ME 57200 Aerodynamic Design

Lecture #2: Aerodynamic Forces

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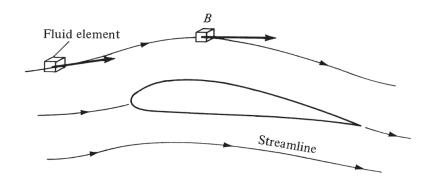
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Fundamental Aerodynamic Variables

Flow velocity:

An extremely important consideration in aerodynamics.

- Flow in motion
- A vector: has both magnitude and direction



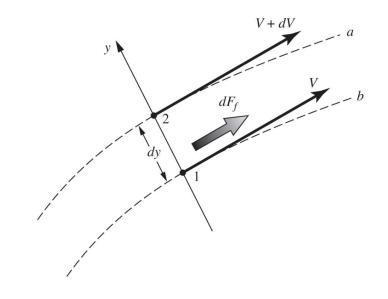
Fundamental Aerodynamic Variables

Friction, shear stress, viscous flow:

Act tangentially along the flow direction.

- Play a role internally in a flow
- Related to velocity gradients

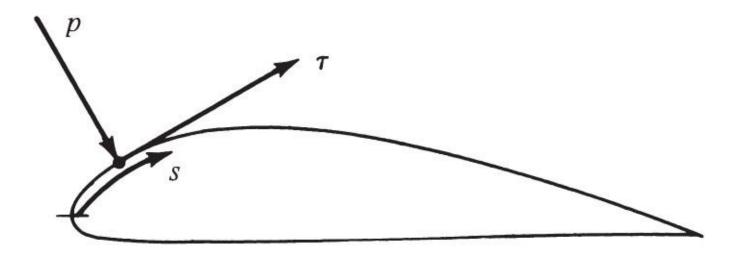
$$\tau = \mu \frac{dV}{dy}$$



Types of forces acting on aircraft?

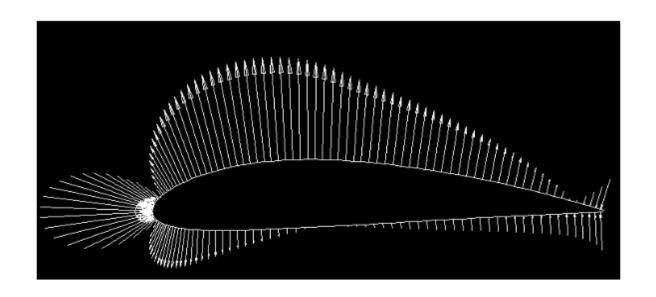


- Types of forces acting on aircraft?
 - Pressure distribution over the surface
 - Acts normal to the surface
 - Shear stress distribution over the surface
 - Acts tangential to the surface
 - No matter how complex the body shape may be, the aerodynamic forces and moments on the body are due to the above two basic sources.

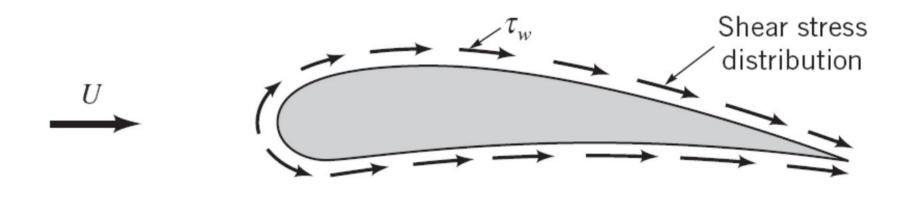


$$p = p(s)$$
 = surface pressure distribution
 $\tau = \tau(s)$ = surface shear stress distribution

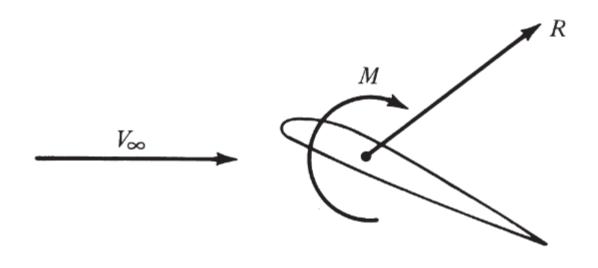
Pressure Distribution around Airfoil

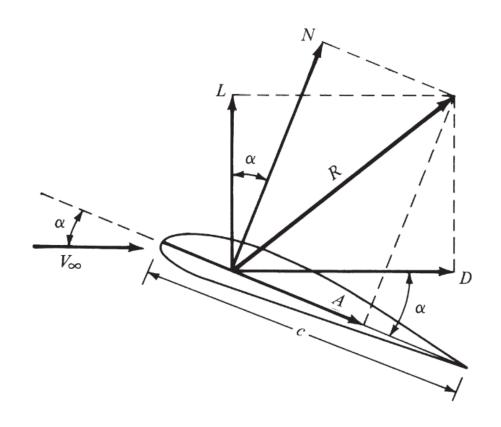


Shear Stress around Airfoil



 The net effect of the pressure and shear stress integrated over the body surface is a resultant aerodynamic force R and moment M on the body

