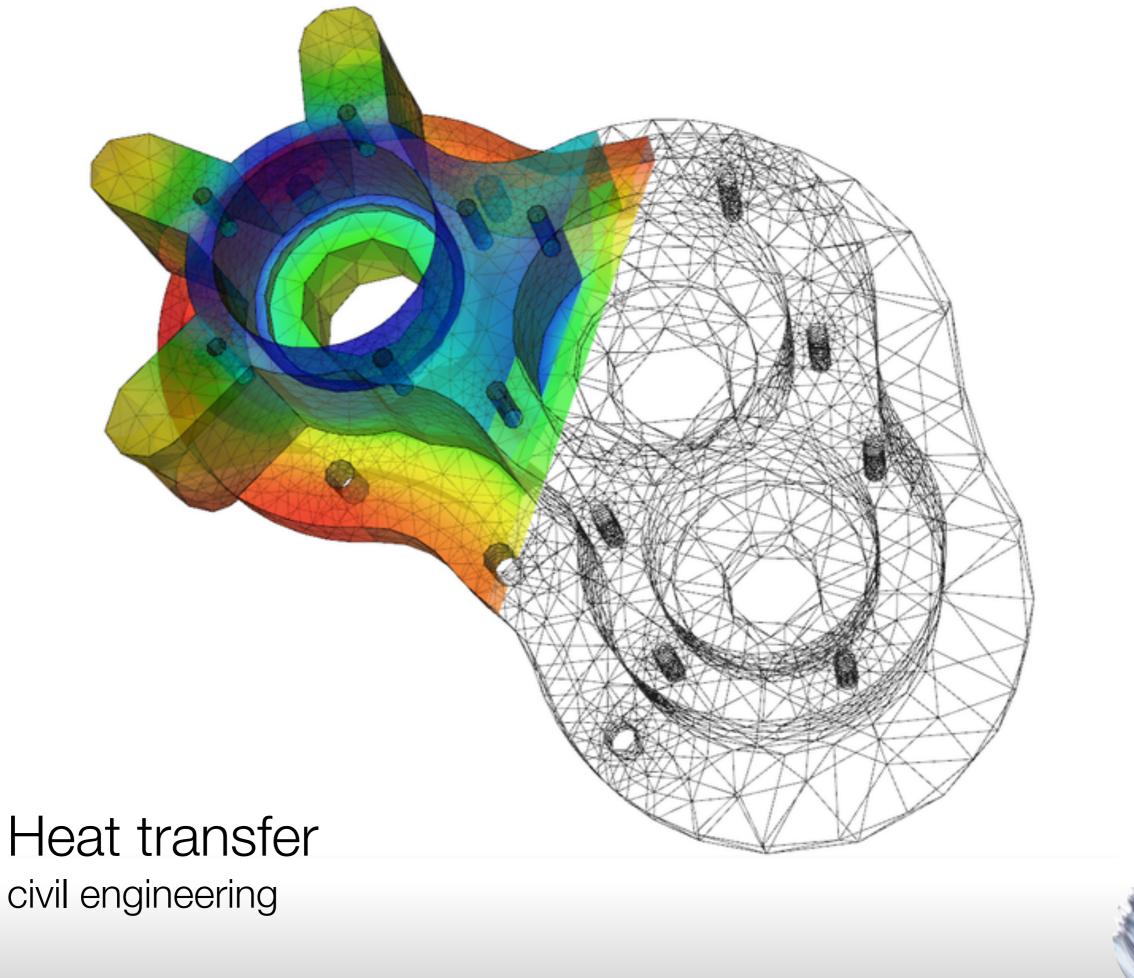
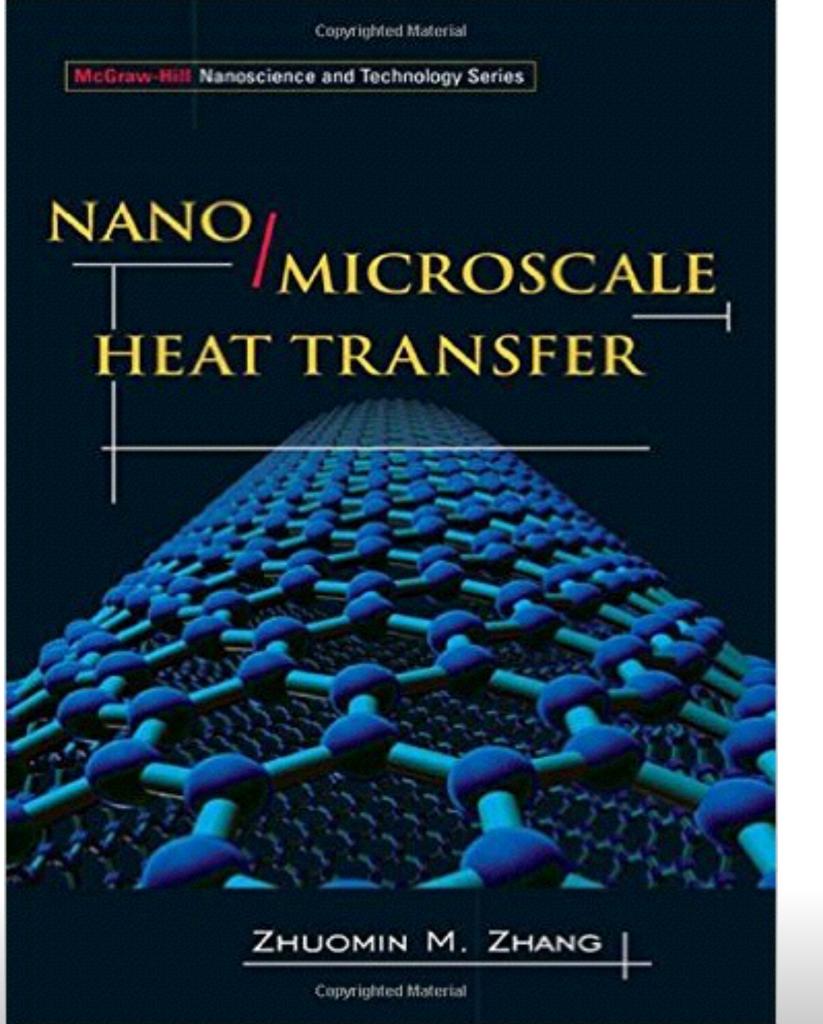
