

Compound Helicopter - Assignment 1

Team Member Contribution

| S.No | Roll Number | Name | Contribution Level (0 - 5) | Specifics of contribution |
|------|-------------|--------------------|----------------------------|--|
| 1 | 25M0016 | Vishwa Karthi | 5 | Performance Estimator, Validation of conceptual design with ref. paper |
| 2 | 23B0023 | Jeet Gurbani | 5 | Mission Planner, Statistical Design, Code Integration |
| 3 | 22B0059 | Muriki Sree Baruni | 5 | Mission Planner |
| 4 | 22B0060 | Priyanshu Kumar | 5 | Engine selection & databasing |

Section 1:

Assumptions & Data

1.1 Physics Assumptions

- **Steady, incompressible flow assumed. Compressibility corrections applied using Prandtl-Glauert relations**
- **2D airfoil characteristics applied locally, No spanwise flow**
- **Tip losses approximated using Prandtl's corrections**

1.2 Environmental Assumptions

- **International Standard Atmosphere (ISA) considered.**
- **Flight operations within Troposphere.**

1.3 Vehicle Assumptions

- **Rotor geometry: 4 blades, Linear taper, Linear twist**
- **Airfoil Aerodynamics data drawn from NACA 0015 Experimental results [\[1\]](#)**

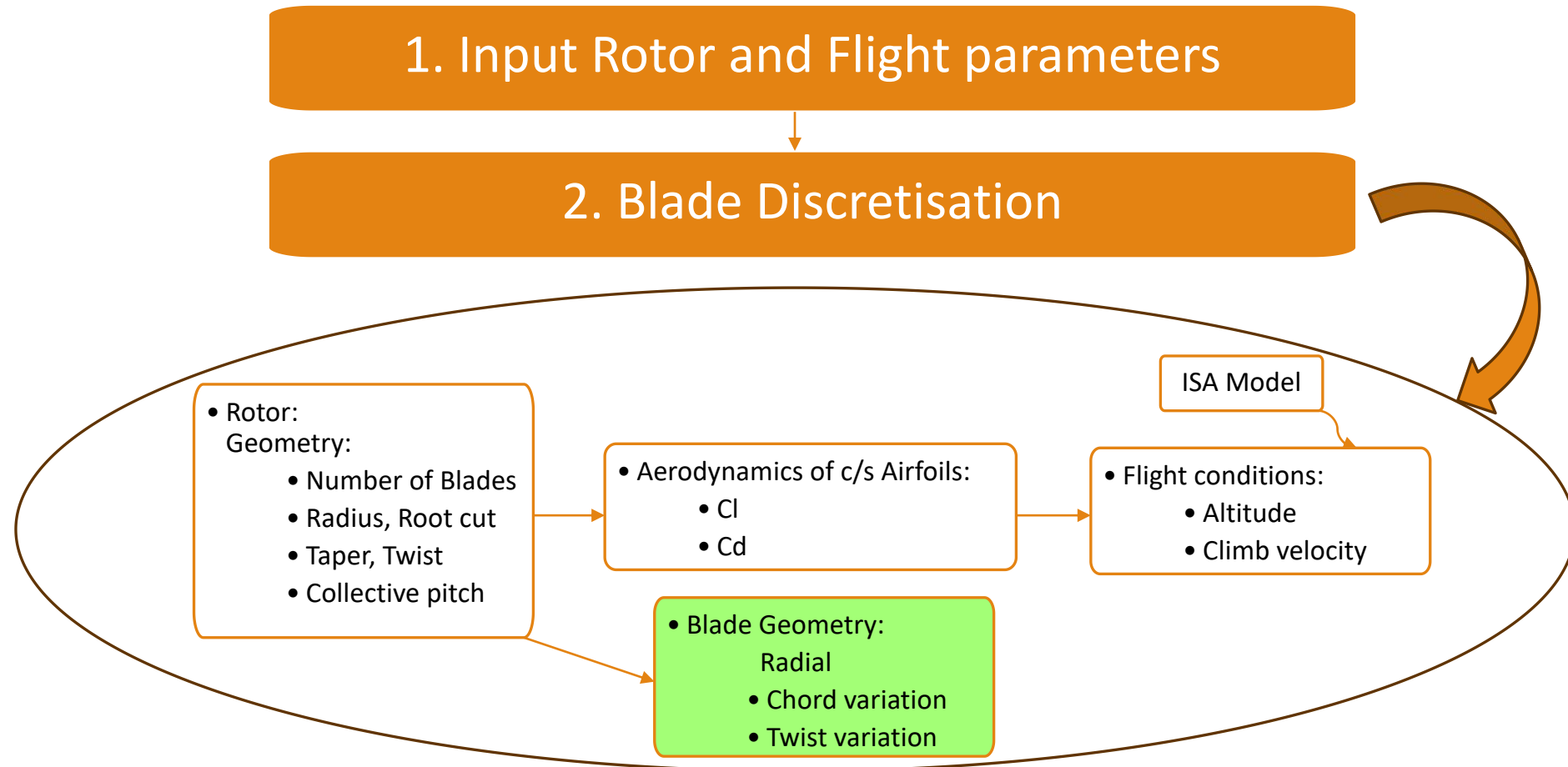
1.4 Flight Condition Assumptions

- **Rotor Performance Estimator Benchmarking carried out at SL**
- **Mission Planner Benchmarking carried out at 2000m AMSL**

Section 2:

Algorithm/Logic Flow Diagrams

2.1: Algorithm



3. Aerodynamics of sectional airfoils

- Computation of Local flow velocities (magnitude, angle), effective AoA
- Sectional Cl, Cd computation using

- Aerodynamics of c/s Airfoils:
 - Cl
 - Cd

- Stall limit check
- Local Mach computation and Compressibility Check
- Application of Prandtl-Glauert Compressibility corrections

Outputs:

Cl, Cd, Perpendicular and tangential velocity, flow angle, Effective angle of attack

The function **aerod.py** is repeatedly called to compute velocity inflow, followed by sectional lift, drag and then Thrust, Torque, Power

4. Inflow distribution

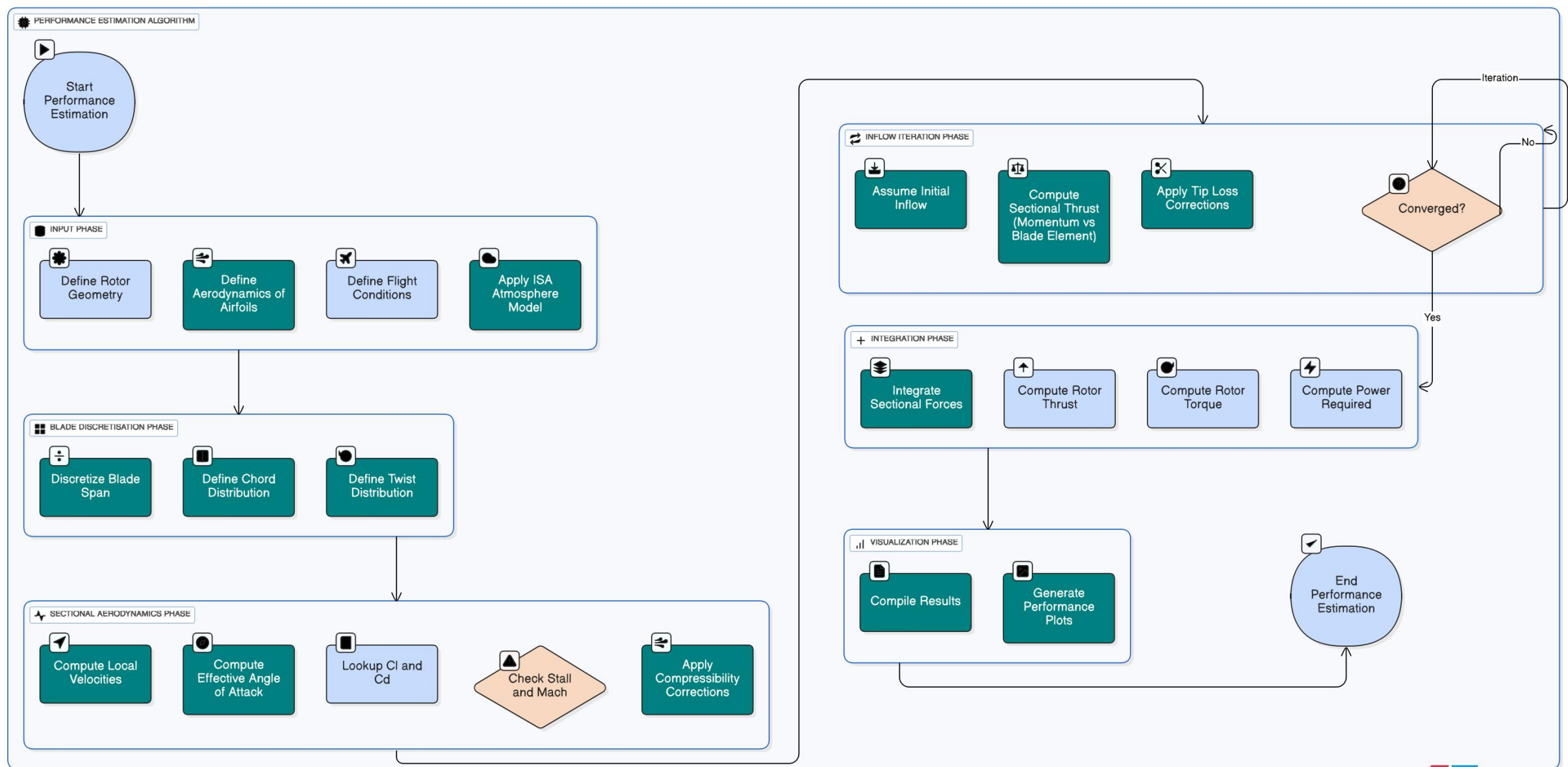
- An initial inflow distribution across blade is assumed
- Sectional thrust computed using Momentum and Blade Element theory are compared. ↓↑ Until convergence
- Inflow is updated and corrected for Tip losses using Prandtl's relation.

