

# Instantaneous $Q_l/Q_{\text{ext}}$ -Measurements in CEBAF incl. Transmission Line Calibration

PIT Meeting

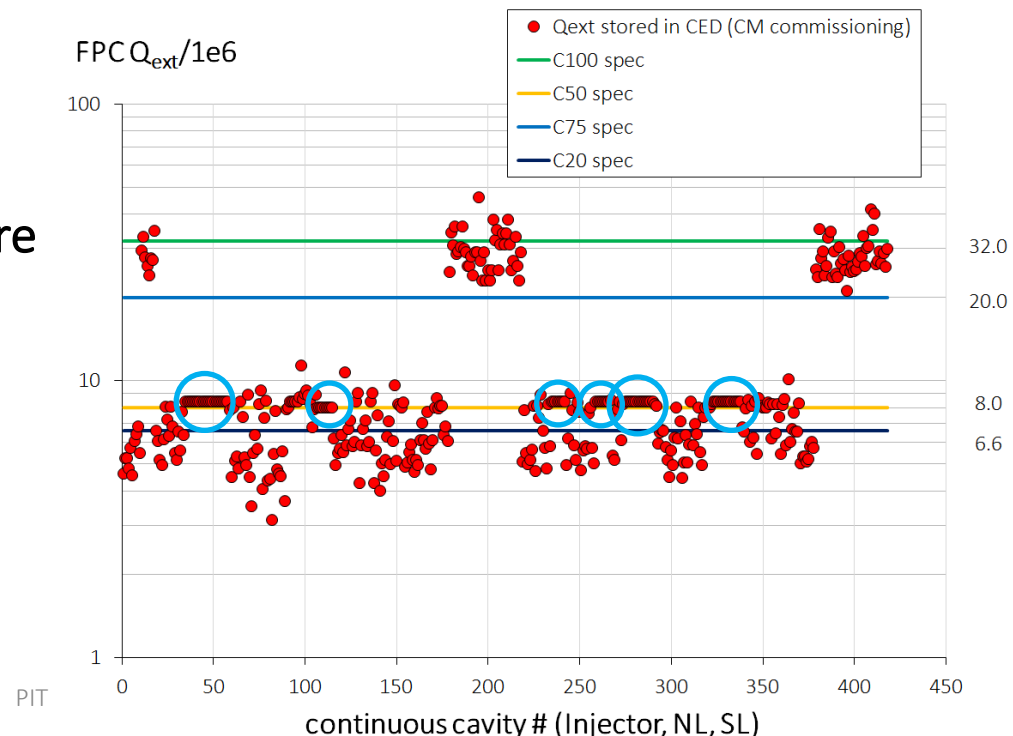
2019-08-12

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Acknowledgement: Thanks to Rongli Geng for “Brown bag” discussions on CEBAF issues

# CEBAF Element Database

- The CED carries  $Q_{\text{ext}}$ -values for cavities as measured during cryomodule commissioning (partially dating back to 2010)
- Not clear whether or not the stub-tuning was done before or after commissioning so that actual  $Q_{\text{ext}}$ -values could have changed since commissioning
- We do not know the discrepancy between commissioning (CED) and actual measured  $Q_{\text{ext}}$ -values after stub tuning
- $Q_{\text{ext}}$ -values measured during/after stub-tuning are not captured electronically
- $Q_{\text{ext}}$ -values in the CED were ever updated to my knowledge
- Values for several C50 cryomodules are just specs, no measured data were recorded in CED  
→ any data-mining of commissioning data is very tedious



# Stub Tuner Installation

O:\ees\RF\WAVEGUIDE\Stub Tuner Info

Thanks to R. Nelson and J. Benesch for providing link

Latest entry/info: 2016-01-04

North Linac (NL): 107 (53.5%) out of 200 cavities have stub tuners

NL02	NL03	NL04	NL05	NL06	NL07	NL08	NL09	NL10	NL11	NL12	NL13	NL14	NL15	NL16	NL17	NL18	NL19	NL20	NL21	NL22	NL23	NL24	NL25	NL26
6.60E+00	8.01E+00	8.40E+00	8.40E+00	8.40E+00	7.80E+00	5.29E+00	8.19E+00	5.43E+00	7.96E+00	8.33E+00	4.94E+00	8.00E+00	5.83E+00	5.83E+00	5.57E+00	4.97E+00	4.87E+00	6.07E+00	8.00E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
6.04E+00	6.83E+00	8.40E+00	8.40E+00	8.40E+00	4.47E+00	4.94E+00	9.22E+00	7.76E+00	8.40E+00	8.26E+00	7.65E+00	6.15E+00	6.69E+00	6.69E+00	7.48E+00	6.05E+00	5.04E+00	7.00E+00	8.60E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
5.15E+00	5.48E+00	8.40E+00	8.40E+00	8.40E+00	8.00E+00	8.90E+00	4.05E+00	4.78E+00	8.40E+00	8.06E+00	7.41E+00	4.96E+00	7.16E+00	3.99E+00	9.61E+00	5.49E+00	6.08E+00	7.90E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
4.94E+00	5.15E+00	8.40E+00	8.40E+00	8.40E+00	5.14E+00	4.48E+00	7.34E+00	4.59E+00	8.40E+00	7.96E+00	6.80E+00	5.46E+00	5.79E+00	5.79E+00	5.00E+00	5.13E+00	5.88E+00	5.67E+00	8.10E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
6.12E+00	6.55E+00	8.40E+00	8.40E+00	8.40E+00	5.30E+00	3.52E+00	8.46E+00	4.51E+00	8.40E+00	8.18E+00	7.66E+00	5.68E+00	5.98E+00	5.98E+00	4.49E+00	8.20E+00	5.15E+00	7.70E+00	8.10E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
8.03E+00	5.57E+00	8.40E+00	8.40E+00	8.40E+00	4.79E+00	5.45E+00	4.36E+00	5.55E+00	8.40E+00	9.63E+00	9.34E+00	6.35E+00	8.36E+00	8.36E+00	5.16E+00	8.09E+00	4.66E+00	5.93E+00	6.36E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
7.22E+00	7.72E+00	8.40E+00	8.40E+00	8.40E+00	8.40E+00	6.37E+00	4.40E+00	3.66E+00	8.67E+00	9.71E+00	7.67E+00	5.49E+00	9.02E+00	9.02E+00	6.28E+00	8.00E+00	5.16E+00	4.77E+00	6.84E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
6.31E+00	6.33E+00	8.40E+00	8.40E+00	8.40E+00	7.40E+00	5.67E+00	3.12E+00	7.89E+00	1.13E+01	8.38E+00	3.52E+00	1.07E+01	4.26E+00	4.26E+00	7.12E+00	8.32E+00	4.95E+00	6.08E+00	6.02E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01

now C50/C75 CM  
(not updated)

South Linac (SL): 140 (70%) out of 200 cavities have stub tuners

SL02	SL03	SL04	SL05	SL06	SL07	SL08	SL09	SL10	SL11	SL12	SL13	SL14	SL15	SL16	SL17	SL18	SL19	SL20	SL21	SL22	SL23	SL24	SL25	SL26
5.07E+00	8.10E+00	8.40E+00	4.96E+00	4.72E+00	5.73E+00	8.50E+00	8.40E+00	6.64E+00	8.20E+00	8.30E+00	5.05E+00	8.00E+00	8.40E+00	8.40E+00	6.78E+00	5.44E+00	6.15E+00	5.84E+00	5.00E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
7.80E+00	7.31E+00	8.40E+00	6.19E+00	5.59E+00	6.74E+00	5.34E+00	8.40E+00	5.82E+00	8.10E+00	6.50E+00	6.35E+00	5.51E+00	8.40E+00	8.40E+00	6.51E+00	8.60E+00	8.18E+00	1.01E+01	5.30E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
5.45E+00	8.91E+00	8.40E+00	9.00E+00	5.78E+00	8.30E+00	5.16E+00	8.40E+00	8.00E+00	5.90E+00	6.43E+00	5.05E+00	4.94E+00	8.40E+00	8.40E+00	7.90E+00	8.10E+00	6.45E+00	5.99E+00	5.30E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
4.97E+00	6.58E+00	8.40E+00	7.80E+00	5.67E+00	8.00E+00	7.60E+00	8.40E+00	4.92E+00	6.50E+00	6.42E+00	5.86E+00	7.38E+00	8.40E+00	8.40E+00	8.50E+00	8.00E+00	8.20E+00	6.69E+00	5.10E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
5.16E+00	5.72E+00	8.40E+00	5.83E+00	7.60E+00	5.78E+00	7.84E+00	8.40E+00	5.98E+00	6.62E+00	8.00E+00	8.40E+00	8.00E+00	8.40E+00	8.40E+00	6.00E+00	8.00E+00	7.40E+00	7.65E+00	5.20E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
5.64E+00	4.79E+00	8.40E+00	5.17E+00	8.00E+00	5.74E+00	8.38E+00	8.40E+00	5.76E+00	6.58E+00	6.66E+00	5.81E+00	8.10E+00	8.40E+00	8.40E+00	8.10E+00	8.00E+00	5.43E+00	6.51E+00	5.80E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
8.10E+00	8.21E+00	8.40E+00	8.30E+00	5.69E+00	6.30E+00	6.10E+00	8.40E+00	8.00E+00	5.76E+00	8.10E+00	6.99E+00	8.00E+00	8.40E+00	8.40E+00	6.23E+00	8.30E+00	8.14E+00	6.51E+00	6.00E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01
4.70E+00	5.80E+00	8.40E+00	7.70E+00	5.02E+00	8.20E+00	8.20E+00	8.40E+00	4.42E+00	5.15E+00	4.98E+00	6.40E+00	8.18E+00	8.40E+00	8.40E+00	8.38E+00	8.20E+00	8.55E+00	8.29E+00	5.70E+00	3.30E+01	3.30E+01	3.30E+01	3.30E+01	3.30E+01

- C20 cavities possess the lowest  $Q_{\text{ext}}$ -values, which are never matched at any beam current level and reasonably achievable  $E_{\text{acc}}$ -values
- Reducing the vulnerability to microphonics might be a reason to favor too low  $Q_{\text{ext}}$ -values (unmatched conditions), but there are counter-arguments
- Operational consequences can be manifold:
- Larger reflections → strong standing waves in transmission lines
  - more frequent waveguide arcing and cavity tripping...
  - enhanced RF losses in waveguide components such as the cold RF windows that deposit heat in He bath → reduce 'combined  $Q_0$ '
  - Combined  $Q_0$ : We cannot differentiate between SRF wall losses and other 2 K losses in standard  $Q_0$ -measurements; the other contributions can yet be significant, e.g. we verified a 50%  $Q_0$ -reduction last year for a C50 cavity (1L13) due to different standing wave pattern in transmission line, while SRF wall losses were kept constant
  - Unnecessary power consumption

