

# Rotation of The Fluid Flow

## A brief introduction of rotation of fluid

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# Outline

## 1. Curl and Rotation

- 1.1 What is angular velocity?
- 1.2 Stream line and Path line
- 1.3 Example

## 2. Circulation and Rotation

- 2.1 Definition of Circulation
- 2.2 Approximation of circulation

## 3. Curl and Circulation

- 3.1 Vector calculus
- 3.2 Example for Cartesian
- 3.3 Example for Cylindrical

## 4. Conclusion

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- 3.2 Example for Cartesian
- 3.3 Example for Cylindrical

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What is angular velocity?

## What is the rotation of a particle?

First we look at a moving particle in a space  $\mathbb{R}^2$ .

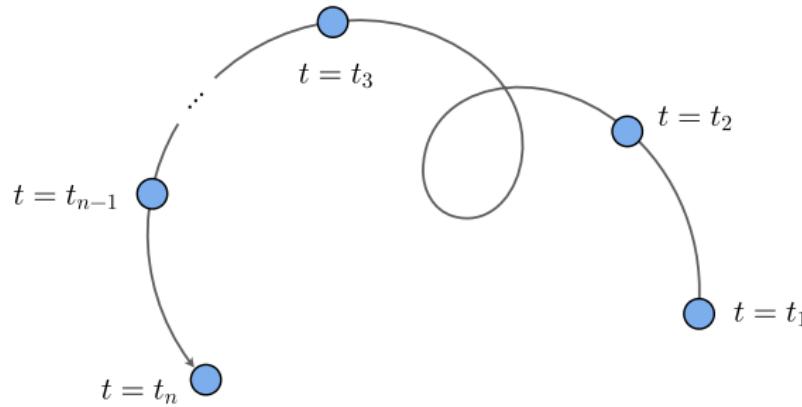
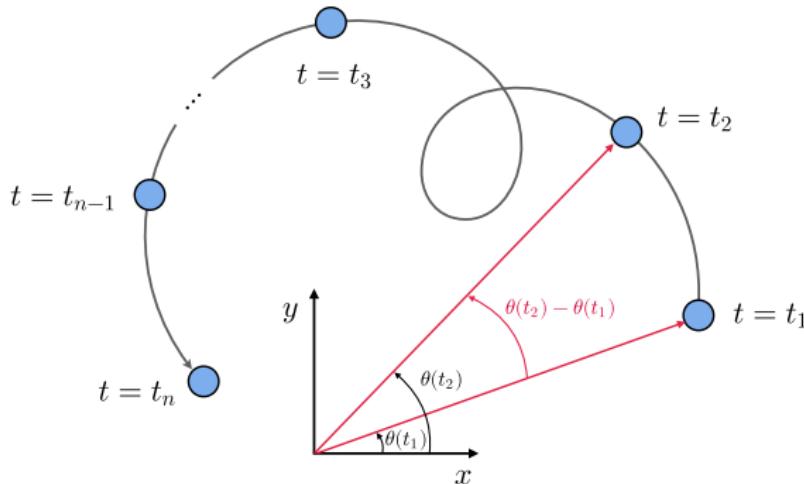


Figure: A moving particle in  $\mathbb{R}^2$

What is angular velocity?

However, if we add a coordinate



And define the magnitude angular velocity to be

$$\omega = \lim_{t_1 \rightarrow t_2} \frac{\theta(t_2) - \theta(t_1)}{t_2 - t_1} = \frac{d\theta}{dt} \quad (1)$$

What is angular velocity?

Notice that, the velocity can be calculated in polar coordinate  $(\mathbb{R}^2)$  by position vector  $\vec{r} = r \cos \theta \hat{e}_x + r \sin \theta \hat{e}_y$ , that is

$$\begin{aligned}
 \vec{v} &= \frac{d\vec{r}}{dt} = \frac{d}{dt}(r(\cos\theta\hat{e}_x + \sin\theta\hat{e}_y)) \\
 &= \frac{dr}{dt}(\cos\theta\hat{e}_x + \sin\theta\hat{e}_y) + r(-\sin\theta\hat{e}_x + \cos\theta\hat{e}_y)\frac{d\theta}{dt} \\
 &= \frac{dr}{dt}\hat{e}_r + r\frac{d\theta}{dt}\hat{e}_\theta
 \end{aligned} \tag{2}$$

Extending the space to  $z$  component, we define the angular velocity for a particle on the  $xy$ -plane in  $\mathbb{R}^3$

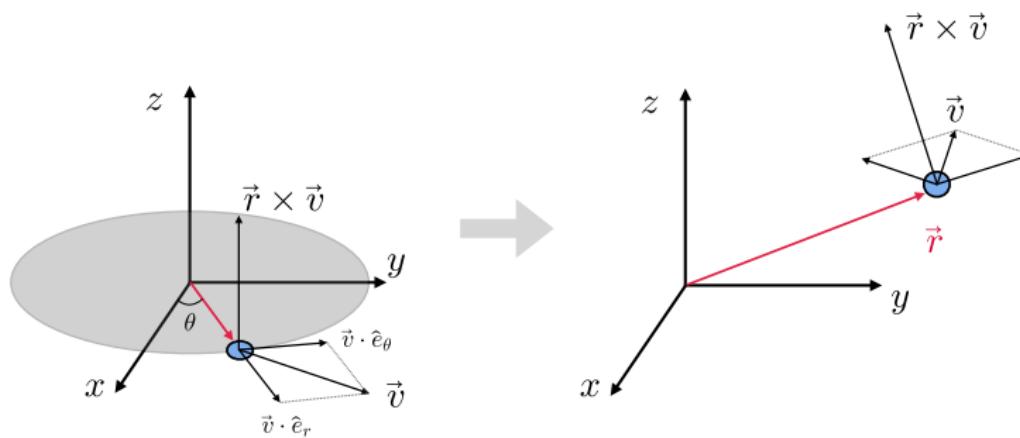
$$\vec{\omega} = \frac{\hat{e}_r \times \vec{v}}{r} = \frac{r(\hat{e}_r \times \hat{e}_\theta)}{r} \frac{d\theta}{dt} = \frac{d\theta}{dt} \hat{e}_z, \quad (3)$$

where  $\hat{e}_r$ ,  $\hat{e}_\theta$  and  $\hat{e}_z$  are the orthonormal basis of cylinder coordinate.

What is angular velocity?

