

Problem 1

Determine the [modulus of resilience] for each of the following metals:

(a) Stainless steel

AISI 302 (annealed):

$$E = 190 \text{ GPa} \quad \sigma_Y = 260 \text{ MPa}$$

(b) Stainless steel 2014-T6

AISI 302 (cold-rolled):

$$E = 190 \text{ GPa} \quad \sigma_Y = 520 \text{ MPa}$$

(c) Malleable cast iron:

$$E = 165 \text{ GPa} \quad \sigma_Y = 230 \text{ MPa}$$

解: a) $MR = \frac{1}{2} \sigma_Y \epsilon_Y = \frac{1}{2} \sigma_Y^2 \cdot \frac{1}{E} = \frac{\frac{1}{2} \times (260 \times 10^6)^2}{190 \times 10^9} = 0.1779 \text{ MPa} = 177.9 \text{ kPa}$

b) $MR = \frac{1}{2} \frac{\sigma_Y^2}{E} = \frac{(520 \times 10^6)^2}{2 \times 190 \times 10^9} = 0.7116 \text{ MPa} = 711.6 \text{ kPa}$

c) $MR = \frac{1}{2} \frac{\sigma_Y^2}{E} = \frac{(230 \times 10^6)^2}{2 \times 165 \times 10^9} = 0.1603 \text{ MPa} = 160.3 \text{ kPa}$

Problem 2

Rod AB is made of a steel for which the (yield strength) is $\sigma_Y = 450 \text{ MPa}$ and $E = 200 \text{ GPa}$; rod BC is made of an aluminum alloy for which $\sigma_Y = 280 \text{ MPa}$ and $E = 73 \text{ GPa}$. Determine the maximum strain energy that can be acquired by the composite rod ABC without causing any permanent deformations.

解: for rod AB

$$P_{AB} = \sigma_{Y1} \cdot A_{AB} = 450 \times 10^6 \times \pi (5 \times 10^{-3})^2 = 11250\pi \text{ N}$$

for rod BC

$$P_{BC} = \sigma_{Y2} \cdot A_{BC} = 280 \times 10^6 \times \pi (7 \times 10^{-3})^2 = 13720\pi \text{ N}$$

$$\text{So } P_{\max} = 11250\pi \text{ N}$$

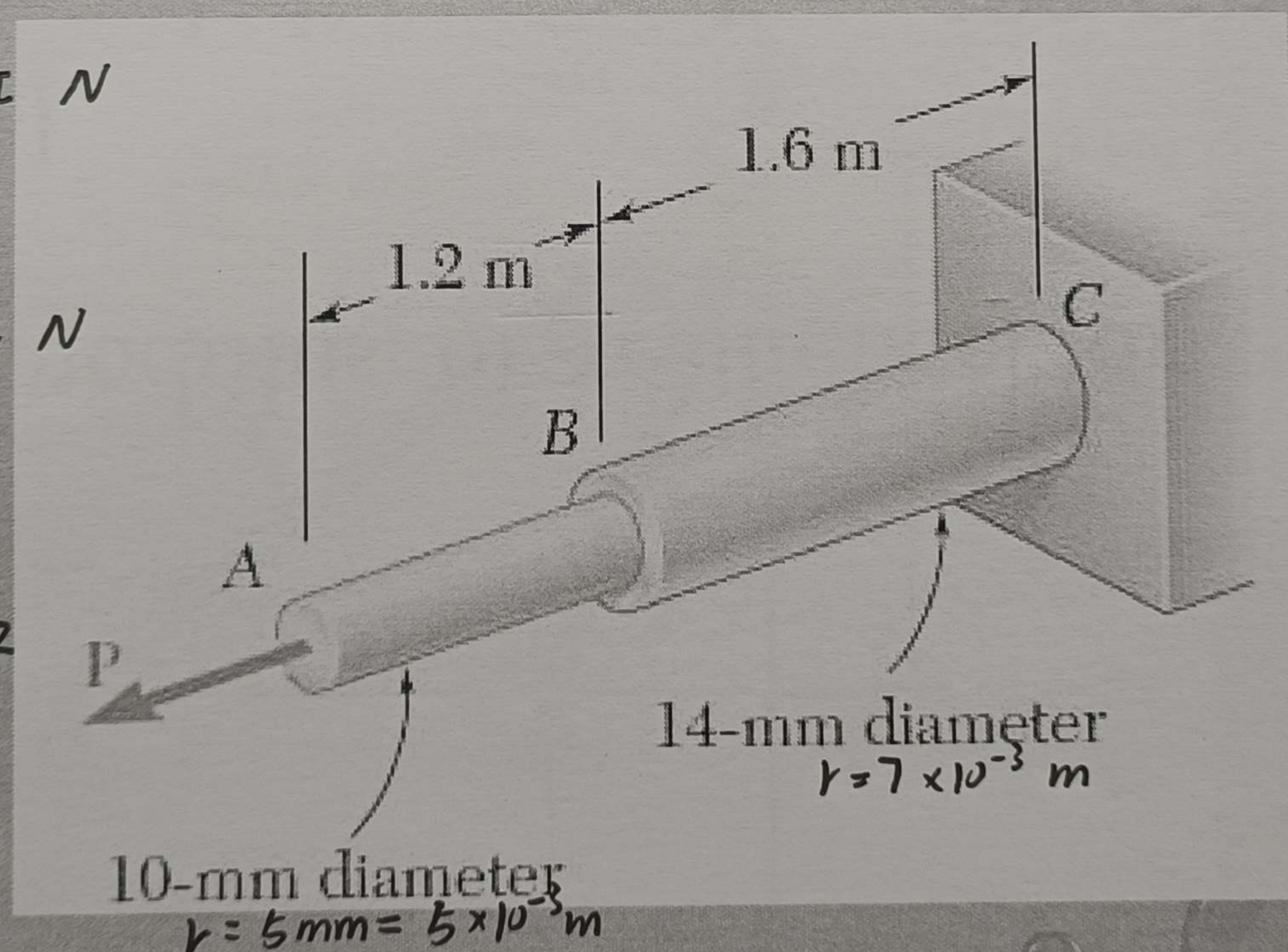
$$U_{AB} = \int \frac{\sigma_Y^2}{2E} dV = \frac{(450 \times 10^6)^2}{2 \times 200 \times 10^9} \times \pi (5 \times 10^{-3})^2 \times 1.2$$