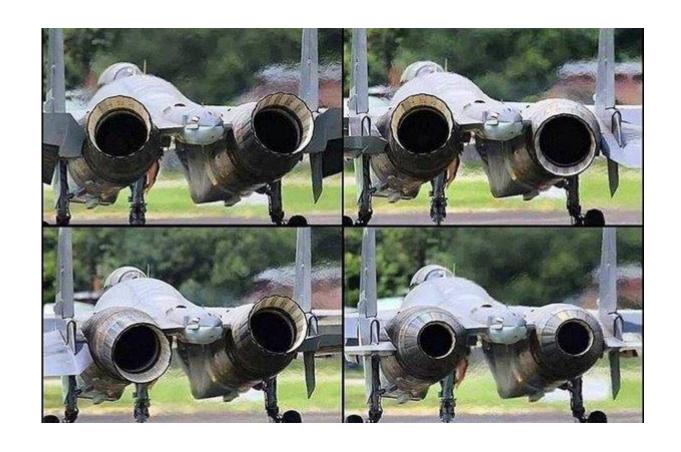




 $L \equiv \text{lift} \equiv \text{component of } R \text{ perpendicular to } V_{\infty}$ $D \equiv \text{drag} \equiv \text{component of } R \text{ parallel to } V_{\infty}$

 $N \equiv \text{normal force} \equiv \text{component of } R \text{ perpendicular to } c$ $A \equiv \text{axial force} \equiv \text{component of } R \text{ parallel to } c$

Vectored Thrust

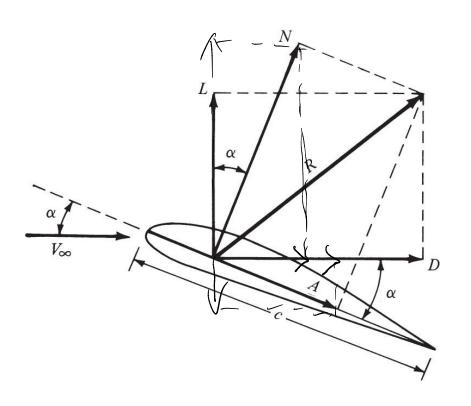


Vectored Thrust



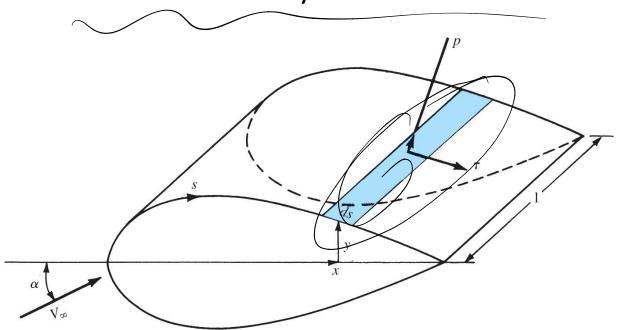
It can give an advantage of low-speed, plus high angle-of-attack maneuverability, compared to conventional-thrust aircraft.

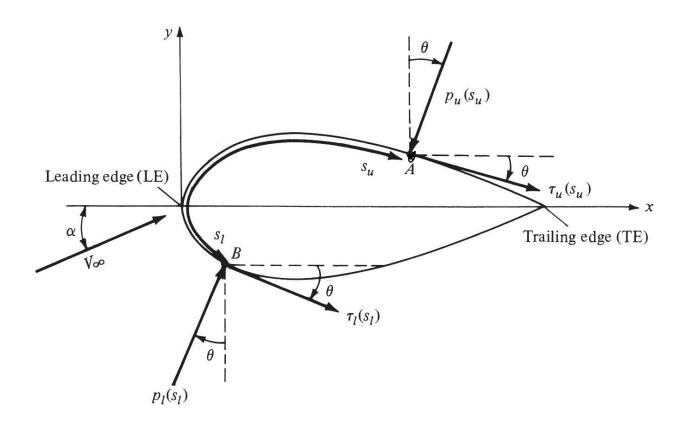
Relations between N & A and L & D?