Now, consider the particle in  $\mathbb{R}^3$  and we still using position vector  $\vec{r}$  rather than the  $r$ -component vector, since  $\hat{e}_r = \vec{r}/r$ , we also can write

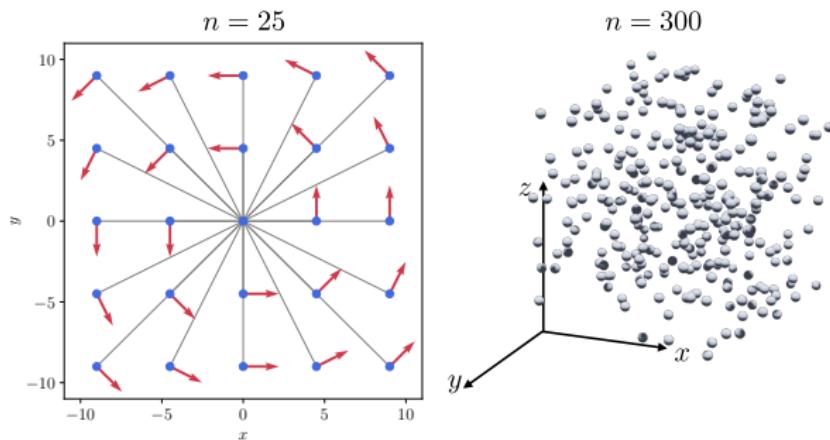
$$\vec{\omega} = \frac{\vec{r} \times \vec{v}}{r^2}. \quad (4)$$



What is angular velocity?

Then, how about a group of particles? Average angular velocity?

$$\tilde{\Omega} = \frac{1}{n} \sum_{i=1}^n \vec{\omega}_i = \frac{1}{n} \sum_{i=1}^n \frac{\vec{r}_i \times \vec{v}}{\|\vec{r}_i\|^2} \quad \text{or} \quad \iint_{\Sigma} \vec{\omega} \cdot d\vec{A} \quad (5)$$

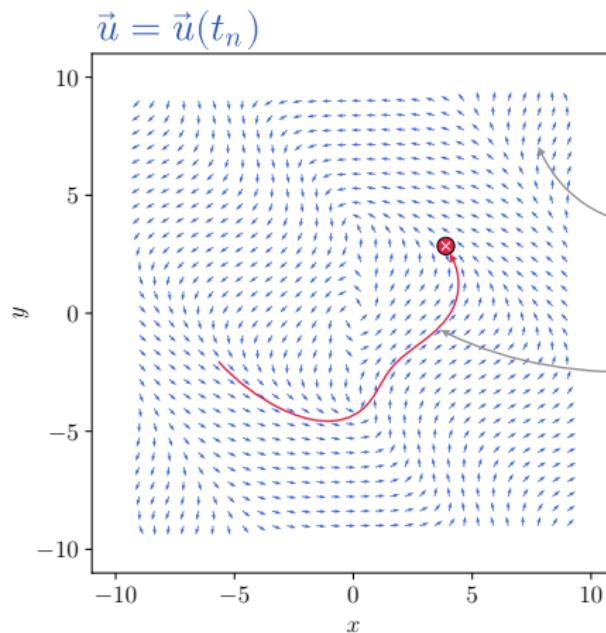


It seems to be some kind of approach method.

## Stream line and Path line

## Stream line and Path line

There are two ways to describe how fluid flow in *Experimental Physics*.



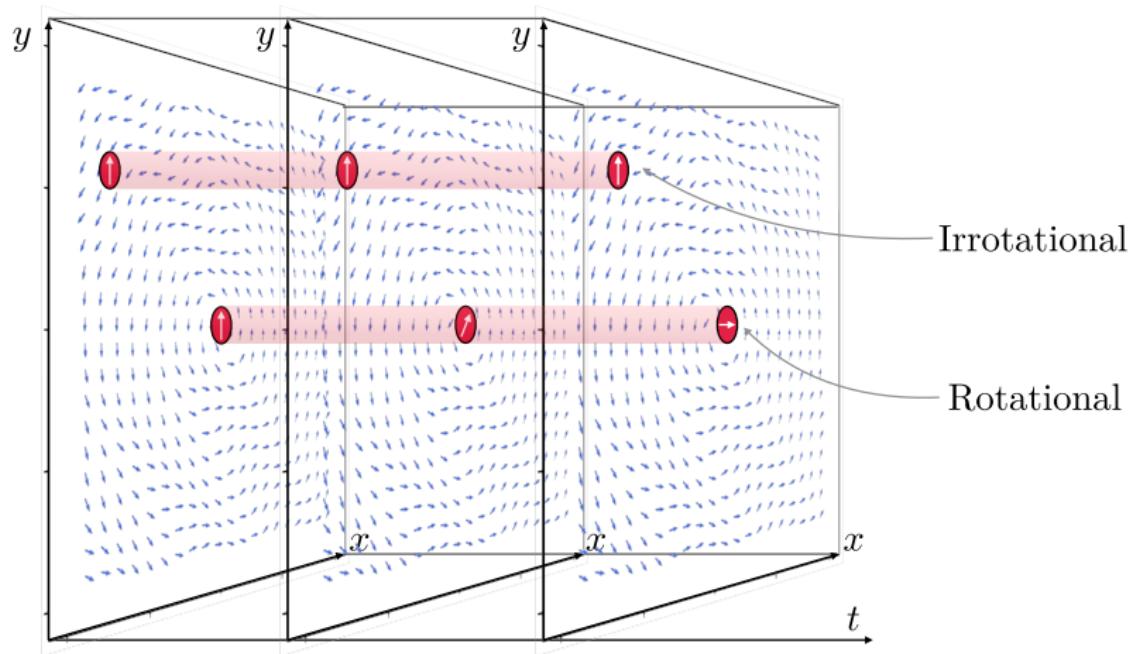
Stream line  $\frac{dy}{dx} = \frac{u_y(x, y)}{u_x(x, y)}$   
at specific time  $t = t_n$

Path line

$$\frac{d\vec{r}(x(t), y(t))}{dt} = \vec{u}(x(t), y(t))$$

## Stream line and Path line

So, a more intuitive way to describe how a group of particles (fluid) rotate, is to place a marker in these particles.



