Rothermel vs. Balbi rate of spread model By: Jeremy Benik

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Outline

- Overview of Rothermel model
- ► Initial Rothermel ROS equation
- Final Rothermel ROS equation
- Overview of the Rothermel model
- Overview of the Balbi model
- Comparisons between the models

Overview of the Rothermel Model

Introduction to the Rothermel ROS model

➤ The original Rothermel model was created by Richard C. Rothermel in 1972 and was based on a heat balance model developed by Fransden in 1971

► The goal of this model was to calculate the rate of spread of a fire in various conditions quickly and accurately

This is a semi-empirical model, meaning the model was formulated using some physical properties and observational/statistical data

Overview of the Rothermel Model

Introduction to the Rothermel ROS model

► The authors initially created the model assuming no wind/slope conditions to make formulating the model easier

➤ The slope and wind parameters were added in later after the initial model was created

Assumptions and simplifications are necessary to reduce Equation 1 down to a more manageable calculation

Initial Rothermel rate of spread equation

$$R = \frac{I_{xig} + \int_{-\infty}^{0} (\frac{\partial I_z}{\partial z})_{z_c} dx}{\rho_{be} * Q_{ig}}$$
(1)

- ► R = Quasi-steady rate of spread, ft./min.
- ▶ I_{xig} = horizontal heat flux absorbed by a unit volume of fuel at the time of ignition, $B.t.u/ft.^2$ -min
- $ho_{be} = \text{Effective bulk density, lb./ft.3}$
- $ightharpoonup Q_{ig} = \text{heat of preignition}, B.T.U./lb$
- $(\frac{\partial I_z}{\partial z})_{z_c}$ = The gradient of the vertical intensity evaluated at a plane at a constant depth, z_c , of the fuel bed, B.t.u./ft.³ -min

Evaluating Each Component

$$Q_{ig} = C_{pd}\Delta T + M_f(C_{pw}\Delta T_B + V)$$
 (2)

$$I_{R} = -\left(\frac{\mathrm{d}w}{\mathrm{d}x}\right)\left(\frac{\mathrm{d}x}{\mathrm{d}t}\right)h\tag{3}$$

$$I_R D = R * h(W_n - W_r) \tag{4}$$

$$\Gamma = \Gamma' \eta_M \eta_s \tag{5}$$

$$\beta = \frac{\rho_b}{\rho_p} \tag{6}$$

$$\sigma = \frac{4}{d} \tag{7}$$

Evaluating Each Component

$$\Gamma' = \frac{\Gamma}{\eta_M \eta_S} \tag{8}$$

$$\Gamma' = \Gamma'_{max}(\frac{\beta}{\beta_{op}})^A exp[A(1 - \frac{\beta}{\beta_{op}})]$$
 (9)

$$(I_P)_o = R_0 \rho_b \epsilon Q_{ig} \tag{10}$$

$$\phi_W = CU^B (\frac{\beta}{\beta_{op}})^{-E} \tag{11}$$

$$\phi_S = 5.275 \beta^{-.3} (\tan \phi)^2 \tag{12}$$

Overview of the Balbi Model

Different versions of the Balbi Model

- ► There are multiple versions of the Balbi model
- ► The first model being created in 2007 and the last revision made this year (2022)
- Improvements have been made to the model over time to make it more accurate by accounting for more physical properties within a fire
- ► The goal of this model is to provide an accurate ROS calculation faster than real time

Overview of the Balbi Model

Physical model

- ► The Balbi model is a fully physics based model
- There are no observations/statistical data used to build the model, only physical processes occurring within a fire
- Like with Rothermel, the initial model was designed without slope and wind in mind to simplify formulating the model
- ► Slope and wind was then added in later since it is a necessary component to fire spread

Evaluating Each Equation

$$\tan \beta_w = \frac{\nu_w}{u_{ff}} \tag{13}$$

$$\gamma = \alpha + \beta_s \tag{14}$$

$$\tan \beta_s = \frac{\nu_s}{u_{fl}} \tag{15}$$

$$H = H^* Q^{\frac{2}{5}} = H^* (\Delta h_{fu} \sigma_{fu} c)^{\frac{2}{5}}$$
 (16)

$$\rho_{g} \frac{\partial u}{\partial t} = (\rho_{a} - \rho_{g})g \tag{17}$$

$$u_{fl} = Q^{\frac{1}{5}} \sqrt{(\frac{T_{fl}}{T_a} - 1)gH^*}$$
 (18)

