

EC 1310- Control System

ROOT LOCUS PLOT

Mini project
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Root Locus

In control systems theory, root locus analysis is a graphical method for examining how the roots of a system change with variation of a certain system parameter, commonly a gain within a feedback system. This is a technique used as a stability criterion in the field of classical control theory developed by Walter R. Evans which can determine stability of the system. The root locus plots the poles of the closed loop transfer function in the complex s-plane as a function of a gain parameter

Root Locus Plot

This is also known as root locus technique in control system and is used for determining the stability of the given system. Now in order to determine the stability of the system using the root locus technique we find the range of values of K for which the complete performance of the system will be satisfactory and the operation is stable.

Now there are some results that one should remember in order to plot the root locus. These results are written below:

- 1. Region where root locus exists: After plotting all the poles and zeros on the plane, we can easily find out the region of existence of the root locus by using one simple rule which is written below,
 - Only that segment will be considered in making root locus if the total number of poles and zeros at the right hand side of the segment is odd.
- 2. How to calculate the number of separate root loci? : A number of separate root loci are equal to the total number of roots if number of roots are greater than the number of poles otherwise number of separate root loci is equal to the total number of poles if number of roots are greater than the number of zeros.

RULES FOR CONSTRUCTION OF ROOT LOCUS

Following are the rules to sketch the root locus plot

RULE 1. The root locus is symmetrical about the real axis

RULE 2. The root locii starts from an open loop pole with K=0

e.g. For the system having

$$G(s)H(s) = \frac{K(s+5)}{s+7}$$

the starting point of the root loci will be s = -7

RULE 3. The root loci will terminate either on an open loop zeros or on infinity with $K = \infty$

e.g. For the system having

$$G(s)H(s) = \frac{K(s+1)}{s+2}$$

The root loci will terminate at s = -1

RULE 4. If N = No. of separate loci

P = No. of finite poles

Z = No. of finite zeros then

number of root loci will be equal to the no. of poles if number of poles are more than number of zeros i.e. P > Z

$$N = P \text{ if } P > Z$$

If Z > P, then number of root loci will be equal to the number of zeros

If P = Z then No. of root locii = Poles = Zeros

e.g. For the system having

$$G(s)H(s) = \frac{K(s+3)}{s+2}$$

Since P = 1, Z = 1 therefore N = 1

RULE 5. ROOT LOCII ON THE REAL AXIS

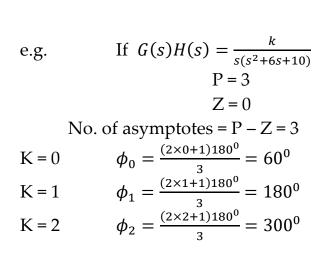
Any point on the real axis is a part of the root locus if and only if the number of poles and zeros to its right is odd.

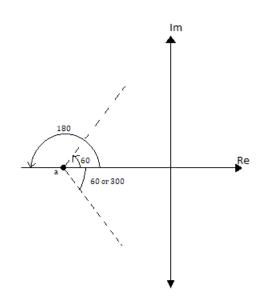
RULE 6. ASYMPTOTES

The branches of root locus tend to infinity along a set of straight line called asymptotes. These asymptotes making an angle with real axis and is given by

$$\phi = \frac{(2k+1)180^0}{P-Z}$$
 where K = 0,1,2,

The total number of asymptotes = P - Z





RULE 7. CENTROID OF ASYMPTOTES

The point of intersection of asymptotes with real axis is called centroid of asymptotes (σ_A) and is given by

$$\sigma_A = \frac{sum\ of\ poles - sum\ of\ zeros}{P-Z \atop P-Z \atop S(s^2+6s+10)}$$
 e.g. If $G(s)H(s) = \frac{k}{s(s^2+6s+10)}$ There are three poles at $s_1 = 0, s_2 = -3+j1, S_3 = -3-j1$ No. of zeros = 0 therefore
$$centroid \qquad \sigma_A = \frac{0-3+j1-3-j1-0}{3} = -2$$

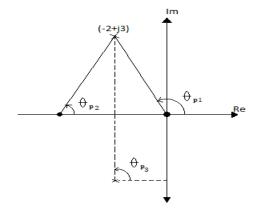
RULE 8. ANGLE OF DEPARTURE & ANGLE OF ARRIVAL OF THE ROOT LOCII

The angle of departure of the root locus from a complex pole is given by

 $\phi_d=180^{\circ}$ - sum of angles of vectors drawn to this pole from other poles + sum of angles of vectors drawn to this pole from zeros

The angle of arrival at a complex zero is given by $\phi_a = 180^0 - sum \ of \ angles \ of \ vectors \ drawn \ to \ this \ zero \ from \ other \ zeros + sum \ of \ angles \ of \ vectors \ drawn \ to \ this \ zero \ from \ poles.$ e.g. For

$$G(s)H(s) = \frac{k}{s(s+6)(s^2+4s+13)}$$



the angle of departure from complex poles.

$$\phi_d = 180^{\circ} - (\theta_{P_1} + \theta_{P_2} + \theta_{P_3}) = -70^{\circ}$$

= $180^{\circ} - (123^{\circ} + 37^{\circ} + 90^{\circ}) = -70^{\circ}$
Therefore, angle of departure at $(-2 + j3) = 70^{\circ}$
angle of departure at $(-2 - j3) = 70^{\circ}$

RULE 9. BREAKAWAY POINT ON REAL AXIS

If the root locus lies between two adjacent open loop poles on the real axis then there will be at least one breakaway point, because the roots move towards each other as K is increased and meet at a point. At this point K is maximum. If we increase the value of K between two poles the root locus breaks in two parts.

