ME 57200 Aerodynamic Design

Lecture #23: Oblique Waves and Expansion Waves

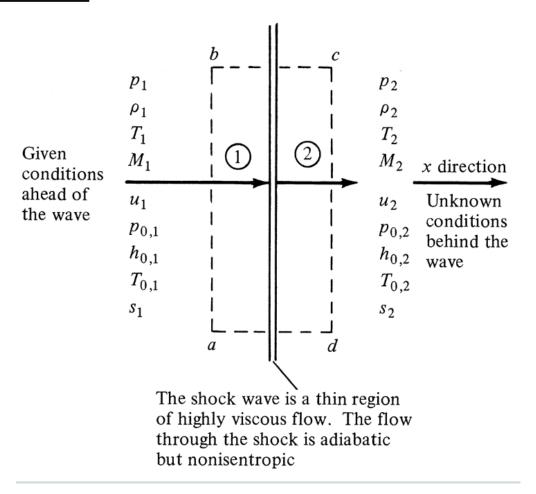
Dr. Yang Liu

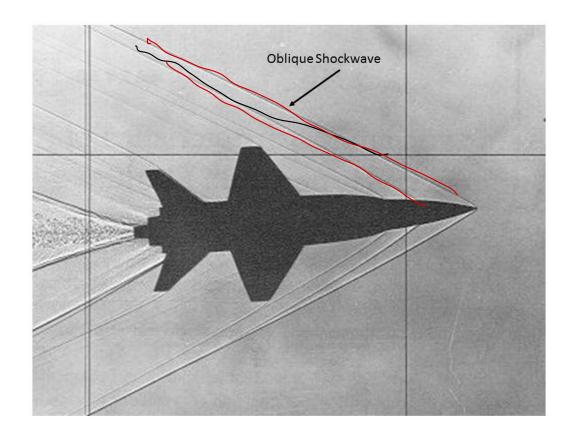
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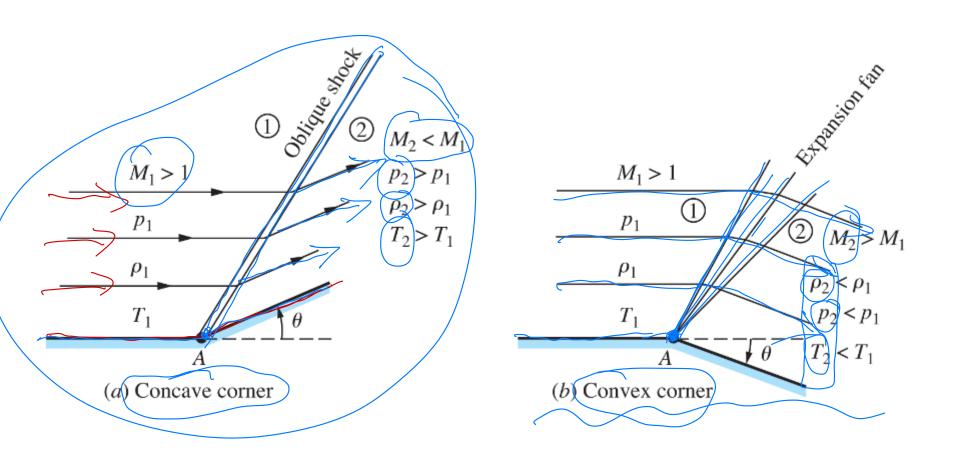
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Normal Shock Waves