$$= \frac{243}{16} \pi \text{ J}$$

$$\sigma_{BC} = \frac{P_{\max}}{A_{BC}}$$

$$U_{BC} = \int \frac{\sigma_{BC}^2}{2E} dV = \frac{P_{\max}^2}{2E A_{BC}^2} \cdot A_{BC} \cdot L_{BC} = \frac{P_{\max}^2}{2E A_{BC}} \cdot L_{BC} = \frac{(11250\pi)^2 \times 1.6}{2 \times 73 \times 10^9 \times \pi (7 \times 10^{-3})^2} = 88.925 \text{ J}$$

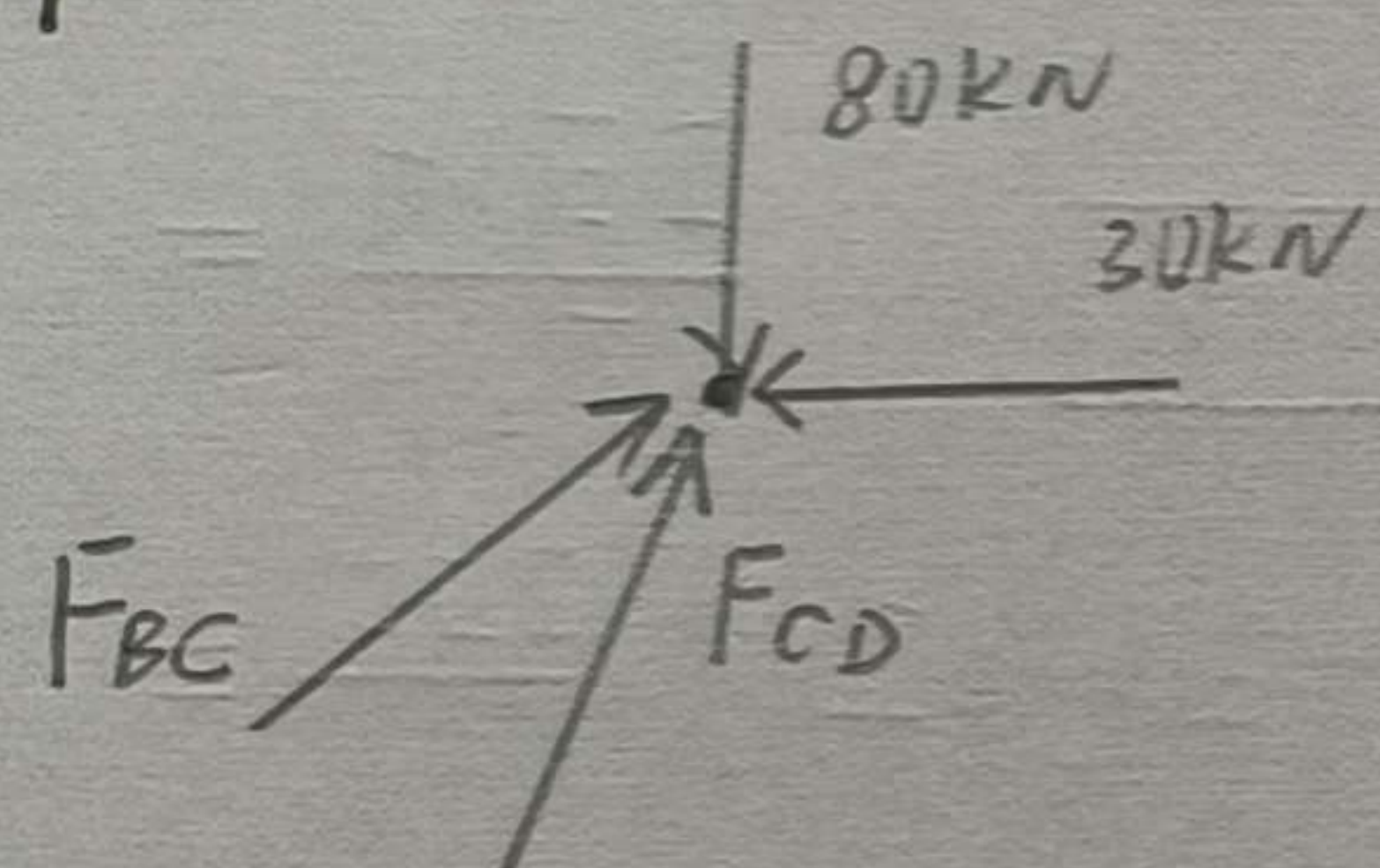
$$\therefore U_{ABC} = U_{AB} + U_{BC} = 136.6 \text{ J} \quad \boxed{\text{ANS}}$$



Problem 3

Each member of the truss shown is made of aluminum and has the cross-sectional area shown. Using $E = 72 \text{ GPa}$, determine the strain energy of the truss for the loading shown.

