

Assignment #1

ELEC 5606

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1

Problem

Require 50MHz first order PLL with a synchronous range of ± 5 kHz. A sinusoidal phase detector with $K_1 = 2$ V/rad and phase error $\Delta\phi = 0.2$ rad.

Find VCO sensitivity, K_3 , and VCO frequency stability, $\frac{\Delta f_0}{f_0}$.

Solution

Solving for K:

synch. range = K

$$2\pi \times 5e3 = K_1 K_3$$

$$K_3 = 5\pi \times 10^3 \text{ rad/s/V} \Rightarrow 2.5 \text{ kHz/V.}$$

Answer: $K_3 = 2.5 \text{ kHz/V}$
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Solving for VCO frequency stability, $\frac{\Delta f_0}{f_0}$.

$$\Delta\phi = 0.2 \text{ rad} = \frac{2\pi\Delta f_0}{K}$$

Solving for f_0 :

$$f_0 = 1 \text{ kHz}$$

$$\frac{\Delta f_0}{f_0} = \frac{1 \text{ kHz}}{50 \text{ MHz}} = 2 \times 10^{-5}$$

Answer: $\frac{\Delta f_0}{f_0} = 2 \times 10^{-5}$
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2

Problem

From Bode Plot of a PLL determine type of PLL, τ_1 , τ_2 and K. Determine loop's ω_n and ζ and phase safety margin.

Solution

Type of loop: Second Order loop \Rightarrow LPF with Phase-Lead Correction

Solving for τ_1 :

$$\text{At } \omega = 1 \text{ rad/sec} \Rightarrow \omega = \frac{1}{\tau_1}$$

$$\tau_1 = 1\text{s}$$

Answer: $\tau_1 = 1\text{s}$

$$\text{Solving for } \tau_2: \text{ At } \omega = 50\text{rad/sec} \Rightarrow \omega = \frac{1}{\tau_2}$$

$$\tau_2 = 0.02\text{s}$$

Answer: $\tau_2 = 0.02\text{s}$
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Solving for K:

$$\text{At } \omega = 1000\text{rad/sec} \Rightarrow \omega = \frac{K\tau_2}{\tau_1}$$

$$K = 50 \times 10^3$$

Answer: $K = 50 \times 10^3$

Solving for ω_n :

$$\omega_n^2 = \frac{K}{\tau_1}$$

$$\omega_n = 223.6 \text{ rad/s}$$

Answer: $\omega_n = 223.6\text{rad/s}$

Solving for ζ :

$$2\zeta\omega_n = \frac{1+K\tau_2}{\tau_1}$$

$$\zeta = 2.24$$

Answer: $\zeta = 2.24$

Solving for phase safety margin:

$$\angle L(j\omega) = -90^\circ - \arctan(\omega\tau_1) + \arctan(\omega\tau_2)$$

Let ω be at the 0dB cross point: $\omega = 1000$ rad/s

$$\angle L(j\omega) = -90^\circ - 89.94 + 87.19 = -92.8^\circ$$

$$\text{Phase Margin} = 180 - 92.8 = 87.2^\circ \Rightarrow 1.52 \text{ rad.}$$

Answer: $\text{Phase Margin} = 87.2^\circ$

Confirmed using MATLAB below in Figure 1

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Problem

the open loop TF of a PLL utilizing a LPF with phase lead correcciton is given by:

$$G(j\omega) = \frac{K(1+j\omega\tau_2)}{j\omega(1+j\omega\tau_1)}$$

Using Root Locus method plot LHS of real part of denominator of the Closed Loop TF when it is forced to be equal to $0 + 0j$ versus σ and explain why the loop is uncondotionally stable.