Output: Sectional Induced velocity

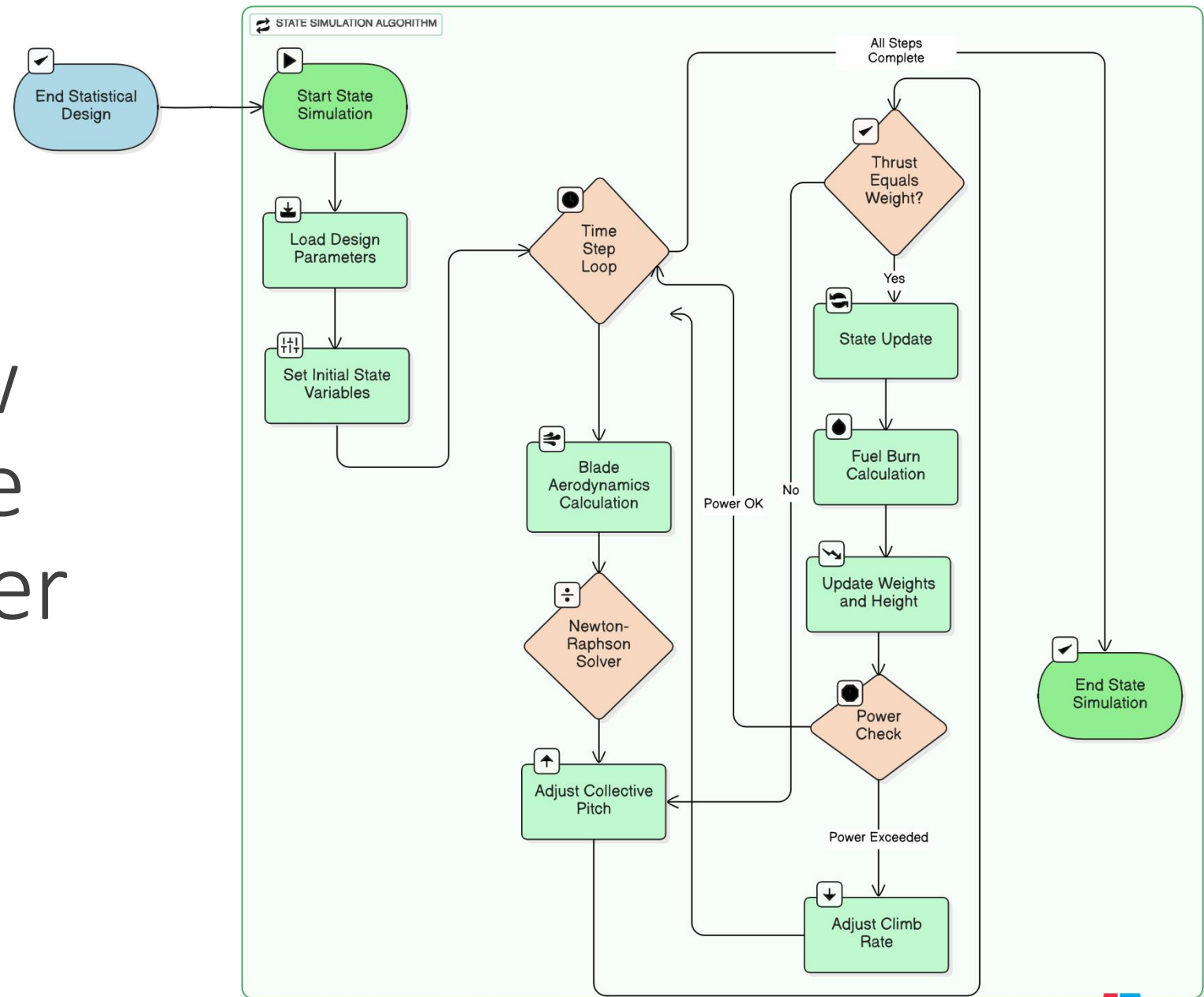
5. Performance Integration

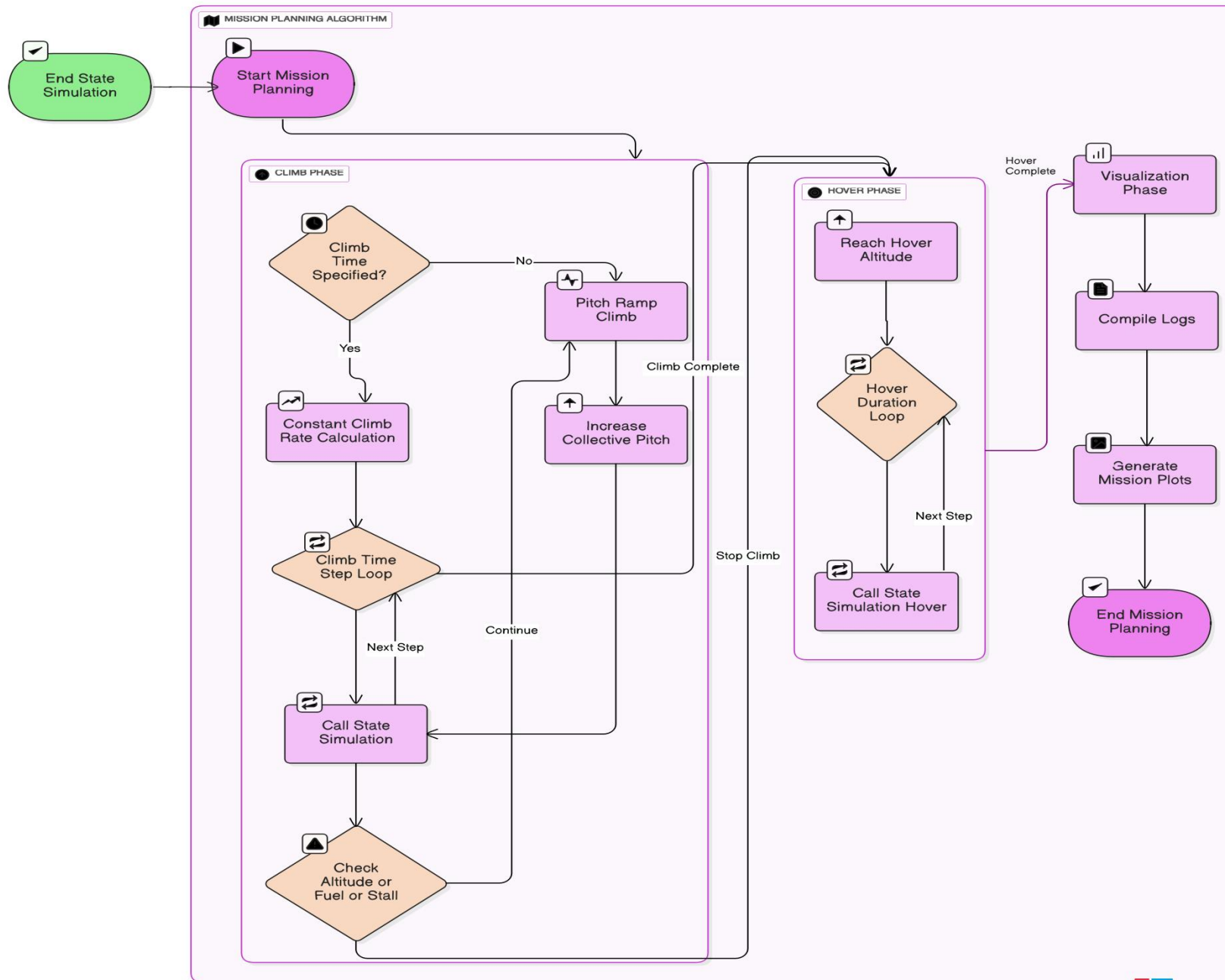
- Section inflow and airfoil characteristics called sequentially to compute blade element performances
- Sectional Thrust generated, Torque produced and power consumed are integrated from hub to tip of blades and scaled for identical blades assumed

