

Robotic Control of an Elastic Beam

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Abstract— This report represents the implementation of a planer control system for manipulating a slender elastic aluminum beam.

I. INTRODUCTION

The objective of this homework is to design a controller such that the beam's middle node follows a prescribed trajectory with the left end remains fixed and the right end actuated by the robot end effector.

II. METHODOLOGY

A. Discretization

The beam is modeled as a discrete mass-spring system with 19 nodes. The system is described by a position vector \mathbf{q}

B. Energy

The total elastic energy is the linear sum of stretching energy and bending energy. The stretching energy for spring k connecting node k and $k+1$ is:

$$E_k^s = \frac{1}{2} EA\Delta L \left(\frac{\ell_k - \Delta L}{\Delta L} \right)^2$$

where ℓ_k is the deformed length.

The bending energy at node k is:

$$E_k^b = \frac{1}{2} \frac{EI}{\Delta L} (\kappa_k - \bar{\kappa}_k)^2$$

The discrete curvature is computed using the turning angle

$$\kappa_k = \frac{2\mathbf{t}_{k-1} \times \mathbf{t}_k}{1 + \mathbf{t}_{k-1} \cdot \mathbf{t}_k}$$

where \mathbf{t}_{k-1} and \mathbf{t}_k are unit tangent vectors of edge $k-1$ and k

C. Forces

The only external force would be gravity on each node:

$$\mathbf{f}_g^{(i)} = \begin{bmatrix} 0 \\ -mg \end{bmatrix}, \quad g = 9.81 \text{ m/s}^2$$

D. Time Integration

As usual, the equations of motion are integrated using an Implicit Euler time-stepping

$$\mathbf{M} \frac{\mathbf{q}^{n+1} - \mathbf{q}^n}{\Delta t^2} - \mathbf{M} \frac{\mathbf{u}^n}{\Delta t} = \mathbf{F}_{\text{elastic}}(\mathbf{q}^{n+1}) + \mathbf{F}_{\text{gravity}}$$

E. Boundary Conditions

The left end is clamped at (0,0):

$$x_1(t_{k+1}) = 0, \quad y_1(t_{k+1}) = 0$$

The rightmost node is controlled by the robot, and using Dirichlet constraints, we have:

$$x_N(t_{k+1}) = x_c(t_{k+1}), \quad y_N(t_{k+1}) = y_c(t_{k+1})$$

$$x_{N-1}(t_{k+1}) = x_c(t_{k+1}) - \Delta L \cos \theta_c(t_{k+1})$$

$$y_{N-1}(t_{k+1}) = y_c(t_{k+1}) - \Delta L \sin \theta_c(t_{k+1})$$

F. Control Law

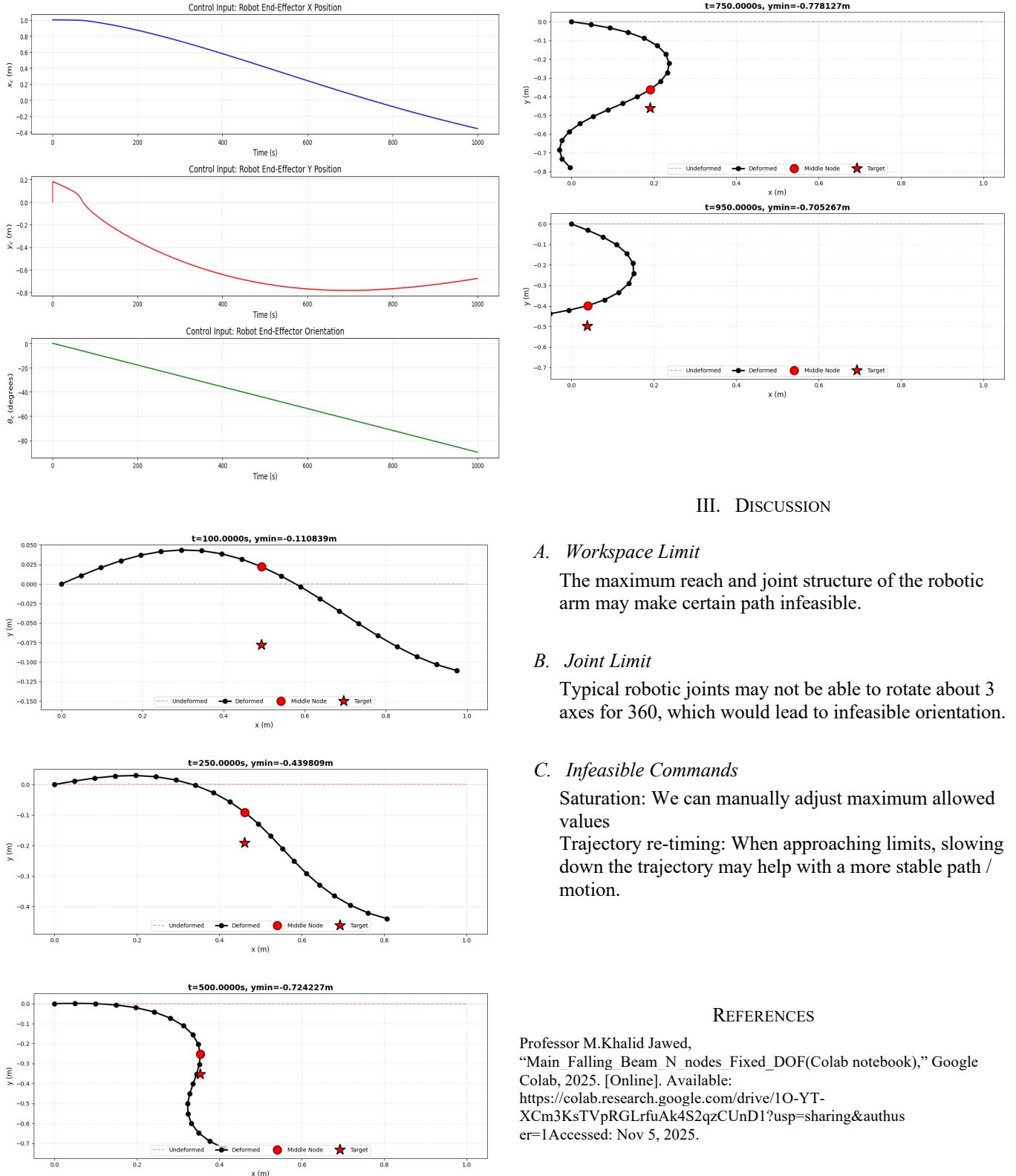
A for-loop based simple controller is implemented. The design is to measure the error in the middle node position and adjust the inputs to reduce the error.

Algorithm 1 Control Law for Robot End-Effector

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1: Input: Current configuration  $\mathbf{q}$ , time  $t$ , current controls  $(x_c, y_c, \theta_c)$ 
2: Output: Updated controls  $(x_c^{\text{new}}, y_c^{\text{new}}, \theta_c^{\text{new}})$ 
3:
4: Compute target position:  $x^* \leftarrow \frac{L}{2} \cos\left(\frac{\pi t}{2000}\right)$ ,  $y^* \leftarrow -\frac{L}{2} \sin\left(\frac{\pi t}{2000}\right)$ 
5:
6: Geometric positioning:  $x_c^{\text{geo}} \leftarrow 2x^*$ ,  $y_c^{\text{geo}} \leftarrow 2y^*$ 
7:
8: Elevation compensation:  $\text{base\_lift} \leftarrow 0.15$ ,  $\text{depth\_factor} \leftarrow 0$ 
9: for  $i = 1$  to  $10$  do
10:    $\text{depth\_factor} \leftarrow \text{depth\_factor} + |y^*|/10$ 
11: end for
12:  $y_c^{\text{geo}} \leftarrow y_c^{\text{geo}} + \text{base\_lift} + 0.3 \cdot \text{depth\_factor}$ 
13:
14: Set orientation:  $\theta_c^{\text{geo}} \leftarrow \arctan 2(y^* - y_c^{\text{geo}}, x^* - x_c^{\text{geo}})$ 
15:
16: Apply smoothing ( $\alpha = 0.95$ ):
17:    $x_c^{\text{new}} \leftarrow \alpha x_c + (1 - \alpha)x_c^{\text{geo}}$ 
18:    $y_c^{\text{new}} \leftarrow \alpha y_c + (1 - \alpha)y_c^{\text{geo}}$ 
19:    $\theta_c^{\text{new}} \leftarrow \alpha \theta_c + (1 - \alpha)\theta_c^{\text{geo}}$ 
20:
21: return  $(x_c^{\text{new}}, y_c^{\text{new}}, \theta_c^{\text{new}})$ 

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III. DISCUSSION

A. Workspace Limit

The maximum reach and joint structure of the robotic arm may make certain path infeasible.

B. Joint Limit

Typical robotic joints may not be able to rotate about 3 axes for 360°, which would lead to infeasible orientation.

C. Infeasible Commands

Saturation: We can manually adjust maximum allowed values

Trajectory re-timing: When approaching limits, slowing down the trajectory may help with a more stable path / motion.

REFERENCES

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