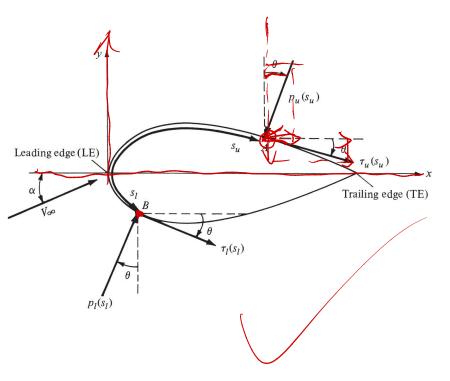


$$L = N \cdot \cos 2 - A - \sin 2$$

$$D = N \cdot \sin 2 + A \cdot \cos 2$$

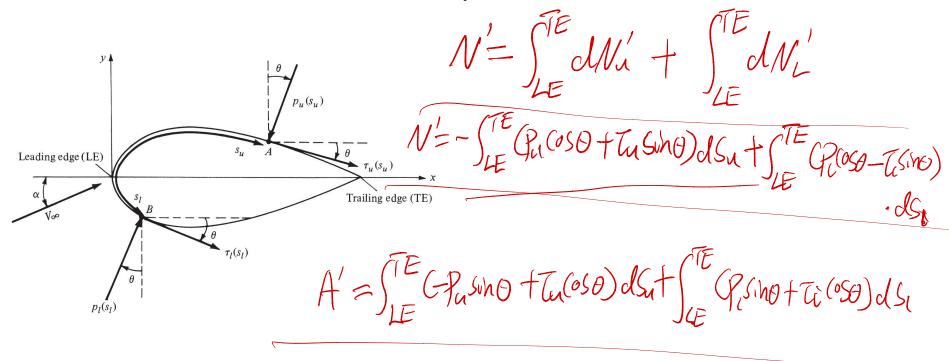




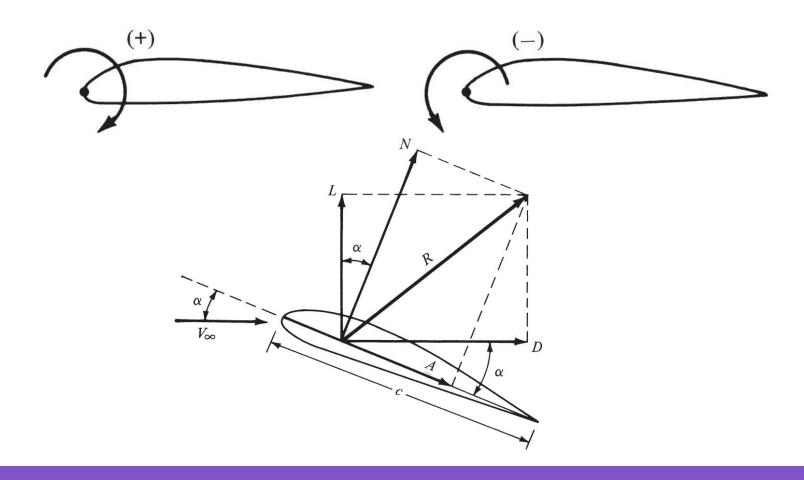


$$dN'_{i} = P_{i}dS_{i}\cos\theta - T_{i}dS_{i}\sin\theta$$

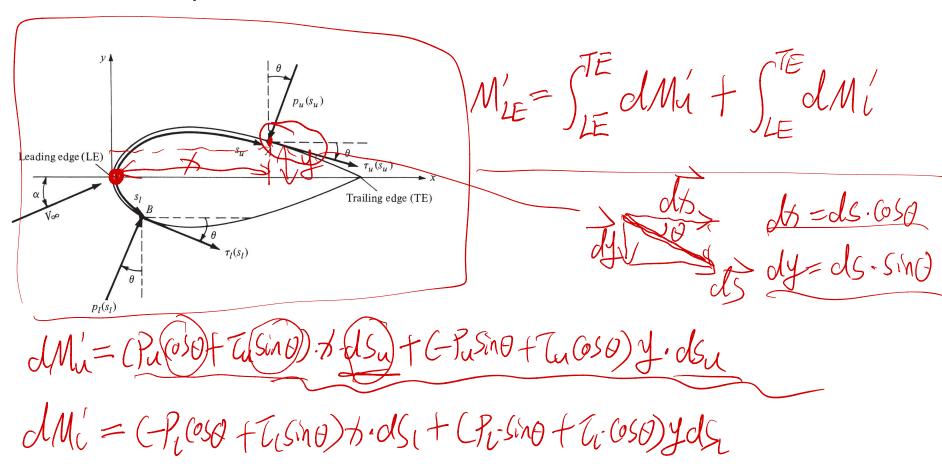
$$dA'_{i} = P_{i}dS_{i}\sin\theta + T_{i}dS_{i}\cos\theta$$