Output: Rotor Thrust, Torque, Power



2.2: Logic Flow Diagram of the Mission Planner



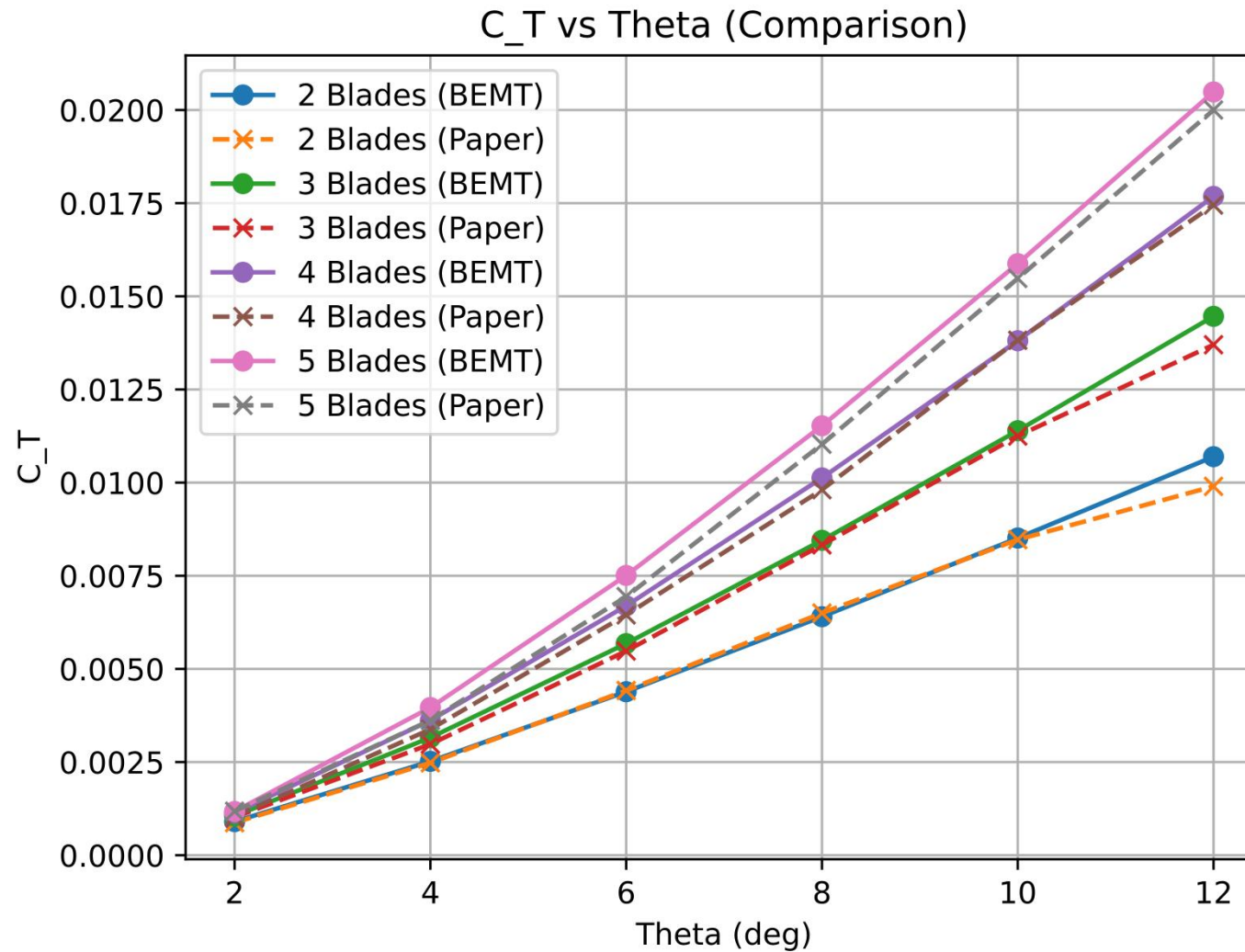


Section 3:

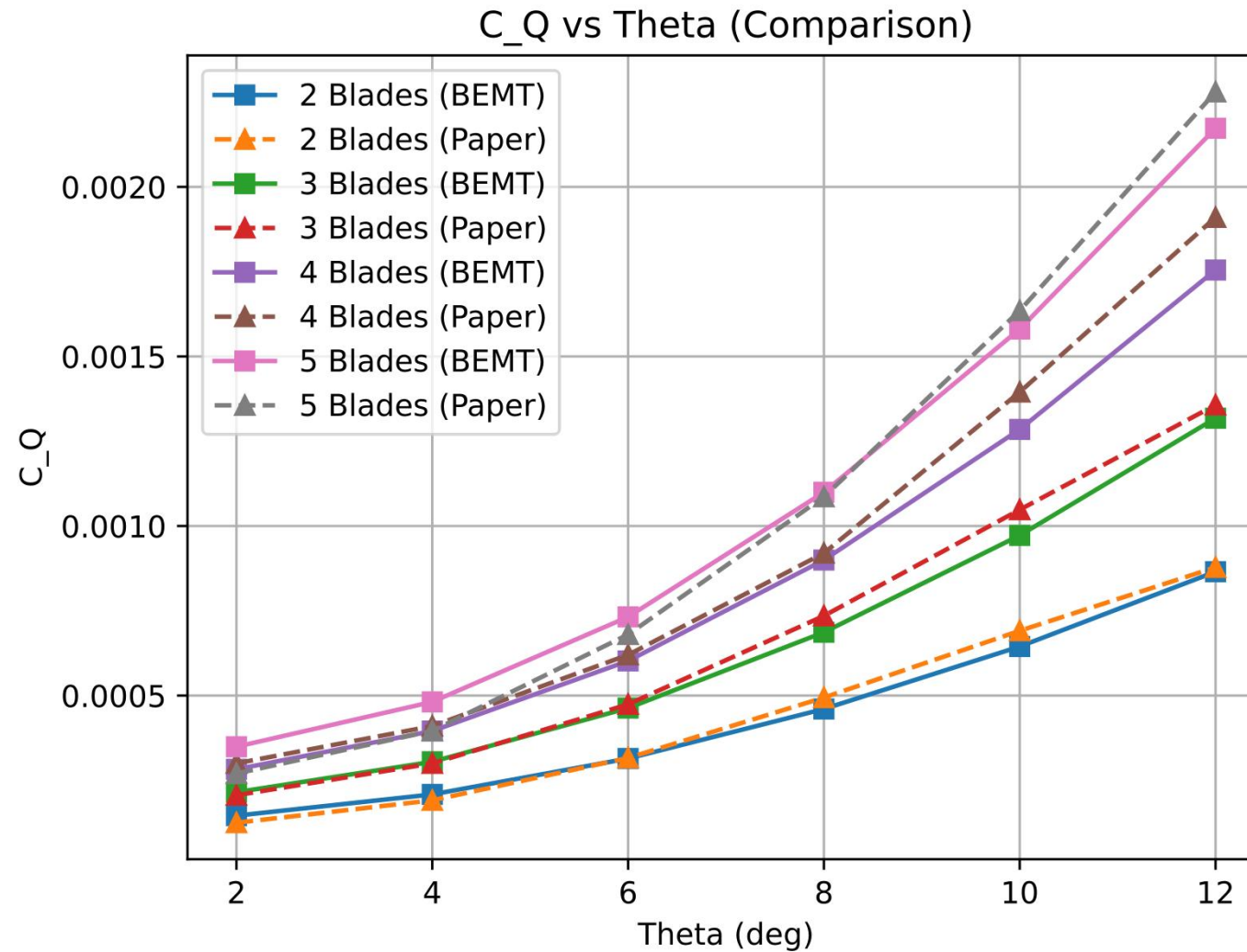
Performance Estimator Tool

Benchmarking

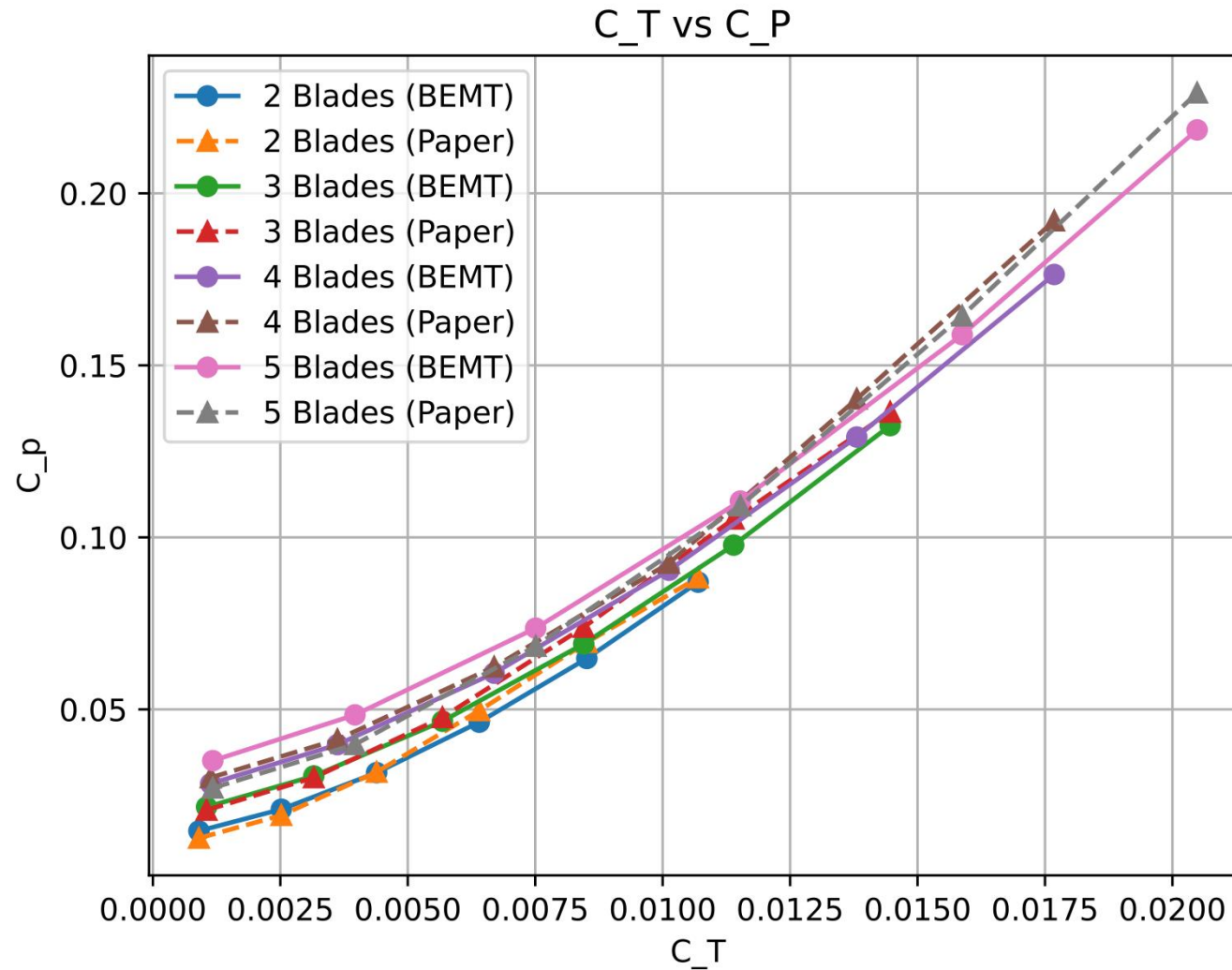
3.1: Thrust vs θ plots



3.2: Torque vs θ plots



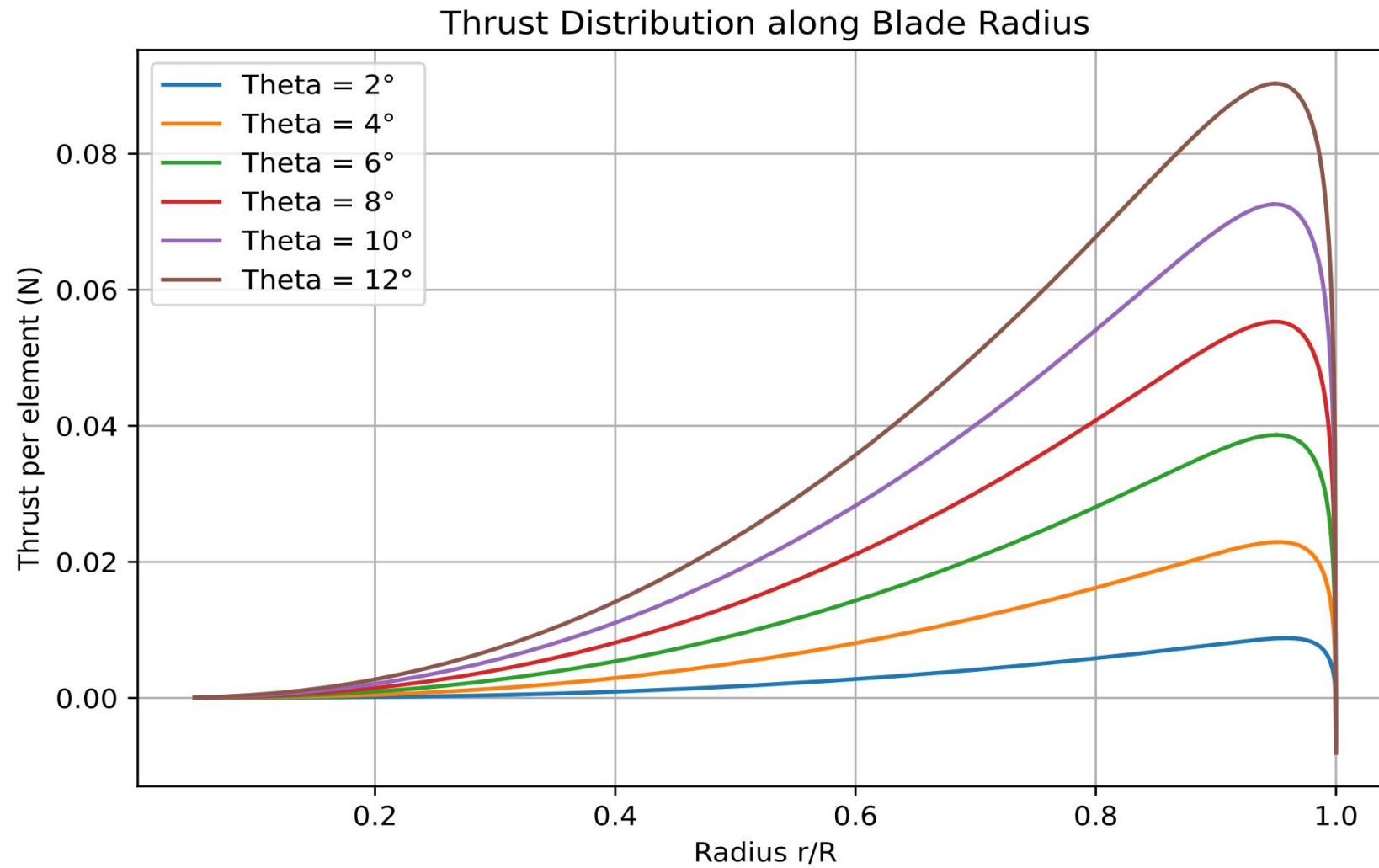
3.3: Thrust vs Power plots



3.4: Observations from the above plots

| | Plots | Comments / Observations |
|-----|--------------------|--|
| 3.1 | Thrust vs θ | <ul style="list-style-type: none">• C_t increases (\simlinearly) with increasing θ for all blade counts.• Close agreement with expt. results, however, thrust is overestimated by BEMT arising from neglected swirl losses, 3D effects. |
| 3.2 | Torque vs θ | <ul style="list-style-type: none">• C_q increases with increasing θ for all blade counts.• Close agreement with expt. results, however, torque (reflecting power requirement) is underestimated by BEMT due to discrepancies in capturing swirl, tip losses, profile drag. |
| 3.3 | Thrust vs Power | <ul style="list-style-type: none">• C_t and C_p show a nearly linear relationship, with good agreement between BEMT and experimental reference data.• However, BEMT slightly underpredicts power requirement at a given thrust (especially at higher loading) arising from simplifications and neglected losses that occur in real world. |