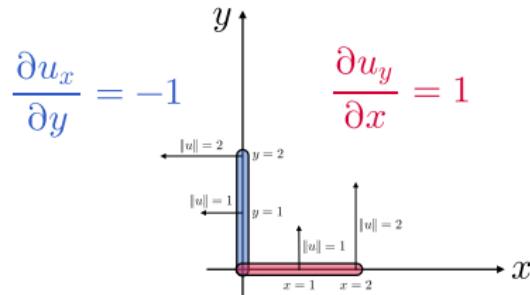
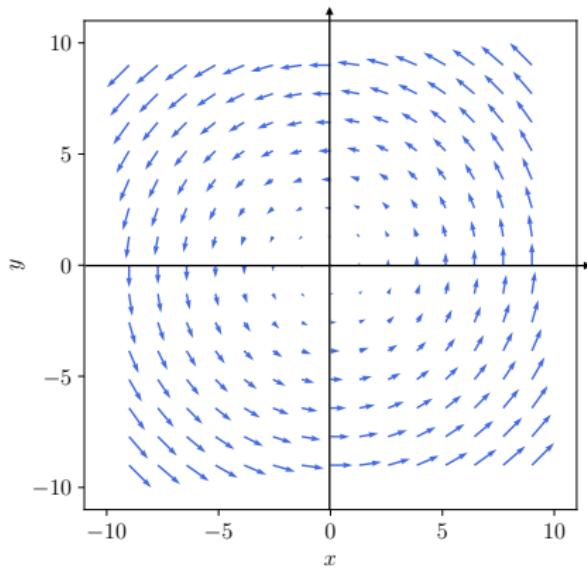
**Figure:** The *world line* of marker and vector field

Example

## Example

Now, consider a fluid flow given by

$$\vec{u}(x, y) = u_x \hat{e}_x + u_y \hat{e}_y = -y \hat{e}_x + x \hat{e}_y \quad (6)$$

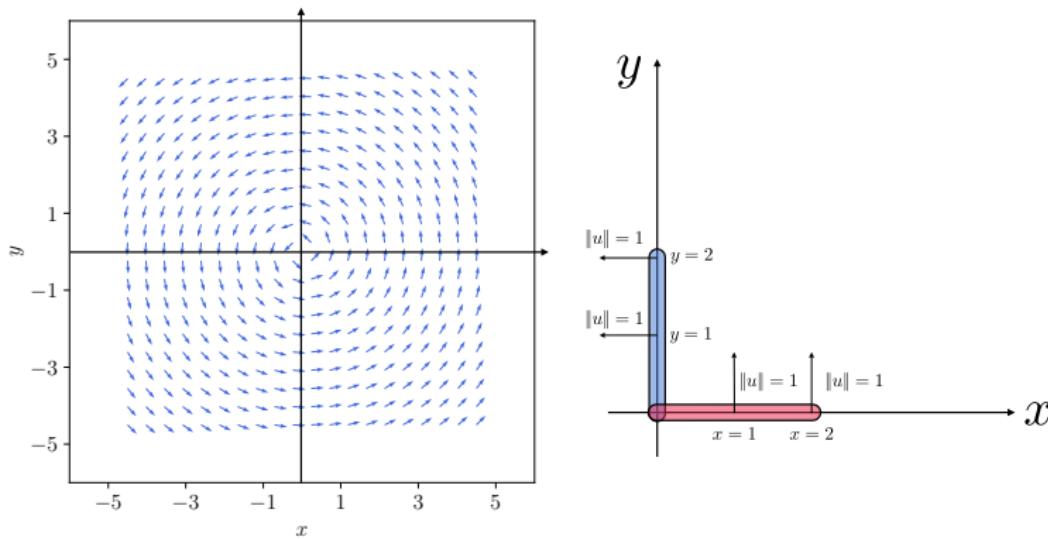


$$\text{curl } \vec{u} = \frac{\partial u_y}{\partial x} - \frac{\partial u_x}{\partial y} = 2$$

## Example

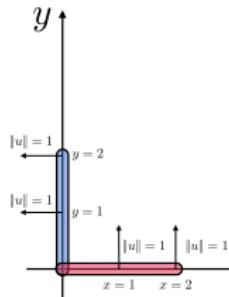
Now, normalize the preview example, we get

$$\vec{u}(x, y) = -\frac{y}{\sqrt{x^2 + y^2}} \hat{e}_x + \frac{x}{\sqrt{x^2 + y^2}} \hat{e}_y \quad (7)$$



## Example

Calculating the curl of  $(-y \hat{e}_x + x \hat{e}_y) / \sqrt{x^2 + y^2}$ , we get


$$\frac{\partial u_y}{\partial x} = -\frac{y^2}{(x^2 + y^2)^{3/2}} \xrightarrow{x=0} -\frac{1}{y}$$
$$\frac{\partial u_x}{\partial y} = \frac{x^2}{(x^2 + y^2)^{3/2}} \xrightarrow{y=0} \frac{1}{x}$$
$$\text{curl } \vec{u} = \left( \frac{y^2}{(x^2 + y^2)^{3/2}} \right) - \left( -\frac{x^2}{(x^2 + y^2)^{3/2}} \right)$$
$$= \frac{1}{\sqrt{x^2 + y^2}}$$

However, for  $x, y \neq 0$ ,  $\vec{u}(0, y) = -\hat{e}_x$  and  $\vec{u}(x, 0) = \hat{e}_y$ , then  $\partial_y \vec{u}(0, y) = \partial_x \vec{u}(x, 0) = 0$ .

## Example

By observing the result of

$$\vec{u}(x, y) = -\frac{y}{\sqrt{x^2 + y^2}} \hat{e}_x + \frac{x}{\sqrt{x^2 + y^2}} \hat{e}_y,$$

the two approach methods give

$$y\text{-axis: } \begin{cases} \operatorname{curl}(\vec{u} \Big|_{x=0}) = 0 \\ \operatorname{curl}(\vec{u}) \Big|_{x=0} = 1/y \end{cases}, \quad x\text{-axis: } \begin{cases} \operatorname{curl}(\vec{u} \Big|_{y=0}) = 0 \\ \operatorname{curl}(\vec{u}) \Big|_{y=0} = 1/x \end{cases} \quad (8)$$

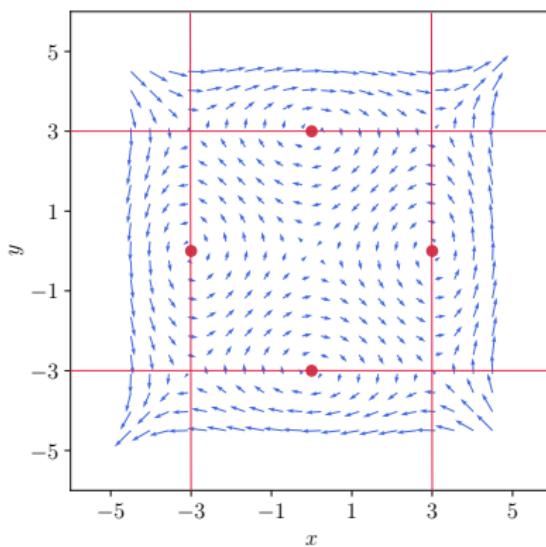
Here state a conclusion,

*We cannot determine the rotational effect by looking at vectors at specific points. Instead, we should examine the changes in the vector field to understand its rotational effect.*