解: for node C



$$+\rightarrow \sum F_x = 0: -30 + F_{BC} \cos \alpha + F_{CD} \cos \beta = 0$$

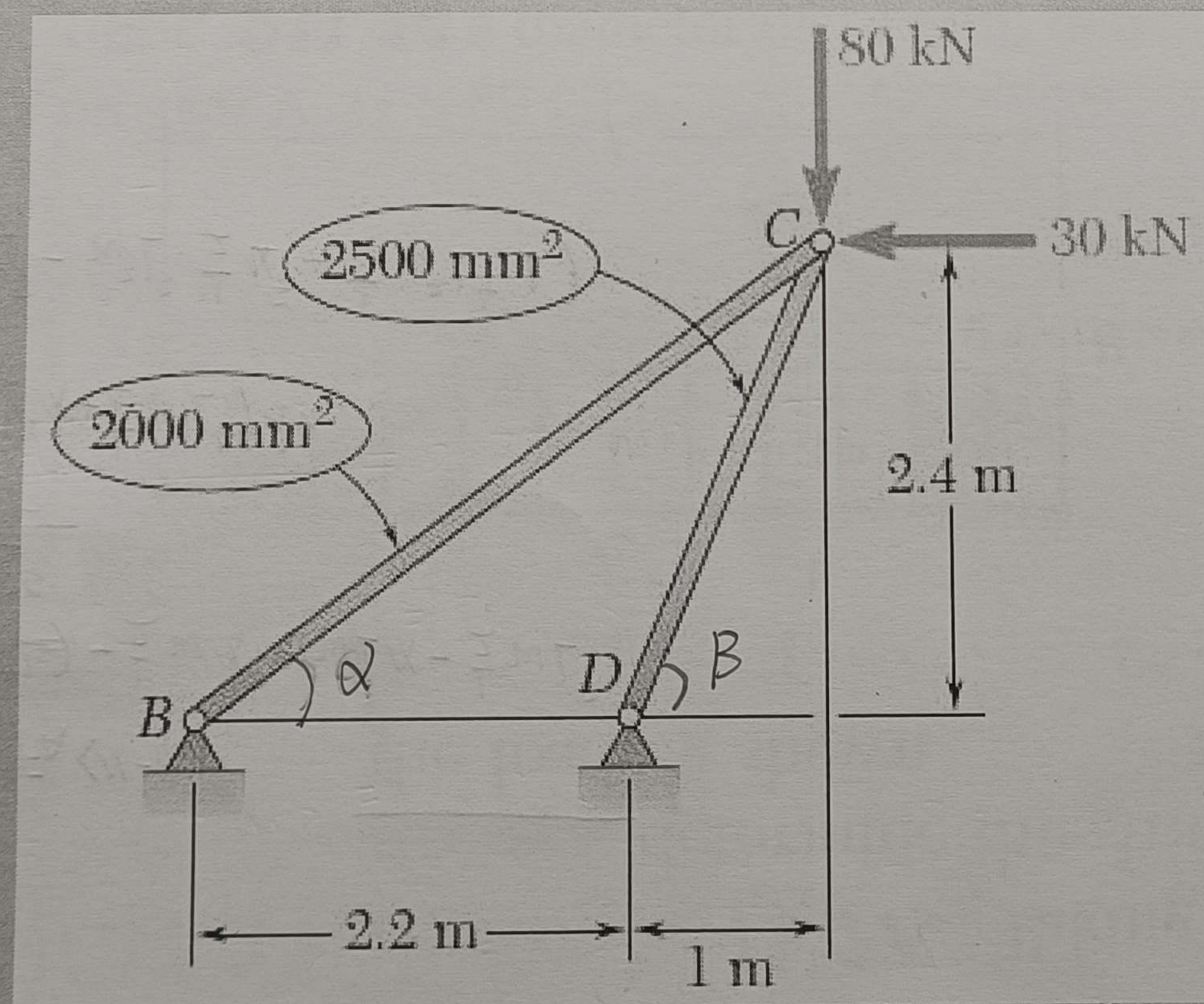
$$+\uparrow \sum F_y = 0: -80 + F_{BC} \sin \alpha + F_{CD} \sin \beta = 0$$

$$\cos \alpha = \frac{3.2}{\sqrt{3.2^2 + 2.4^2}} = 0.8, \sin \alpha = 0.6$$

$$\cos \beta = \frac{1}{\sqrt{1 + 2.4^2}} = \frac{5}{13}, \sin \beta = \frac{12}{13}$$

$$\Rightarrow F_{BC} = -\frac{200}{33} \text{ kN}, \quad G_{BC} = \frac{F_{BC}}{A_{BC}}$$