Similarly, if root locus lies between two adjacent zeros on real axis then there will be at least one break in point. If the root locus lies between an open loop pole and zero, then there will be no breakaway point or breaking point or may be both occur. The breakaway or break in points can be determined from the roots

of
$$\frac{dK}{ds} = 0$$

e.g. If
$$G(s)H(s) = \frac{k}{s(s^2+6s+10)}$$

then breakaway point can be calculated as

$$1 + G(s)H(s) = 1 + \frac{k}{s(s^2 + 6s + 10)}$$

$$s(s^2 + 6s + 10) + k = 0$$
or, $K = -s^3 - 6s^2 - 10s$

$$\frac{dK}{ds} = -3s^2 - 12s - 10 = 0$$
or, $3s^2 + 12s + 10 = 0$

 $s_1 = -1.1835 \& s_2 = -2.815$ are the breakaway points

RULE 10. The intersection of root locus branches with $j\omega$ -axis can be determined through Routh-Hurwitz criterion

e.g. If $G(s)H(s) = \frac{k}{s(s^2+6s+10)}$ so, intersection of the root locii with the imaginary axis can be found as

The characteristic equation is $s^3 + 6s^2 + 10s + K = 0$

$$s^{3}$$
 1 10
 s^{2} 6 K
 s^{1} $\frac{60-K}{6}$
 s^{0} K

Hence, we get a zero row if K = 60

The auxiliary equation $A(s) = 6s^2 + K$

$$6s^2 + K = 0$$
$$6s^2 + 60 = 0$$

$$s = \pm j3.16$$

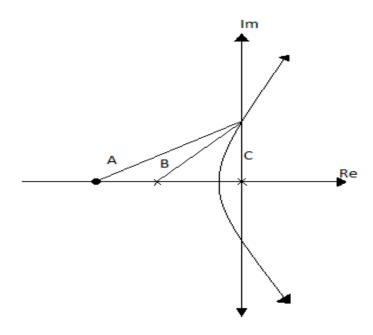
The root locus branches cross the imaginary axis at $s = \pm j3.16$ for K = 60

DETERMINATION OF K ON ROOT LOCII

The value of K can be determined by

 $K = \frac{\textit{Product of all vector lengths drawn from the poles of G(s)H(s) to the point}}{\textit{Product of all vector lengths drawn from the zeros of G(s)H(s) to the point}}$

e.g. in the figure



the value of K at the point of intersection of root locus branch with imaginary axis is

$$K = \frac{B.C}{A}$$

PART B

For a unity feedback system the open loop transfer function is given by

$$G(s) = \frac{k}{s(s+2)(s^2+6s+25)}$$

- (a) Sketch the root locus for $0 \le K \le \infty$
- (b) At what value of 'K' the system becomes unstable
- (c) At this point of instability determine the frequency of oscillation of the system