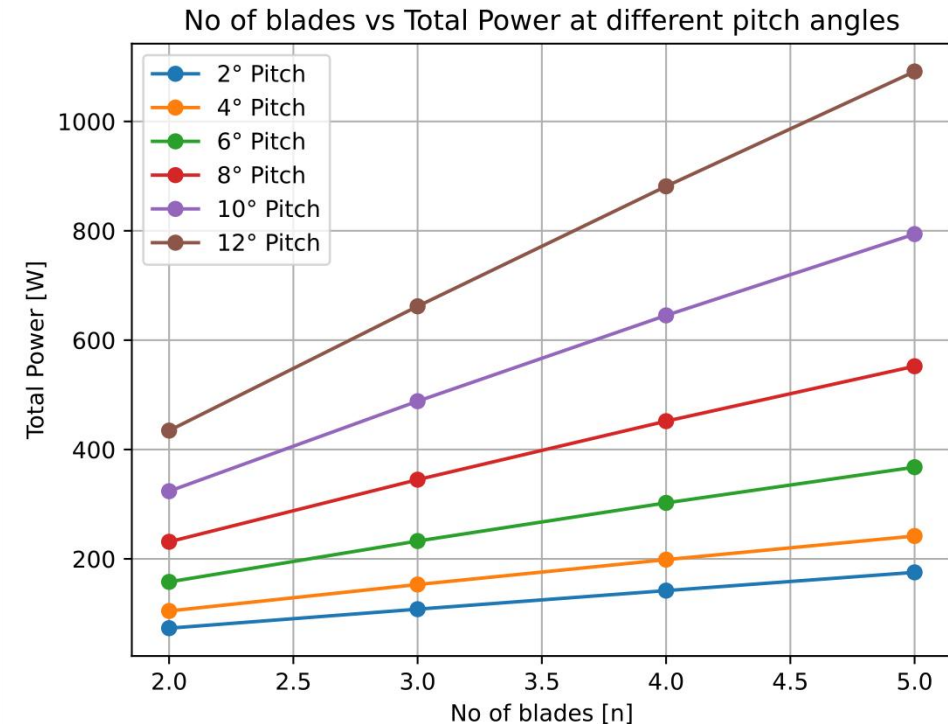
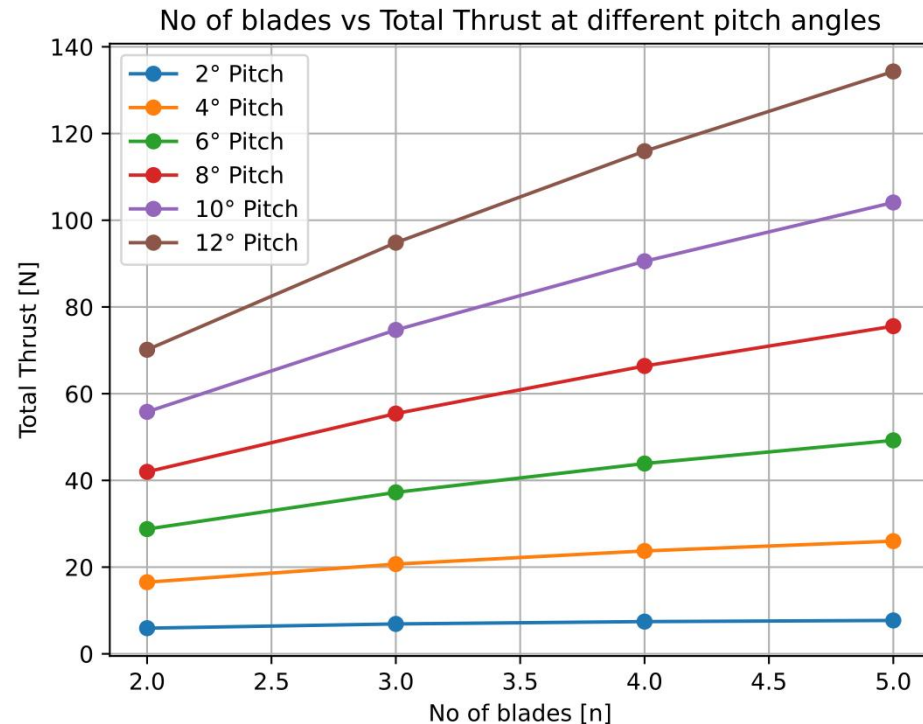
4.1: Sectional thrust from BEMT



Section 5:

Design Variable Variations

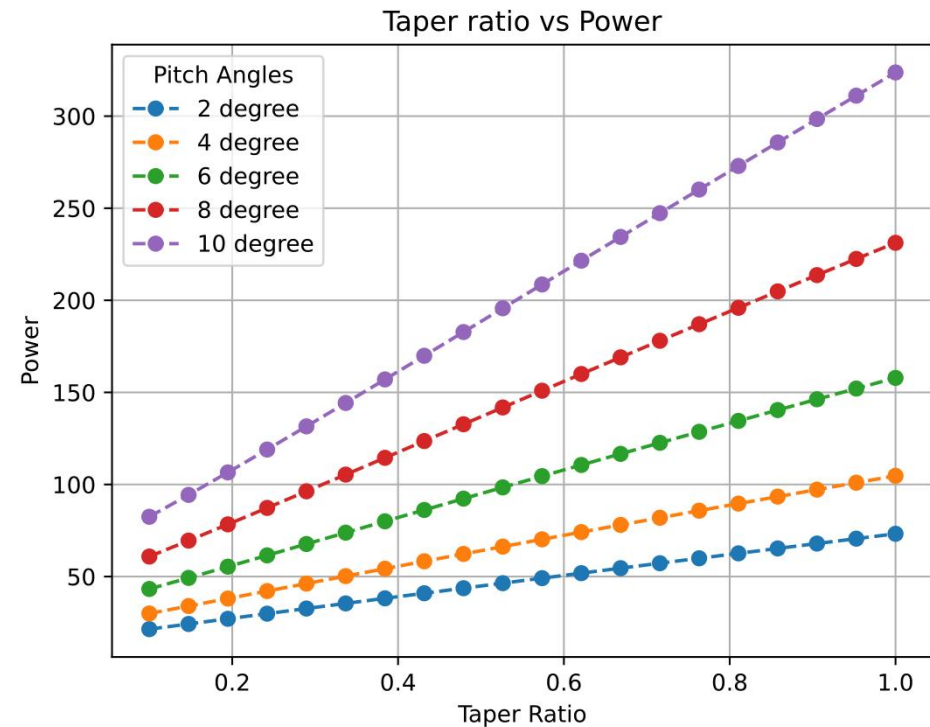
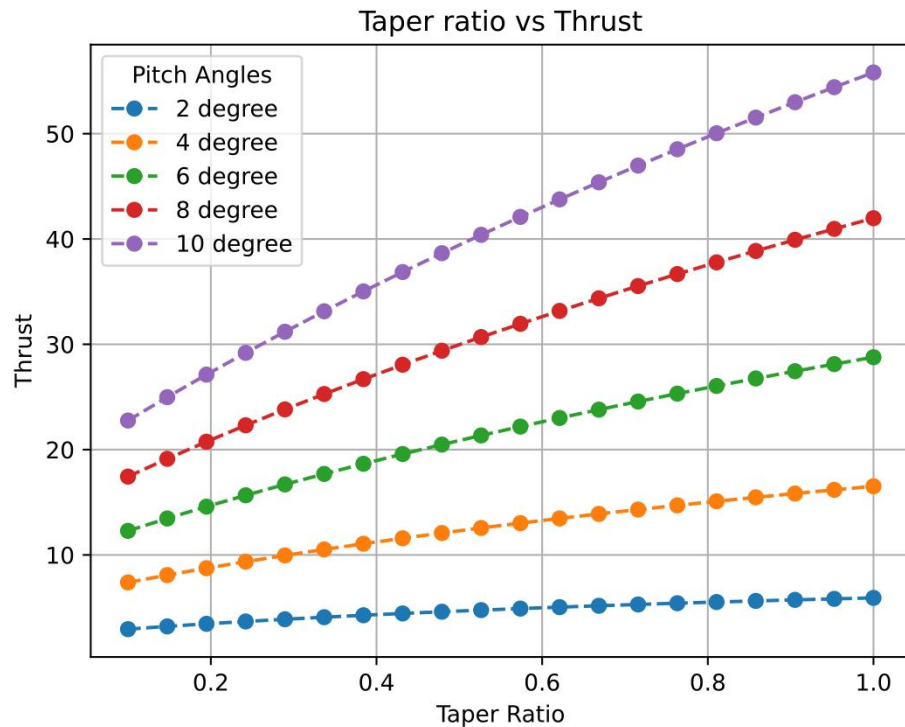
5.1: Thrust vs Blades & Power vs Blades



Discussion / Interpretation

- **Thrust generation and Power requirement increase with number of blades due to increased number of lifting surfaces.** Beyond a certain blade number, **efficiency gain diminishes**, as added blades mainly add drag and power loss rather than proportional thrust benefit.