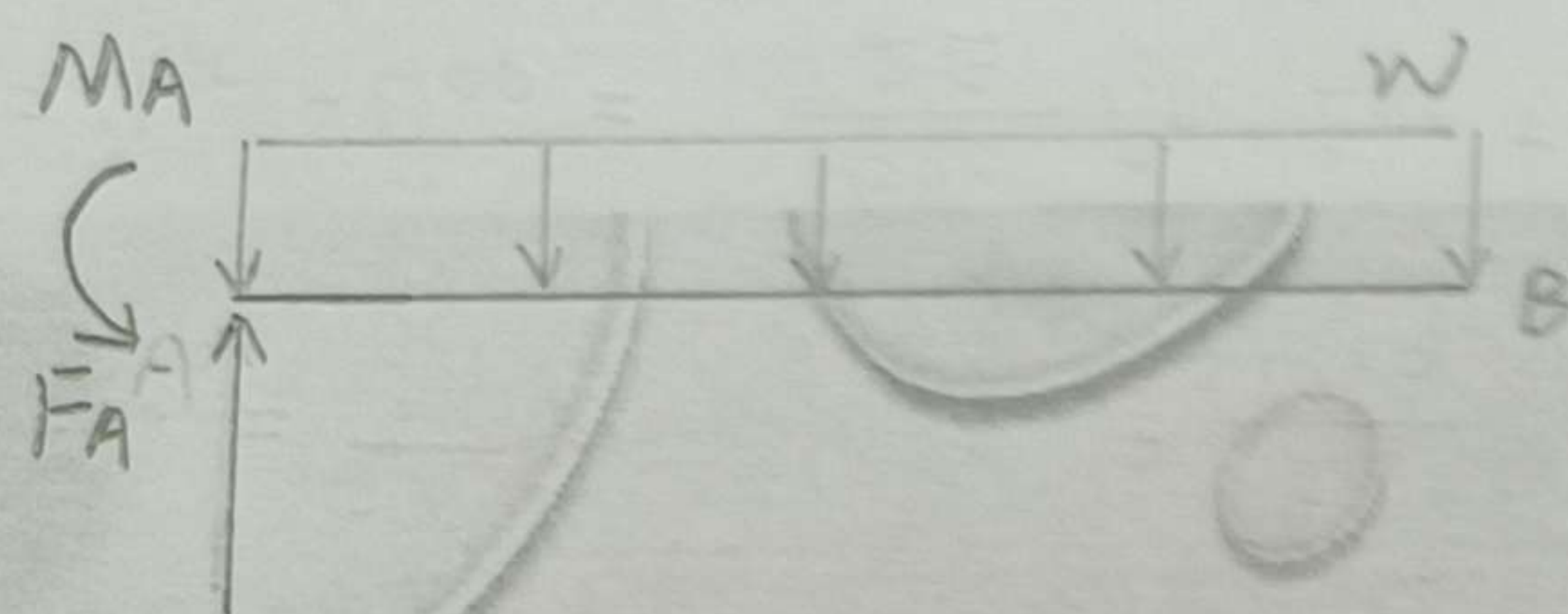
$$F_{CD} = \frac{2990}{33} \text{ kN}, \quad G_{CD} = \frac{F_{CD}}{A_{CD}}$$



$$U = U_{BC} + U_{CD} = \frac{G_{BC}^2}{2E} A_{BC} \cdot L_{BC} + \frac{G_{CD}^2}{2E} A_{CD} \cdot L_{CD} = \frac{F_{BC}^2}{2E \cdot A_{BC}} \cdot L_{BC} + \frac{F_{CD}^2}{2E \cdot A_{CD}} \cdot L_{CD}$$

$$= \frac{\left(\frac{200}{33} \times 10^3\right)^2 \times 4}{2 \times 72 \times 10^9 \times 2000 \times 10^{-6}} + \frac{\left(\frac{2990}{33} \times 10^3\right)^2 \times 2.6}{2 \times 72 \times 10^9 \times 2500 \times 10^{-6}} = 59.80 \text{ J} \quad \boxed{\text{ANS}}$$

11.24 解:



$$\begin{aligned} \uparrow \sum F_y = 0: F_A - wL &= 0 \\ \curvearrowright \sum M_A = 0: M_A - wL \cdot \frac{L}{2} &= 0 \\ \Rightarrow F_A &= wL \\ M_A &= \frac{1}{2} wL^2 \end{aligned}$$

Problem 4

$$\begin{aligned} w(x) &= w \langle x-0 \rangle^0 \\ V(x) &= -w \langle x-0 \rangle^1 + F_A \langle x-0 \rangle^0 \\ M(x) &= -\frac{1}{2} w \langle x-0 \rangle^2 + F_A \langle x-0 \rangle^1 - M_A \langle x-0 \rangle^0 = -\frac{1}{2} w x^2 + wLx - \frac{1}{2} wL^2 \end{aligned}$$

$$\begin{aligned} U &= \int_0^L \frac{M^2(x)}{2EI} dx \\ &= \frac{1}{2EI} \int_0^L \left(\frac{1}{4} w^2 x^4 - w^2 L x^3 + \frac{3}{2} w^2 L^2 x^2 - w^2 L^3 x + \frac{1}{4} w^2 L^4 \right) dx \\ &= \frac{1}{2EI} \left(\frac{1}{4} w^2 \cdot \frac{1}{5} L^5 - w^2 L \cdot \frac{1}{4} L^4 + \frac{3}{2} w^2 L^2 \cdot \frac{1}{3} L^3 - w^2 L^3 \cdot \frac{1}{2} L + \frac{1}{4} w^2 L^4 \cdot L \right) \\ &= \frac{w^2 L^5}{40EI} \quad \boxed{\text{ANS}} \end{aligned}$$

11.24 through 11.27 Taking into account only the effect of normal stresses, determine the strain energy of the prismatic beam AB for the loading shown.