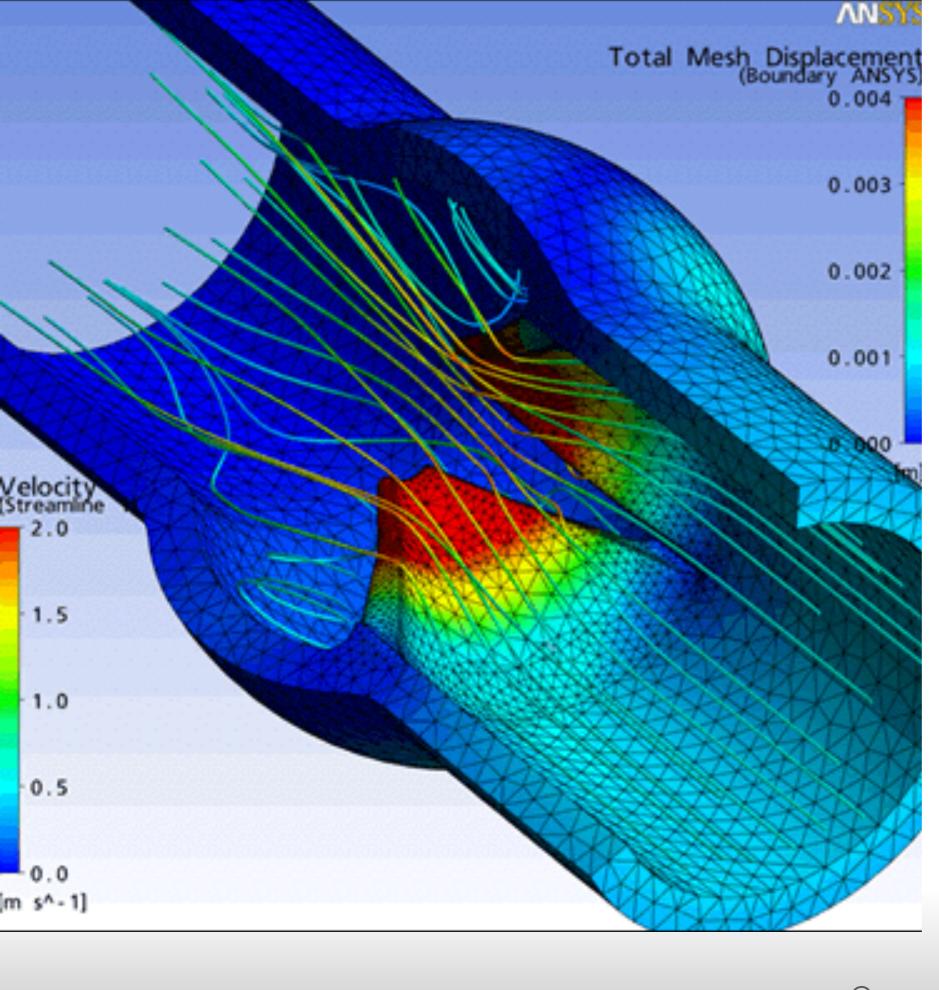
Finite-element methods