# Forward & Reflected Power

- Recall general relationships of forward and reflected power (on crest):

$$P_f = \frac{V_c^2}{R/Q \cdot Q_l} \cdot \frac{1 + \beta}{4\beta} \cdot \left\{ \left[ 1 + \frac{I_{tot} R/Q Q_l}{V_c} \right]^2 + \tan^2 \Psi \right\}$$

$$P_r = \underbrace{\frac{V_c^2}{R/Q \cdot Q_l} \cdot \frac{1 + \beta}{4\beta}}_{R_l} \cdot \left\{ \left[ \frac{\beta - 1}{\beta + 1} - \frac{I_{tot} R/Q Q_l}{V_c} \right]^2 + \tan^2 \Psi \right\}$$

$$\underbrace{P_f - P_r}_{P_{cav}} = \frac{V_c^2}{R/Q \cdot Q_0} + \underbrace{I_{tot} \cdot V_c}_{\text{beam loading}}$$

for optimum match:

$$\frac{\beta - 1}{\beta + 1} - \frac{I_{tot} R}{(\beta + 1) V_c} = 0$$

$$\rightarrow \beta_{opt} = 1 + \frac{I_{tot} R}{V_c}$$

$$\tan(\Psi) = Q_l \cdot \left( \frac{\omega_0}{\omega} - \frac{\omega}{\omega_0} \right)$$

$$\frac{1}{Q_l} = \frac{1}{Q_{ext}} + \frac{1}{Q_0}$$

$$Q_l \approx Q_{ext}$$

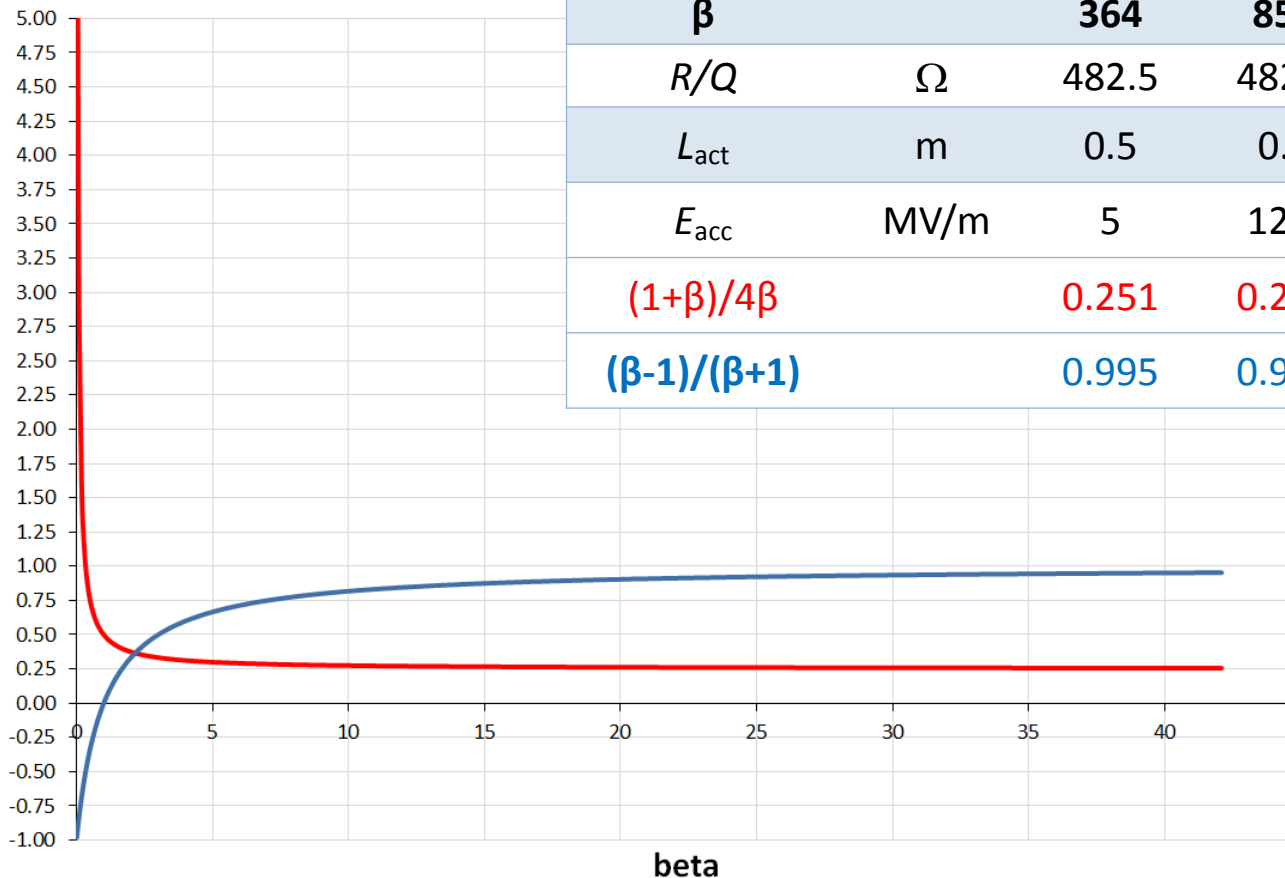
$$\text{with } \beta = \frac{Q_0}{Q_{ext}}$$

$$\rightarrow \frac{Q_0}{Q_l} = \beta + 1$$

$$R_l = \frac{R/Q \cdot Q_0}{\beta + 1} = \frac{R}{\beta + 1}$$

# CEBAF Cavity Specs and Coupling Beta

$$\frac{1 + \beta}{4\beta} \text{ and } \frac{\beta - 1}{\beta + 1}$$



Parameter	Units	C20	C50	C75	C100
$Q_0$ at 2.07 K		2.4e9	6.8e9	8.0e9	7.2e9
$Q_{\text{ext}}$ spec		6.6e6	8.0e6	2.0e7	3.2e7
$\beta$		<b>364</b>	<b>850</b>	<b>400</b>	<b>225</b>
$R/Q$	$\Omega$	482.5	482.5	525.4	868.9
$L_{\text{act}}$	m	0.5	0.5	0.4916	0.7
$E_{\text{acc}}$	MV/m	5	12.5	19.1	19.2
$(1+\beta)/4\beta$		0.251	0.250	0.251	0.251
$(\beta-1)/(\beta+1)$		0.995	0.998	0.994	0.991

for  $\beta \gg 1$ :

$$\frac{\beta - 1}{\beta + 1} \approx 1$$

$$\frac{1 + \beta}{4\beta} \approx \frac{1}{4}$$

# Forward Power & Reflected Power

- Good approximations with non-significant penalty for CEBAF:

$$P_f \approx \frac{V_c^2}{R/Q \cdot Q_l} \cdot \frac{1}{4} \cdot \left\{ \left[ 1 + \frac{I_{tot} R/Q Q_l}{V_c} \right]^2 + \tan^2 \Psi \right\}$$

$$P_r \approx \frac{V_c^2}{R/Q \cdot Q_l} \cdot \frac{1}{4} \cdot \left\{ \left[ 1 - \frac{I_{tot} R/Q Q_l}{V_c} \right]^2 + \tan^2 \Psi \right\}$$

- Each equation can be solved for  $Q_l$

# Solve for $Q_l$ using $P_{\text{fwd}}$ (no approximation yet)

$$Q_l = \frac{V_c^2}{R/Q \cdot P_f} \cdot \frac{1 + \beta}{4\beta} \cdot \left\{ \left[ 1 + \frac{R/Q I_{\text{tot}} Q_l}{V_c} \right]^2 + \tan^2 \Psi \right\}$$

$$Q_l = 2A \cdot D(\beta) \cdot \{ [1 + B \cdot Q_l]^2 + C \}$$

$$Q_l^2 + Q_l \cdot \frac{(2ABD(\beta) - 1)}{AB^2 D(\beta)} + \frac{(1 + C)}{B^2} = 0$$

$$\begin{aligned} A &= \frac{V_c^2}{R/Q \cdot P_f} & C &= \tan^2 \Psi \\ B &= \frac{I_{\text{tot}} R/Q}{V_c} & D(\beta) &= \frac{1 + \beta}{4\beta} \end{aligned}$$

$$Q_l = - \frac{(2ABD(\beta) - 1) \pm \sqrt{1 - 4ABD(\beta) - (2ABD(\beta))^2 C}}{2AB^2 D(\beta)}$$

$$AB = \frac{V_c^2}{R/Q \cdot P_f} \cdot \frac{I_{\text{tot}} R/Q}{V_c} = \frac{I_{\text{tot}} V_c}{P_f} \quad AB^2 = \frac{I_{\text{tot}} V_c}{P_f} \cdot \frac{I_{\text{tot}} R/Q}{V_c} = \frac{R/Q \cdot I_{\text{tot}}^2}{P_f}$$

$$Q_l = \frac{\frac{P_f}{2 \cdot \left( \frac{1 + \beta}{4\beta} \right)} - I_{\text{tot}} V_c \mp \frac{P_f}{2 \cdot \left( \frac{1 + \beta}{4\beta} \right)} \cdot \sqrt{1 - \frac{4I_{\text{tot}} V_c}{P_f} \left( \frac{1 + \beta}{4\beta} \right) - \frac{4I_{\text{tot}}^2 \cdot V_c^2}{P_f^2} \left( \frac{1 + \beta}{4\beta} \right)^2 \tan^2 \Psi}}{R/Q I_{\text{tot}}^2}$$



# Solve for $Q_l$ using $P_{\text{ref}}$ (no approximation yet)

- We get a similar expression when utilizing the reflected power

$$P_r = \frac{V_c^2}{R_L} \frac{1+\beta}{4\beta} \left\{ \left[ \frac{\beta-1}{1+\beta} - \frac{I_{\text{tot}} R_L}{V_c} \right]^2 + \tan^2 \Psi \right\}$$

$$Q_l = \frac{\frac{P_r}{2 \cdot \left( \frac{1+\beta}{4\beta} \right)} + I_{\text{tot}} V_c \left( \frac{\beta-1}{\beta+1} \right) \pm \frac{P_r}{2 \cdot \left( \frac{1+\beta}{4\beta} \right)} \sqrt{1 + \frac{4I_{\text{tot}} V_c}{P_r} \left( \frac{1+\beta}{4\beta} \right) \left( \frac{\beta-1}{\beta+1} \right) - \frac{4I_{\text{tot}}^2 \cdot V_c^2}{P_r^2} \left( \frac{1+\beta}{4\beta} \right)^2 \tan^2 \Psi}}{R/Q I_{\text{tot}}^2}$$

- Now let's approximate:

$$\frac{1+\beta}{4\beta} \approx \frac{1}{4} \quad \frac{\beta-1}{\beta+1} \approx 1$$

# Solve for $Q_l$ using $P_{\text{fwd}}$ and $P_{\text{ref}}$

$$Q_l(P_f, I_{\text{tot}}, V_c, \Psi, \frac{R}{Q}) = \frac{2P_f - I_{\text{tot}}V_c \oplus 2P_f \sqrt{1 - \frac{I_{\text{tot}}V_c}{P_f} - \frac{I_{\text{tot}}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi}}{R/Q I_{\text{tot}}^2}$$

$$Q_l(P_r, I_{\text{tot}}, V_c, \Psi, \frac{R}{Q}) = \frac{2P_r + I_{\text{tot}}V_c \oplus 2P_r \sqrt{1 + \frac{I_{\text{tot}}V_c}{P_r} - \frac{I_{\text{tot}}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi}}{R/Q I_{\text{tot}}^2}$$

- All dependent variables are measurable, cavity parameters are known
- **We theoretically have all information to record the loaded  $Q$  (~external  $Q$ ) of any cavity in CEBAF at any instant of time**
- **Only negative signs are valid**

# Solve for $Q_l$ using $P_{\text{fwd}}$ and $P_{\text{ref}}$

$$Q_l(P_f, I_{\text{tot}}, V_c, \Psi, \frac{R}{Q}) = \frac{2P_f - I_{\text{tot}}V_c - 2P_f \sqrt{1 - \frac{I_{\text{tot}}V_c}{P_f} - \frac{I_{\text{tot}}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi}}{R/Q I_{\text{tot}}^2}$$

$$Q_l(P_r, I_{\text{tot}}, V_c, \Psi, \frac{R}{Q}) = \frac{2P_r + I_{\text{tot}}V_c - 2P_r \sqrt{1 + \frac{I_{\text{tot}}V_c}{P_r} - \frac{I_{\text{tot}}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi}}{R/Q I_{\text{tot}}^2}$$

## Cavity parameter

CRFP (kW)

CRRP (kW)

GMES (MV/m)  $\rightarrow V_c = \text{GMES} \cdot L_{\text{act}}$

Detuning angle (T)DETA (deg.)

