

**National University of Singapore**  
**Department of Electrical & Computer Engineering**  
**EE-4502: Electric Drives and Control**  
**Tutorial - 4 (Induction Motor Drives - Solution)**  
**Year 2022-23**

1. The synchronous speed is given by

$$N_s = \frac{120 \times 50}{4} = 1500 \text{ rpm}$$

The input power is given by

$$P_{in} = \sqrt{3} V_L I_L \cos \phi = \sqrt{3} \times 480 \text{ V} \times 60 \text{ A} \times 0.85 = 42.4 \text{ kW}$$

The air-gap power is given by

$$P_{ag} = P_{in} - P_{SCL} - P_{core} = 42.4 \text{ kW} - 2 \text{ kW} - 1.8 \text{ kW} = 38.6 \text{ kW}$$

The slip is given by

$$P_{RCL} = s \times P_{ag} \Rightarrow s = \frac{700 \text{ W}}{38.6 \text{ kW}} = 0.018$$

The rotor speed is given by

$$N_m = (1 - s) \times N_s = (1 - 0.018) \times 1500 \text{ rpm} = 1473 \text{ rpm}$$

The rotor frequency,  $f_r$  is given by

$$f_r = s \times f_s = 0.018 \times 50 \text{ Hz} = 0.9 \text{ Hz}$$

The converted output power is given by

$$P_{conv.} = P_{ag} - P_{RCL} = 38.6 \text{ kW} - 0.7 \text{ kW} = 37.9 \text{ kW}$$

The shaft output power is given by

$$P_{out} = P_{conv.} - P_{F\&W} = 37.9 \text{ kW} - 0.6 \text{ kW} = 37.3 \text{ kW}$$

The shaft torque at rated load is given by

$$T_e = \frac{P_{out}}{\omega_m} = \frac{37.3 \text{ kW}}{\frac{2\pi}{60} \times 1473 \text{ rpm}} = 241.8 \text{ N.m}$$

The efficiency is given by

$$\eta = \frac{P_{out}}{P_{in}} = \frac{37.3 \text{ kW}}{42.4 \text{ kW}} = 88\%$$

2. The parameters given for the IM are:

$$400 \text{ V}, 3\text{-phase}, f = 50 \text{ Hz}, N_{r(\text{rated})} = 1370 \text{ rpm}, \Delta\text{-connected}$$

$$R_s = 2.0 \text{ } \Omega, R_{r'} = 5.0 \text{ } \Omega, X_s = 5.0 \text{ } \Omega, X_{r'} = 5.0 \text{ } \Omega, X_m = 80 \text{ } \Omega,$$

The rated-slip is:

$$s_{\text{rated}} = \frac{1500 \text{ rpm} - 1370 \text{ rpm}}{1500 \text{ rpm}} = 0.0867$$

The rated rotor current referred to the stator side is:

$$I_{r'} = \frac{400 \text{ V}}{\sqrt{\left(2 + \frac{5}{0.0867}\right)^2 + (5 + 5)^2}} = 6.61 \text{ A}$$

The rated torque is given by

$$T_{\text{rated}} = \frac{3}{\frac{2\pi}{60} \times 1500} \times (6.61)^2 \times \frac{5}{0.0867} = 48.14 \text{ N.m}$$

It is given that load-torque varies in a square manner with the speed. Thus, we have

$$T_l = k\omega_m^2 = k \times [\omega_{ms}(1 - s)]^2 = k'(1 - s)^2$$

At rated and steady-state condition, we have

$$T_{e(\text{rated})} = T_l = 48.14 \text{ N.m} = k'(1 - 0.0867)^2 \Rightarrow k' = 57.7 \Rightarrow T_l = 57.7(1 - s)^2$$

The parameter given is  $N_r = 1200 \text{ rpm}$ .