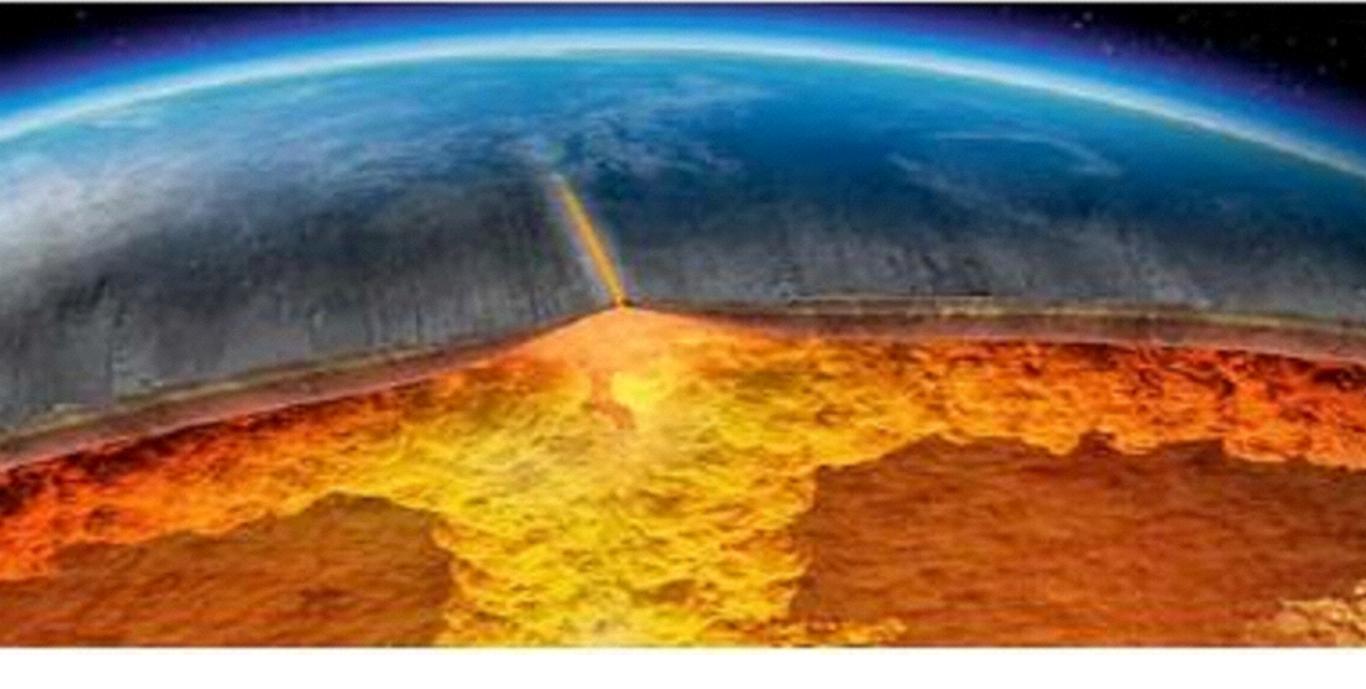


Heat transfer nano-scales

Computational Geophysics