$R/Q$

## South linac with Hall D beam current

$$I_{\text{tot}} = \begin{pmatrix} \text{Hall A injected } I \\ \text{Hall B injected } I \\ \text{Hall C injected } I \\ \text{Hall D injected } I \end{pmatrix} \cdot \begin{pmatrix} \text{passes to Hall A} \\ \text{passes to Hall B} \\ \text{passes to Hall C} \\ 5 \end{pmatrix}^T$$

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## Beam currents and recirculating passes

IBC1H04CRCUR2 ( $\mu\text{A}$ ), MMSHLAPASS

IBC2C24CRCUR3 (nA), MMSHLBPASS

IBC3H00CRCUR4 ( $\mu\text{A}$ ), MMSHLCPASS

IBCAD00CRCUR6 (nA), MMSHLDPASS

## North linac with Hall D 6<sup>th</sup> pass in NL

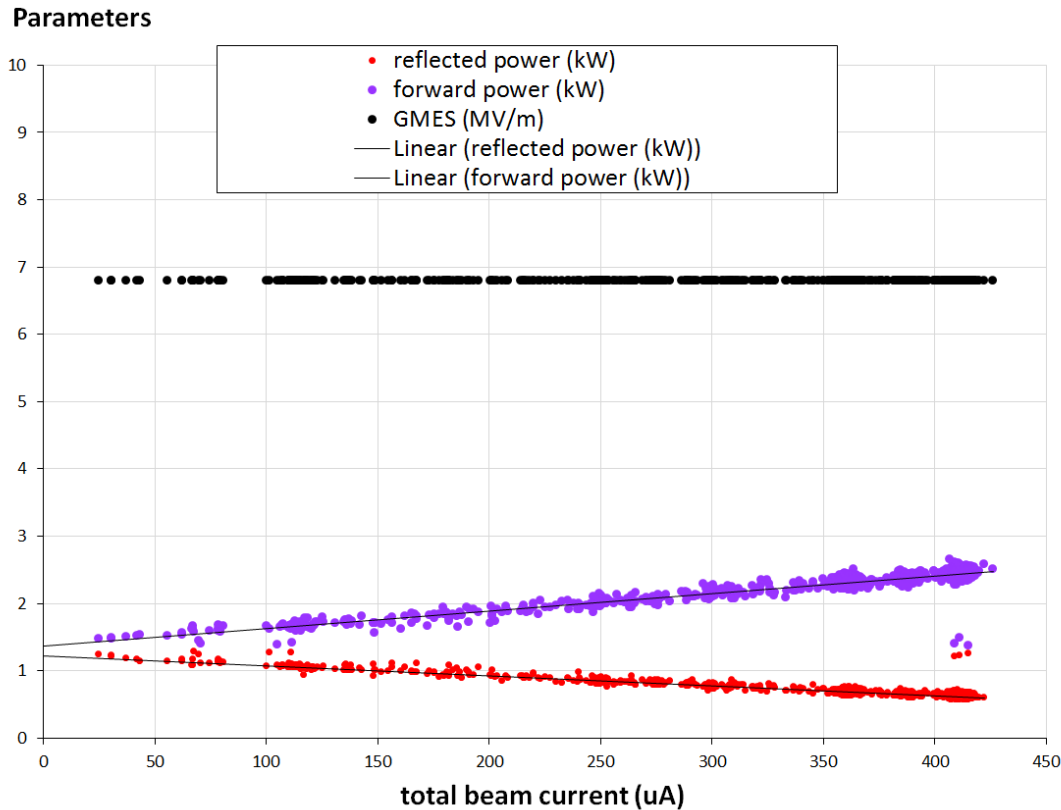
$$I_{\text{tot}} = \begin{pmatrix} \text{Hall A injected } I \\ \text{Hall B injected } I \\ \text{Hall C injected } I \\ \text{Hall D injected } I \end{pmatrix} \cdot \begin{pmatrix} \text{passes to Hall A} \\ \text{passes to Hall B} \\ \text{passes to Hall C} \\ 6 \end{pmatrix}^T$$

PIT Meeting

# Example (1L19)

## C20 cavity

### R1J4: North Linac Zone J Cavity 4



- Used archived CEBAF data
- Time Stamping:  
2018/4/6 to 2018/4/8,  
when CEBAF beam current  
was ramped up  
Same period as used for  
G.A. Krafft's in a PIT meeting  
talk for C100 cavities

Load Data

Load Data

From: Apr 6 2018 07:24

To: Apr 8 2018 08:24

☐ GMES ☐ TDETA ☒ GASK ☒ CRFP ☒ CRRP

☐ PASK ☐ PMES ☐ KMAI ☐ KCCU ☐ KFVM

☐ KMAV

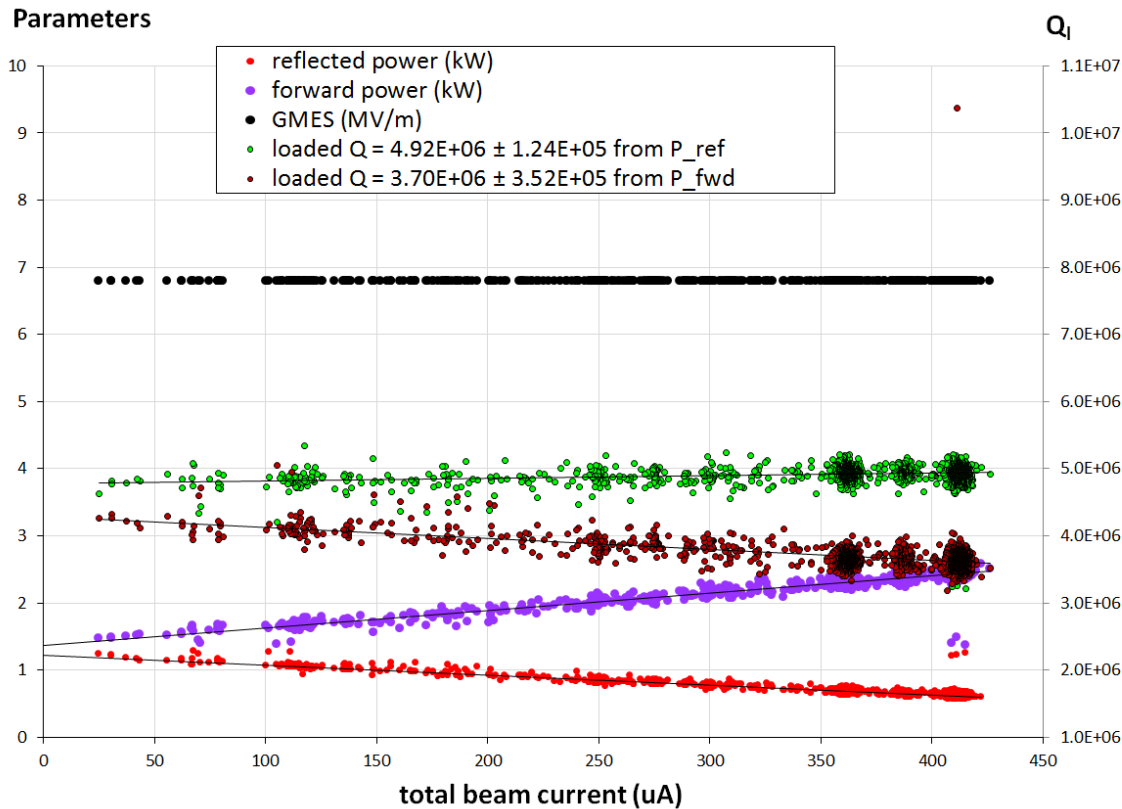
Load Close

# Example (1L19)

Mismatched cavity, no stub tuner installed → too small  $Q_i$

C20 cavity

R1J4: North Linac Zone J Cavity 4



LEM	
CavityType	C25
MaxGSET	8.8 MeV/m
OpsGsetMax	7 MeV/m
PhaseRMS	0.045 volts
Q0	1.43E+9
Qexternal	5.88E+6
TripOffset	8.051 Trips/shift
TripSlope	0.955 Trips/shift

$Q_i$  from  $P_r$

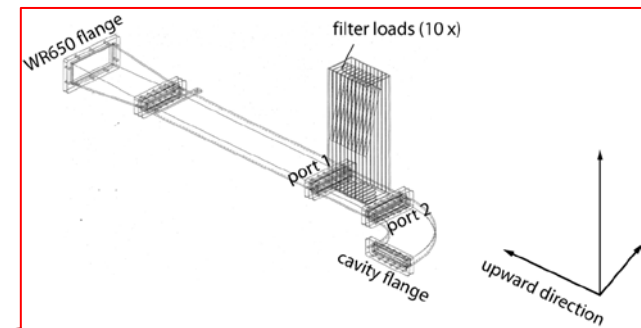
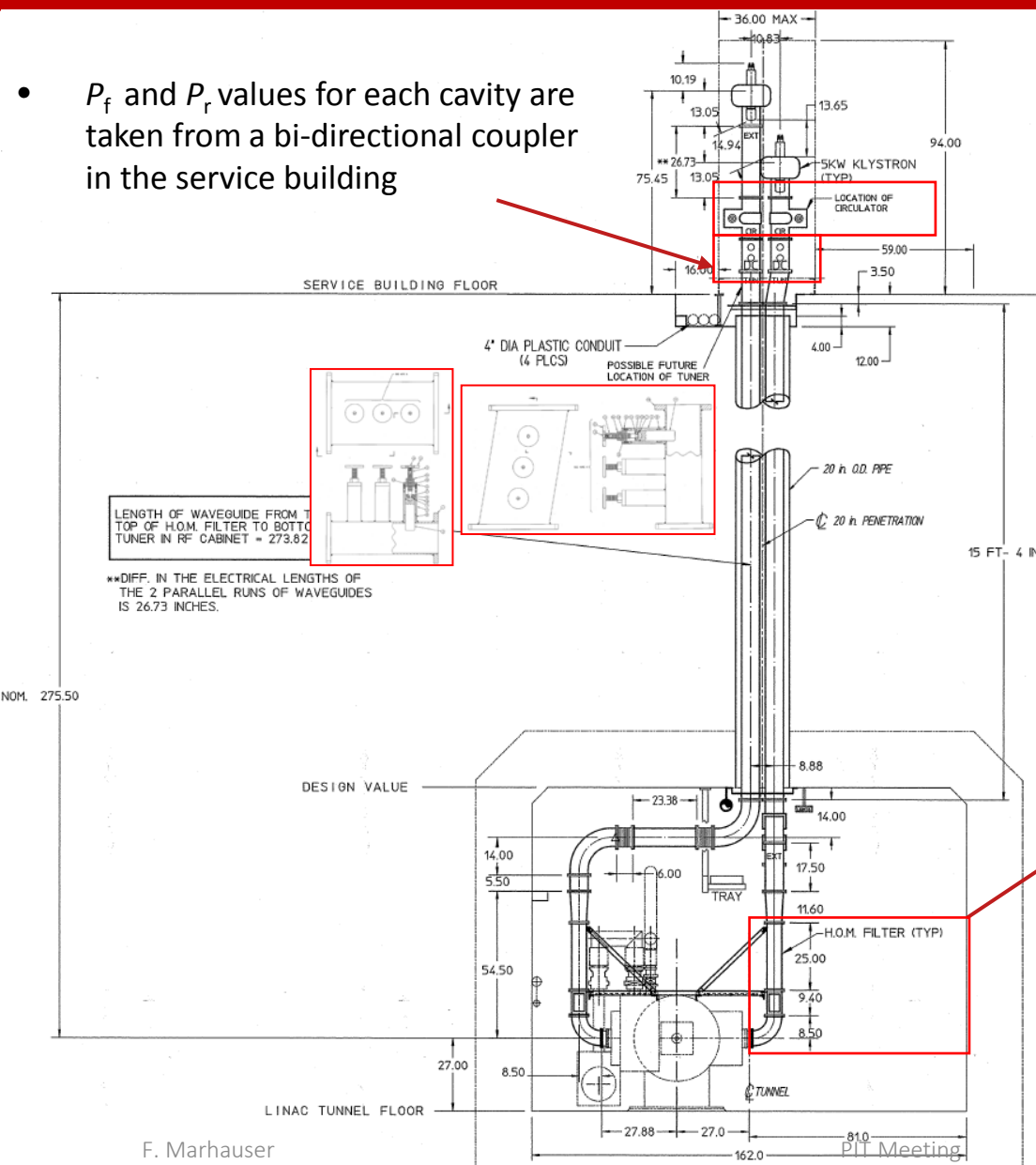
$Q_i$  from  $P_f$

Why discrepancy ?