At this speed the slip is

$$s = \frac{1500 \text{ rpm} - 1200 \text{ rpm}}{1500 \text{ rpm}} = 0.2$$

$$T_l = 57.7(1 - 0.2)^2 = 36.9 \text{ N.m}$$

At 1200 rpm with the load torque of 36.9 N.m, we have

$$T_{l@1200\text{rpm}} = 36.9 \text{ N.m} = \frac{3}{\frac{2\pi}{60} \times 1500} \times \left( \frac{V_{ph}^2}{\left(2 + \frac{5}{0.2}\right)^2 + (5 + 5)^2} \right)^2 \times \frac{5}{0.2} \Rightarrow V_{ph} = 253.2 \text{ V}$$

$$I_{r'} = \frac{253.2 \text{ V}}{\left(2 + \frac{5}{0.2}\right) + j(5 + 5)} = 8.246 - j3.054$$

$$I_m = \frac{V_{ph}}{jX_m} = \frac{253.2}{j80} = -j3.165 \text{ A}$$

$$I_s = I_{r'} + I_m = 8.246 - j6.219 = 10.328 \angle -37^\circ$$

Line current is

$$I_{sL-L} = \sqrt{3} \times 10.33 = 17.9 \text{ A}$$

3. The parameters given for the IM are:

$$440 \text{ V}, f = 60 \text{ Hz}, P = 4, N_{r(\text{rated})} = 1746 \text{ rpm}, T_{\text{rated}} = 40 \text{ N.m}$$

The synchronous speed is:

$$N_s = \frac{120 \times 60}{4} = 1800 \text{ rpm}$$

The slip-speed at rated load is:

$$N_{sl(\text{rated})} = 1800 - 1746 = 54 \text{ rpm}$$

(a) The torque-speed characteristics at different frequencies are shown in Fig. 1.

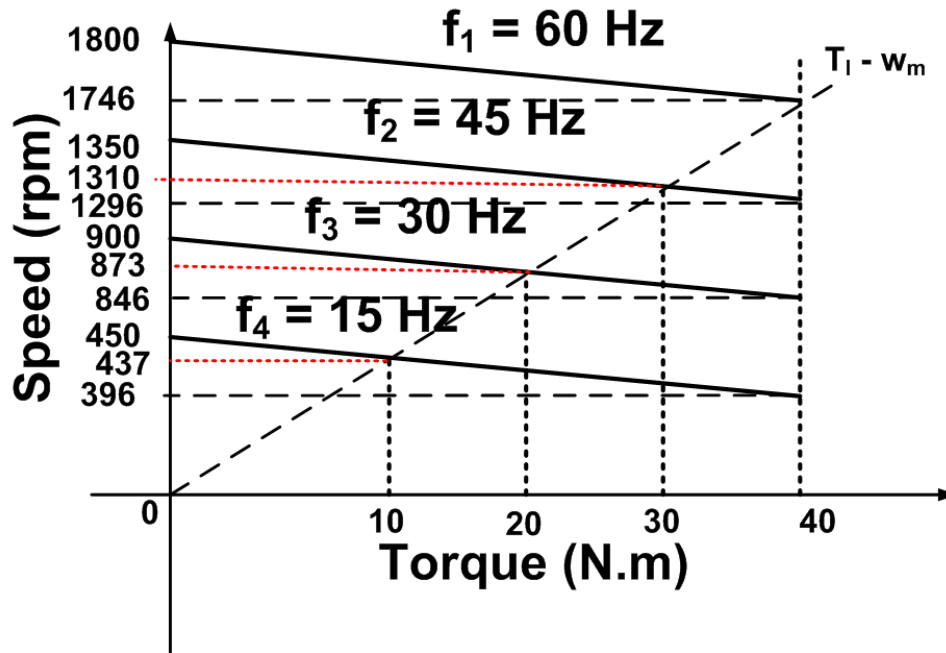


Figure 1:

(b) The load-torque is proportional to speed and is given by:

$$T_l = k \times \omega_m \Rightarrow 40 \text{ N.m} = k \times 1746 \Rightarrow k = 0.0229 \text{ N.m/rpm}$$

The electromagnetic torque is given by:

$$N_r = m \times T_e + N_s \Rightarrow$$

At rated condition we have

$$1746 \text{ rpm} = m \times 40 \text{ N.m} + 1800 \text{ rpm} \Rightarrow m = -1.35$$

Thus,

$$T_e = \frac{N_s - N_r}{1.35}$$

At steady-state we have

$$T_e = T_l \Rightarrow \frac{N_s - N_r}{1.35} = 0.0229 \times N_r \Rightarrow N_r = \frac{N_s}{1.0309}$$