Aerodynamic Moments



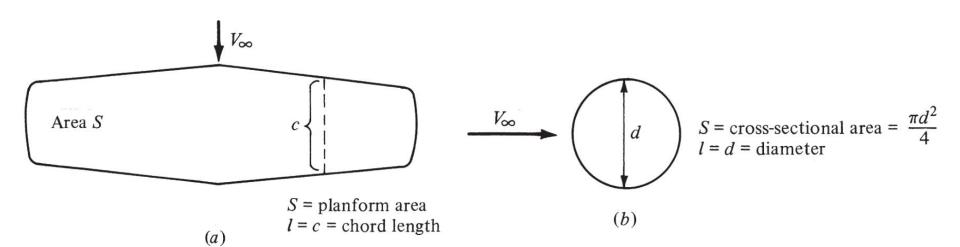
Aerodynamic moments



- Is it good enough to just know the aerodynamic forces moments?
- Why do we need dimensionless force and moment coefficients?

Dynamic pressure

$$q_{\infty} \equiv \frac{1}{2} \rho_{\infty} V_{\infty}^2$$



Lift coefficient:

$$C_L \equiv \frac{\widehat{L}}{q_{\omega}\widehat{S}}$$

A. M. T.

Drag coefficient:

$$C_D \equiv \frac{D}{q_{\infty}S}$$

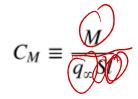
Normal force coefficient:

$$C_N \equiv \frac{N}{q_{\infty}S}$$

Axial force coefficient:

$$C_A \equiv \frac{A}{q_{\infty}S}$$

Moment coefficient:



M: X: M

- The symbols in capital letters (i.e., C_L , C_D , C_A , C_N , C_M) denote the force and moment coefficients for a complete three-dimensional body such as an airplane or a finite wing.
- For a two-dimensional body, the forces and moments are per unit span. The aerodynamic coefficients are denoted by lowercase letters:

$$c_l \equiv \frac{L'}{q_{\infty}c}$$
 $c_d \equiv \frac{D'}{q_{\infty}c}$ $c_m \equiv \frac{M'}{q_{\infty}c^2}$

where the reference area S = c(1) = c.

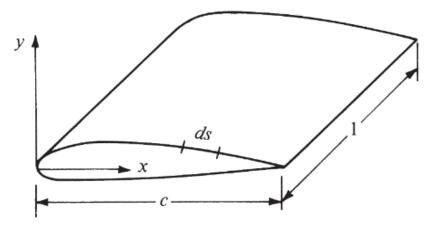
Two additional dimensionless quantities:

$$C_p \equiv \frac{p - p_{\infty}}{q_{\infty}}$$

$$c_f \equiv \frac{\tau}{q_{\infty}}$$



$$dx = ds \cos \theta$$

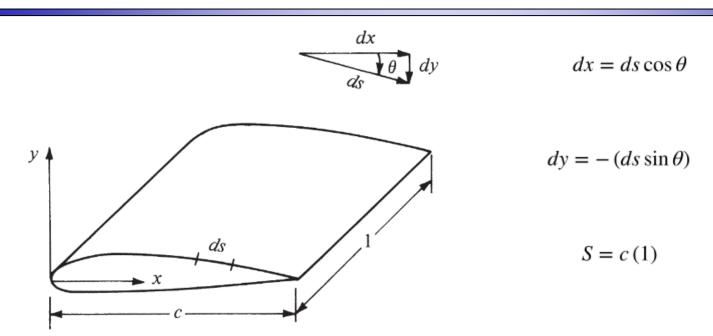


$$dy = -\left(ds\sin\theta\right)$$

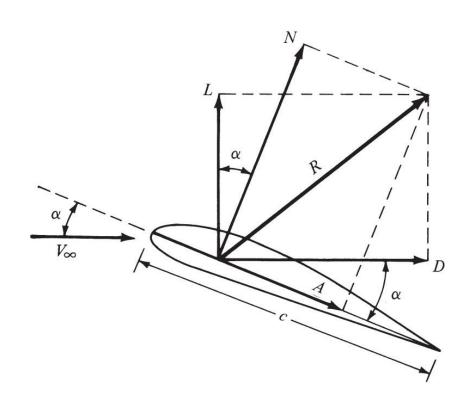
$$S = c(1)$$

$$c_n = \frac{1}{c} \left[\int_0^c \left(C_{p,l} - C_{p,u} \right) dx + \int_0^c \left(c_{f,u} \frac{dy_u}{dx} + c_{f,l} \frac{dy_l}{dx} \right) dx \right]$$