$$\rho_{g} u_{fl} I = \rho_{ga} h \nu_{u} + D \dot{\sigma}_{fu} \tag{19}$$

$$\rho_{\mathsf{a}} h \nu_{\mathsf{u}} = \upsilon \mathsf{D} \dot{\sigma}_{\mathsf{f} \mathsf{u}} \tag{20}$$

$$T_{fl} = T_a + \frac{(1-\chi)Q}{(v+1)D\dot{\sigma}_{fu}c_{pg}} = T_a + \frac{1-\chi)\Delta h_{fu}}{(v+1)c_{pg}}$$
 (21)

$$R_b = \sigma T_{ff}^4 d(\delta - x) \tag{22}$$

$$R_{ff} = \epsilon_{ff} \sigma \frac{T_{ff}^4}{2} (1 - \cos \theta) \tag{23}$$

$$\sigma_{fu}c_{pfu}\frac{\mathrm{d}T_{fu}}{\mathrm{d}t}=R_b+R_{fl}-\Delta h_w\frac{\mathrm{d}\sigma_w}{\mathrm{d}t}$$
 (24)

$$c_1 = \frac{\sigma T_{fl}^4 d\delta^2}{2\sigma_{fu}(c_{pfu}(T_{ig} - T_a) + \Delta h_w \eta)}$$
(25)

$$c_h = c_l + \frac{\epsilon_{fl} \sigma T_{fl}^4 H}{2\sigma_{fu} (c_{pfu} (T_{ig} - T_a) + \Delta h_w \eta)} (1 + \sin \gamma - \cos \gamma) \quad (26)$$

$$\varepsilon_{\rm fl}\sigma T_{\rm fl}^4 = \chi Q/H \tag{27}$$

$$\phi_c = \frac{\Delta H}{2\tau_0} \sigma smin(h, \delta) \tan \gamma_c \tag{28}$$

$$\tan \gamma_c = \tan \alpha + \frac{U(L)}{u_c} \tag{29}$$

$$R_{c} = a_{M} min(\frac{W_{0}}{50}, 1) * \frac{\Delta H \rho_{a} T_{a} s \sqrt{h}}{2q(s_{t} + 1)\rho_{v} T} (\frac{(s_{t} + 1)\rho_{v} T}{\tau_{0} \rho_{a} T_{a}} * min(S, \frac{2\pi S}{S_{t}} \tan \alpha + U \exp(-\frac{\beta_{t}}{min(\frac{W_{0}}{50}, 1)} R))$$
(30)

Wind Speed Comparison

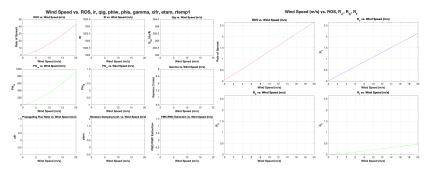


Figure: Rothermel Model

Figure: Balbi Model

Slope Comparison

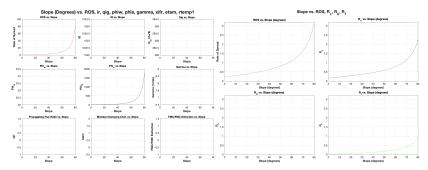


Figure: Rothermel Model

Figure: Balbi Model

FMC Comparison

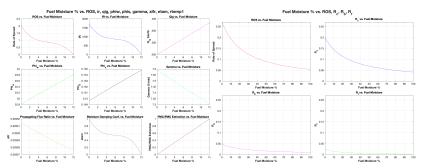


Figure: Rothermel Model

Figure: Balbi Model

FMC Rothermel

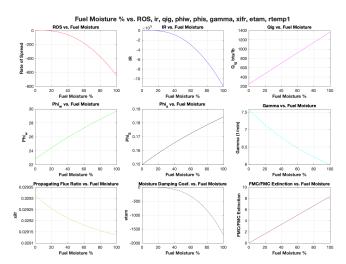


Figure: Rothermel model FMC without considering extinction FMC

Fuel Height Comparison

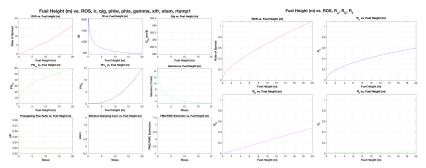


Figure: Rothermel Model

Figure: Balbi Model

SAVR Comparison

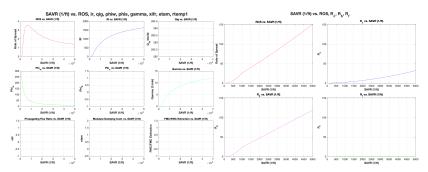


Figure: Rothermel Model

Figure: Balbi Model

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