For

$$f = 60 \text{ Hz}, N_s = 1800 \text{ rpm} \Rightarrow N_r = \frac{1800}{1.0309} = 1746 \text{ rpm}$$

$$\Rightarrow T_l = 0.0229 \times 1746 = 40 \text{ N.m}$$

$$f = 45 \text{ Hz}, N_s = 1350 \text{ rpm} \Rightarrow N_r = \frac{1350}{1.0309} = 1309.5 \text{ rpm}$$

$$\Rightarrow T_l = 0.0229 \times 1309.5 = 30 \text{ N.m}$$

$$f = 30 \text{ Hz}, N_s = 900 \text{ rpm} \Rightarrow N_r = \frac{900}{1.0309} = 873 \text{ rpm}$$

$$\Rightarrow T_l = 0.0229 \times 873 = 20 \text{ N.m}$$

$$f = 15 \text{ Hz}, N_s = 450 \text{ rpm} \Rightarrow N_r = \frac{450}{1.0309} = 436.5 \text{ rpm}$$

$$\Rightarrow T_l = 0.0229 \times 436.5 = 10 \text{ N.m}$$

4. The parameters given for the IM are:

$$400 \text{ V}, 3 - \text{phase}, f = 50 \text{ Hz}, N_{r(\text{rated})} = 925 \text{ rpm}, \Delta - \text{connected}$$

$$R_s = 0.2 \text{ } \Omega, R_{r'} = 0.3 \text{ } \Omega, X_s = 0.5 \text{ } \Omega, X_{r'} = 1.0 \text{ } \Omega,$$

(a)

$$T_{max} = \frac{3}{2a\omega_{ms}} \times \frac{v_{ph}^2}{R_s + \sqrt{R_s^2 + a^2 (X_s + X_{r'})^2}}$$

At rated frequency we have,  $f = 50 \text{ Hz}$ ,  $a = 1$ .

$$T_{max(a=1)} = \frac{3}{2 \times 1 \times \frac{2\pi}{60} 1000} \times \frac{400^2}{0.2 + \sqrt{0.2^2 + 1^2 (0.5 + 1.0)^2}} = 1337.7 \text{ N.m}$$

At frequency ,  $f = 100 \text{ Hz}$ , we have  $a = 2$ .

$$T_{max(a=2)} = \frac{3}{2 \times 2 \times \frac{2\pi}{60} 1000} \times \frac{400^2}{0.2 + \sqrt{0.2^2 + 2^2 (0.5 + 1.0)^2}} = 357.35 \text{ N.m}$$

The ratio of maximum torques is:

$$\frac{T_{max(a=2)}}{T_{max(a=1)}} = \frac{357.35}{1337.7} = 0.267$$

(b)

$$I_{r'(rated)} = \frac{400 \text{ V}}{\sqrt{\left(0.2 + \frac{0.3}{0.075}\right)^2 + (0.5 + 1.0)^2}} = 89.7 \text{ A}$$

$$T_{rated} = \frac{3}{\frac{2\pi}{60} \times 1000} \times (89.7)^2 \times \frac{0.3}{0.075} = 921.8 \text{ N.m}$$

$$I_{r'} = 89.7 \text{ A} = \frac{400 \text{ V}}{\sqrt{\left(0.2 + \frac{0.3}{s}\right)^2 + \left(\frac{75}{50}(0.5 + 1.0)\right)^2}} \Rightarrow s = 0.082$$

$$T_{(a=1.5)} = \frac{3}{(1.5) \times \frac{2\pi}{60} \times 1000} \times (89.7)^2 \times \frac{0.3}{0.082} = 560.9 \text{ N.m}$$

The ratio of maximum torques is:

$$\frac{T_{max(a=2)}}{T_{max(a=1)}} = \frac{560.9}{921.8} = 0.608$$

(c)

$$f = 30 \text{ Hz}, a = \frac{30}{50} = 0.6, s = \frac{60}{\frac{120 \times 30}{6}} = 0.1$$

$$T_e = \frac{3}{(0.6) \times \frac{2\pi}{60} \times 1000} \times \frac{(0.6 \times 400 \text{ V})^2}{\left(0.2 + \frac{0.3}{0.1}\right)^2 + ((0.6) \times (0.5 + 1.0))^2} \times \frac{0.3}{0.1}$$

$$= 746.66 \text{ N.m}$$

5. The parameters given for the IM are:

$$440 \text{ V}, 3 - \text{phase}, f = 50 \text{ Hz}, N_{r(rated)} = 925 \text{ rpm}, \Delta - \text{connected}$$

