118.1					54	47.14	-88.19	298.1
			12	23	-55.56	83.15	123.8				28	55	55.56	-83.15	303.8
				24	-63.44	77.30	129.4					56	63.44	-77.30	309.4
2	4	7	13	25	-70.71	70.71	135.0	4	8	15	29	57	70.71	-70.71	315.0
				26	-77.30	63.44	140.6					58	77.30	-63.44	320.6
			14	27	-83.15	55.56	146.3				30	59	83.15	-55.56	326.3
				28	-88.19	47.14	151.9					60	88.19	-47.14	331.9
		8	15	29	-92.39	38.27	157.5			16	31	61	92.39	-38.27	337.5
				30	-95.69	29.03	163.1					62	95.69	-29.03	343.1
			16	31	-98.08	19.51	168.8				32	63	98.08	-19.51	348.8
				32	-99.52	9.80	174.4					64	99.52	-9.80	354.4

Pinout Diagram

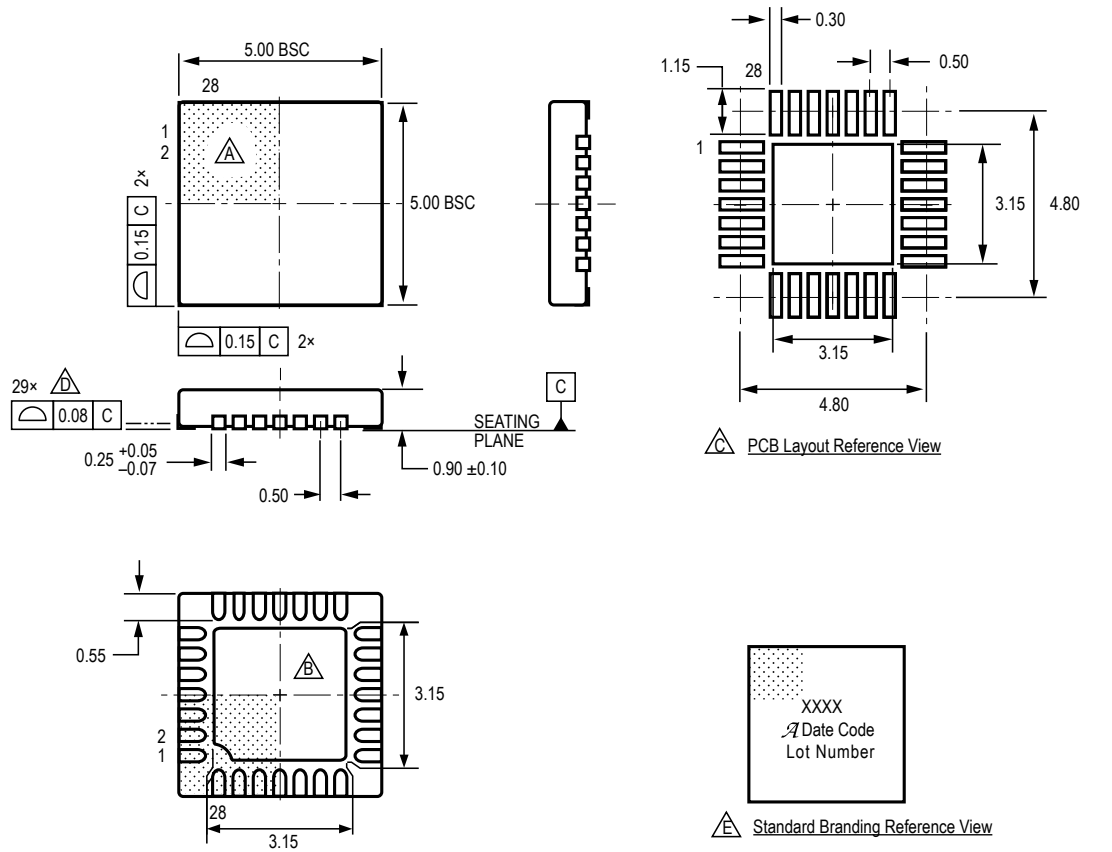


Terminal List Table

Name	Number	Description
CP1	4	Charge pump capacitor terminal
CP2	5	Charge pump capacitor terminal
VCP	6	Reservoir capacitor terminal
VREG	8	Regulator decoupling terminal
MS1	9	Logic input
MS2	10	Logic input
MS3	11	Logic input
$\overline{\text{RESET}}$	12	Logic input
ROSC	13	Timing set
$\overline{\text{SLEEP}}$	14	Logic input
VDD	15	Logic supply
STEP	16	Logic input
REF	17	G_m reference voltage input
GND	3, 18	Ground*
DIR	19	Logic input
OUT1B	21	DMOS Full Bridge 1 Output B
VBB1	22	Load supply
SENSE1	23	Sense resistor terminal for Bridge 1
OUT1A	24	DMOS Full Bridge 1 Output A
OUT2A	26	DMOS Full Bridge 2 Output A
SENSE2	27	Sense resistor terminal for Bridge 2
VBB2	28	Load supply
OUT2B	1	DMOS Full Bridge 2 Output B
$\overline{\text{ENABLE}}$	2	Logic input
NC	7, 20, 25	No connection
PAD	–	Exposed pad for enhanced thermal dissipation*

*The GND pins must be tied together externally by connecting to the PAD ground plane under the device.

ET Package, 28-Pin QFN with Exposed Thermal Pad



For Reference Only; not for tooling use
(reference DWG-0000378, Rev. 3)
Dimensions in millimeters
Exact case and lead configuration at supplier discretion within limits shown

- Terminal #1 mark area
- Exposed thermal pad (reference only, terminal #1 identifier appearance at supplier discretion)
- Reference land pattern layout (reference IPC7351 QFN50P500X500X100-29V1M);
All pads a minimum of 0.20 mm from all adjacent pads; adjust as necessary to meet application process requirements and PCB layout tolerances; when mounting on a multilayer PCB, thermal vias at the exposed thermal pad land can improve thermal dissipation (reference EIA/JEDEC Standard JESD51-5)
- Coplanarity includes exposed thermal pad and terminals
- Branding scale and appearance at supplier discretion

XXXX
Date Code
Lot Number

Line 1: Part Number
Line 2: Logo A, 4-Digit Date Code
Line 3: Characters 5, 6, 7, 8 of Assembly Lot Number

Revision History

Number	Date	Description
4	January 27, 2012	Updated I_{OCPST}
5	May 7, 2014	Revised text on page 9; revised Figure 8 and Table 2
6	January 14, 2016	Updated VBB, IBB, and IDD in Electrical Characteristics table
7	April 9, 2020	Minor editorial updates
8	April 5, 2022	Updated package drawing (page 19)

Copyright 2022, Allegro MicroSystems.

Allegro MicroSystems reserves the right to make, from time to time, such departures from the detail specifications as may be required to permit improvements in the performance, reliability, or manufacturability of its products. Before placing an order, the user is cautioned to verify that the information being relied upon is current.

Allegro's products are not to be used in any devices or systems, including but not limited to life support devices or systems, in which a failure of Allegro's product can reasonably be expected to cause bodily harm.

The information included herein is believed to be accurate and reliable. However, Allegro MicroSystems assumes no responsibility for its use; nor for any infringement of patents or other rights of third parties which may result from its use.

Copies of this document are considered uncontrolled documents.

For the latest version of this document, visit our website:

www.allegromicro.com