## Example

Using another example fluid flow given by

$$\vec{u}(x, y) = (y^3 - 9y)\hat{e}_x + (x^3 - 9x)\hat{e}_y \quad (9)$$



$$\vec{u}(x(t), y(t)) = \frac{d\vec{r}}{dt} \quad \begin{cases} \frac{dx}{dt} = y^3 - 9y \\ \frac{dy}{dt} = x^3 - 9x \end{cases}$$

$$\vec{r}_3 = x(t_3)\hat{e}_x + y(t_3)\hat{e}_y$$

$$\vec{u} = \vec{u}(\vec{r}_3) \quad t = t_3$$

Path line

$$\vec{r}_2 = x(t_2)\hat{e}_x + y(t_2)\hat{e}_y$$

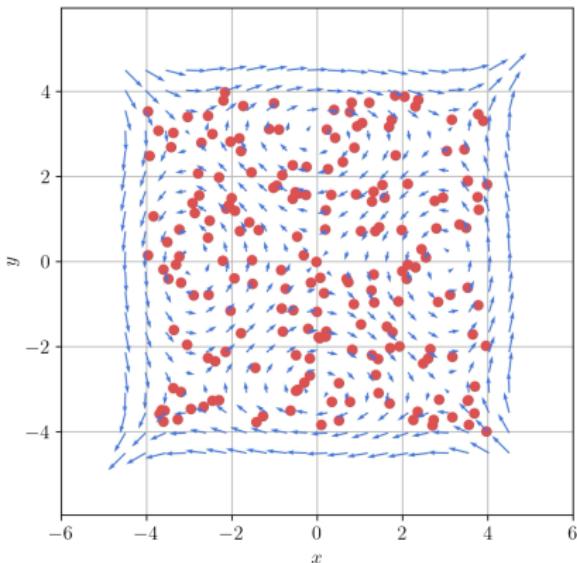
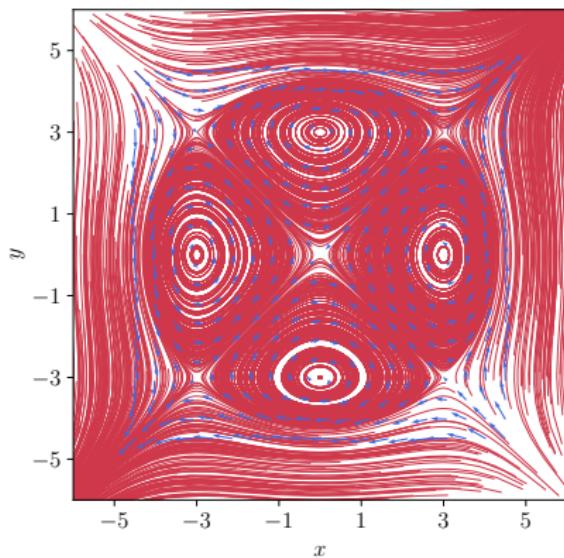
$$\vec{u} = \vec{u}(\vec{r}_2) \quad t = t_2$$

$$\vec{u} = \vec{u}(\vec{r}_1) \quad t = t_1$$

$$\vec{r}_1 = x(t_1)\hat{e}_x + y(t_1)\hat{e}_y$$

## Example

After we solving the system of non-linear differential equations, we have the path line and moving particles (click [here](#) to see video).



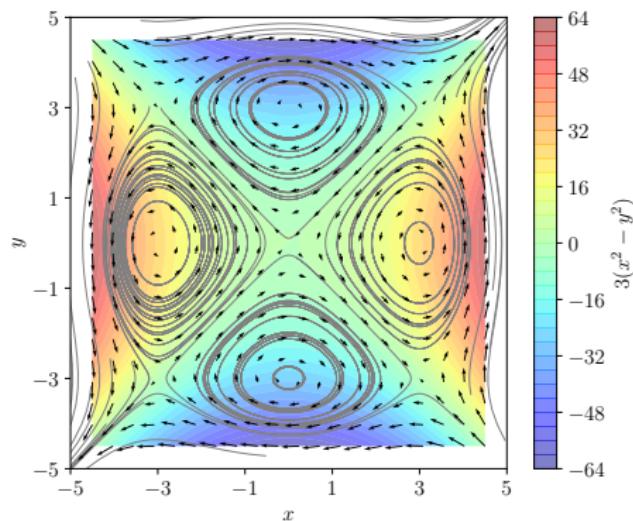
**Figure:** Left figure is the path line of vector field, reft figure is a snapshot of the simulation video

## Example

Also calculate the curl of vector field

$$\begin{aligned}\operatorname{curl} \vec{u} &= \partial_x(x^3 - 9x) - \partial_y(y^3 - 9y) \\ &= 3(x^3 - y^2),\end{aligned}\tag{10}$$

and make a contour:



Here state a conclusion,

*The curl is to measure the rotation at specific point.*

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## Definition of Circulation

## Definition of Circulation

Now, consider a simple closed oriented curve  $C$ , the *circulation*  $\Gamma_C$  of vector field  $\vec{u}$  on  $C$  is given by

$$\Gamma_C = \oint_C \vec{u} \cdot d\vec{\ell}, \quad (11)$$

where  $d\vec{\ell}$  is the infinitesimal displacement vector on  $C$ . More precisely,

Definition of circulation in  $\mathbb{R}^2$ 

For a vector field  $\vec{u} : S \subseteq \mathbb{R}^2 \rightarrow \mathbb{R}^2$ , given a piecewise smooth oriented curve  $C$  parametrized by  $\vec{\ell}(t) = x(t)\hat{e}_x + y(t)\hat{e}_y$ , where  $a \leq t \leq b$  and  $\vec{\ell}(a) = \vec{\ell}(b)$ , the circulation  $\Gamma$  of  $\vec{u}$  on  $C$  is given by

$$\Gamma_C = \oint_C \vec{u} \cdot \frac{d\vec{\ell}(t)}{dt} dt = \int_a^b \vec{u}(x(t), y(t)) \cdot \frac{d\vec{\ell}(t)}{dt} dt. \quad (12)$$

## Definition of Circulation

But why are we using circulation ? By Stokes' theorem we have

$$\oint_{\partial\Sigma} \vec{u} \cdot d\vec{\ell} = \int_{\Sigma} (\operatorname{curl} \vec{u}) \cdot d\vec{\Sigma}, \quad (13)$$

where  $\ell = \partial\Sigma$  is the boundary of  $\Sigma$ , and  $\Sigma$  is smooth oriented surface.  
If we only consider  $\mathbb{R}^2$ , we have the circulation

$$\Gamma_{\partial\Sigma} = \oint_{\partial\Sigma} \vec{u} \cdot d\vec{\ell} = \iint_{\Sigma} (\operatorname{curl} \vec{u}) \, dx \, dy. \quad (14)$$

