ME 57200 Aerodynamic Design

Lecture #14: Incompressible Flow over Airfoils

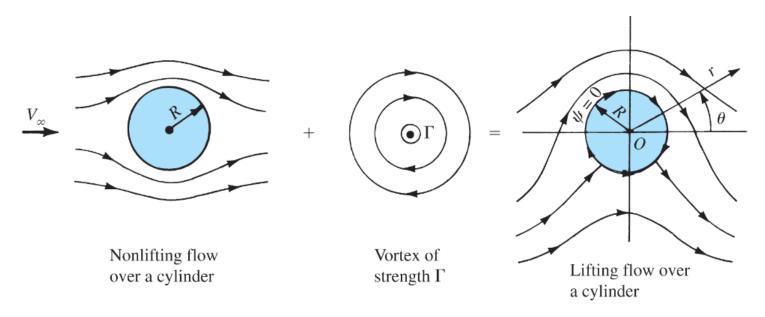
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How to synthesize a lifting flow over a cylinder with the elementary flows?



What is the stream function of the synthesized flow?

$$\psi = (V_{\infty}r\sin\theta)\left(1 - \frac{R^2}{r^2}\right) + \frac{\Gamma}{2\pi}\ln\frac{r}{R}$$

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What are the velocities in the flow field?

$$V_r = \left(1 - \frac{R^2}{r^2}\right) V_\infty \cos \theta$$

$$V_{\theta} = -\left(1 + \frac{R^2}{r^2}\right) V_{\infty} \sin \theta - \frac{\Gamma}{2\pi r}$$

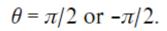
How to locate the stagnation points in the flow?

$$V_r = \left(1 - \frac{R^2}{r^2}\right) V_\infty \cos \theta = 0$$

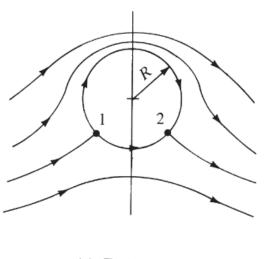
$$V_{\theta} = -\left(1 + \frac{R^2}{r^2}\right) V_{\infty} \sin \theta - \frac{\Gamma}{2\pi r} = 0$$

$$\theta = \arcsin\left(-\frac{\Gamma}{4\pi V_{\infty}R}\right)$$

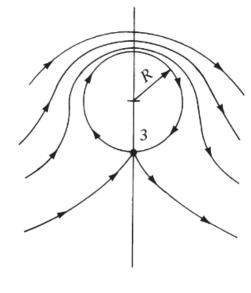
$$r = R$$
.



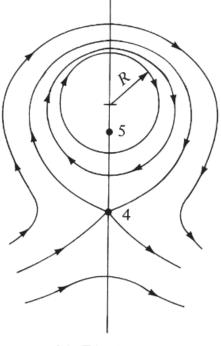
$$r = \frac{\Gamma}{4\pi V_{\infty}} \pm \sqrt{\left(\frac{\Gamma}{4\pi V_{\infty}}\right)^2 - R^2}$$







(b)
$$\Gamma = 4\pi V_{\infty} R$$



(c)
$$\Gamma > 4\pi V_{\infty}R$$

What are the velocities at the cylinder surface?

$$r = R$$
: $V = V_{\theta} = -2V_{\infty} \sin \theta - \frac{\Gamma}{2\pi R}$

What are the pressures at the cylinder surface?

$$C_p = 1 - \left(\frac{V}{V_{\infty}}\right)^2 = 1 - \left(-2\sin\theta - \frac{\Gamma}{2\pi RV_{\infty}}\right)^2$$

$$C_p = 1 - \left[4\sin^2\theta + \frac{2\Gamma\sin\theta}{\pi RV_{\infty}} + \left(\frac{\Gamma}{2\pi RV_{\infty}}\right)^2 \right]$$

How to obtain the aerodynamic drag coefficient?

$$c_d = c_a = \frac{1}{c} \int_{LE}^{TE} (C_{p,u} - C_{p,l}) dy$$

$$c_d = -\frac{1}{2} \int_0^{\pi} C_p \cos\theta \, d\theta - \frac{1}{2} \int_{\pi}^{2\pi} C_p \cos\theta \, d\theta$$

$$c_d = -\frac{1}{2} \int_0^{2\pi} C_p \cos\theta \, d\theta$$

$$c_d = 0$$

How to obtain the aerodynamic lift coefficient?