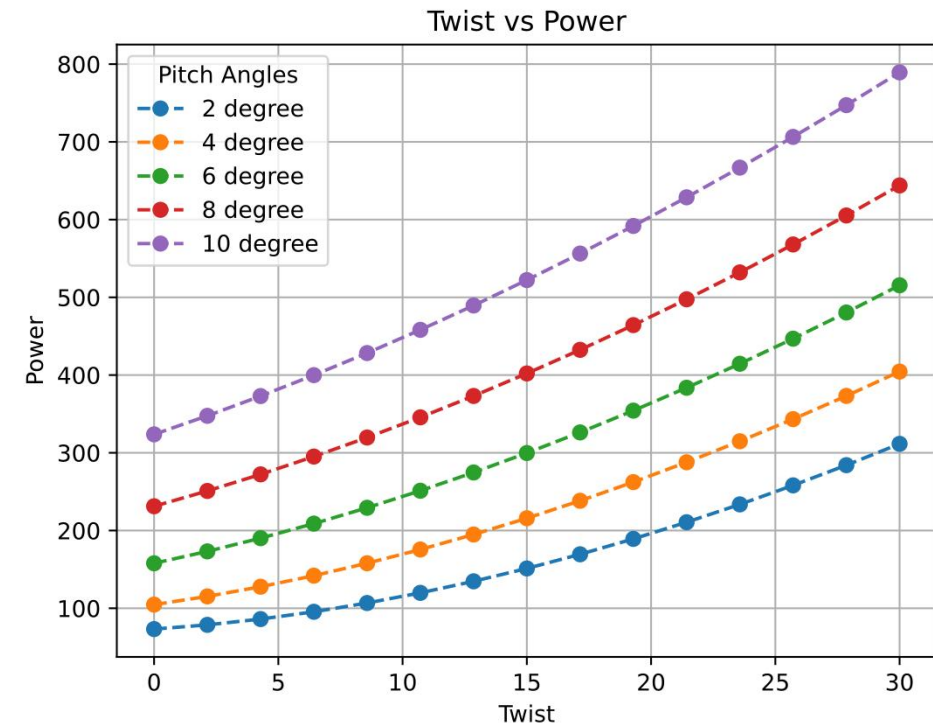
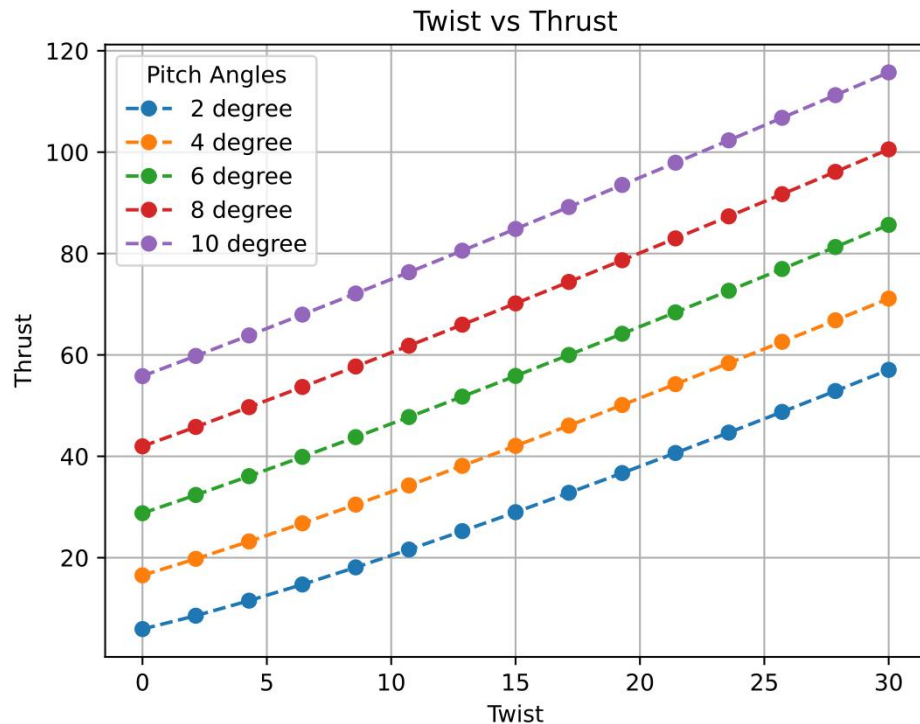
5.2: Thrust vs Taper ratio & Power vs Taper ratio



Discussion / Interpretation

- Both thrust and power rise with taper ratio. An optimal taper ratio is needed to balance thrust gains against power penalties.

5.2: Thrust vs Taper ratio & Power vs Taper ratio



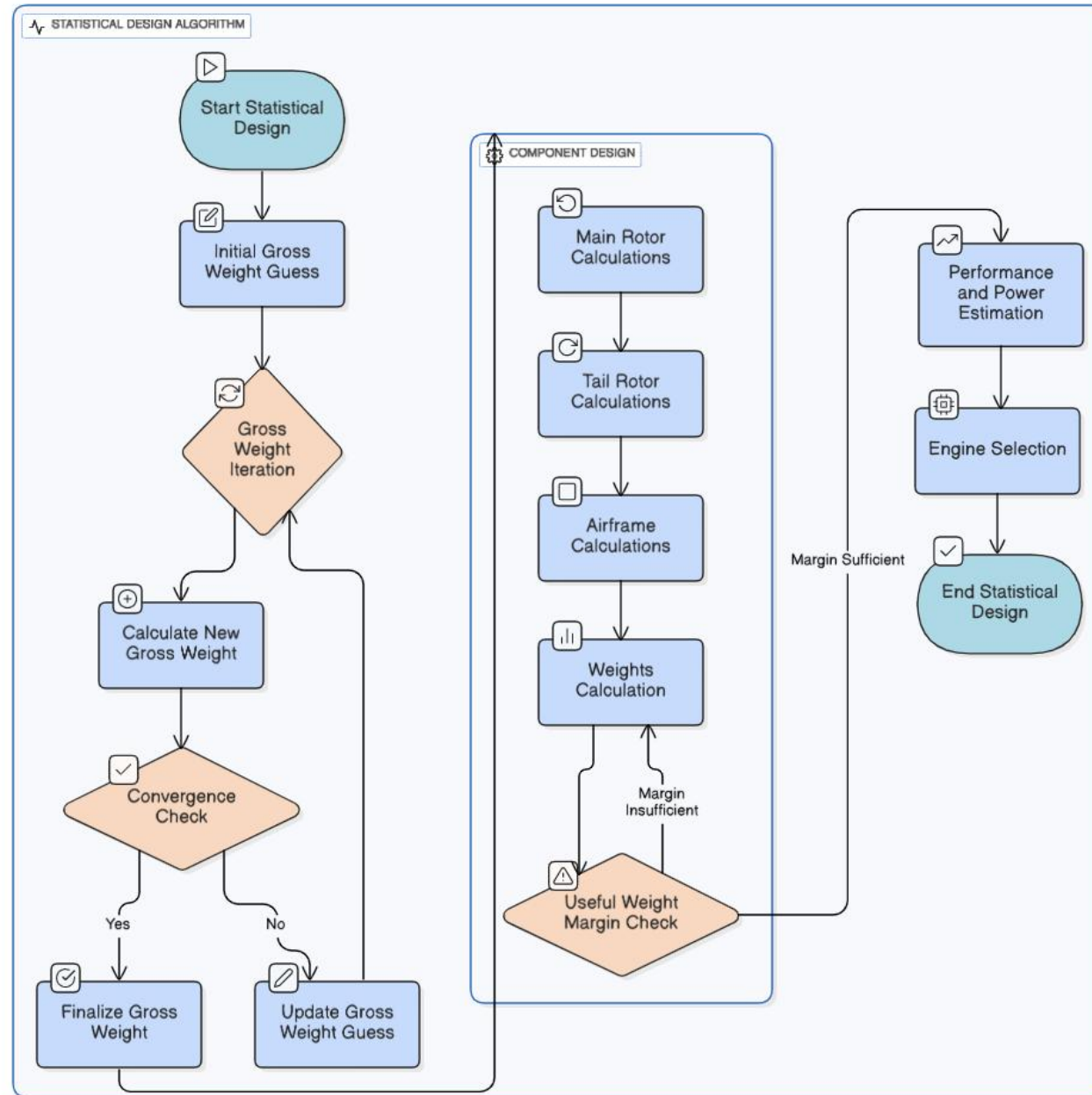
Discussion / Interpretation

- More twist improves thrust, but also increases power consumption disproportionately. The root moves slower than the tip (lower tangential speed), so increasing its angle of attack helps it contribute more lift. **Too much twist is inefficient**, as it loads the root excessively.

