

$$1) \quad \begin{aligned} \dot{x}_1 &= -x_1 \\ \dot{x}_2 &= x_1 x_2 \\ \dot{x}_3 &= x_2 \end{aligned}$$

$y = x_3 \quad j = x_2 \quad \dot{j} = x_1 x_2 + u \quad \text{System relative degree: } \gamma = 2$

$\gamma = 2$  so we need to find  $\eta$  with  $z_1 = x_3 \quad z_2 = x_2$

the jacobian of the coordinate transformation is:

$$\partial \bar{\Phi} = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & 0 \\ \frac{\partial \eta}{\partial x_1} & \frac{\partial \eta}{\partial x_2} & \frac{\partial \eta}{\partial x_3} \end{bmatrix} \quad \text{and require} \quad \text{rank}(\partial \bar{\Phi}) = 3$$

$$\text{Lg} \eta = 0$$

We can let  $\eta = -x_1 + x_2 + x_2^3$

$$\bar{\Phi} = \begin{pmatrix} x_3 \\ x_2 \\ -x_1 + x_2 + x_2^3 \end{pmatrix}$$

$$\dot{\eta} = x_1 - (1+3x_2^2)u + x_1 x_2 + u + 3x_2^2 \cdot (x_1 x_2 + u)$$

When  $z_1 = 0 \quad z_2 = 0 \quad \dot{\eta} = x_1 \quad \eta = -x_1 \quad \text{let } V_0 = \frac{1}{2} \bar{\eta}^T \bar{\eta} \text{, then } V_0 \text{ is ncl}$

so it is minimum phase

2)

$$a) \begin{pmatrix} \dot{w}_1 \\ \dot{w}_2 \\ \dot{w}_3 \end{pmatrix} = \begin{pmatrix} a_1 w_2 w_3 \\ a_2 w_1 w_3 \\ a_3 w_1 w_2 \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \cdot u_1 + \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} u_2 \quad \text{and } y = \begin{pmatrix} w_1 \\ w_2 \end{pmatrix}$$

$L_f$        $L_g_1$        $L_g_2$

differentiate  $y$ :

$$\dot{y} = \begin{pmatrix} \dot{w}_1 \\ \dot{w}_2 \end{pmatrix} = \begin{pmatrix} a_1 w_2 w_3 + u_1 \\ a_2 w_1 w_3 + u_2 \end{pmatrix}$$

let virtual input  $V = \dot{y}$ , then  $u_1 = V_1 - a_1 w_2 w_3$

$$u_2 = V_2 - a_2 w_1 w_3$$

let  $e = W - W_d$  then,  $\dot{e} = \dot{w} = V$      $\ddot{e} = \ddot{w}$

let  $\dot{e} = -k_p e$      $k_1, k_2 > 0$

$k_p$  is p.d and symmetric, so  $V = \begin{pmatrix} -k_1(w_1 - w_{1d}) \\ -k_2(w_2 - w_{2d}) \end{pmatrix}$     so  $u_1 = -k_1(w_1 - w_{1d}) - a_1 w_2 w_3$   
 $u_2 = -k_2(w_2 - w_{2d}) - a_2 w_1 w_3$

relative degree is 1,1. So we need to find  $\eta$

$\eta$  need to satisfy:  $\partial \bar{\Phi} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ \frac{\partial \bar{\Phi}}{\partial w_1} & \frac{\partial \bar{\Phi}}{\partial w_2} & \frac{\partial \bar{\Phi}}{\partial w_3} \end{pmatrix}$      $\text{rank}(\partial \bar{\Phi}) = 3$  and  $\nabla \bar{\Phi} \cdot g_1 = 0$   
 $\nabla \bar{\Phi} \cdot g_2 = 0$

we can let  $\eta = w_3$  then.  $\bar{\Phi} = \begin{pmatrix} w_1 \\ w_2 \\ w_3 \end{pmatrix}$

$$\dot{\eta} = a_3 w_1 w_2$$

when  $w_1 = w_2 = 0$      $\dot{\eta} = 0$ , so the zero dynamic is stable.

so it is not minimum phase

$$2) b) \quad y = \begin{pmatrix} w_1 \\ w_3 \end{pmatrix} \quad \dot{y} = \begin{pmatrix} a_1 w_1 w_3 + u_1 \\ a_3 w_1 w_2 \end{pmatrix} \quad \dot{y} = \begin{pmatrix} a_1(a_2 w_1 w_3 + u_2) w_3 + a_1 w_2 a_3 w_1 w_2 + \dot{u}_1 \\ a_3(a_1 w_2 w_3 + u_1) w_2 + a_3 w_1 (a_2 w_1 w_3 + u_2) \end{pmatrix}$$

$$= \begin{pmatrix} a_1 a_2 w_1 w_3^2 + a_1 a_3 w_1 w_2^2 \\ a_2 a_3 w_1^2 w_3 + a_1 a_3 w_2^2 w_3 + a_3 w_2 u_1 \end{pmatrix} + \begin{pmatrix} 1 & a_1 w_3 \\ 0 & a_3 w_1 \end{pmatrix} \begin{pmatrix} \dot{u}_1 \\ u_2 \end{pmatrix}$$