$$c_{l} = c_{n} = \frac{1}{c} \int_{0}^{c} C_{p,l} dx - \frac{1}{c} \int_{0}^{c} C_{p,u} dx$$

$$c_{l} = -\frac{1}{2} \int_{\pi}^{2\pi} C_{p,l} \sin \theta d\theta + \frac{1}{2} \int_{\pi}^{0} C_{p,u} \sin \theta d\theta$$

$$c_{l} = -\frac{1}{2} \int_{0}^{2\pi} C_{p} \sin \theta d\theta$$

$$c_{l} = \frac{\Gamma}{RV_{\infty}} \qquad \qquad L' = q_{\infty} Sc_{l} = \frac{1}{2} \rho_{\infty} V_{\infty}^{2} Sc_{l}$$

$$L' = \frac{1}{2} \rho_{\infty} V_{\infty}^{2} 2R \frac{\Gamma}{RV_{\infty}}$$

$$L' = \rho_{\infty} V_{\infty} \Gamma$$

Example: Consider the lifting flow over a circular cylinder with a diameter of 0.5 m. The freestream velocity is 25 m/s, and the maximum velocity on the surface of the cylinder is 75 m/s. The freestream conditions are those for a standard altitude of 3 km. Calculate the lift per unit span on the cylinder.

 $\rho = 0.90926 \text{ kg/m}^3$.

The maximum velocity occurs at the top of the cylinder, where $\theta = 90^{\circ}$

Example: Consider the lifting flow over a circular cylinder with a diameter of 0.5 m. The freestream velocity is 25 m/s, and the maximum velocity on the surface of the cylinder is 75 m/s. The freestream conditions are those for a standard altitude of 3 km. Calculate the lift per unit span on the cylinder.

$$\rho = 0.90926 \text{ kg/m}^3$$
.

The maximum velocity occurs at the top of the cylinder, where $\theta = 90^{\circ}$

$$V_{\theta} = -2V_{\infty} \sin \theta - \frac{\Gamma}{2\pi R} \qquad V_{\theta} = -2V_{\infty} - \frac{\Gamma}{2\pi R} \qquad \Gamma = -2\pi R(V_{\theta} + 2V_{\infty})$$

 Γ is positive in the clockwise direction, and V_{θ} is negative in the clockwise direction

$$V_{\theta} = -75 \text{m/s}$$

$$\Gamma = -2\pi R (V_{\theta} + 2V_{\infty}) = -2\pi (0.25) [-75 + 2(25)]$$

$$\Gamma = -2\pi (0.25) (-25) = 39.27 \text{ m}^2/\text{s}$$

$$L' = \rho_{\infty} V_{\infty} \Gamma$$

$$L' = (0.90926)(25)(39.27) = \boxed{892.7 \text{ N/m}}$$

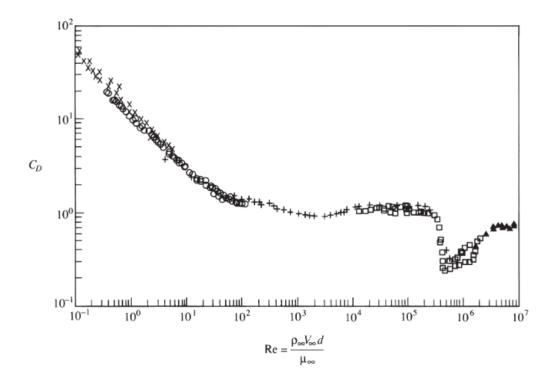
Flow over a Cylinder – the Real Case

Consider the real flow over a circular cylinder.

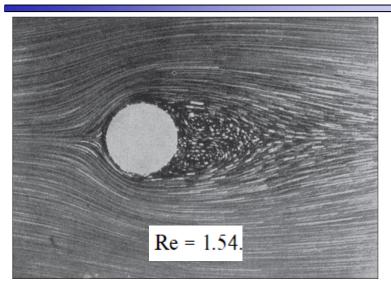
Would the flow be different?

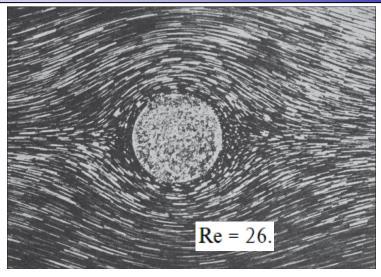
Where are the differences from?

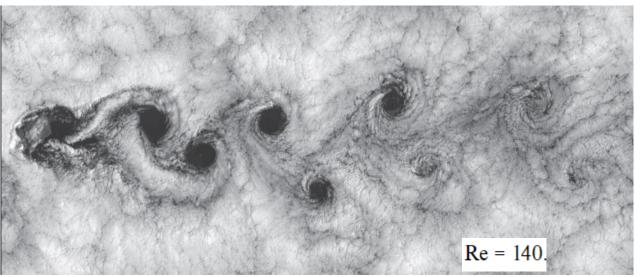
Friction



Flow over a Cylinder – the Real Case

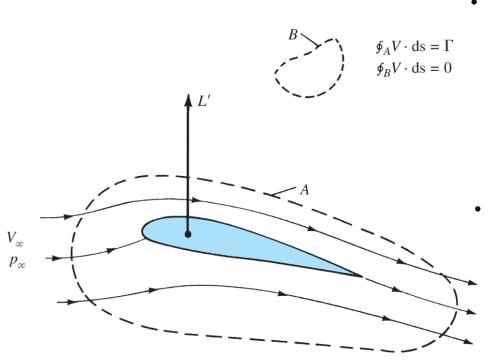






The Kutta-Joukowski Theorem

Consider the incompressible flow over an airfoil section. Let curve A be a curve in the flow enclosing the airfoil.