# Accuracy of $P_{\text{fwd}}$ and $P_{\text{ref}}$

- $P_f$  and  $P_r$  values for each cavity are taken from a bi-directional coupler in the service building

- Though cables to the digital LLRF systems might be well calibrated, the losses in the power transmission line down to the cavities are not included



filter spec:	$\leq 0.3$ dB
insertion loss at $1497 \pm 10$ MHz	up to 5 kW CW maximally with both ports matched with VSWR 1.1:1 (-26.45 dB) or less
thermal load	64 Watts at 5 kW CW max. (loads are convection cooled)

# Determination of Unknown Transmission Line Attenuation

$$Q_l \left( P_f, I_{tot}, V_c, \Psi, \frac{R}{Q} \right) = Q_l \left( P_r, I_{tot}, V_c, \Psi, \frac{R}{Q} \right)$$

$$\frac{2P_f - I_{tot}V_c - 2P_f \sqrt{1 - \frac{I_{tot}V_c}{P_f} - \frac{I_{tot}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi}}{R/Q I_{tot}^2} = \frac{2P_r + I_{tot}V_c - 2P_r \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi}}{R/Q I_{tot}^2}$$

$$2P_f - I_{tot}V_c - 2P_f \sqrt{1 - \frac{I_{tot}V_c}{P_f} - \frac{I_{tot}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi} = 2P_r + I_{tot}V_c - 2P_r \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi}$$

- To include attenuation  $\alpha$  of transmission line (in dB):  $P_f \cdot 10^{-\alpha/10}$
- For reflected power:  $P_r \cdot 10^{(\alpha-\gamma)/10}$ ,  $\gamma$  (dB) = eventual calibration error of 'stamped' BC

$$2P_f \cdot 10^{-\alpha/10} - I_{tot}V_c - 2P_f \cdot 10^{-\alpha/10} \sqrt{1 - \frac{I_{tot}V_c}{P_f} - \frac{I_{tot}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi} =$$

$$2P_r \cdot 10^{(\alpha-\gamma)/10} + I_{tot}V_c - 2 \cdot 10^{(\alpha-\gamma)/10} \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi}$$

# Determination of Unknown Transmission Line Attenuation

$$2P_f \cdot 10^{-\alpha/10} - I_{tot}V_c - 2P_f \cdot 10^{-\alpha/10} \sqrt{1 - \frac{I_{tot}V_c}{P_f} - \frac{I_{tot}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi} =$$

$$2P_r \cdot 10^{(\alpha-\gamma)/10} + I_{tot}V_c - 2P_r \cdot 10^{(\alpha-\gamma)/10} \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi}$$

**Substitution:**  $Att = 10^{\alpha(dB)/10}$  (attenuation factor)

**Sorting:**

$$Att^2 - \frac{I_{tot}V_c \cdot Att}{P_r \cdot 10^{-\frac{\gamma}{10}} \left( \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi} - 1 \right)} - \frac{P_f \left( \sqrt{1 - \frac{I_{tot}V_c}{P_f} - \frac{I_{tot}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi} - 1 \right)}{P_r \cdot 10^{-\frac{\gamma}{10}} \left( \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi} - 1 \right)} = 0$$

**Solution:**

$$Att = \frac{I_{tot}V_c \pm \sqrt{(I_{tot}V_c)^2 + 4P_f \cdot P_r \cdot 10^{-\frac{\gamma}{10}} \left( \sqrt{1 - \frac{I_{tot}V_c}{P_f} - \frac{I_{tot}^2 \cdot V_c^2}{4P_f^2} \tan^2 \Psi} - 1 \right) \left( \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi} - 1 \right)}}{2P_r \cdot 10^{-\frac{\gamma}{10}} \left( \sqrt{1 + \frac{I_{tot}V_c}{P_r} - \frac{I_{tot}^2 \cdot V_c^2}{4P_r^2} \tan^2 \Psi} - 1 \right)}$$

**Attenuation is:**  $\alpha(dB) = 10 \cdot \text{Log}_{10}(Att)$

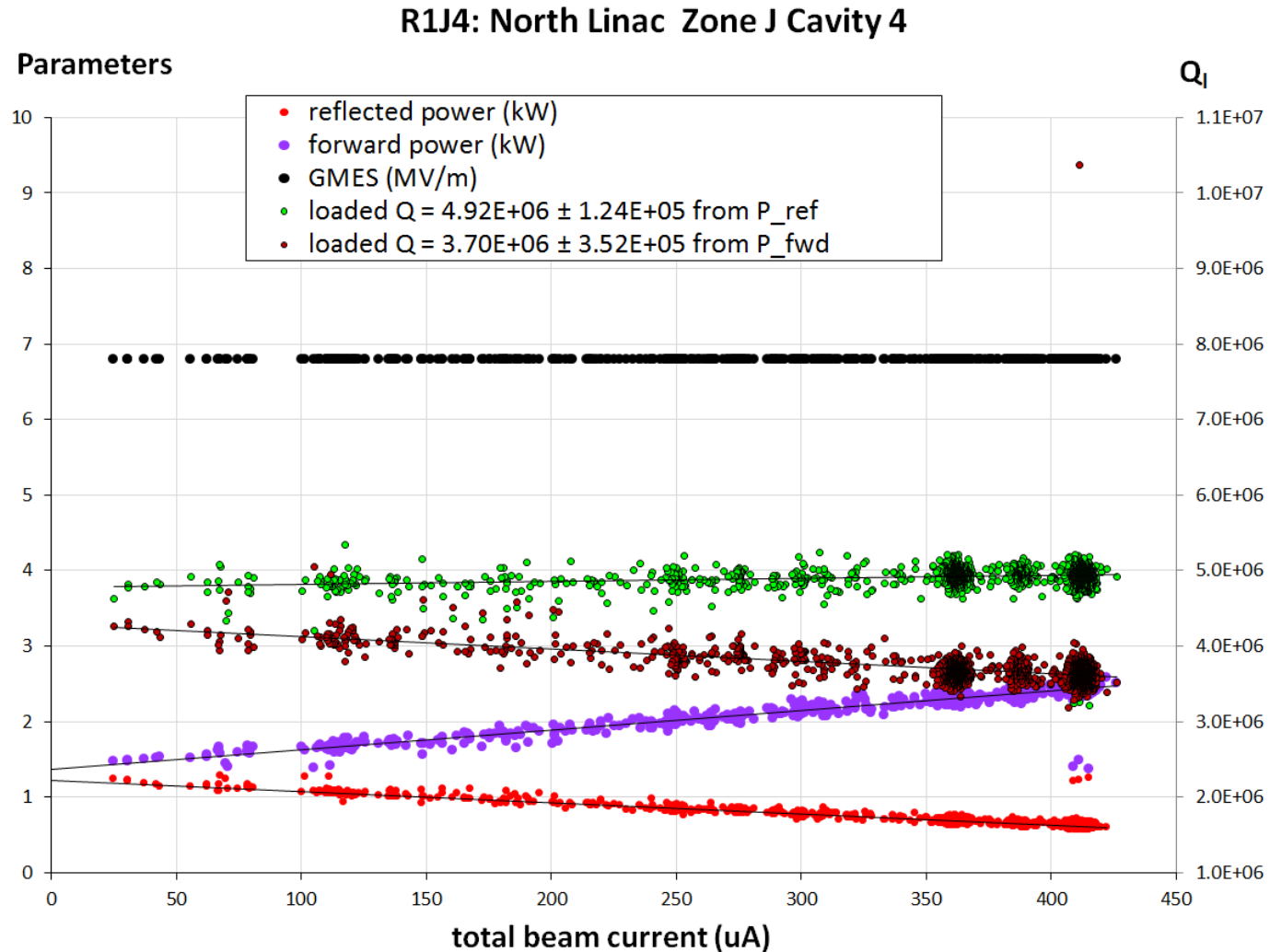
**only negative sign is valid**

**instantaneous calibration**



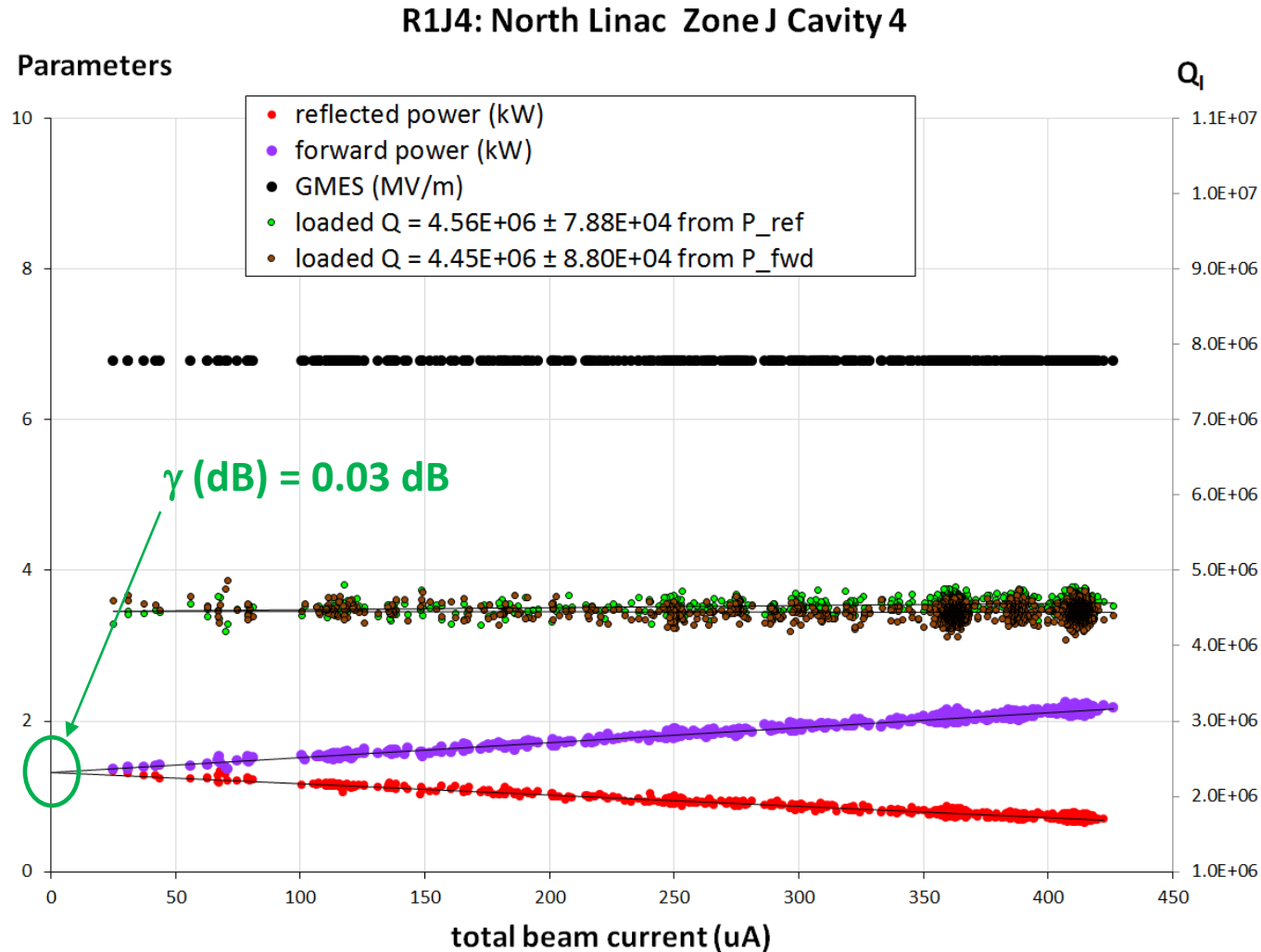
# Example (1L19-4)

Before Correction:



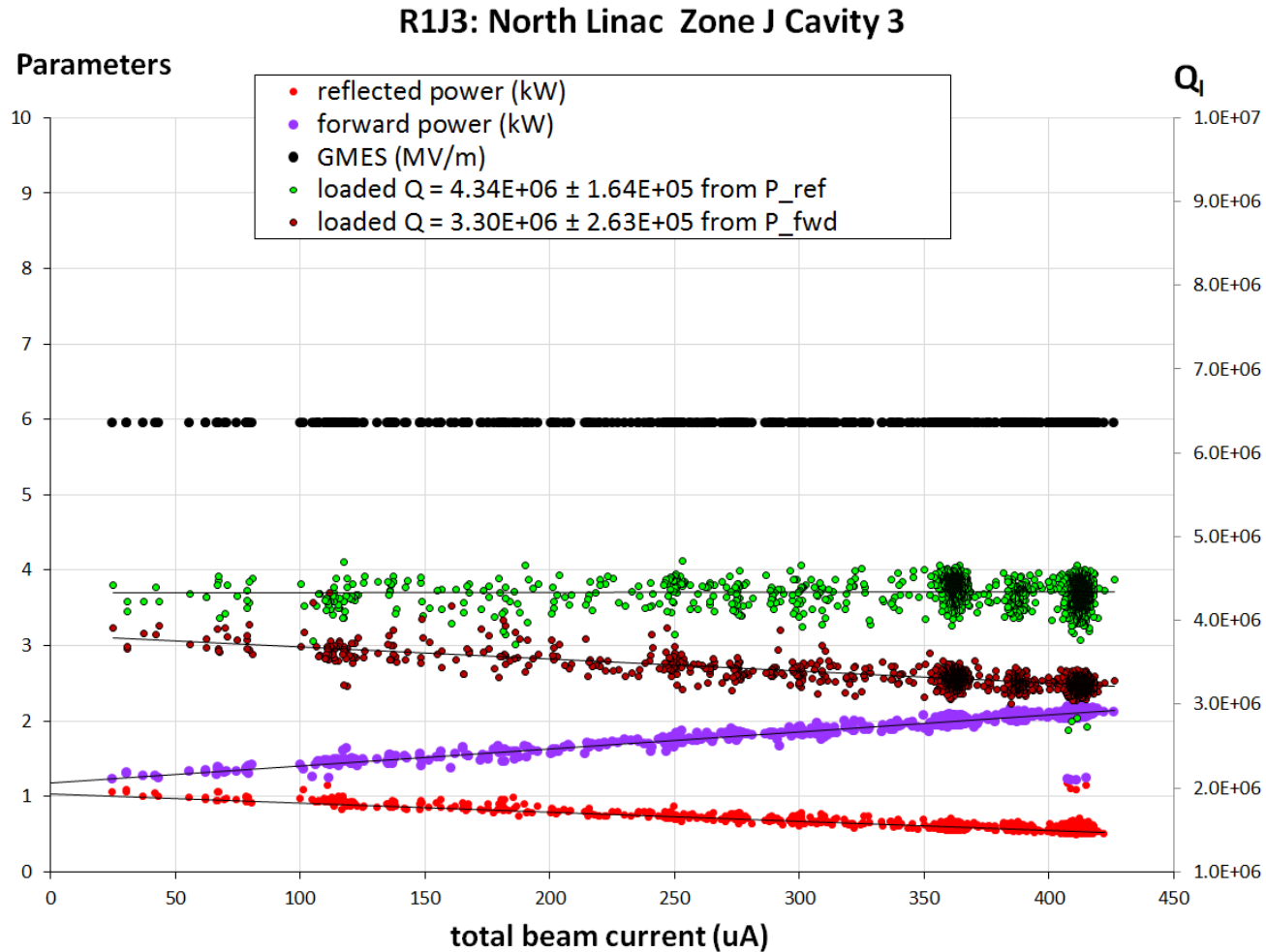
# Example (1L19-4)

After Correction:



# Example

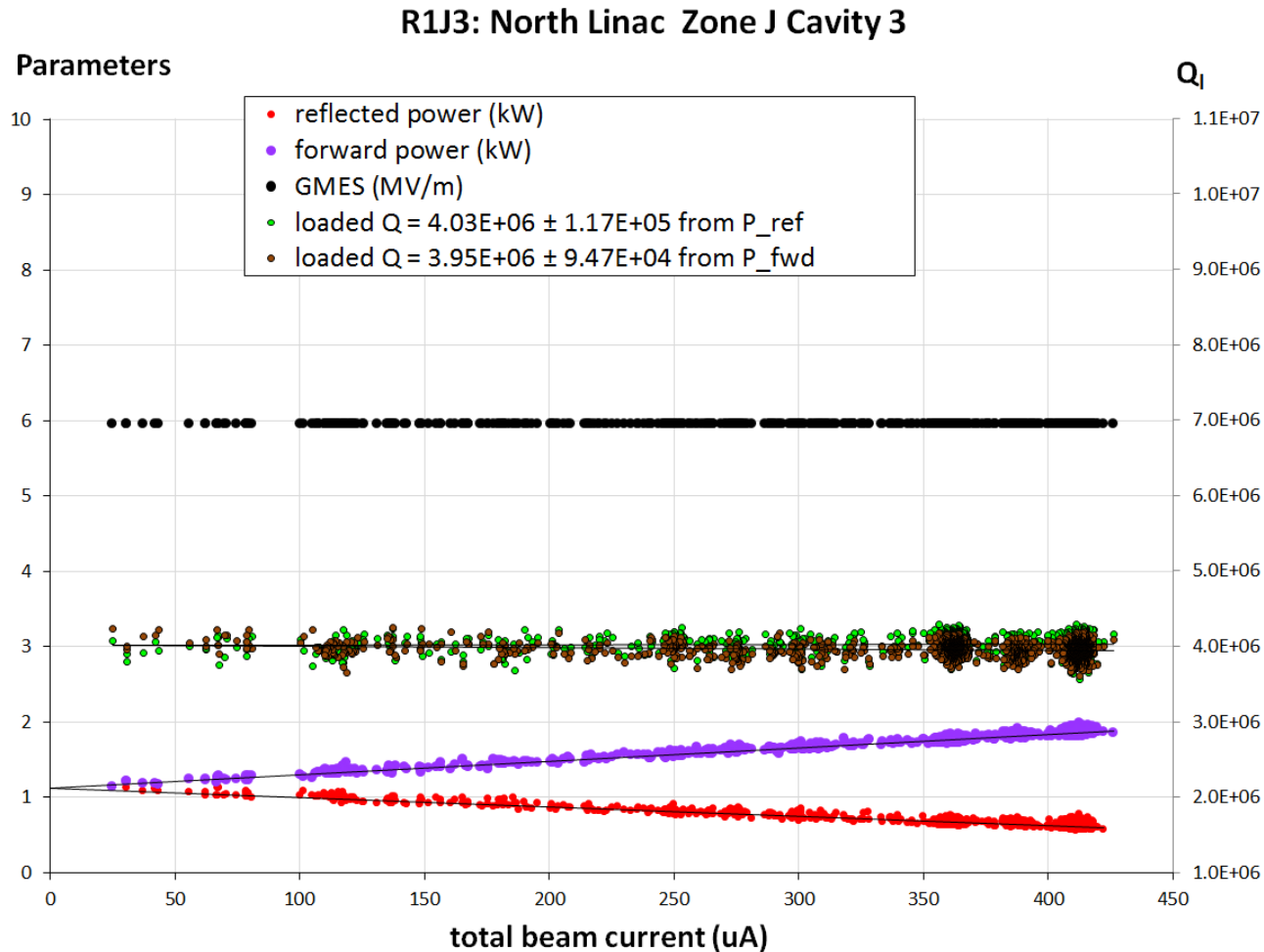
## Before Correction:



# Example

After Correction:

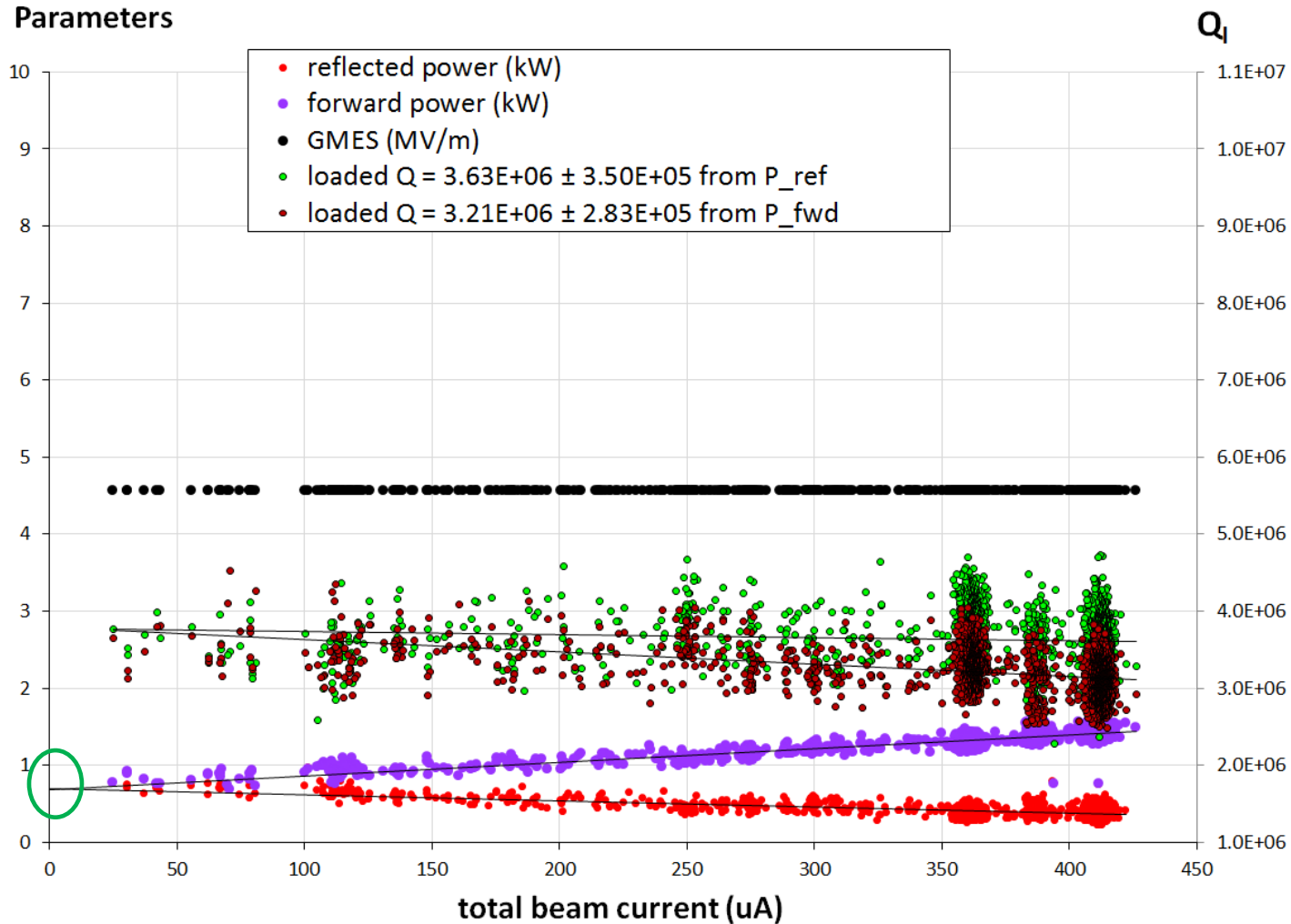
$$\gamma \text{ (dB)} = 0.03 \text{ dB}$$



# Example

Before Correction:

R1J5: North Linac Zone J Cavity 5

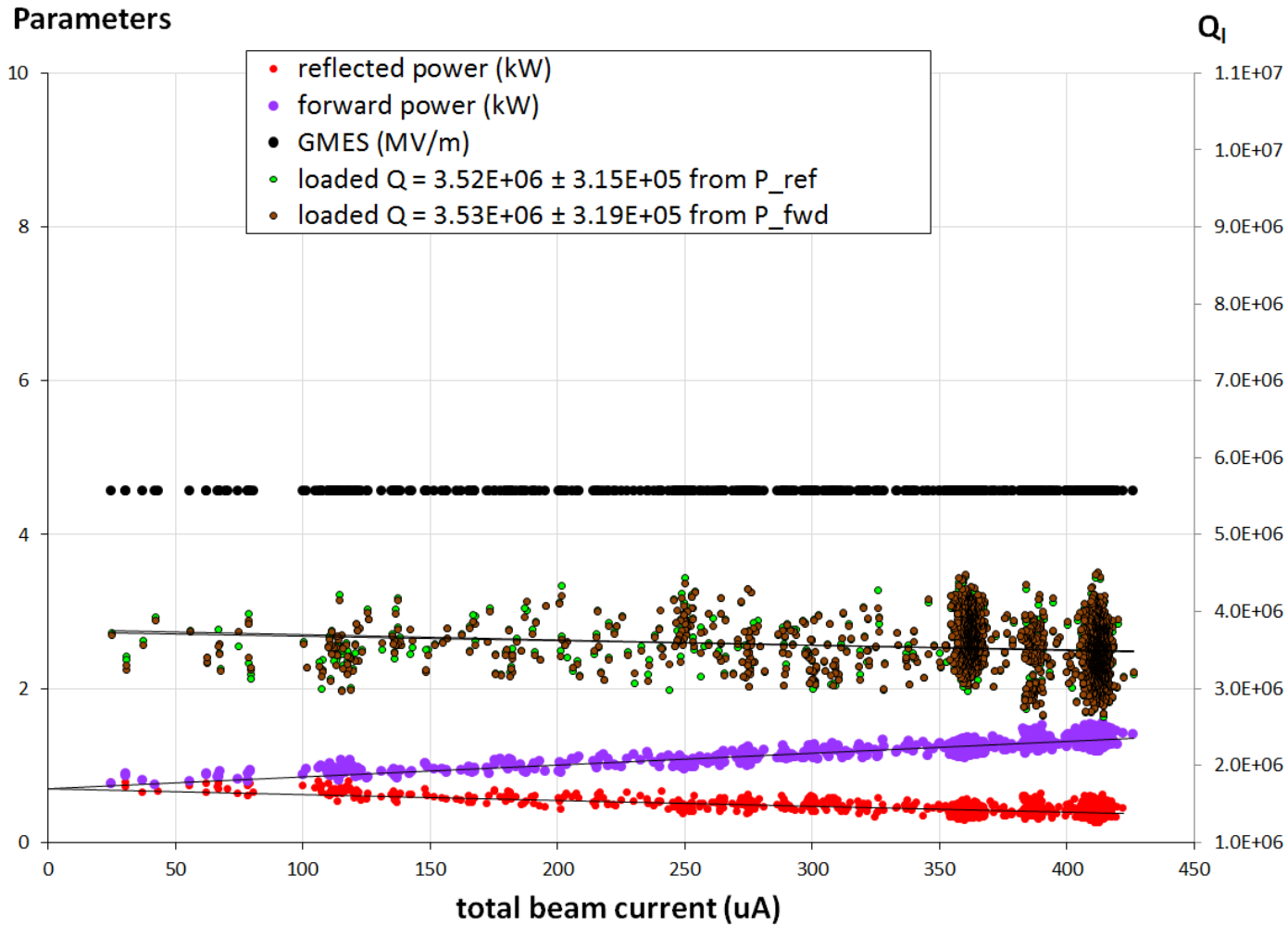


# Example

After Correction:

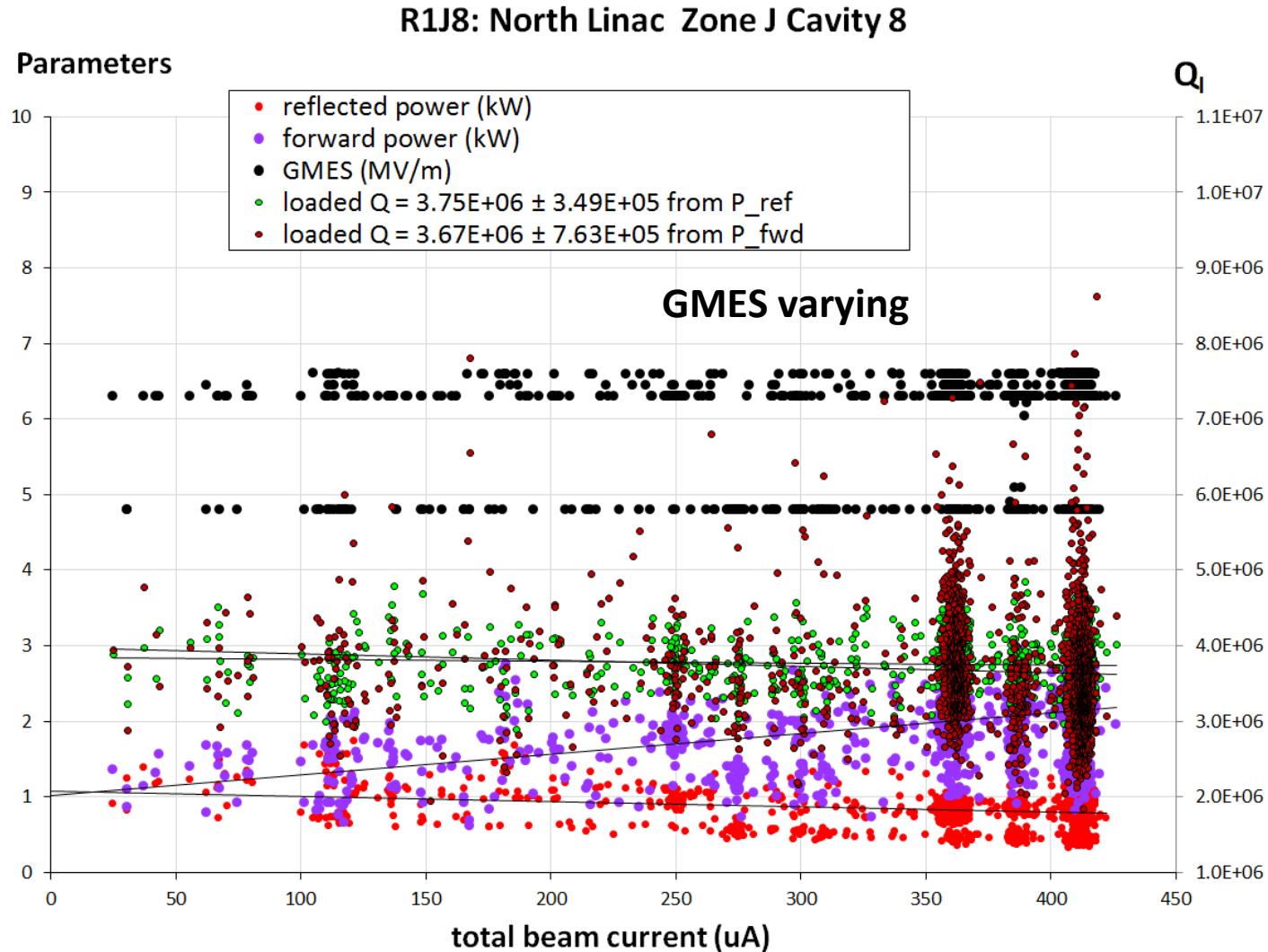
$$\gamma \text{ (dB)} = 0 \text{ dB}$$

R1J5: North Linac Zone J Cavity 5



# Example

Before Correction:

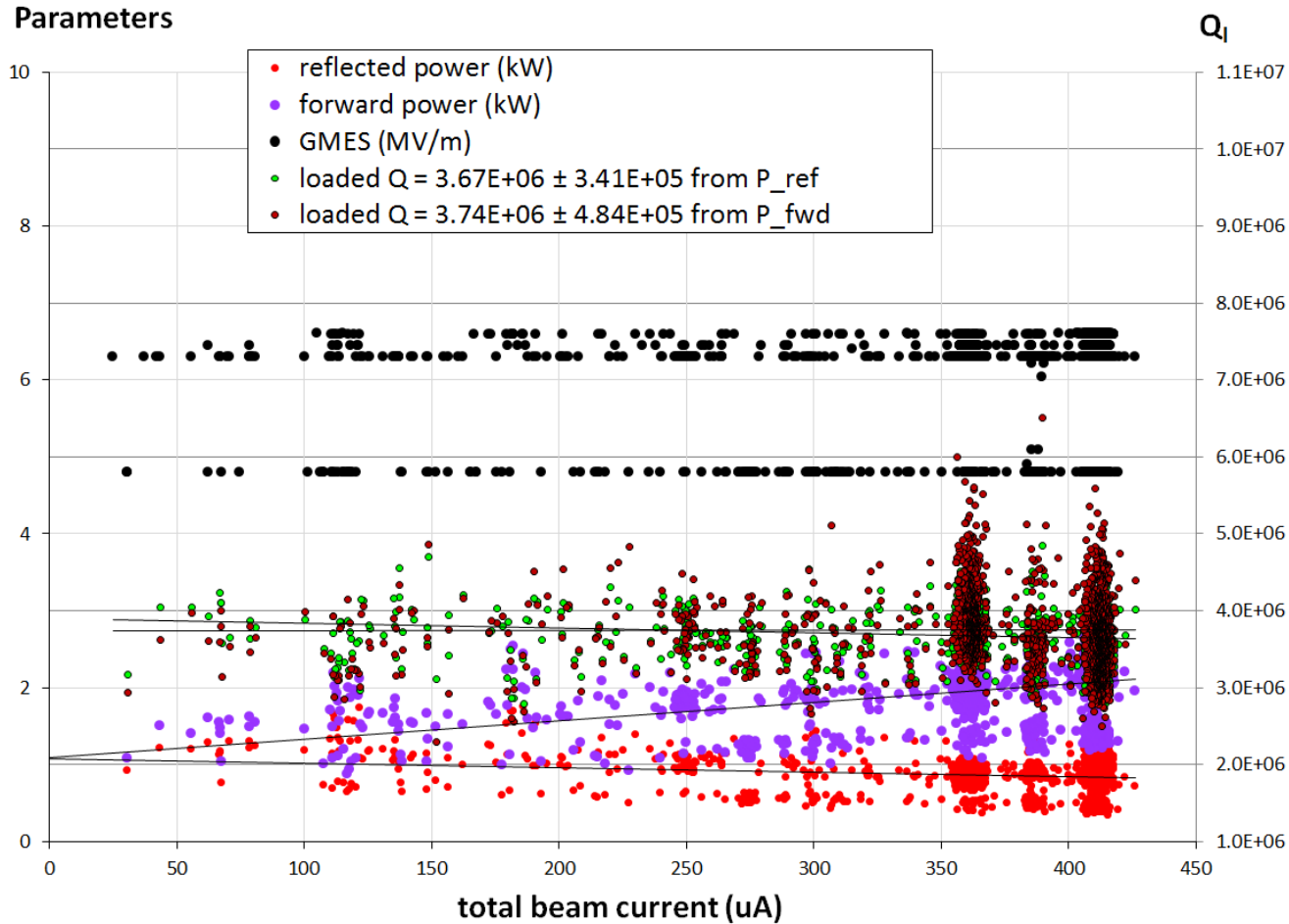


# Example

After Correction:

$$\gamma \text{ (dB)} = 0 \text{ dB}$$

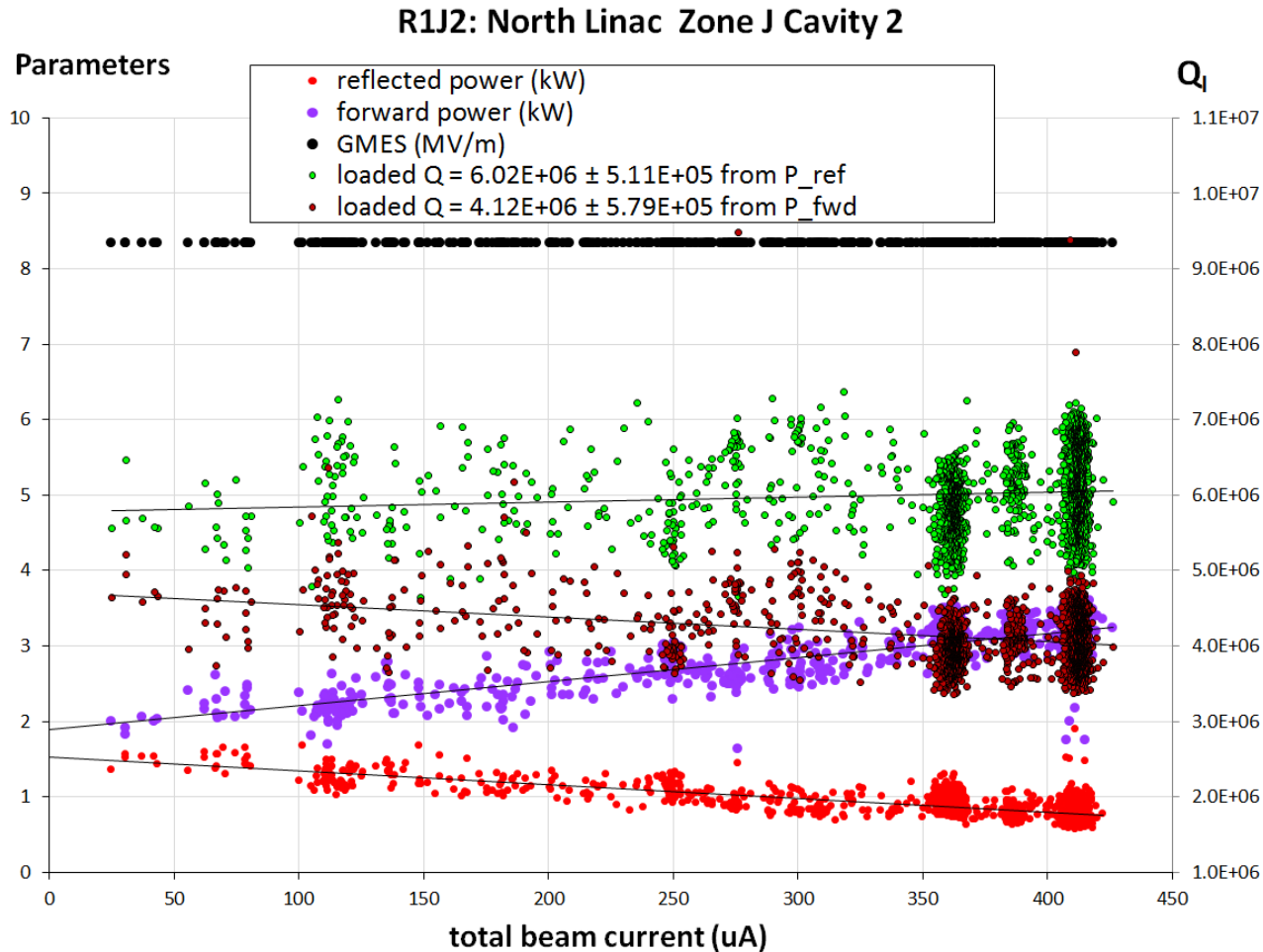
R1J8: North Linac Zone J Cavity 8





# Example

Before Correction:



} ~1 kW fwd. power fluctuations !

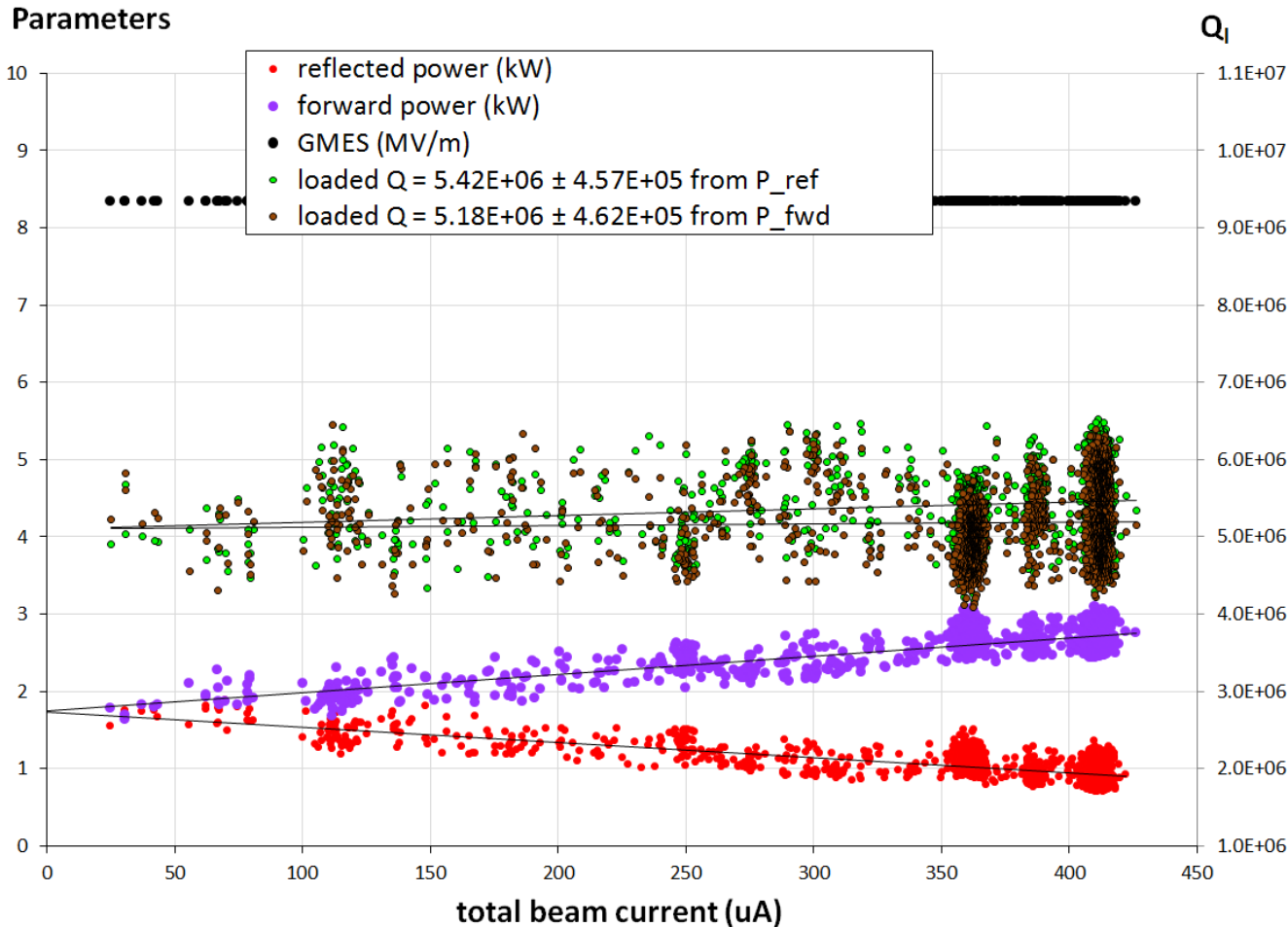
# Example

LEM	Jefferson Lab <b>CED</b>	
Cavity		C25
MaxGSET		6.8 MeV/m
PhaseRMS		0.05 volts
Q0		6.89E+9
Qexternal		4.95E+6
TripOffset		6.388 Trips/shift
TripSlope		1.62 Trips/shift

After Correction:

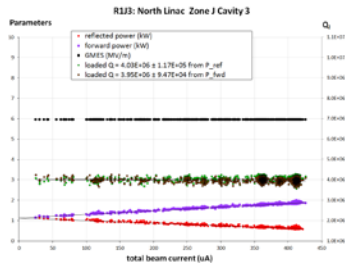
$$\gamma \text{ (dB)} = 0.07 \text{ dB}$$

## R1J2: North Linac Zone J Cavity 2

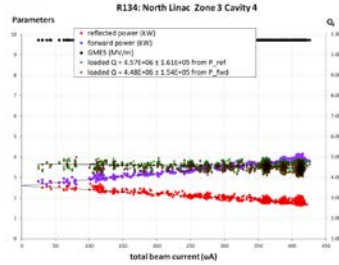


# More Examples: NL (C20/C50 CMs)

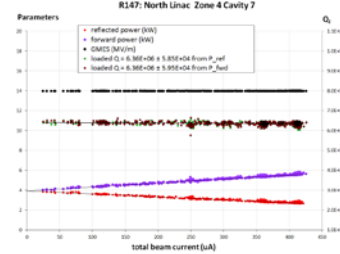
R13 – C20



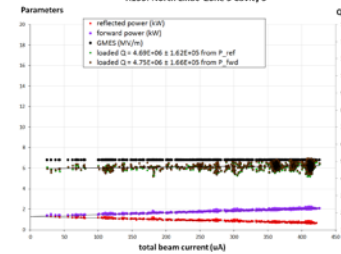
R14 – C20



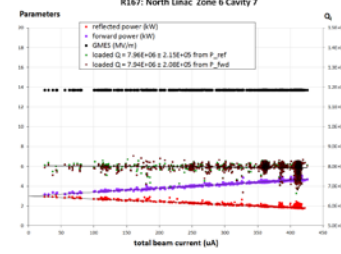
R14 – C50



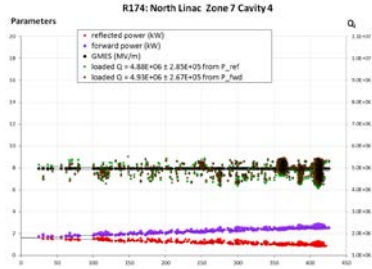
R15 – C50



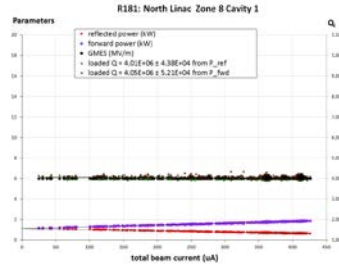
R16 – C50



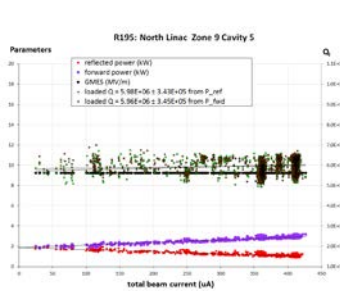
R17 – C20



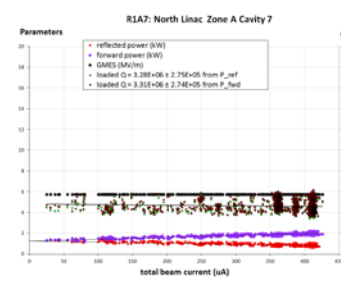
R18 – C20



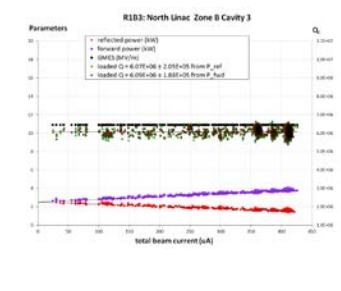
R19 – C20



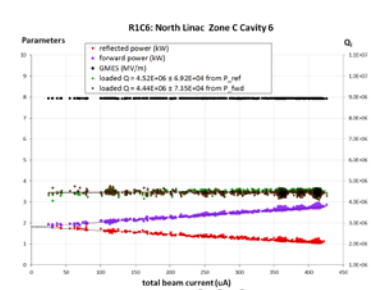
R1A – C20



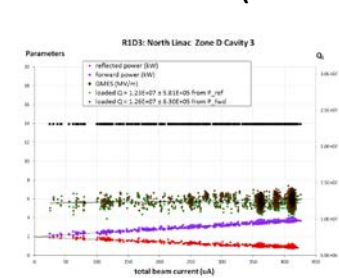
R1B – C50



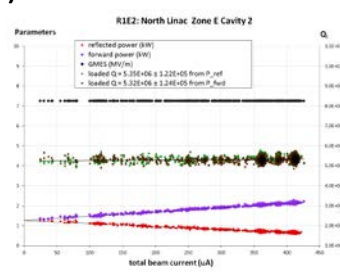
R1C – C50



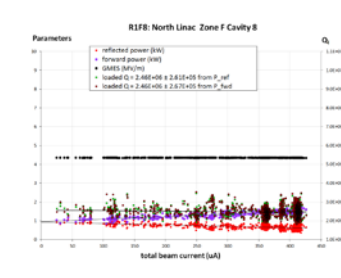
R1D – C50 (incl. C75)