Solution

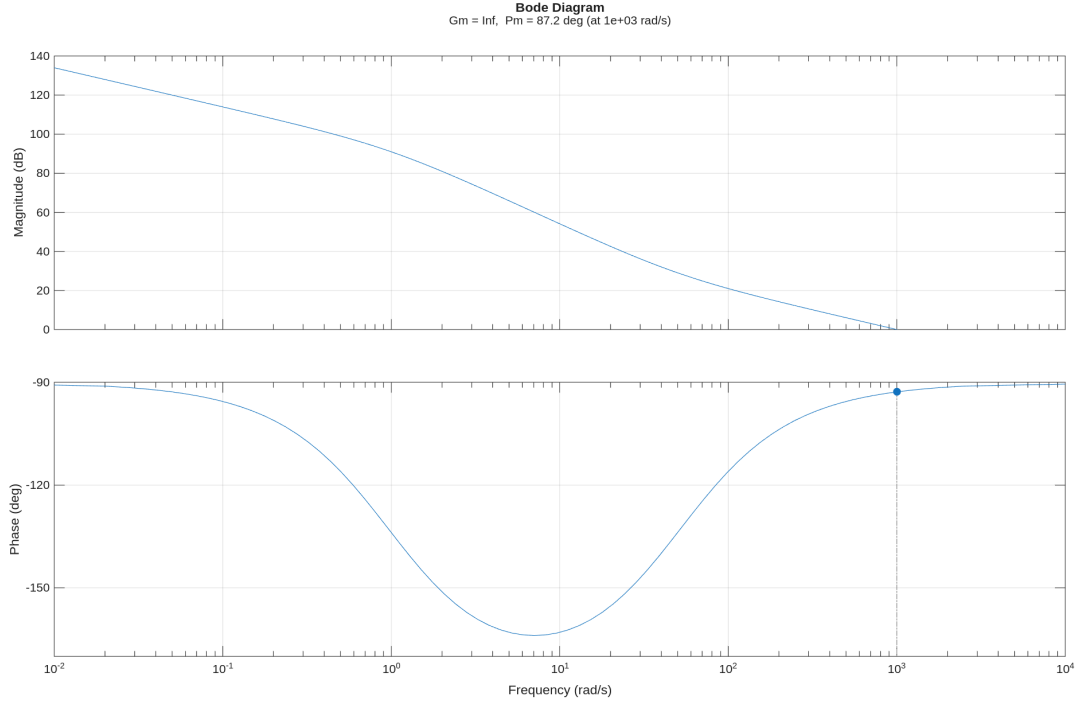


Figure 1: Bode Plot of PLL from computed values

$$G(s) = \frac{K(1+s\tau_2)}{s(1+s\tau_1)} \Rightarrow H(s) = \frac{G(s)}{1+G(s)}$$

The denominator of $H(s)$ is therefore:

$$D(s) = \tau_1 s^2 + (1 + K\tau_2)s + K$$

let $s = \sigma + j\omega$

Real:

$$\tau_1(\sigma^2 - \omega^2) + \sigma(1 + K\tau_2) + K = 0$$

Imaginary:

$$2\tau_1\sigma\omega + \omega(1 + K\tau_2) = 0j$$

We must isolate K and for nontrivial roots we therefore obtain the following for the Imaginary part:

$$2\tau_1\sigma + 1 + K\tau_2 = 0$$

and therefore:

$$K = \frac{-2\tau_1\sigma-1}{\tau_2}$$

Subbing this back into the Real part:

$$\tau_1(\sigma^2 - \omega^2) + \sigma(1 + \frac{-2\tau_1\sigma-1}{\tau_2}\tau_2) + \frac{-2\tau_1\sigma-1}{\tau_2}\tau_2 = 0$$

$$\tau_1\sigma^2 - \tau_1\omega^2 + \sigma(-2\tau_1\sigma) + \frac{-2\tau_1\sigma-1}{\tau_2} = 0$$

$$\omega^2 = \sigma^2 + \frac{\sigma(-2\tau_1\sigma)}{\tau_1} + \frac{-2\tau_1\sigma-1}{\tau_1\tau_2}$$

$$\omega^2 = -\sigma^2 + \frac{-2\tau_1\sigma-1}{\tau_1\tau_2} \quad (1)$$

Setting $\tau_1 = 1$ and $\tau_2 = 0.02$, the above is plotted in MATLAB as seen in Figure 2.