Approximation of circulation

# Definition of Circulation

Let the area of  $\Sigma$  to be  $A = \iint_{\Sigma} dx dy$ , we have

$$\Gamma_{\partial\Sigma} = A \cdot \frac{\iint_{\Sigma} (\operatorname{curl} \vec{u}) dx dy}{\iint_{\Sigma} dx dy} \approx \text{Area} \times \text{mean of } \operatorname{curl} \vec{u} \text{ in } \Sigma. \quad (15)$$

Here state a conclusion,

*The circulation is to measure the rotation in a region.*

## Approximation of circulation

So, now the method to estimate the rotation of the fluid flow with fluid velocity  $\vec{u}$  are

- ① Curl  $\nabla \times \vec{u}(\vec{r}) = \text{curl } \vec{u}(\vec{r})$  is to measure the rotation at point  $\vec{r}$ .
- ② Circulation  $\Gamma_C = \oint_C \vec{u} \cdot d\vec{\ell}$  is to measure the rotation in a region  $C$ .

So, now let us consider some special case for  $\nabla \times \vec{u} = 0$ .

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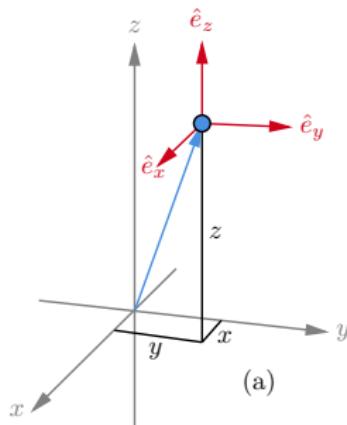
## 4. Conclusion

## Vector calculus

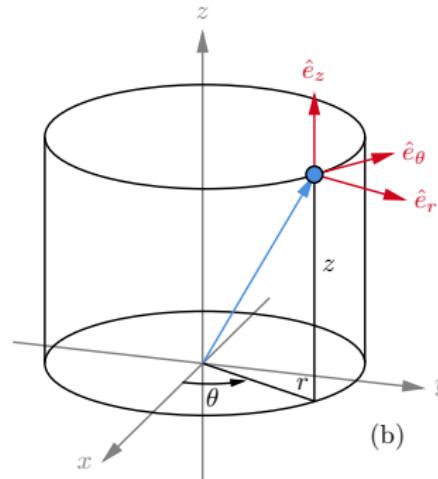
## Vector calculus

First, let us specify our coordinates, that is

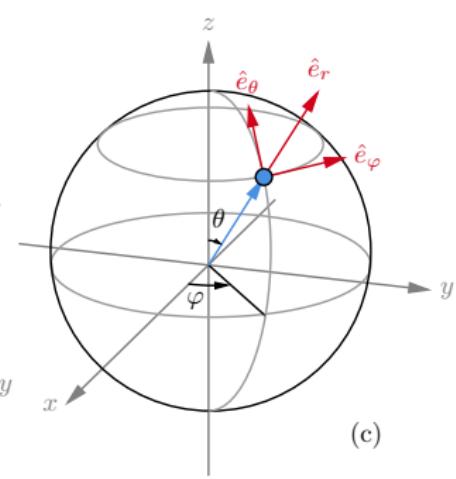
Cartesian  
coordiante



Cylindrical  
coordiante



Spherical  
coordiante



## Vector calculus

The curl in three different coordinate are

- ① For a vector field  $\vec{A} = A_x \hat{e}_x + A_y \hat{e}_y + A_z \hat{e}_z$

$$\nabla \times \vec{A} = \begin{vmatrix} \hat{e}_x & \hat{e}_y & \hat{e}_z \\ \partial_x & \partial_y & \partial_z \\ A_x & A_y & A_z \end{vmatrix} \quad (16)$$

- ② For a vector field  $\vec{A} = A_r \hat{e}_r + A_\theta \hat{e}_\theta + A_z \hat{e}_z$

$$\nabla \times \vec{A} = \begin{vmatrix} \hat{e}_r & r\hat{e}_\theta & \hat{e}_z \\ \partial_r & \partial_\theta & \partial_z \\ A_r & rA_\theta & A_z \end{vmatrix} \quad (17)$$

- ③ For a vector field  $\vec{A} = A_r \hat{e}_r + A_\theta \hat{e}_\theta + A_\varphi \hat{e}_\varphi$

$$\nabla \times \vec{A} = \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{e}_r & r\hat{e}_\theta & r \sin \theta \hat{e}_\varphi \\ \partial_r & \partial_\theta & \partial_z \\ A_r & rA_\theta & r \sin \theta A_z \end{vmatrix} \quad (18)$$

Or, expanding ...

- ① For a vector field  $\vec{A} = A_x \hat{e}_x + A_y \hat{e}_y + A_z \hat{e}_z$

$$\nabla \times \vec{A} = \left( \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) \hat{e}_x - \left( \frac{\partial A_z}{\partial x} - \frac{\partial A_x}{\partial z} \right) \hat{e}_y + \left( \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) \hat{e}_z \quad (19)$$

- ② For a vector field  $\vec{A} = A_r \hat{e}_r + A_\theta \hat{e}_\theta + A_z \hat{e}_z$

$$\nabla \times \vec{A} = \left( \frac{1}{r} \frac{\partial A_z}{\partial \theta} - \frac{\partial A_\theta}{\partial z} \right) \hat{e}_r + \left( \frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right) \hat{e}_\theta + \frac{1}{r} \left( \frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \hat{e}_z \quad (20)$$

- ③ For a vector field  $\vec{A} = A_r \hat{e}_r + A_\theta \hat{e}_\theta + A_\varphi \hat{e}_\varphi$

$$\begin{aligned} \nabla \times \vec{A} = & \frac{1}{r \sin \theta} \left( \frac{\partial}{\partial \theta} (A_z \sin \theta) - \frac{\partial A_\theta}{\partial \varphi} \right) \hat{e}_r \\ & + \frac{1}{r} \left( \frac{1}{\sin \theta} \frac{\partial A_r}{\partial \varphi} - \frac{\partial}{\partial r} (r A_\varphi) \right) \hat{e}_\theta + \frac{1}{r} \left( \frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \hat{e}_\varphi \end{aligned} \quad (21)$$