let virtual input  $V = \dot{y}$

$$\begin{pmatrix} \dot{u}_1 \\ u_2 \end{pmatrix} = \begin{pmatrix} 1 & -\frac{a_1 w_3}{a_3 w_1} \\ 0 & \frac{1}{a_3 w_1} \end{pmatrix} \cdot \begin{pmatrix} V_1 \\ V_2 \end{pmatrix} - \begin{pmatrix} a_1 a_2 w_1 w_3^2 + a_1 a_3 w_1 w_2^2 \\ a_2 a_3 w_1^2 w_3 + a_1 a_3 w_2^2 w_3 + a_3 w_2 u_1 \end{pmatrix}$$

dynamic compensator  $\Sigma = U_1$ , when  $w_1 \neq 0$  controller is valid.

$$\text{and } V = -k_p(y - y_d) - k_d(\dot{y} - \dot{y}_d) + \ddot{y}_d$$

$$\text{since } y_d \text{ is constant, } V = -k_p(y - y_d) - k_d \dot{y}$$

2, c)

$k_p, k_d$  are pd and symmetric

$$\text{in a)} \quad U_1 = -k_1(w_1 - w_{1d}) - a_1 w_2 w_3$$

$$U_2 = -k_2(w_2 - w_{2d}) - a_2 w_1 w_3$$

in b)

$$\begin{pmatrix} \dot{u}_1 \\ u_2 \end{pmatrix} = \begin{pmatrix} 1 & -\frac{a_1 w_3}{a_3 w_1} \\ 0 & \frac{1}{a_3 w_1} \end{pmatrix} \cdot \begin{pmatrix} V_1 \\ V_2 \end{pmatrix} - \begin{pmatrix} a_1 a_2 w_1 w_3^2 + a_1 a_3 w_1 w_2^2 \\ a_2 a_3 w_1^2 w_3 + a_1 a_3 w_2^2 w_3 + a_3 w_2 u_1 \end{pmatrix}$$

I suggest we can first follow controller in a)

after get into some near region of  $(w_{1d}, w_{2d})$  use controller in b)

after get into some near region of  $(w_{1d}, w_{3d})$  use controller in a)

in the process, we can shrink the boundary of region

to force the state get to  $(w_{1d}, w_{2d}, w_{3d})$

$$3) m \begin{bmatrix} \ddot{x} \\ \ddot{y} \end{bmatrix} = \begin{bmatrix} 0 \\ mg \end{bmatrix} + \begin{bmatrix} -\sin\theta \\ \cos\theta \end{bmatrix} u_1, \quad J_0 \ddot{\theta} = u_2 - u_3, \quad a \ddot{\varphi} = u_3 - \ell_0 u_1 \sin\varphi - \frac{a}{J_0}(u_2 - u_3),$$

$$\begin{pmatrix} X_1^{(3)} \\ X_2^{(3)} \end{pmatrix} = \frac{1}{m} R(x_3) \cdot \begin{pmatrix} -u_1 \dot{x}_3 \\ \ddot{u}_1 \end{pmatrix} \quad R(x) = \begin{pmatrix} \cos x & -\sin x \\ \sin x & \cos x \end{pmatrix}$$

denote  $\gamma$  as  $X_2$ .  $\theta$  as  $X_3$   $\varphi$  as  $X_4$

$$\text{since } J_0 \ddot{x}_3 = u_2 - u_3, \quad \begin{pmatrix} X_1^{(4)} \\ X_2^{(4)} \end{pmatrix} = \frac{R(x_3)}{m} \begin{pmatrix} -2\ddot{u}_1 \dot{x}_3 \\ -u_1 \dot{x}_3^2 \end{pmatrix} + \frac{R(x_3)}{m} \begin{pmatrix} -u_1/J_0 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} u_2 - u_3 \\ \ddot{u}_1 \end{pmatrix}$$

let virtual input be  $V = \begin{pmatrix} X_1^{(4)} \\ X_2^{(4)} \end{pmatrix}$ , dynamic compensator:  $\xi = \begin{pmatrix} u_1 \\ \ddot{u}_1 \end{pmatrix}$

We can set  $V = y_d^{(4)} - \sum_{i=0}^4 k_i (y^{(i)} - y_d^{(i)})$  ( $k_i$  are P,I and symmetric)

let  $y = \begin{pmatrix} X_1 \\ X_2 \end{pmatrix} \quad y_d = \begin{pmatrix} X_{1d} \\ X_{2d} \end{pmatrix} \quad$  We can use  $u_2 - u_3, \ddot{u}_1$  in controller

$$\text{then, } \begin{pmatrix} u_2 - u_3 \\ \ddot{u}_1 \end{pmatrix} = \begin{bmatrix} -\frac{J_0}{\xi_1} & 0 \\ 0 & 1 \end{bmatrix} \left[ m R^T(x_3) \cdot V + \begin{pmatrix} 2\xi_2 \dot{x}_3 \\ u_1 \dot{x}_3^2 \end{pmatrix} \right]$$