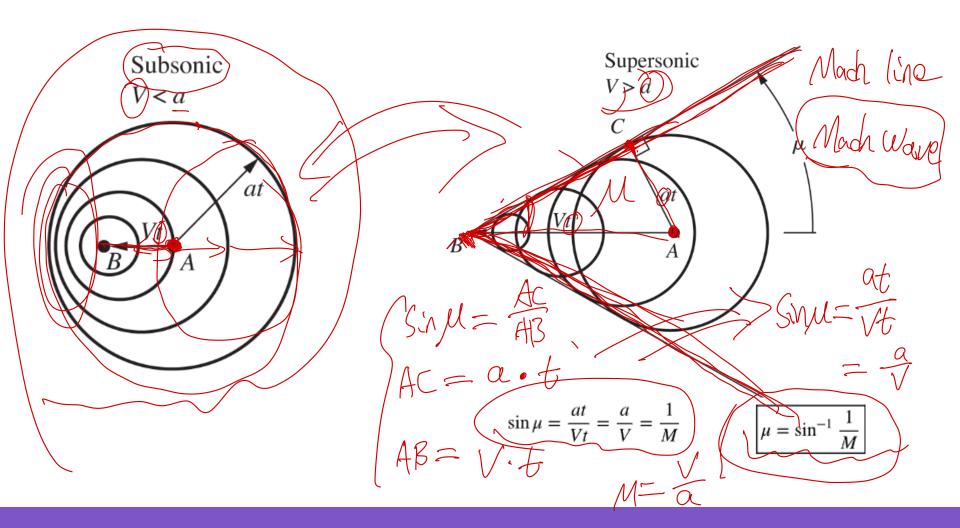


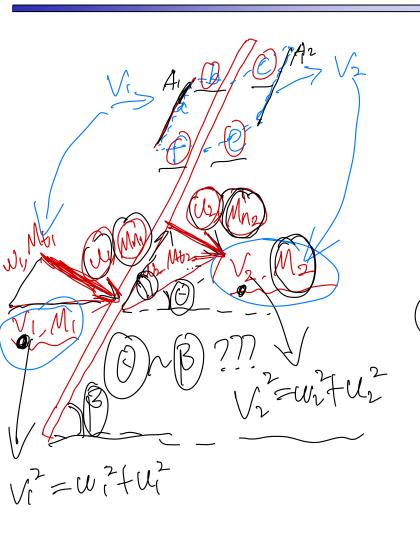


Oblique Shock VS. Expansion Wave



Source of Oblique Waves





Continuity Equation:

$$\oint \int \vec{V} \cdot d\vec{S} = 0$$

$$-\int_{1} u_{1} A_{1} + \int_{2} u_{2} A_{2} = 0$$

$$\Rightarrow \left[P_{1} u_{1} = I_{2} u_{2} \right]$$
Momentum Equation:
$$\oint (P\vec{V} \cdot d\vec{S}) \omega = -\oint (PdS) \text{ Importal.}$$

$$- (P_{1} u_{1} A_{1}) \omega_{1} + (P_{2} u_{2} A_{2}) \cdot \omega_{2} = 0$$

$$\oint (PV \cdot dS) U = - \oint GdS)_{Namm}$$

$$- CP_{1}U_{1}A_{1}) \cdot U_{1} + CP_{2}U_{2}A_{1}) \cdot U_{2} = - (P_{1}A_{2} + P_{2}A_{2})$$

$$\Rightarrow P_{1} + P_{1}U_{1}^{2} = P_{2} + P_{2}U_{2}^{2}$$
Energy Equation:
$$\oint P(C + \sqrt{2}) \cdot V \cdot dS = - \oint PV \cdot dS$$

$$for the flow tangent to faces $V \cdot dS = 0$

$$\Rightarrow -P_{1}(C_{1} + \sqrt{2}) \cdot U_{1}A_{1} + P_{2}(C_{2} + \sqrt{2}) \cdot U_{2}A_{2} = -CP_{1}U_{1}A_{1} + P_{2}U_{1}A_{2}$$

$$\Rightarrow -P_{1}U_{1}(C_{1} + P_{1}) + P_{2}U_{2}(C_{2} + P_{2}) + P_{2}U_{2}(C_{2} + P_{2}) = 0$$

$$\Leftrightarrow -P_{1}U_{1}(C_{1} + P_{1}) + P_{2}U_{2}(C_{2} + P_{2}) = 0$$$$

$$\Rightarrow \int_{1}^{1} u_{1} \left(h_{1} + \frac{v_{1}^{2}}{2}\right) = \int_{2}^{1} u_{2} \left(h_{2} + \frac{v_{2}^{2}}{2}\right)$$

$$\Rightarrow h_{1} + \frac{v_{2}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{1} + \frac{v_{2}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{2} + \frac{v_{2}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{3} + \frac{v_{3}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{4} + \frac{v_{3}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{5} + \frac{v_{4}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{1} + \frac{v_{3}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{2} + \frac{v_{3}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{3} + \frac{v_{4}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{4} + \frac{v_{4}^{2}}{2} = h_{2}$$

$$\Rightarrow h_{5} + \frac{v_{5}^{2}}{2} = h_{5}$$

$$\Rightarrow h_{6} + \frac{v_{6}^{2}}{2} = h_{6}$$

$$\Rightarrow h_{7} + \frac{v_{7}^{2}}{2} = h_{6}$$

$$\Rightarrow h_{8} + \frac{v_{7}^{2}}{2} = h_{6}$$

$$\Rightarrow h_{8} + \frac{v_{7}^{2}}{2} = h_{6}$$

$$\Rightarrow h_{1} + \frac{v_{1}^{2}}{2} = h_{1}$$

$$\Rightarrow h_{1} + \frac{v_{1}^{2}}{2} = h_{2}$$

If The changes across an oblique shock work are governed only by the component of velocity normal to the wave. $= M_1 \cdot Sin B$

#: Mn1 depends on both M, and B

The charges agross an oblique shock were depend

on two parameters — M1, and B.