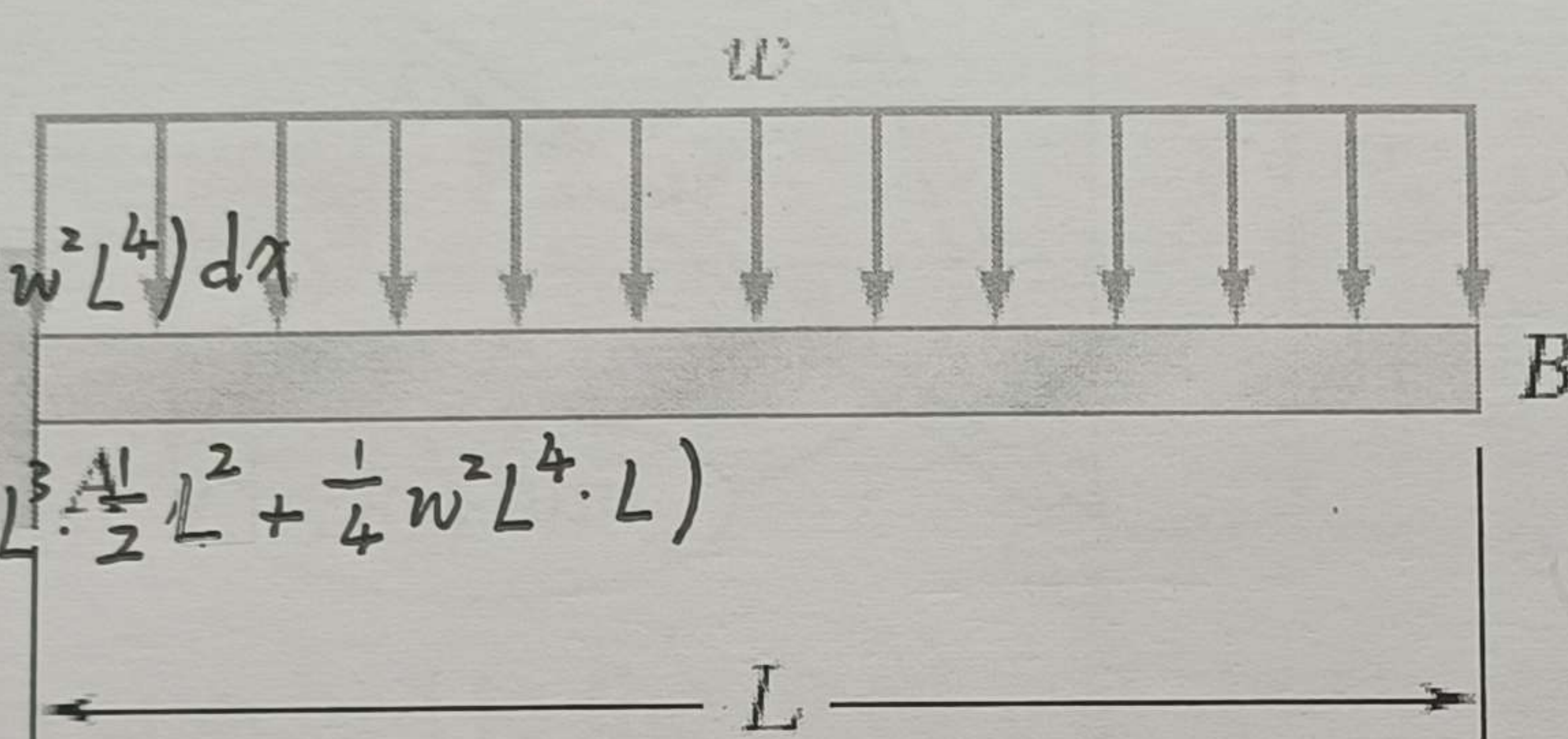
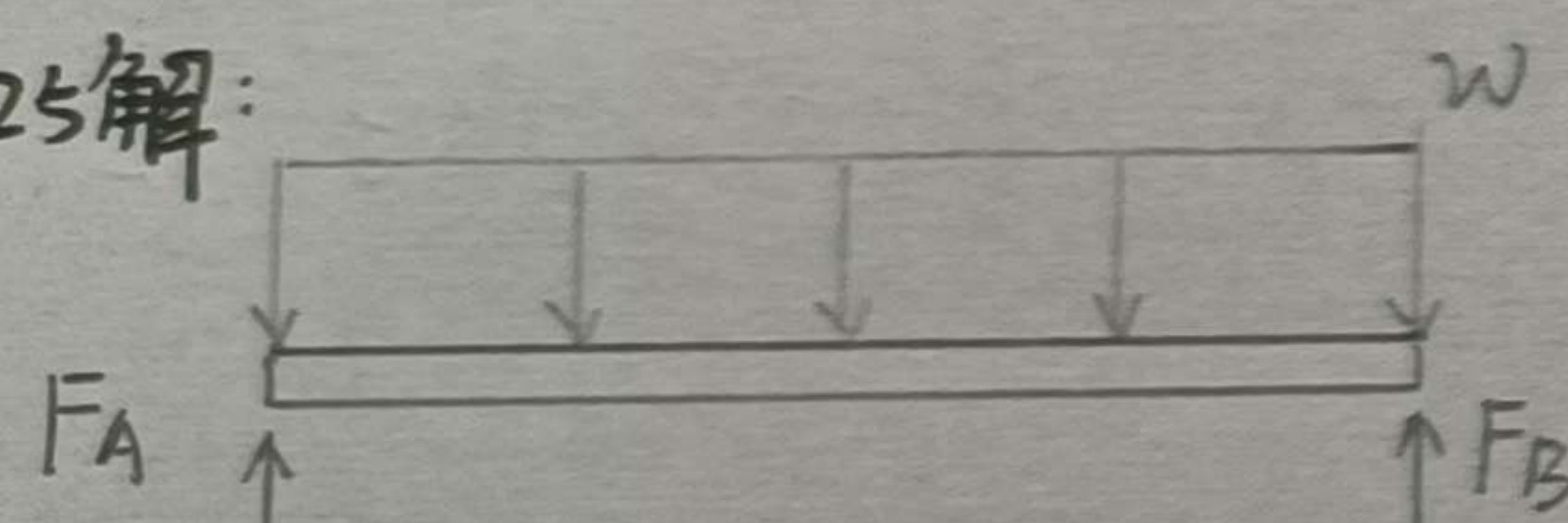