(a) For  $f = 30 \text{ Hz}$  and  $T_m = \frac{1}{4}T_{fl}$ , we have

$$N_r = \frac{120 \times 30}{6} - \frac{75}{4} = 581.25 \text{ rpm}$$

(b) For  $N_r = 500 \text{ rpm}$  and  $T_m = 0.6 \times T_{fl}$ , we have

$$N_s = 500 + 0.6 \times 75 = 545 \text{ rpm} \Rightarrow f_s = 27.25 \text{ Hz}$$

$$I_{r'} = \frac{\frac{27.25}{50} \times 440 \text{ V}}{\sqrt{\left(0.2 + \frac{0.3}{0.082}\right)^2 + \frac{27.25}{50}(1 + 0.5)^2}} = 61.24 \text{ A}$$

(c) For  $N_r = 750 \text{ rpm}$  and  $f_s = 40 \text{ Hz}$ , we have

$$f_s = 40 \text{ Hz} \Rightarrow N_s = 800 \text{ rpm} \Rightarrow N_{sl} = 800 - 750 = 50 \text{ rpm} \Rightarrow T_m = \frac{50}{75} \times T_{fl}$$

$$I_r' = \frac{440 \text{ V}}{\sqrt{\left(0.2 + \frac{0.3}{0.075}\right)^2 + (0.5 + 1.0)^2}} = 98.7 \text{ A} \Rightarrow T_{fl} = 1116.31 \text{ N.m} \Rightarrow \frac{50}{75} \times T_{fl} = 744.2 \text{ N.m}$$

6. The parameters given for the IM are:

$$440 \text{ V}, 3 - \text{phase}, f = 50 \text{ Hz}, P = 4, N_{r(\text{rated})} = 1370 \text{ rpm}, Y - \text{connected}$$

$$R_s = 1.9 \text{ } \Omega, R_{r'} = 2.0 \text{ } \Omega, X_s = 3.0 \text{ } \Omega, X_{r'} = 3.0 \text{ } \Omega$$

$$v_1 = \frac{400}{\sqrt{3}} = 254 \text{ V}, v_5 = 100 \text{ V}, v_7 = 40 \text{ V},$$

The rated slip is

$$s_{\text{rated}} = \frac{1500 \text{ rpm} - 1370 \text{ rpm}}{1500 \text{ rpm}} = 0.087$$

The rated rotor current referred to the stator side is:

$$I_{r'} = \frac{254 \text{ V}}{\sqrt{\left(1.9 + \frac{2}{0.087}\right)^2 + (3 + 3)^2}} = 9.9 \text{ A}$$

The rated torque is given by

$$T_{\text{rated}} = \frac{3}{\frac{2\pi}{60} \times 1500} \times (9.9)^2 \times \frac{2}{0.087} = 43.1 \text{ N.m}$$

The 5th harmonic current is given by

$$I_{s5} = \frac{v_5}{5(X_s + X_{r'})} = \frac{100 \text{ V}}{5(3 + 3)} = 3.33 \text{ A}$$

The 7th harmonic current is given by

$$I_{s7} = \frac{v_7}{7(X_s + X_{r'})} = \frac{40 \text{ V}}{7(3 + 3)} = 0.95 \text{ A}$$

The rms stator current is given by

$$I_{s(\text{rms})} = \sqrt{I_1^2 + I_5^2 + I_7^2} = \sqrt{9.9^2 + 3.33^2 + 0.95^2} = 10.5 \text{ A}$$

The output power is given by

$$P_{\text{out}} = T_e \times \omega_m = 43.1 \text{ N.m} \times \left(\frac{2\pi}{60} \times 1370 \text{ rpm}\right) = 6182 \text{ W}$$

The copper losses are given by

$$\begin{aligned} P_{cu, \text{loss}} &= 3 \left[ (9.9)^2 \times (1.9 + 2) + (3.33)^2 \times (1.9 + 2) + (0.95)^2 \times (1.9 + 2) \right] \\ &= 1284.7 \text{ W} \end{aligned}$$

The efficiency(neglecting iron loss) is given by

$$\eta = \frac{6182}{6182 + 1284.7} = 82.8\%$$

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