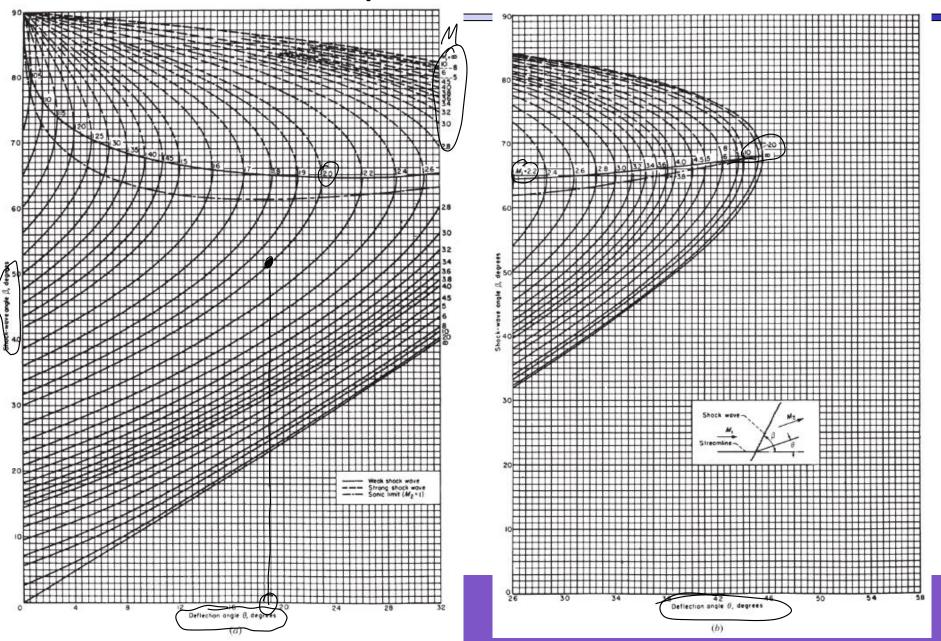
* normal shock is the analitim when
$$\beta = \frac{\pi}{2}$$
 $\frac{\pi}{2}$
 $\frac{\pi}{2}$

$$\frac{\tan (\beta - \beta)}{\tan \beta} = \frac{2 + (\gamma - 1) M_1^2 \sin^2 \beta}{(\gamma + 1) M_1^2 \sin^2 \beta}$$

$$\Rightarrow \frac{\tan \beta}{\tan \beta} = 2 \cdot \cot^2 \beta \frac{M_1^2 \sin^2 \beta}{M_1^2 \cot^2 \beta} - 1$$

$$M_1 \quad \text{and} \quad B$$

$$3 = 90^{\circ} \text{ for novinal shalk}$$



APPENDIX B

Normal Shock Properties

| M | $\frac{p_2}{p_1}$ | $\frac{\rho_2}{\rho_1}$ | $\frac{T_2}{T_I}$ | $\frac{p_{\theta_2}}{p_{\theta_I}}$ | $\frac{p_{\theta_2}}{p_1}$ | M_2 |
|-------------|-------------------|-------------------------|-------------------|-------------------------------------|----------------------------|-------------|
| 0.1000 + 01 | 0.1000 + 01 | 0.1000 + 01 | 0.1000 + 01 | 0.1000 + 01 | 0.1893 + 01 | 0.1000 + 01 |
| 0.1020 + 01 | 0.1047 + 01 | 0.1033 + 01 | 0.1013 + 01 | 0.1000 + 01 | 0.1938 + 01 | 0.9805 + 00 |
| 0.1040 + 01 | 0.1095 + 01 | 0.1067 + 01 | 0.1026 + 01 | 0.9999 + 00 | 0.1984 + 01 | 0.9620 + 00 |
| 0.1060 + 01 | 0.1144 + 01 | 0.1101 + 01 | 0.1039 + 01 | 0.9998 + 00 | 0.2032 + 01 | 0.9444 + 00 |
| 0.1080 + 01 | 0.1194 + 01 | 0.1135 + 01 | 0.1052 + 01 | 0.9994 + 01 | 0.2082 + 01 | 0.9277 + 00 |
| 0.1100 + 01 | 0.1245 + 01 | 0.1169 + 01 | 0.1065 + 01 | 0.9989 + 00 | 0.2133 + 01 | 0.9118 + 00 |
| 0.1120 + 01 | 0.1297 + 01 | 0.1203 + 01 | 0.1078 + 01 | 0.9982 + 00 | 0.2185 + 01 | 0.8966 + 00 |
| 0.1140 + 01 | 0.1350 + 01 | 0.1238 + 01 | 0.1090 + 01 | 0.9973 + 00 | 0.2239 + 01 | 0.8820 + 00 |