Fig. P11.24

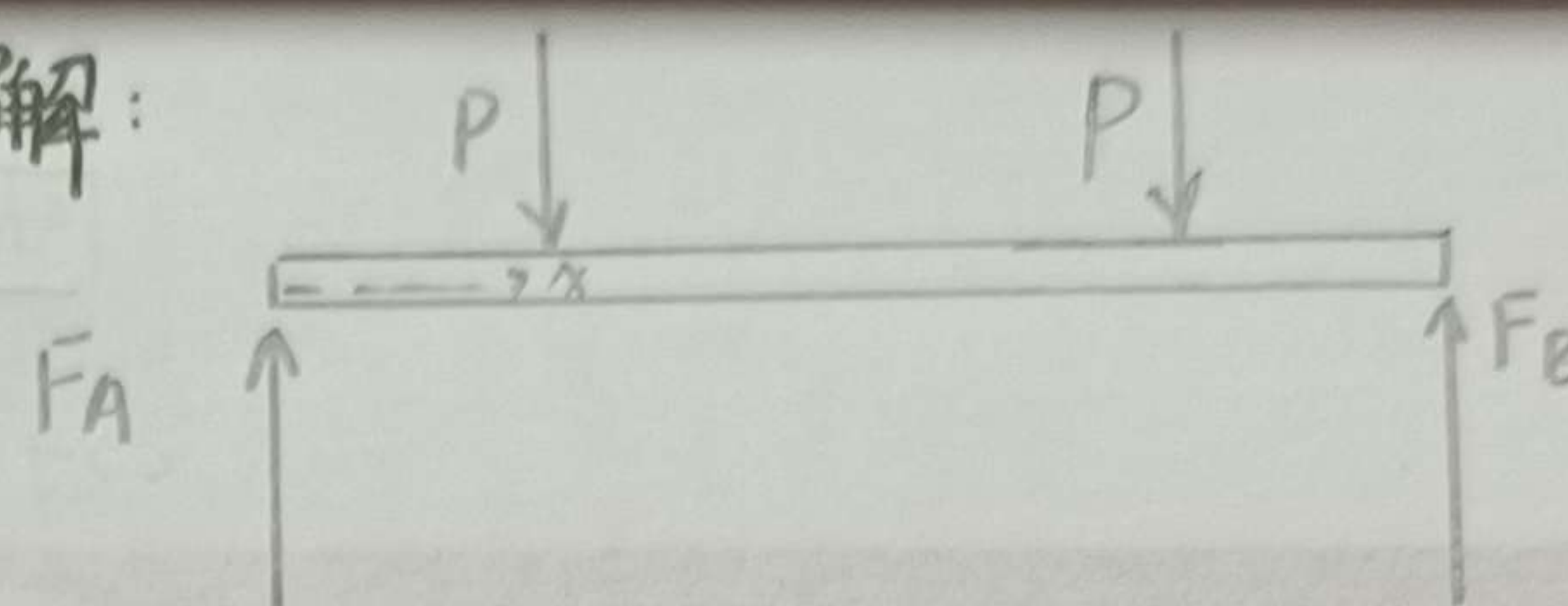
11.25 解:



$$\begin{aligned} \uparrow \sum F_y = 0: F_A + F_B - wL &= 0 \\ \curvearrowright \sum M_A = 0: -wL \cdot \frac{L}{2} + F_B \cdot L &= 0 \end{aligned} \Rightarrow \begin{aligned} F_A &= \frac{1}{2} wL \\ F_B &= \frac{1}{2} wL \end{aligned}$$

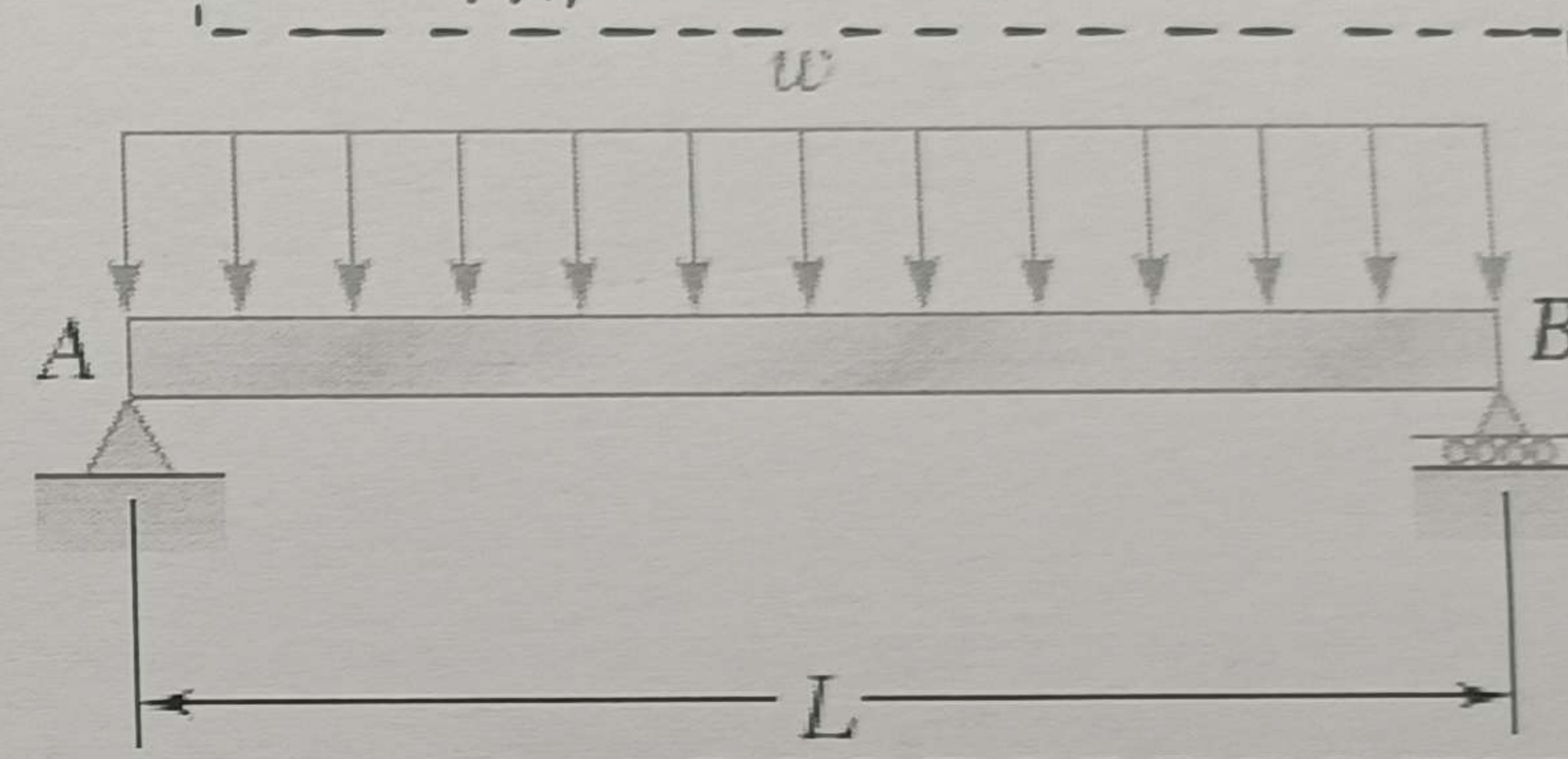
$$\begin{aligned} w(x) &= w \langle x-0 \rangle^0 \\ V(x) &= -w \langle x-0 \rangle^1 + F_A \langle x-0 \rangle^0 \\ M(x) &= -\frac{1}{2} w \langle x-0 \rangle^2 + F_A \langle x-0 \rangle^1 = -\frac{1}{2} w x^2 + \frac{1}{2} wLx \\ U &= \int_0^L \frac{M^2(x)}{2EI} dx = \frac{1}{2EI} \int_0^L \left(\frac{1}{4} w^2 x^4 + \frac{1}{4} w^2 L^2 x^2 - \frac{1}{2} w^2 L x^3 \right) dx \\ &= \frac{1}{2EI} \left(\frac{1}{4} w^2 \cdot \frac{1}{5} L^5 + \frac{1}{4} w^2 L^2 \cdot \frac{1}{3} L^3 - \frac{1}{2} w^2 L \cdot \frac{1}{4} L^4 \right) \\ &= \frac{w^2 L^5}{240EI} \quad \boxed{\text{ANS}} \end{aligned}$$