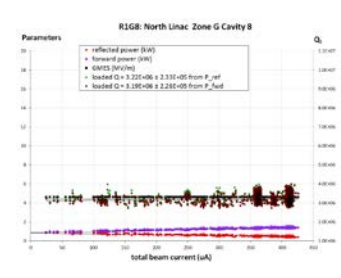
R1E – C20



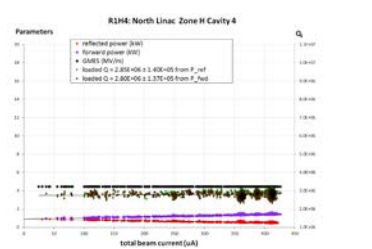
R1F – C20



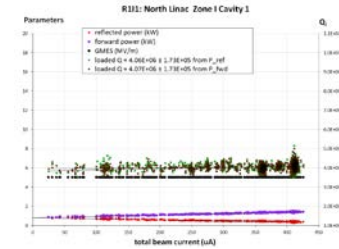
R1G – C20



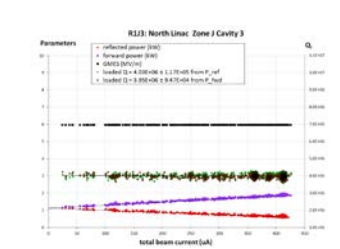
R1H – C20



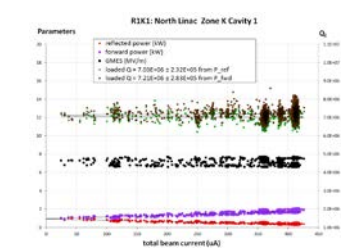
R1I – C20



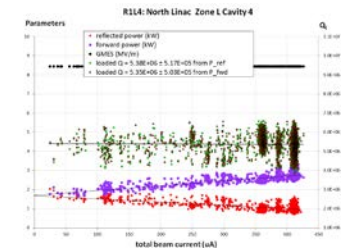
R1J – C20



R1K – C20

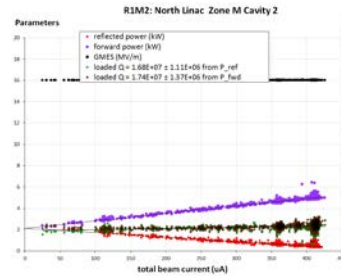


R1L – C20

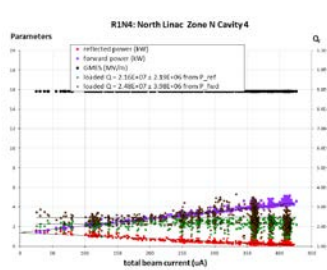


# More Examples: NL (C100 CMs)

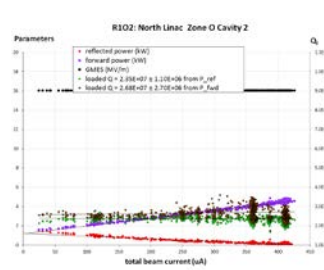
R1M – C100



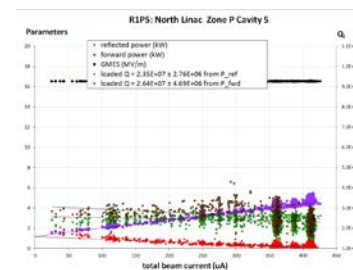
R1N – C100



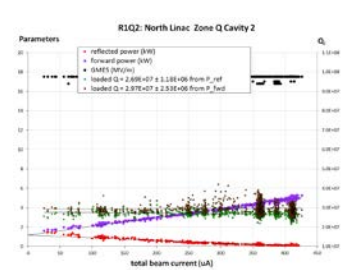
R1O – C100



R1P – C100

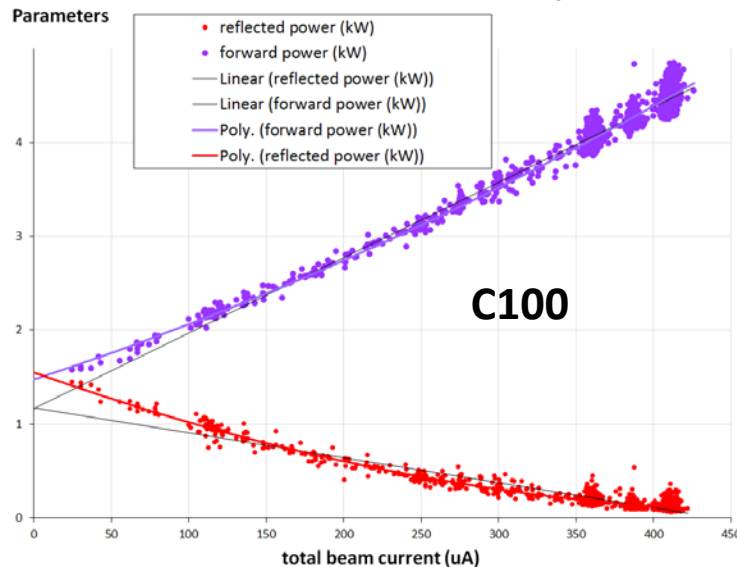


R1Q – C100

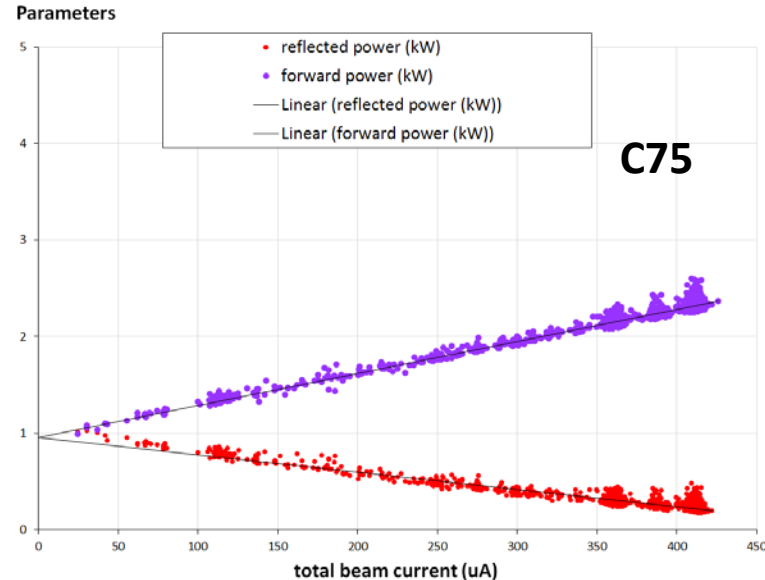


- Typical non-linear behavior of  $P_f$  and  $P_r$  observed for C100 cavities

R1O2: North Linac Zone O Cavity 2

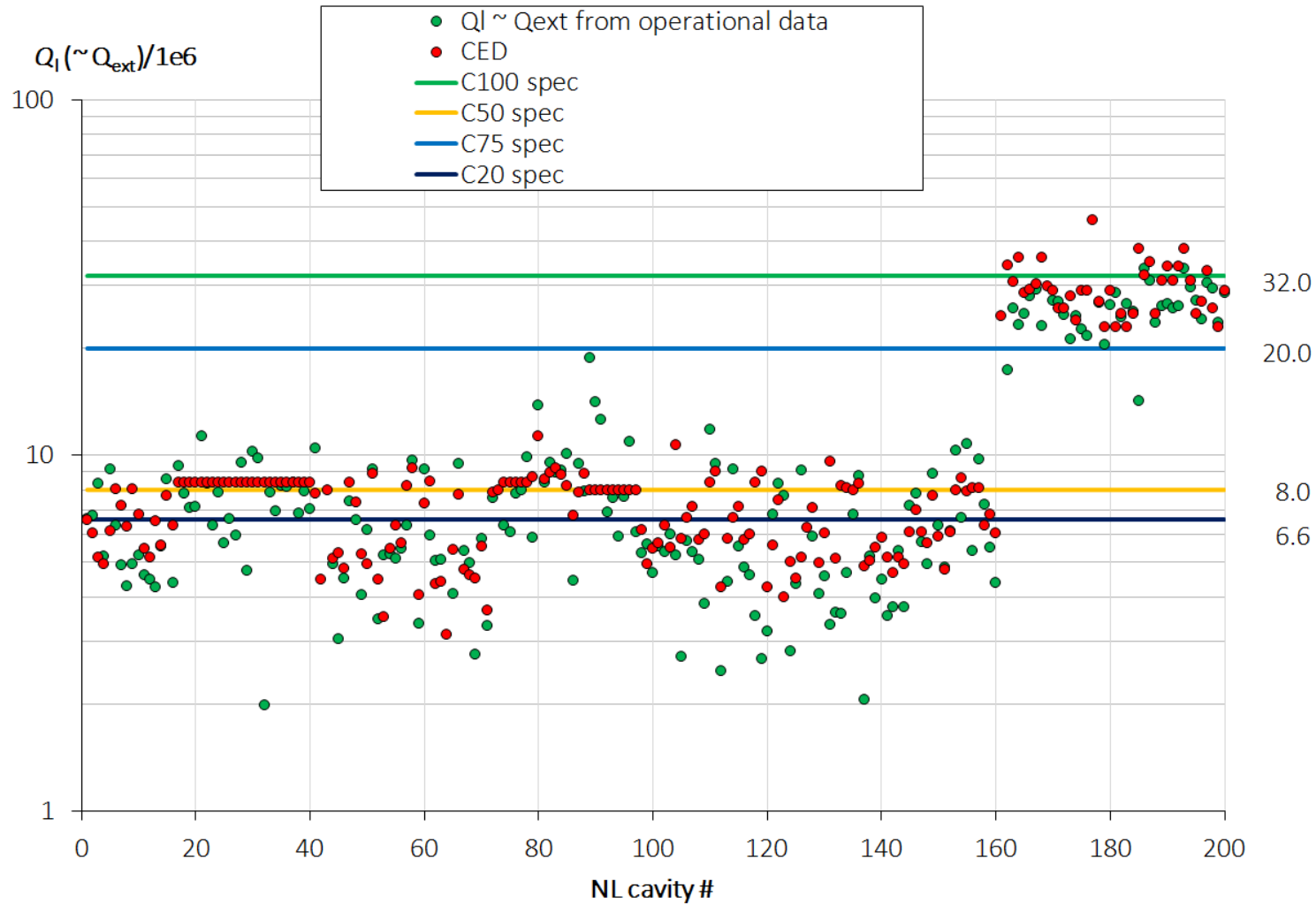


R1D2: North Linac Zone D Cavity 2



# North Linac

## Comparison and Update of CED Data



# Summary

- **Instantaneous  $Q_l$  ( $Q_{ext}$ ) measurements possible with instantaneous power transmission line calibration**
- **Could be applied for other accelerators, and those with adjustable tuners to verify coupling online**
- **Use as diagnostic tool? E.g. calibration issues...**
- **Can missing calibration explain CEBAF energy ‘fudge factor’?**  
Per Arne: Nominally 1-2 % but “...SRF calibration can sometimes be off by 5-10%.”
- **Plan forward: Implement new method into EPICS at CEBAF using highly synchronized parameters available from digital RF system**
  - talked already to Tomasz Plawski to get started...
- **TDB: Identifying worst mismatched cavities and tuning  $Q_l$ ...**