$$c_a = \frac{1}{c} \left[\int_0^c \left(C_{p,u} \frac{dy_u}{dx} - C_{p,l} \frac{dy_l}{dx} \right) dx + \int_0^c \left(c_{f,u} + c_{f,l} \right) dx \right]$$



$$\begin{split} c_{m_{\text{LE}}} &= \ \frac{1}{c^2} \left[\int_0^c \left(C_{p,u} - C_{p,l} \right) \, x \, dx - \int_0^c \left(c_{f,u} \frac{dy_u}{dx} + c_{f,l} \frac{dy_l}{dx} \right) \, x \, dx \right] \\ &+ \int_0^c \left(C_{p,u} \frac{dy_u}{dx} + c_{f,u} \right) \, y_u \, dx + \int_0^c \left(- C_{p,l} \frac{dy_l}{dx} + c_{f,l} \right) \, y_l \, dx \end{split}$$



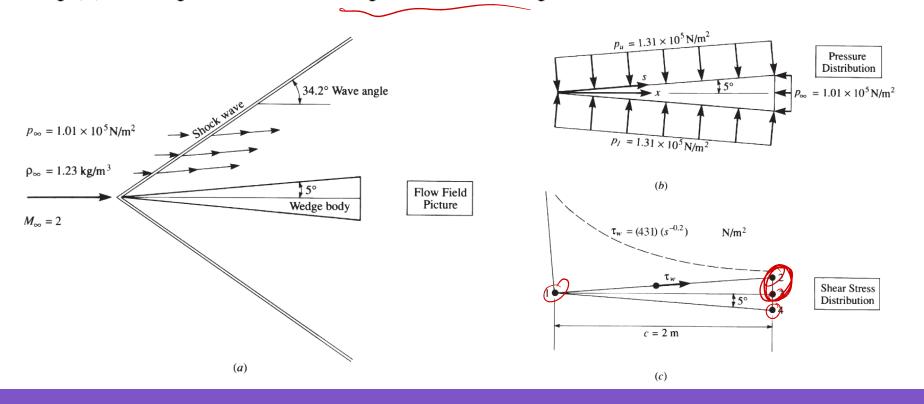
$$L = N\cos\alpha - A\sin\alpha$$

$$D = N \sin \alpha + A \cos \alpha$$

$$c_l = c_n \cos \alpha - c_a \sin \alpha$$

$$c_d = c_n \sin \alpha + c_a \cos \alpha$$

Consider the supersonic flow over a 5° half-angle wedge at zero angle of attack, as sketched in Figure 1.23a. The freestream Mach number ahead of the wedge is 2.0, and the freestream pressure and density are $1.01 \times 10^5 \text{ N/m}^2$ and 1.23 kg/m^3 , respectively (this corresponds to standard sea level conditions). The pressures on the upper and lower surfaces of the wedge are constant with distance s and equal to each other, namely, $p_u = p_l = 1.31 \times 10^5 \text{ N/m}^2$, as shown in Figure 1.23b. The pressure exerted on the base of the wedge is equal to p_∞ . As seen in Figure 1.23c, the shear stress varies over both the upper and lower surfaces as $r_w = 431s^{-0.2}$. The chord length, c, of the wedge is 2 m. Calculate the drag coefficient for the wedge.



$$D' = \int_{LE}^{TE} (-Pu \sin \theta + Tu \cos \theta) ds_{u} + \int_{LE}^{TE} (Pl \sin \theta + Tu \cos \theta) ds_{u}$$

$$\int_{LE}^{TE} (-Pu \sin \theta) ds_{u} = \int_{S_{1}}^{S_{2}} - (l \cdot 3| \times |\delta|) \cdot \sin(-5^{\circ}) ds_{u}$$

$$+ \int_{S_{2}}^{S_{3}} - (l \cdot 0| \times (\delta^{\circ}) \sin(-5^{\circ})) ds_{u}$$

$$= 5260 \text{ N}$$

$$\int_{LE}^{TE} P_{u} \sin \theta ds_{u} = 5260 \text{ N}$$

An alternate solution?

- 1. Calculate the pressure coefficients and skin friction coefficients.
- 2. Then integrate the pressure coefficients and skin friction coefficients to obtain the drag coefficient.

In-Class Quiz