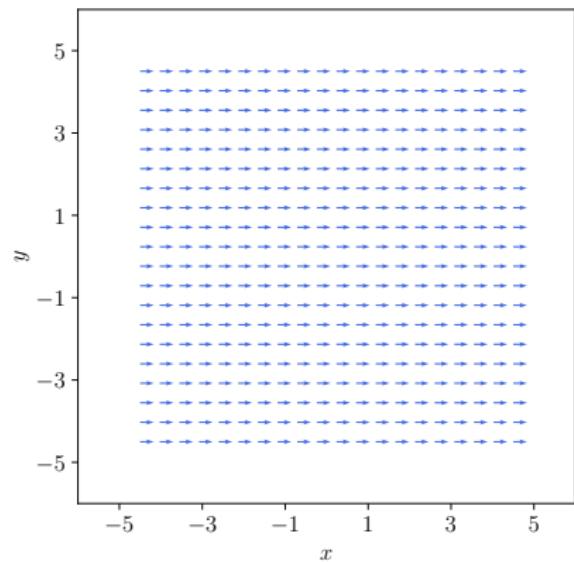
## Example for Cartesian

## Example for Cartesian

Here, for simplicity, we only consider the flow on the  $xy$ -plane and using the Cartesian coordinate to describe. We consider a flow velocity

$$\vec{u}(x, y) = 1 \cdot \hat{e}_x. \quad (22)$$

Obviously, the curl is zero,  $\nabla \times \vec{u} = 1$ , since it is a uniform flow.



## Example for Cartesian

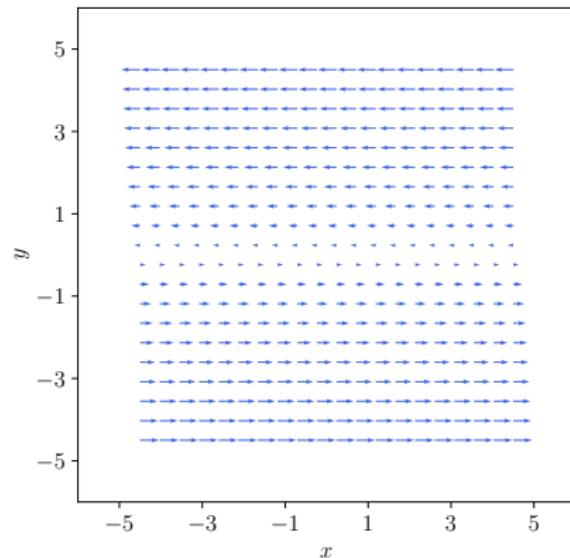
Another example is to consider the flow velocity

$$\vec{u}(x, y) = -y \cdot \hat{e}_x, \quad (23)$$

so that the velocity grows when  $y$  becomes larger. Now, the curl is

$$\nabla \times \vec{u} = 1 \cdot \hat{e}_z, \quad (24)$$

Although, the curl is not zero, we still can not see any rotation in the arrow graph of vector field.



## Example for Cartesian

Even the stream and path line, we still cannot see any rotation.

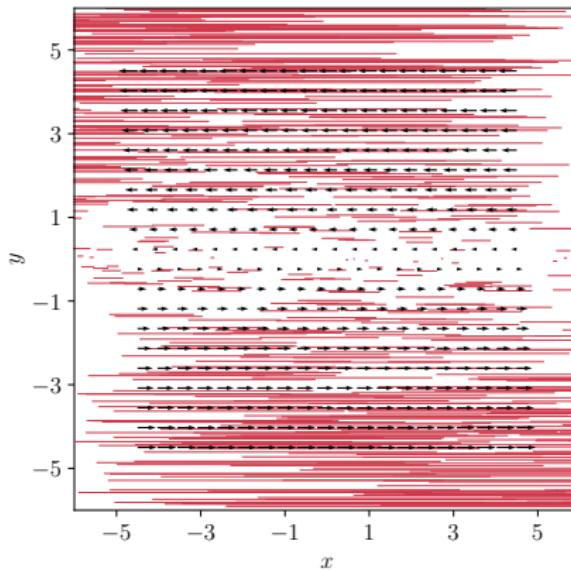


Figure: Given random initial position condition to solve *path line*.

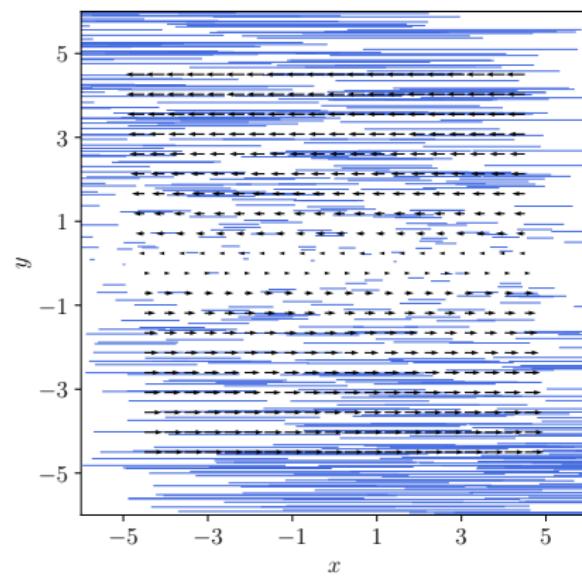
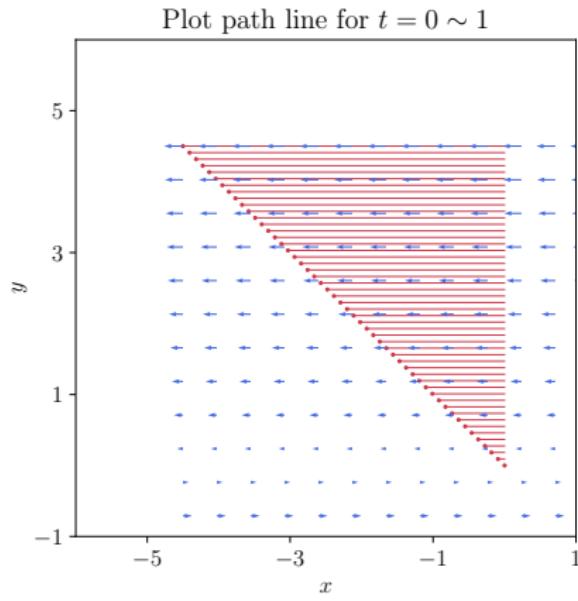
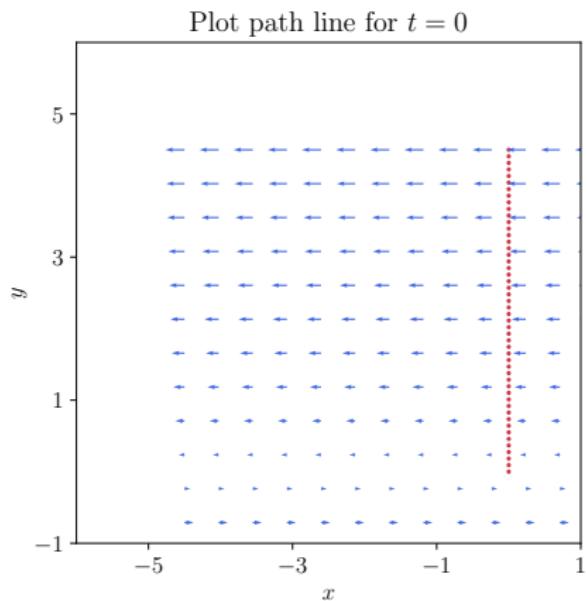


Figure: Given random initial position condition to solve *stream line*.