 If the airfoil is producing lift, the velocity field around the airfoil will be such that the line integral of velocity around A will be finite, that is, the circulation is finite

$$\Gamma \equiv \oint_A \mathbf{V} \cdot \mathbf{ds}$$

The lift per unit span on the airfoil will be give by *Kutta-Joukowski theorem*

$$L' = \rho_{\infty} V_{\infty} \Gamma$$

The Kutta-Joukowski Theorem

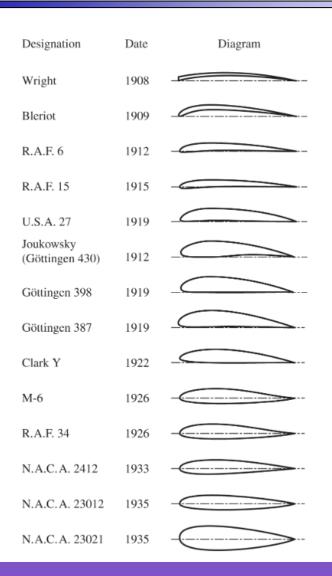
Kutta-Joukowski theorem: Lift per unit span on a two-dimensional body is directly proportional to the circulation around the body.

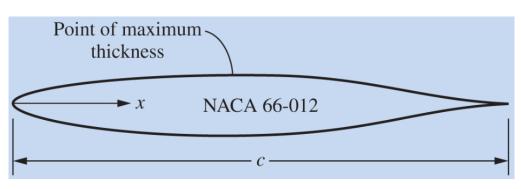
$$L' = \rho_{\infty} V_{\infty} \Gamma$$

- The value of Γ must be evaluated around a closed curve that encloses the body.
- The curve can be arbitrary, but it must have the body inside it.

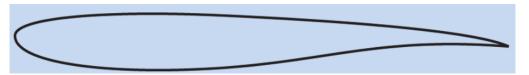
How can we calculate the circulation for a given body (airfoil) in a given incompressible, inviscid flow?

Incompressible Flow over Airfoils

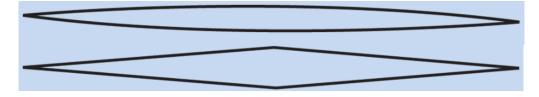




Laminar-flow airfoil (1938): to encourage laminar flow in the boundary layer over the airfoil to reduce skin friction drag

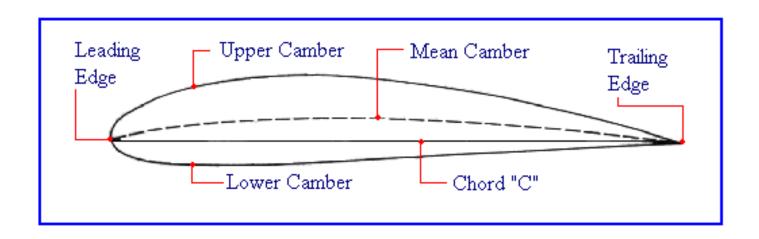


Supercritical airfoil (1965): designed for efficient flight near Mach one



Supersonic airfoil: designed for supersonic flow

Airfoil Characteristics

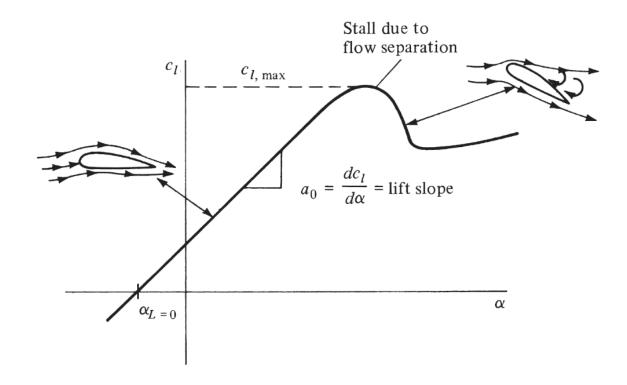


How to obtain the lift or lift coefficient of an airfoil?