11.27 解:



$$\begin{aligned} \uparrow \sum F_y = 0: F_A + F_B &= 2P \\ \curvearrowright \sum M_A = 0: -P \cdot a - P(L-a) + F_B \cdot L &= 0 \\ \Rightarrow F_A &= P \quad F_B = P \\ V(x) &= F_A \langle x-0 \rangle^0 - P \langle x-a \rangle^0 - P \langle x-L+a \rangle^0 \\ M(x) &= F_A \langle x-0 \rangle^1 - P \langle x-a \rangle^1 - P \langle x-L+a \rangle^1 \end{aligned}$$

$$M(x) = \begin{cases} F_A x & 0 < x < a \\ F_A x - P(x-a) & a < x < L-a \\ F_A x - P(x-a) - P(x-L+a) & L-a < x < L \end{cases}$$



$$\begin{aligned} \text{Fig. P11.25 } U &= \int_0^L \frac{M^2(x)}{2EI} dx = \frac{1}{2EI} \left(\int_0^a P^2 x^2 dx + \int_a^{L-a} a^2 P^2 dx + \int_{L-a}^L (PL-Px)^2 dx \right) \\ &= \frac{1}{2EI} \left(\frac{1}{3} P^2 a^3 + a^2 P^2 (L-a) + \frac{1}{3} P^2 (L-a)^3 \right) \\ &= \frac{P^2 a^2}{6EI} (3L-4a) \quad \boxed{\text{ANS}} \end{aligned}$$