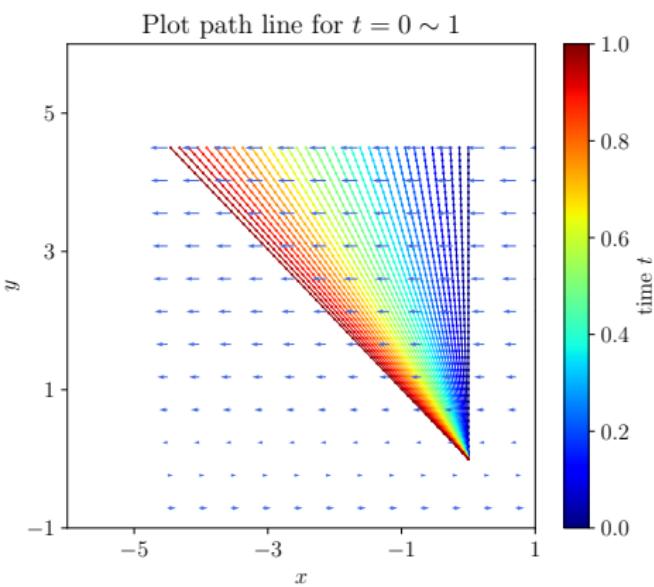
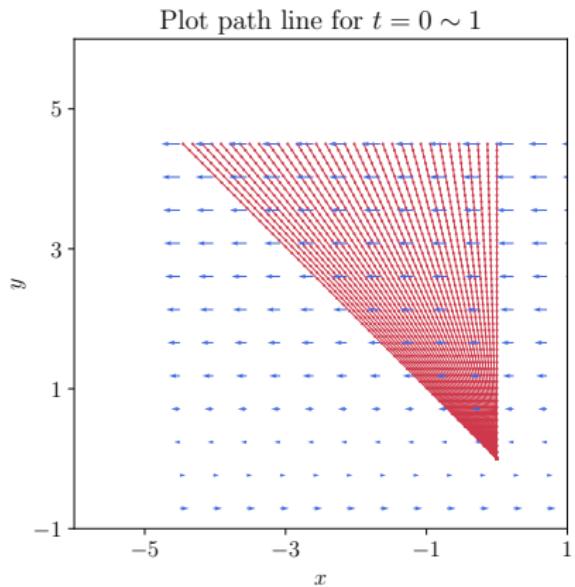
## Example for Cartesian

But if we look at some specific particle in space:



## Example for Cartesian

And link the particles in each time, and color them in different colors:



## Example for Cartesian

Here, for simplicity, we only consider the flow on the  $xy$ -plane and using the cylindrical coordinate to describe. So, the fluid velocity now becomes

$$\vec{u}(r, \theta) = u_r(r, \theta)\hat{e}_r + u_\theta(r, \theta)\hat{e}_\theta, \quad (25)$$

and then the curl

$$\nabla \times \vec{u} = \left( \frac{1}{r} \frac{\partial u_z}{\partial \theta} - \frac{\partial u_\theta}{\partial z} \right) \hat{e}_r + \left( \frac{\partial u_r}{\partial z} - \frac{\partial u_z}{\partial r} \right) \hat{e}_\theta + \frac{1}{r} \left( \frac{\partial}{\partial r} (ru_\theta) - \frac{\partial u_r}{\partial \theta} \right) \hat{e}_z \quad (26)$$

becomes

$$\nabla \times \vec{u} = \frac{1}{r} \left( \frac{\partial}{\partial r} (ru_\theta) - \frac{\partial u_r}{\partial \theta} \right) \hat{e}_z, \quad (27)$$

also notice that the differential displacement in this case is

$$d\vec{l} = dr \hat{e}_r + rd\theta \hat{e}_\theta. \quad (28)$$

## Example for Cylindrical

## Example for Cylindrical

Now, let  $\vec{u}(r, \theta) = u_\theta(r, \theta)\hat{e}_\theta$ , and solve for  $0 = \nabla \times \vec{u}$ , we have

$$0 = \frac{1}{r} \left( \frac{\partial}{\partial r} (ru_\theta(r, \theta)) - \frac{\partial 0}{\partial \theta} \right) \hat{e}_z \quad (29)$$

$$\Rightarrow 0 = u_\theta(r, \theta) + r \frac{\partial u_\theta(r, \theta)}{\partial r}, \quad \text{for } r \neq 0 \quad (30)$$

$$\Rightarrow \frac{\partial u_\theta(r, \theta)}{\partial r} = -\frac{u_\theta(r, \theta)}{r}. \quad (31)$$

By experience, the general solution is  $u_\theta(r, \theta) = r^{-1}f(\theta)$ , where  $f$  is a function of  $\theta$ . We can check by plug into the equation

$$\frac{\partial u_\theta(r, \theta)}{\partial r} = -r^{-2}f(\theta) = -\frac{r^{-1}f(\theta)}{r} = -\frac{u_\theta(r, \theta)}{r}.$$

## Example for Cylindrical

Then we can calculate the circulation for  $\vec{u}(r, \theta) = u_\theta(r, \theta)\hat{e}_\theta$  such that  $\nabla \times \vec{u} = 0$ , the general solution is  $u_\theta(r, \theta) = r^{-1}f(\theta)$ , then the circulation in cylindrical coordinate (polar coordinate) is

$$\Gamma_C = \oint_C \vec{u} \cdot d\vec{\ell} = \oint_C u_\theta(r, \theta) r d\theta = \oint_C f(\theta) d\theta. \quad (32)$$

Now, we can observing that, although the curl is zero, if  $f(\theta) > 0$  on  $C$ , then  $\Gamma_C > 0$ , on the other hand, if  $f(\theta) < 0$  on  $C$ , then  $\Gamma_C < 0$ .