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|--|
| given Cr(s) = K |
| 2(2+2)+2+25) |
| H(U) = 1 |
| - Treat Jacoul - 14/03 To with a fee |
| G(S)H(S) = K |
| 5(5+2)(5+3-34)(5+3+34) |
| 6 (0. 2-3+14 - 3-14) - 6 |
| |
| Poles - J. = D |
| S. = -2 ., P = 4 |
| 5, = -3+14 |
| Sy = +3-j4 |
| Zenos - O Z= O |
| 5-9 |
| The segment on the real axus between |
| S=0 & S=-2 is the part of root locus |
| I - M real DEL LIVIN F 1879 |
| Since P>2 No of root locii N=P=4 |
| No of yout local |
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| (entroècle of the adjustates 6a = Jum of poles - Symot Zenos P - Z 6a = (0 - 2 - 3 + j 4 - 3 - j 4) - 0 4 - 0 4 - 0 4ngle of asymptotes P - Z 4ngle of asymptotes P - Z 4ngle of asymptotes P - Z 4x0 + 1 x180 = 45° (for K = 0) 4 - (2x0 + 1)x180 = 135° (for K = 1) 4 - (2x2 + 1)x180 = 225° (for K = 2) 4 - (2x3 + 1)x180 = 315° (for K = 3) 4 | | | |
|--|-------|--|---|
| (entroid of the asymptotes 6a = Jum of poles - Symot Zenos P - Z 6a = (0-2-3+j4-3-j4)-0 4-0 Angle of asymptotes P - Z Angle of asymptotes Ang | | Date Page | |
| $G_{A} = \int_{A}^{A} u $ | | | |
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| 6a = (0-2-3+j4-3-j4)-0 4-0 4ngle of asymptotes p-7 P-7 (2x0+1)x180 = 45° (for K=0) y 1 = (2x2+1)x180 = 135° (for K=1) y 1 = (2x2+1)x180 = 225° (for K=2) | | | |
| 6a = (0-2-3+j4-3-j4)-0 4-0 4ngle of asymptotes p-7 P-7 (2x0+1)x180 = 45° (for K=0) y 1 = (2x2+1)x180 = 135° (for K=1) y 1 = (2x2+1)x180 = 225° (for K=2) | | 6A - Sum of poles - Symot Zenos | |
| Angle of asymptotes | | P - Z | |
| Angle of asymptotes | | 2) (H) -5 x 2) (cx 2) 2 | _ |
| Angle of asymptotes | | G= 10-2-3+14-3-14-0 | |
| $Q_{1} = (2 \times 0 + 1) \times 180^{\circ} = 45^{\circ} \text{ (for } K = 0)$ $Q_{2} = (2 \times 1 + 1) \times 180^{\circ} = 135^{\circ} \text{ (for } K = 1)$ $Q_{3} = (2 \times 2 + 1) \times 180^{\circ} = 225^{\circ} \text{ (for } K = 2)$ | | | _ |
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| $Q_{1} = (2 \times 0 + 1) \times 180^{\circ} = 45^{\circ} \text{ (for } K = 0)$ $Q_{2} = (2 \times 1 + 1) \times 180^{\circ} = 135^{\circ} \text{ (for } K = 1)$ $Q_{3} = (2 \times 2 + 1) \times 180^{\circ} = 225^{\circ} \text{ (for } K = 2)$ | | Angle of asymptotes. | |
| $Q_{1} = (2 \times 0 + 1) \times 180^{\circ} = 45^{\circ} \text{ (for } K = 0)$ $Q_{2} = (2 \times 1 + 1) \times 180^{\circ} = 135^{\circ} \text{ (for } K = 1)$ $Q_{3} = (2 \times 2 + 1) \times 180^{\circ} = 225^{\circ} \text{ (for } K = 2)$ | 0 | 0 = 2 K+1. 180° | |
| 0 = (2x1+1)x180 = 135° (for K=1) | | P-Z | |
| 0 = (2x1+1)x180 = 135° (for K=1) | 75.55 | 0 = (2x0 + 1)x183 - 45° (Ax 1/-0) | |
| 03 = (3x2+1) x180 = 225° (for K=2) | 1 1 | 19 () () () () () () () () () | |
| (3 = (2x2+1)x180 = 225° (for K=2) | | D: - (2x1 +1) 125° (1 | |
| 03 = (3x2+1) x180 = 225° (for K=2) | | 4 x 180 = 135 (for K=1) | |
| $\phi_{4} = (2 \times 3 + 1) \times 180 = 225^{\circ} (for K = 2)$ | | | |
| Du = (2 x 3 + 1) x 180 = 315° (for K = 3) | | (3 - (2x2 +1) x180 = 225 (lon K = 2) | |
| $9u = (2 \times 3 + 1) \times 180 = 315^{\circ} (for K = 3)$ | | 1 (| |
| 4 | | Qu = (2x3+1) x180 = 215° (1= x=3) | |
| | | 4 | |
| | | | |
| | | | |
| | | | - |
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Broad away point

Chanacteristic equation 1+ Cr(c) H(c) = 0

1 + K = 0

S(s+2)(s+6s+25) K + 54 + 8 53 + 375 + 505 = 0 dK = - (453+745+345+50)=0 07 453+245 + 745 + 50 =0 S = - 0.898 S= -2.5509 ± j 2.7224 Neglited because outsick the ranges of for Break away point S=-0.898 81,981

| 1 | PogeO |
|----------|---|
| 6=1 | Determination of 3W (20688 ver by (Routh Hurwitz) |
| | Charequestra 54 + 853 + 375 + 505 + K=0 |
| | 5 ⁴ 1 3 7 K |
| 0 | 10253 11 8 2 114 15 0 P) - NB |
| | 52 30.75 K |
| 4 55.8.5 | 30.75 30.75 |
| 10 10 1 | (3 to 2) |
| | 30.75 - 9K = 0 30.75 3. K = 192.18 |
| | |
| | 30.75 s' + K = 0 30.75 s' = - 192.18 |
| | s = + 3 2.5 |
| | |

| 17 156 | |
|--------|--|
| | Angle of departure from upper complement de = 180°- (104°+30°+127°) |
| | Pa = -141° |
| (7) | The range of values for Stability is O(K < 192.18 |
| (() | At this point of instability the goin is K = 192.18 |
| | $30.75 s^2 + 192.18 = 0$ |
| | Putting S= j W -30.75 w +192.18 = 0 |
| | 30.45 |
| | w = 2.5 mad sac |
| | at the point of instability = 2.5 nad/se |
| | |

The root locus plot is as follows -3443 E 1270