Section 6:

Mission Planner Test

Helicopter design (Conceptual)



Helicopter Parameters Overview

| Parameter | Value |
|--------------------------|--------|
| Disc Loading (kg/m²) | 26.56 |
| Diameter (m) | 11.2 |
| Chord (m) | 0.42 |
| Tip Speed (m/s) | 211.61 |
| Angular Velocity (rad/s) | 37.79 |
| blades | 2 |

Main Rotor

| Parameter | Value |
|--------------------|---------|
| Gross Weight (kg) | 2246.78 |
| Useful Weight (kg) | 1022.35 |
| Fuel Weight (kg) | 322.35 |
| Empty Weight (kg) | 1224.43 |

| Parameter | Value |
|--------------------------|--------|
| Never Exceed Speed (m/s) | 221.05 |
| Long Range Speed (m/s) | 176.31 |

| Parameter | Value |
|--------------------------|--------|
| Diameter (m) | 1.84 |
| Arm (m) | 6.63 |
| Tip Speed (m/s) | 202.11 |
| Angular Velocity (rad/s) | 219.79 |
| Chord (m) | 0.17 |
| bladdes | 2 |

Tail Rotor

| Parameter | Value (kW) |
|-------------------------------------|------------|
| Take-off Power (P_to) | 527.6 |
| Take-off Transmission (T_to) | 418.04 |
| Main Continuous Power (P_mc) | 891.22 |
| Main Continuous Transmission (T_mc) | 810.9 |

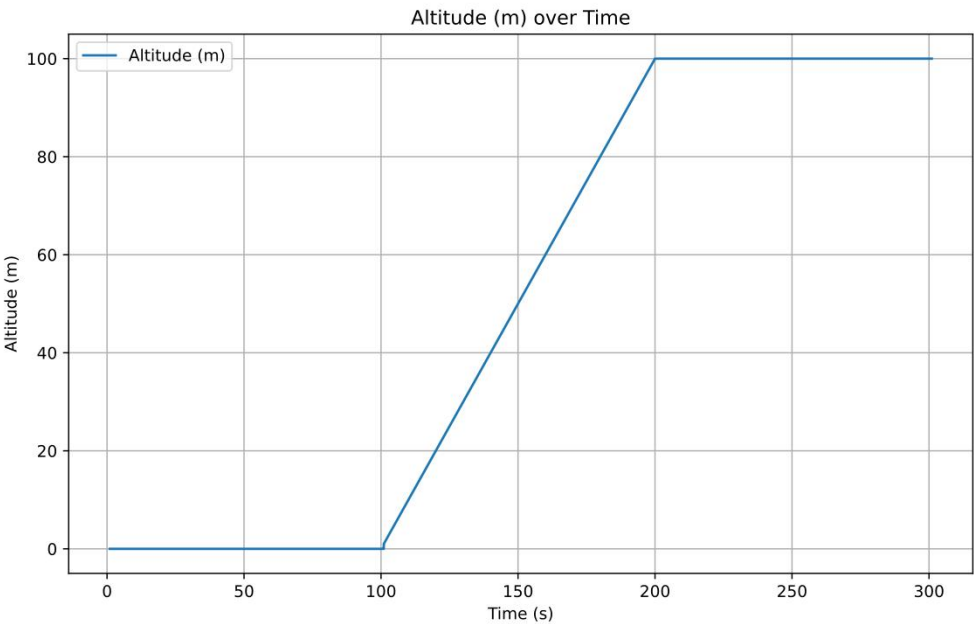
| Parameter | Value |
|-----------------------------------|-------|
| Fuselage Length (m) | 10.56 |
| Rotor-to-Tail-End Length (m) | 13.12 |
| Helicopter Height (m) | 3.29 |
| Helicopter Width (m) | 2.35 |
| Horizontal Tail Arm (m) | 5.30 |
| Horizontal Tail Surface Area (m²) | 0.73 |
| Vertical Tail Arm (m) | 6.54 |
| Avg. Vertical Tail Chord (m) | 0.46 |

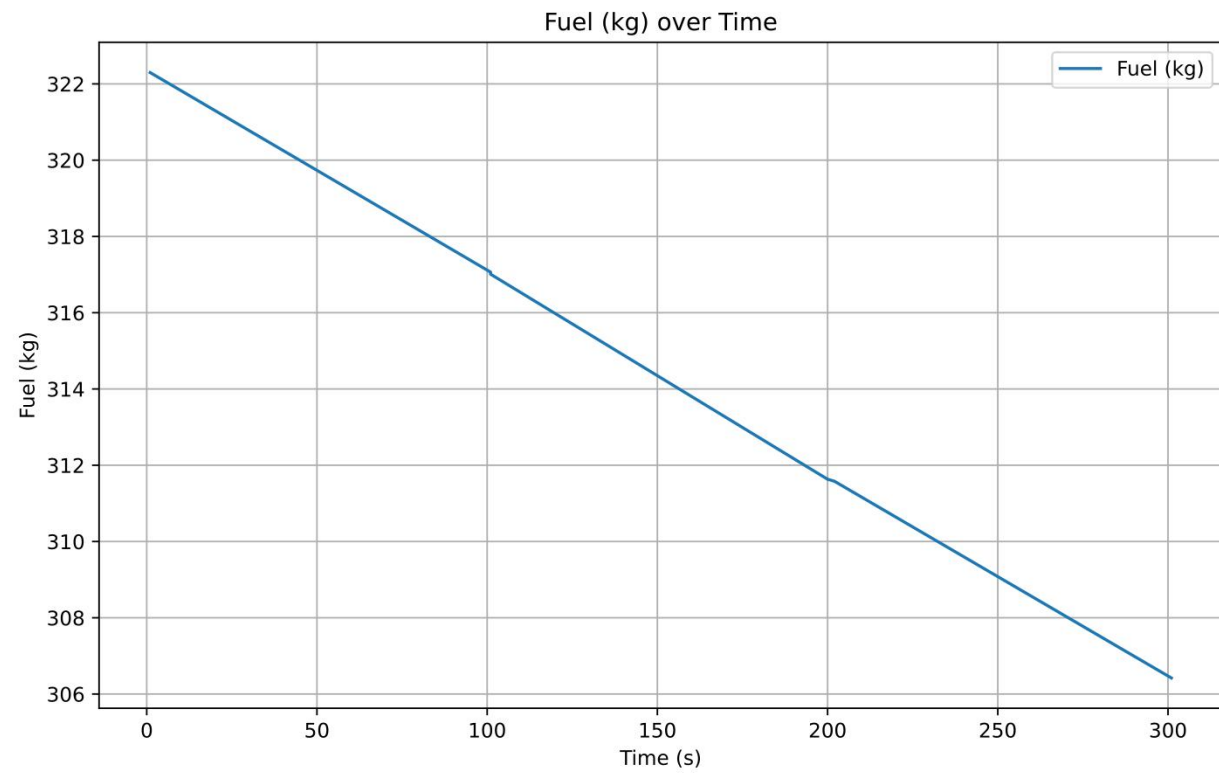
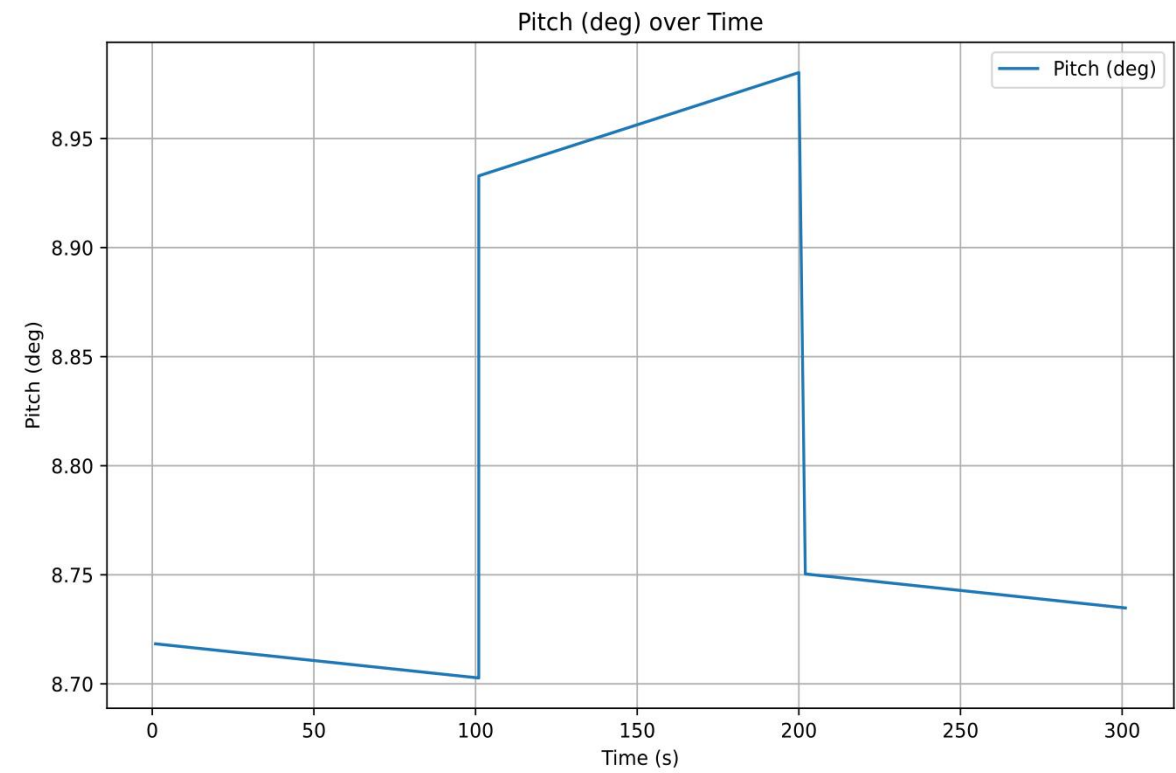
| | Plots | Value |
|-----|---|-------------|
| 6.1 | Maximum Take Off Weight based on blade stall at 2000 m AMSL | 4553.65 kgf |
| 6.2 | Maximum Take Off Weight based on power requirement at 2000 m AMSL | 3511.74 kgf |