## Example for Cylindrical

Now, consider a more general case, let  $\vec{u}(r, \theta) = u_r(r, \theta)\hat{e}_r + u_\theta(r, \theta)\hat{e}_\theta$ , and solve for  $\nabla \times \vec{u} = 0$ , we have

$$0 = \frac{\partial}{\partial r} (ru_\theta(r, \theta)) - \frac{\partial u_r(r, \theta)}{\partial \theta}, \quad (33)$$

Also, by experience, let  $u_r(r, \theta) = r^{-1}f(r, \theta)$ , we have

$$\frac{\partial f(r, \theta)}{\partial r} = \frac{\partial u_r(r, \theta)}{\partial \theta}, \quad (34)$$

which is the first equation in *Cauchy–Riemann equations*.

## Example for Cylindrical

In order to solve  $\partial f(r, \theta) / \partial r = \partial u_r(r, \theta) / \partial \theta$ , we can suppose there exists a potential function  $\phi(r, \theta)$  such that

$$f(r, \theta) = \frac{\partial \phi(r, \theta)}{\partial \theta} \quad \text{and} \quad u_r(r, \theta) = \frac{\partial \phi(r, \theta)}{\partial r}. \quad (35)$$

With this assumption, the equation is automatically satisfied:

$$\frac{\partial f(r, \theta)}{\partial r} = \frac{\partial^2 \phi(r, \theta)}{\partial r \partial \theta} = \frac{\partial^2 \phi(r, \theta)}{\partial \theta \partial r} = \frac{\partial u_r(r, \theta)}{\partial \theta}.$$

Now, the solution is

$$\vec{u} = \frac{\partial \phi(r, \theta)}{\partial r} \hat{e}_r + \frac{1}{r} \frac{\partial \phi(r, \theta)}{\partial \theta} \hat{e}_\theta = \nabla \phi \quad (36)$$

where  $\phi$  is any function of  $r$  and  $\theta$ .

## Example for Cylindrical

Then we can calculate the circulation for  $\vec{u} = u_r(r, \theta)\hat{e}_r + u_\theta(r, \theta)\hat{e}_\theta$  such that  $\nabla \times \vec{u} = 0$ . The general solution is

$u_\theta(r, \theta) = \partial_r \phi \hat{e}_r + r^{-1} \partial_\theta \phi \hat{e}_r$ , where  $\phi$  is any function of  $r$  and  $\theta$ . The circulation in cylindrical coordinate (polar coordinate) is

$$\Gamma_C = \oint_C \vec{u} \cdot d\vec{\ell} = \oint_C \left( u_r(r, \theta) dr + u_\theta(r, \theta) r d\theta \right) \quad (37)$$

$$= \oint_C \frac{\partial \phi(r, \theta)}{\partial r} dr + \frac{1}{r} \frac{\partial \phi(r, \theta)}{\partial \theta} r d\theta \quad (38)$$

$$= \oint_C \frac{\partial \phi(r, \theta)}{\partial r} dr + \frac{\partial \phi(r, \theta)}{\partial \theta} d\theta \quad (39)$$

$$= \oint_C \nabla \phi \cdot d\vec{\ell} = \oint_C d\phi, \quad (40)$$

where  $d\phi$  is the total differential.

## Example for Cylindrical

Usually,  $\phi$  is a continuous function; however, not always. If a piecewise smooth oriented path  $C$  can be parameterized by

$$\vec{\ell}(t) = x(r(t), \theta(t))\hat{e}_x + y(r(t), \theta(t))\hat{e}_y, \quad (41)$$

where  $t \in [a, b]$  and  $\vec{\ell}(a) = \vec{\ell}(b)$ , then the circulation becomes

$$\Gamma_C = \phi(\vec{r}(b)) - \phi(\vec{r}(a)). \quad (42)$$

However, if  $\phi(r, \theta) = \theta$ , the vector field is  $\vec{u} = \nabla\phi = 1/r\hat{e}_\theta$ . If the path  $C$  surrounds the origin, which is the pole  $r = 0$ , the circulation becomes  $\Gamma_C = 2\pi - 0 = 2\pi > 0$ , which means the circulation still can be measurement of rotation.

## Example for Cylindrical

This is because function  $\theta$  is *multivalued function*. Here we know that for all potential flow, the curl is zero (irrotational/vorticity-free)

$$\nabla \times \vec{u} = 0,$$

However,

$$\begin{cases} \text{if } \phi \text{ is single-valued} & \Rightarrow \Gamma_C = 0, \text{ for any closed curve } C, \\ \text{if } \phi \text{ is multivalued} & \Rightarrow \Gamma_C \neq 0, \text{ for some closed curves } C. \end{cases}$$

## Example for Cylindrical

Here, I list some potential flow in cylindrical coordinate:

| $\phi(r, \theta)$                 | $\vec{u} = \nabla\phi$   |
|-----------------------------------|--|
| $\theta$                          | $(1/r) \hat{e}_\theta$   |
| $c_0 + c_1 \cdot \theta$          | $(c_1/r) \hat{e}_\theta$   |
| $\sum_{s=0}^n c_s \cdot \theta^s$ | $(\sum_{s=1}^n s c_s \cdot \theta^{s-1}/r) \hat{e}_\theta$       |
| $f(\theta)$                       | $(f'(\theta)/r) \hat{e}_\theta$                                  |
| $\cos \theta$                     | $(-\sin \theta/r) \hat{e}_\theta$                                |
| $\sin \theta$                     | $(\cos \theta/r) \hat{e}_\theta$                                 |
| $g(r) \cdot f(\theta)$            | $(g'(r)f(\theta)) \hat{e}_r + (g(r)f'(\theta)/r) \hat{e}_\theta$ |
| $\vdots$                          | $\vdots$   |

where  $c_0, c_1, \dots, c_n$  are constants, and  $f$  is any function of  $\theta$ ,  $g$  is any function of  $r$ .

Note that if the function depends on  $\theta$ ,  $\hat{e}_\theta$  component of  $\vec{u}$  is not zero.

# Outline

## 1. Curl and Rotation

- 1.1 What is angular velocity?
- 1.2 Stream line and Path line
- 1.3 Example

## 2. Circulation and Rotation

- 2.1 Definition of Circulation
- 2.2 Approximation of circulation

## 3. Curl and Circulation

- 3.1 Vector calculus
- 3.2 Example for Cartesian
- 3.3 Example for Cylindrical

## 4. Conclusion

# Conclusion

In conclude,

- ① The ***curl*** is to measure the rotation at specific point.
- ② The ***circulation*** is to measure the rotation in a region.
- ③ If the potential function depends on the variable  $\theta$ , the fluid velocity may have an  $\hat{e}_\theta$  component.
- ④ If the potential function is discontinuous on the closed path, even if curl is zero, the circulation can still be nonzero.

Thanks!