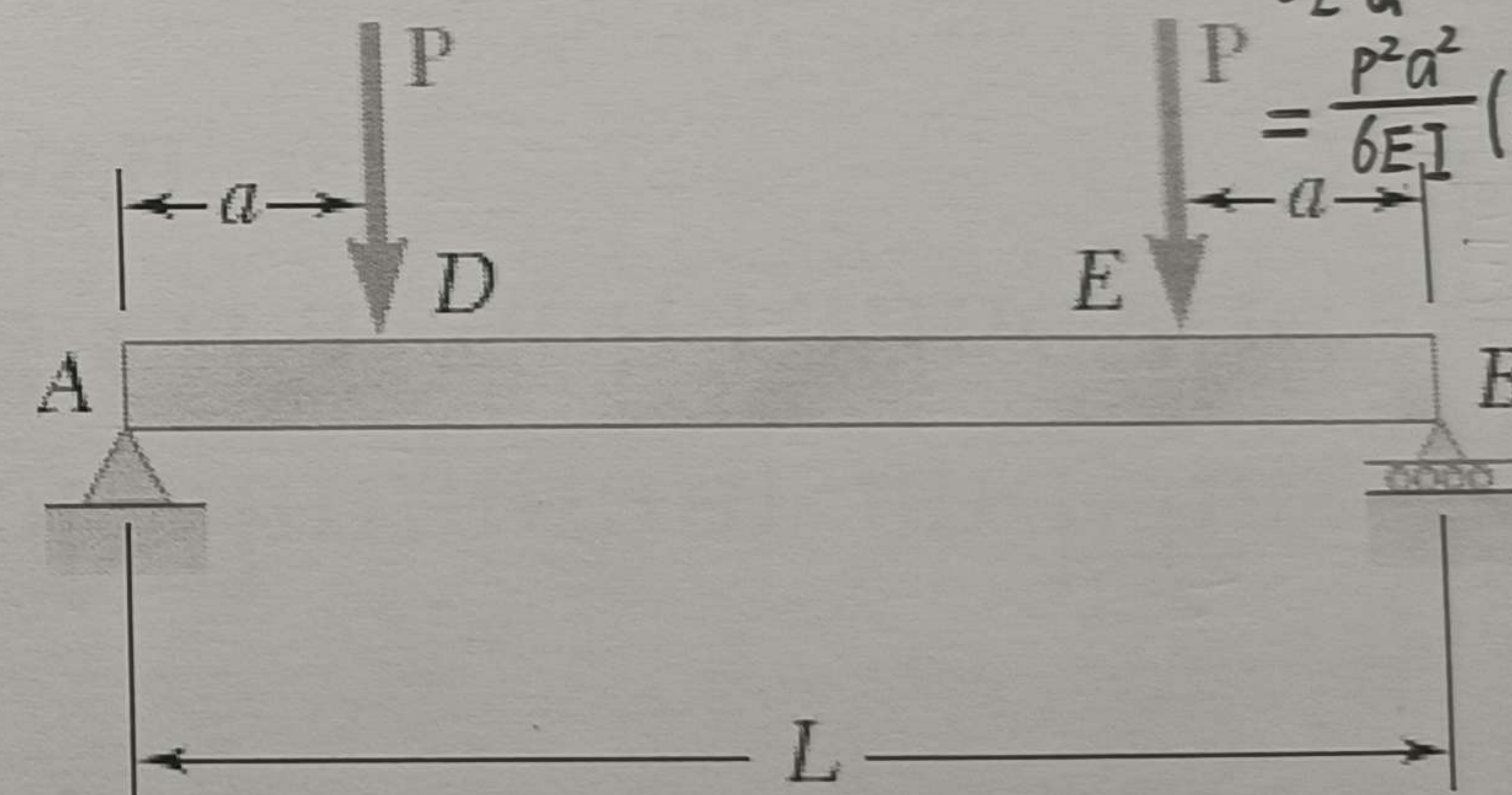
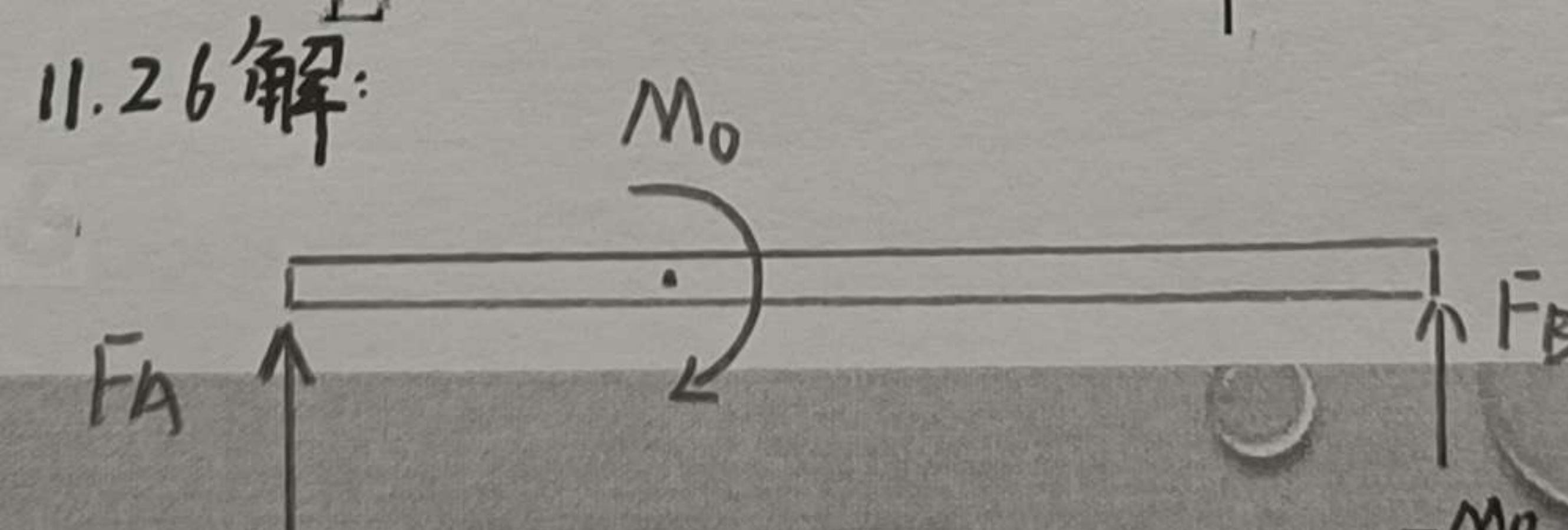


Fig. P11.27

$$\begin{aligned} U &= \int_0^a \frac{M^2(x)}{2EI} dx + \int_a^{a+b} \frac{M^2(x)}{2EI} dx \\ &= \frac{1}{2EI} \int_0^a \frac{M_0^2 x^2}{L^2} dx + \frac{1}{2EI} \int_a^{a+b} \left(M_0^2 + \frac{M_0^2 x^2}{L^2} - \frac{2xM_0^2}{L} \right) dx \\ &= \frac{1}{2EI} \left(\frac{M_0^2}{L^2} \cdot \frac{1}{3} a^3 + M_0^2 \cdot b + \frac{M_0^2}{L^2} \cdot \frac{1}{3} [(a+b)^3 - a^3] - \frac{2M_0^2}{L} [a(a+b) - \frac{1}{2} a^2] \right) \\ &= \frac{M_0^2}{2EI} \left(\frac{a^3 + b^3}{3L^2} \right) = \frac{M_0^2 (a^3 + b^3)}{6EIL^2} \quad \boxed{\text{ANS}} \end{aligned}$$

11.26 解:



$$\begin{aligned} \uparrow \sum F_y = 0: F_A + F_B &= 0 \\ \curvearrowright \sum M_A = 0: -M_0 + F_B \cdot L &= 0 \\ \Rightarrow F_A &= \frac{-M_0}{L} \\ F_B &= \frac{M_0}{L} \\ V(x) &= F_A \langle x-0 \rangle^0 \\ M(x) &= F_A \langle x-0 \rangle^1 + M_0 \langle x-a \rangle^0 = \begin{cases} \frac{-M_0}{L} x & 0 < x < a \\ \frac{-M_0}{L} x + M_0 & a < x < L \end{cases} \end{aligned}$$