--- 3.1: Max Take-off Weight based on blade stall at 2000m AMSL ---
Stalling at 18.00 deg, $\alpha = 12.02$ deg.
Stall pitch for main rotor found at 18.00 deg $\max_alpha = 12.02$ deg
Maximum Take-Off Weight (Stall) at 2000.0m AMSL: 4553.65 kg

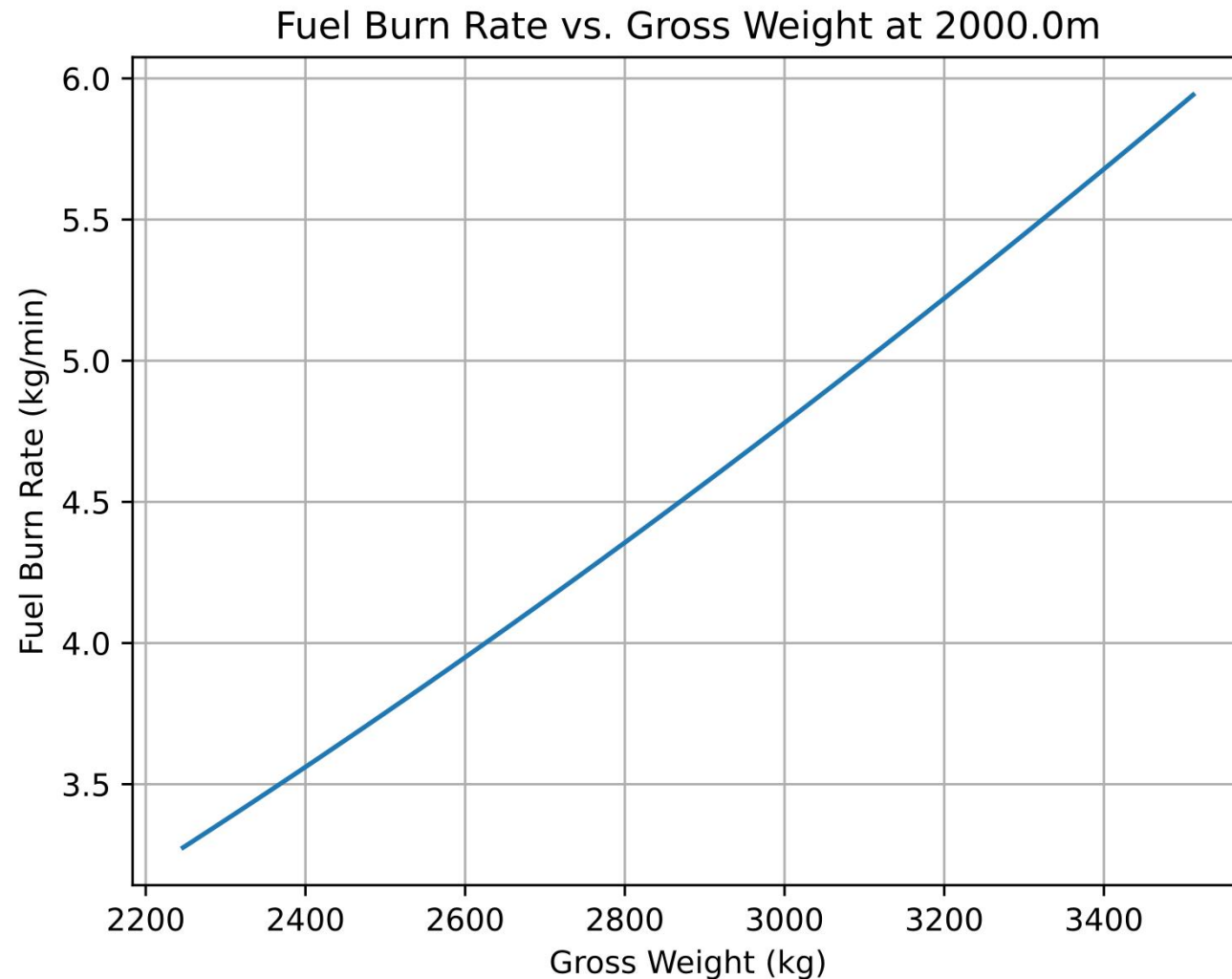
--- 3.2: Max Take-off Weight based on power requirement at 2000m AMSL ---
Maximum Take-Off Weight (Power) at 2000.0m AMSL: 3511.74 kg

| S. No. | Flight Segment | Altitude | Duration |
|--------|----------------|----------|----------|
| 1 | Hover | 0 m | 100s |
| 2 | Vertical Climb | 0 - 100m | 100s |
| 3 | Hover | 100m | 100s |

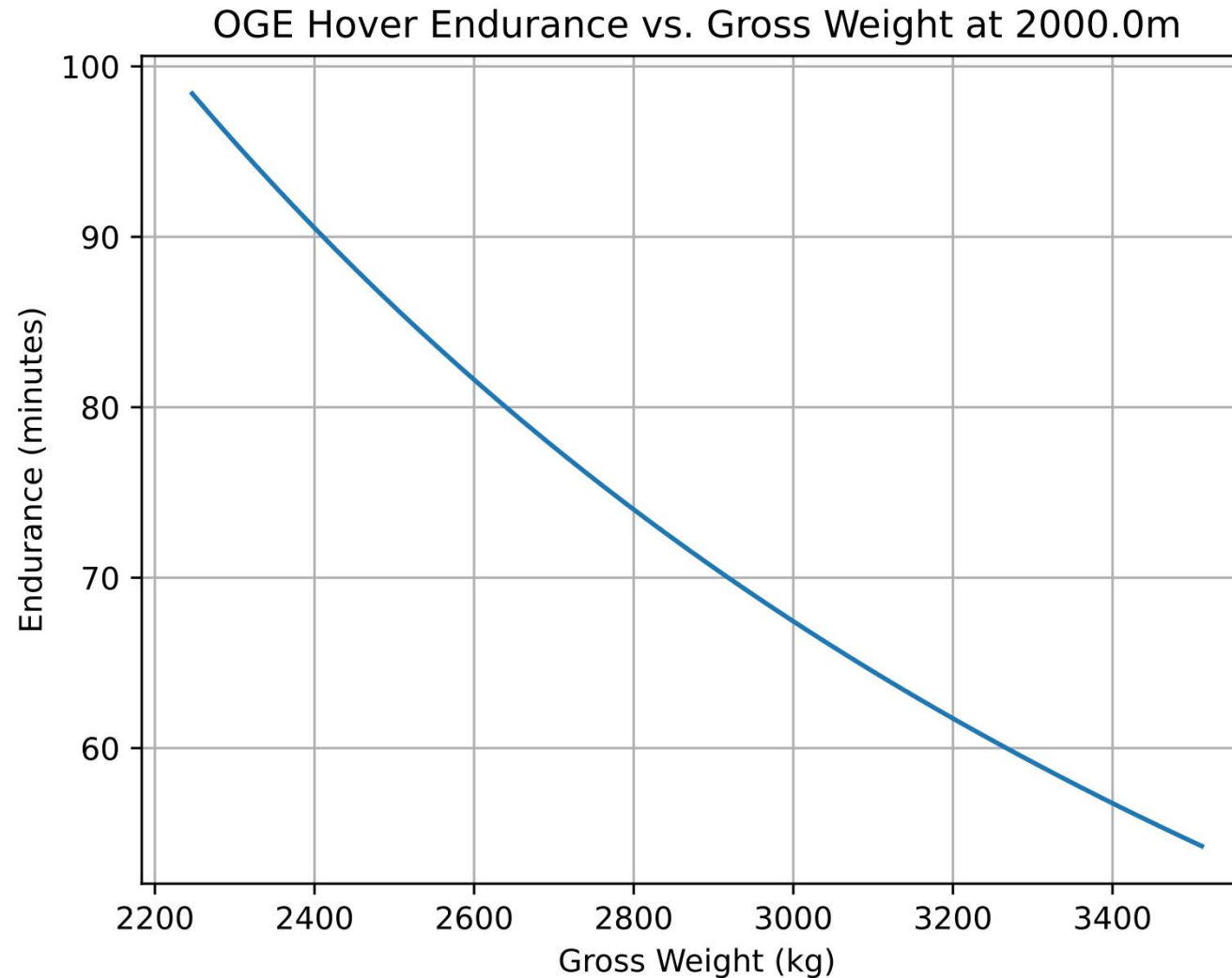




6.3: Fuel Burn Rate vs Gross Weight Plot



6.4: OGE Hover Endurance vs Take-Off-Weight plot



Acknowledgement

References

- [1] <https://ntrs.nasa.gov/archive/nasa/casi.ntrs.nasa.gov/19930081433.pdf>
- [2] [Fundamentals of Helicopter Dynamics](#)