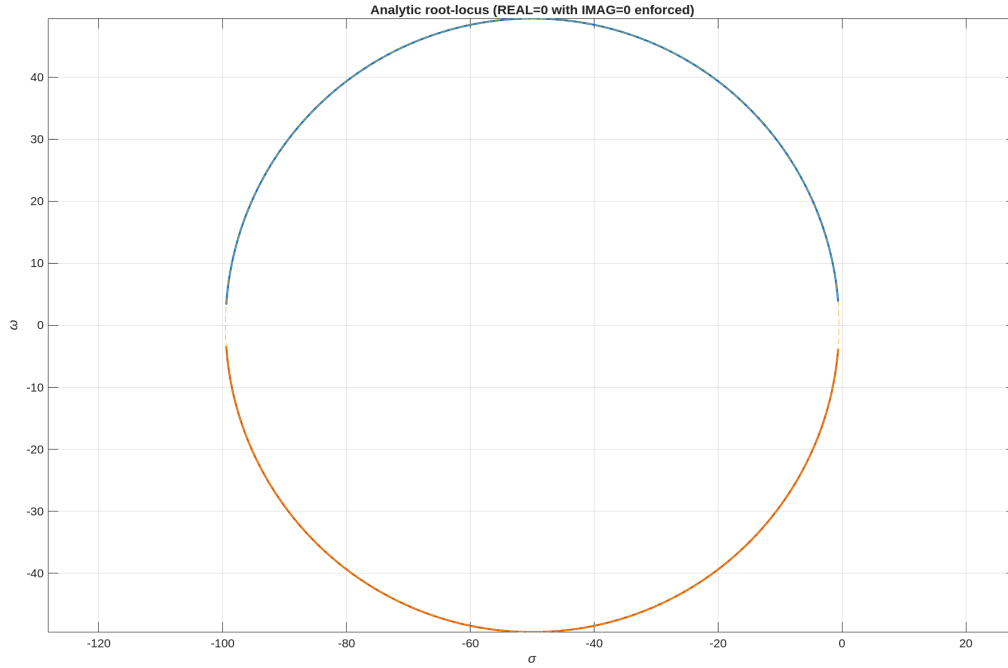


Figure 2: LHS of real part of D(s) plotted vs σ

From Figure 2 and from equation 1 for any $K > 0$ (with $\tau_1 > 0$, $\tau_2 > 0$ and $\tau_1 \geq \tau_2$), we see that the loop is unconditionally stable.

The entire circle lies strictly in the left half-plane, never crossing the imaginary axis.

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Problem

When excited by a frequency step, $\Delta\omega$, of 200 rad/sec, the phase response for a second order loop incorporating a LPF with phase lead correction with damping constant of 1 is shown in the diagram.

Determine loop gain, K , and natural frequency, ω_n .

Solution

From the phase response: Steady state error, $SSE = 0.1$ rad

Solving for K :

$$K = \frac{\Delta\omega}{SSE} = 2000$$

Answer: $K = 2000$

Solving for ω_n : From Blanchard P.93, eqn. 5.10:

$$\phi(t) = \frac{\Delta\omega}{K} + \frac{\Delta\omega}{\omega_n} e^{-\omega_n t} \left(\omega_n t - \frac{\omega_n^2}{K} t - \frac{\omega_n}{K} \right)$$

This becomes:

$$\phi(t) = \frac{\Delta\omega}{K} + \Delta\omega e^{-\omega_n t} \left(t - \frac{\omega_n}{K} t - \frac{1}{K} \right)$$

Differentiating $\phi(t)$ for $\dot{\phi}(t)$:

$$\dot{\phi}(t) = \Delta\omega e^{-\omega_n t} \left(1 - \omega_n t \left(1 - \frac{\omega_n}{K} \right) \right)$$