$\uparrow$  we can track  $x(t), y(t)$

then let  $\ddot{x}_4 = \ddot{x}_{4d} - k_4(x_4 - x_{4d}) - k_5(\dot{x}_4 - \dot{x}_{4d}), k_4, k_5 > 0$

$$\text{so } u_3 = a \ddot{x}_4 + L_0 u_1 \sin x_4 + \frac{a}{J_0}(u_2 - u_3) \quad \text{get } u_1, u_2 - u_3 \text{ from there}$$

3) b)

$$\theta(t) + \varphi(t) = x_3 + x_4 \quad \text{let } x_5 = x_3 + x_4$$

$$\ddot{x}_5 = \ddot{x}_{5d} - k_6(x_5 - x_{5d}) - k_7(\dot{x}_5 - \dot{x}_{5d}), k_6, k_7 > 0$$

$$\begin{aligned} \ddot{x}_5 = \ddot{x}_3 + \ddot{x}_4 &= \frac{u_3}{a} - \frac{L_0}{a} u_1 \sin x_4 - \frac{1}{J_0}(u_2 - u_3) + \frac{1}{J_0}(u_2 - u_3) \\ &= \frac{u_3}{a} - \frac{L_0}{a} u_1 \sin x_4 \end{aligned}$$

$$u_3 = a \ddot{x}_5 + L_0 u_1 \sin x_4$$

reuse  $u_2 - u_3$ , and  $\ddot{u}_1$  get before.

$$4) \quad a) \quad \dot{y} = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}$$

$$\ddot{y} = \begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{pmatrix} = \begin{pmatrix} -\sin x_3 \cdot u_2 x_4^2 + \beta \cos x_3 u_2 \cdot x_4^2 + \cos x_3 u_1 + \beta \sin x_3 u_1 \\ \cos x_3 \cdot u_2 x_4^2 + \beta \sin x_3 u_2 \cdot x_4^2 + \sin x_3 u_1 - \beta \cos x_3 u_1 \end{pmatrix}$$

$$\text{Virtual input } v = \begin{pmatrix} \cos x_3 + \beta \sin x_3 & -\sin x_3 \cdot x_4^2 + \beta \cos x_3 x_4^2 \\ \sin x_3 - \beta \cos x_3 & \cos x_3 x_4^2 + \beta \cos x_3 x_4^2 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}$$

↳ denote this as  $A$ .

let error dynamic:  $e = y - y_d$

$$\text{let } \begin{pmatrix} \dot{e} \\ \ddot{e} \end{pmatrix} = \begin{pmatrix} 0 & I \\ k_p & -k_d \end{pmatrix} \begin{pmatrix} e \\ \dot{e} \end{pmatrix} \quad k_p, k_d \text{ and p.d and symmetric}$$

$$\text{then, } V = \ddot{y}_d - k_p(y - y_d) - k_d(\dot{y} - \dot{y}_d)$$

$$\text{and then } u = A^{-1} \cdot v$$

$$4b) \quad S = \begin{pmatrix} (\beta - \hat{\beta}) \sin x_3 \cdot x_4 \\ (\hat{\beta} - \beta) \cos x_3 \cdot x_4 \end{pmatrix} = (\beta - \hat{\beta}, \hat{\beta} - \beta) \cdot \begin{pmatrix} \sin x_3 \\ \cos x_3 \end{pmatrix} \cdot x_4$$

$$(\beta - \hat{\beta}, \hat{\beta} - \beta) \cdot \begin{pmatrix} \sin x_3 \\ \cos x_3 \end{pmatrix} \leq \|(\beta - \hat{\beta}, \hat{\beta} - \beta)\| \cdot \|( \sin x_3, \cos x_3 )\|$$

$$= \sqrt{2} |\beta - \hat{\beta}|$$

$$\text{So. } |S| \leq \sqrt{2} |\beta - \hat{\beta}| \cdot |x_4|$$

↑  $\alpha_1$

$$5) \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} 0 \\ x_2 \\ 0 \end{pmatrix} + \begin{pmatrix} \cos x_3 \\ \sin x_3 \\ 0 \end{pmatrix} u_1 + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} u_2$$

$\underbrace{\quad}_{g_0}$        $\underbrace{\quad}_{g_1}$        $\underbrace{\quad}_{g_2}$

$$[g_1, g_2] = - \begin{bmatrix} 0 & 0 & -\sin x_3 \\ 0 & 0 & \cos x_3 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} \sin x_3 \\ -\cos x_3 \\ 0 \end{bmatrix} = g_3$$

$$\det([g_1, g_2, g_3]) = 1 \quad \text{LARC of degree 2}$$

there is no bad brackets of degree  $\leq 2$

so LARC is satisfied, the system is STLC