- Experimental measurements
- Calculation: Circulation theory of lift
- Numerical simulations

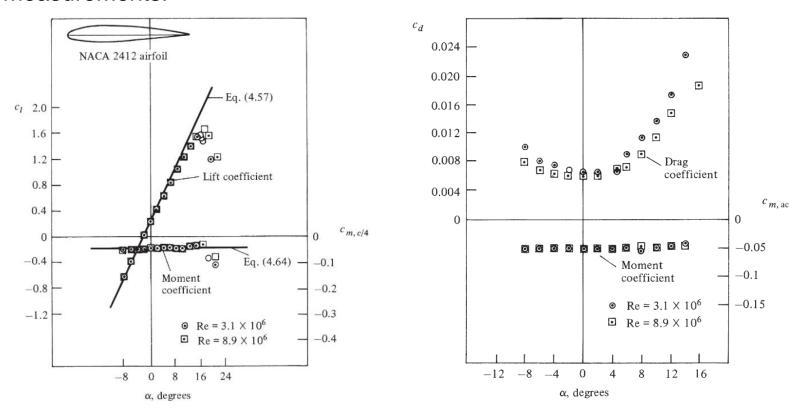
Airfoil Characteristics

Experimental measurements: Some typical results through wind tunnel measurements.



Airfoil Characteristics

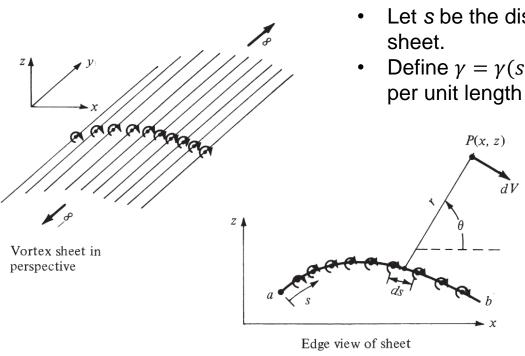
Experimental measurements: Some typical results through wind tunnel measurements.



Can we calculate the $c_{l,max}$ with the inviscid flow airfoil theory?

Calculation: Circulation theory of lift

Consider an infinite number of straight vortex filaments side by side, where the strength of each filament is infinitesimally small.



- Let s be the distance measured along the vortex sheet
- Define $\gamma = \gamma(s)$ as the strength of the vortex sheet, per unit length along s.

The strength of an infinitesimal portion ds of the sheet is γds

The induced velocity at point P

$$dV = -\frac{\gamma \, ds}{2\pi r}$$

Calculation: Circulation theory of lift

The strength of an infinitesimal portion ds of the sheet is γds

The induced velocity at point P

$$dV = -\frac{\gamma \, ds}{2\pi r}$$

The increment in velocity potential dφ

$$d\phi = -\frac{\gamma \, ds}{2\pi} \theta$$

The velocity potential at P due to the entire vortex sheet from a to b

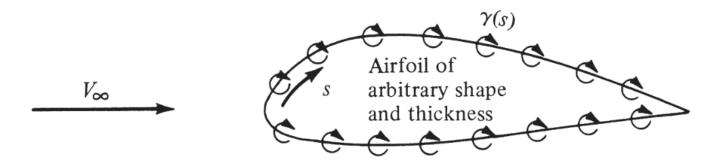
$$\phi(x,z) = -\frac{1}{2\pi} \int_{a}^{b} \theta \gamma \, ds$$

The circulation around the vortex sheet is the sum of the strengths of the elemental vortices from a to b

$$\Gamma = \int_{a}^{b} \gamma \, ds$$

Calculation: Circulation theory of lift

Consider an airfoil of arbitrary shape and thickness in a freestream with velocity V_{∞} . Replace the airfoil surface with a vortex sheet of variable strength $\gamma(s)$



The circulation around the airfoil will be given by

$$\Gamma = \int \gamma \, ds$$

• The resulting lift is given by the Kutta-Joukowski theorem:

$$L' = \rho_{\infty} V_{\infty} \Gamma$$

Calculation: Circulation theory of lift

Consider an airfoil of arbitrary shape and thickness in a freestream with velocity V_{∞} . Replace the airfoil surface with a vortex sheet of variable strength $\gamma(s)$

The need for analytical solutions for $\gamma = \gamma(s)$

No general analytical solution exists...

The circulation around the airfoil will be given by

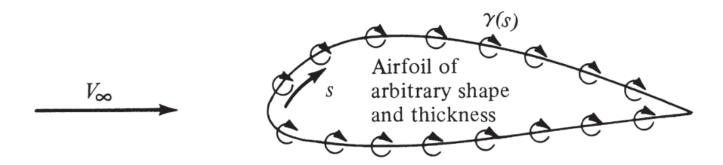
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Calculation: Circulation theory of lift

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- The concept of replacing the airfoil surface with a vortex sheet is more than just a mathematical device.
- In real life, there is a thin boundary layer on the surface, due to the action of friction between the surface and the airflow, in which the large velocity gradients produce substantial vorticity.
- There is a distribution of vorticity along the airfoil surface due to viscous effects.