Setting the above to 0 and solving for ω_n when $\Delta\omega = 200$, $t = 8\text{ms}$ and $K = 2000$:

$$\omega_n = 133.97 \text{ rad/s}$$

Answer: $\omega_n = 133.97 \text{ rad/s}$
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The above are confirmed with MATLAB in Figure 3

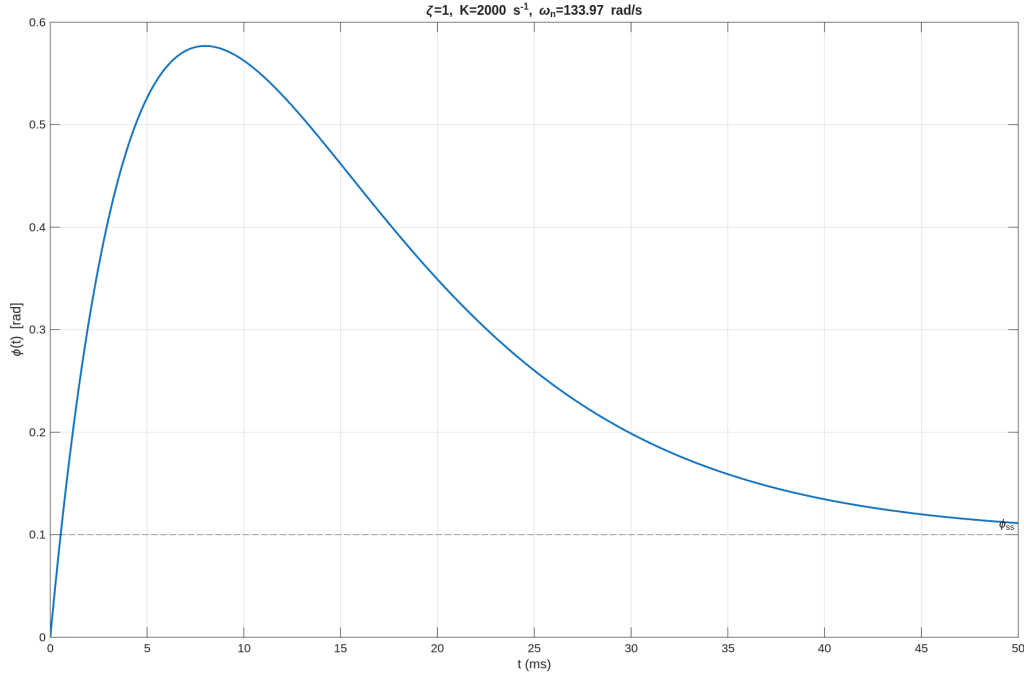


Figure 3: Phase Response of Loop with $K = 2000$ and $\omega_n = 133.97 \text{ rad/s}$

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Problem

Second order loop with integrator and phase lead correction. Input signal is a 4MHz frequency modulated signal with a frequency deviation of 500 Hz. Maximum phases error, $\Delta\phi$, is 0.35 rad and occurs at modulating frequency $\Omega = 1\text{kHz}$.

Determine ζ , ω_n and for what frequency deviation does the maximum phase serror remain below 0.2 rad?

Solution

We know the maximum occurs at ω_n , therefore:

$$\omega_n = 2\pi(1\text{kHz}) = 6283 \text{ rad/s}$$

Solving for ζ :

$$\Delta\phi_M = \frac{\Delta\omega_i}{s\zeta\omega_n}$$

$$0.35 = \frac{s\pi \times 500}{2\zeta(6283)} \Rightarrow \zeta = 0.714$$

Answer: $\zeta = 0.714$

Now for what $\Delta\omega_i$ does $\Delta\phi$ remain below 0.2 rad:

$$\Delta\omega_i = 2\Delta\phi_M\zeta\omega_n = 1794 \text{ rad/ or } 286 \text{ Hz.}$$

Answer: $\Delta\omega_i = 286 \text{ Hz}$
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