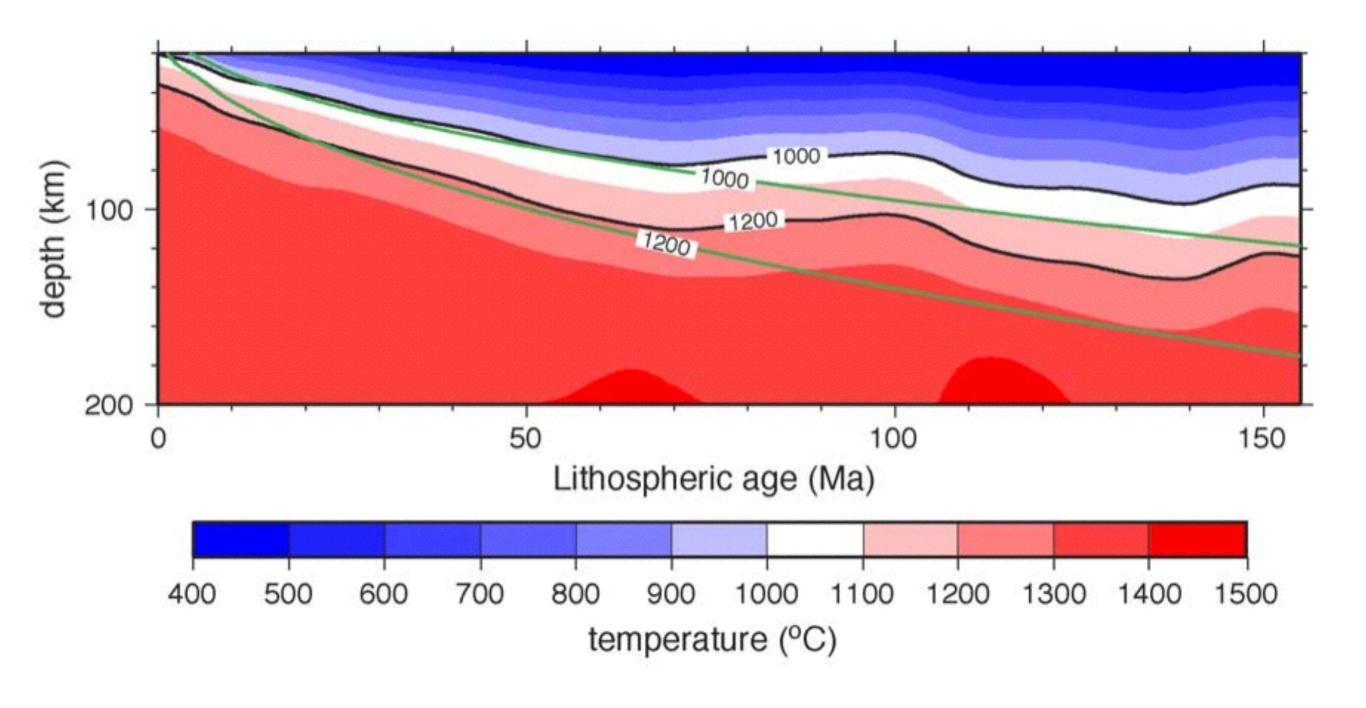


Heat transfer biological tissue

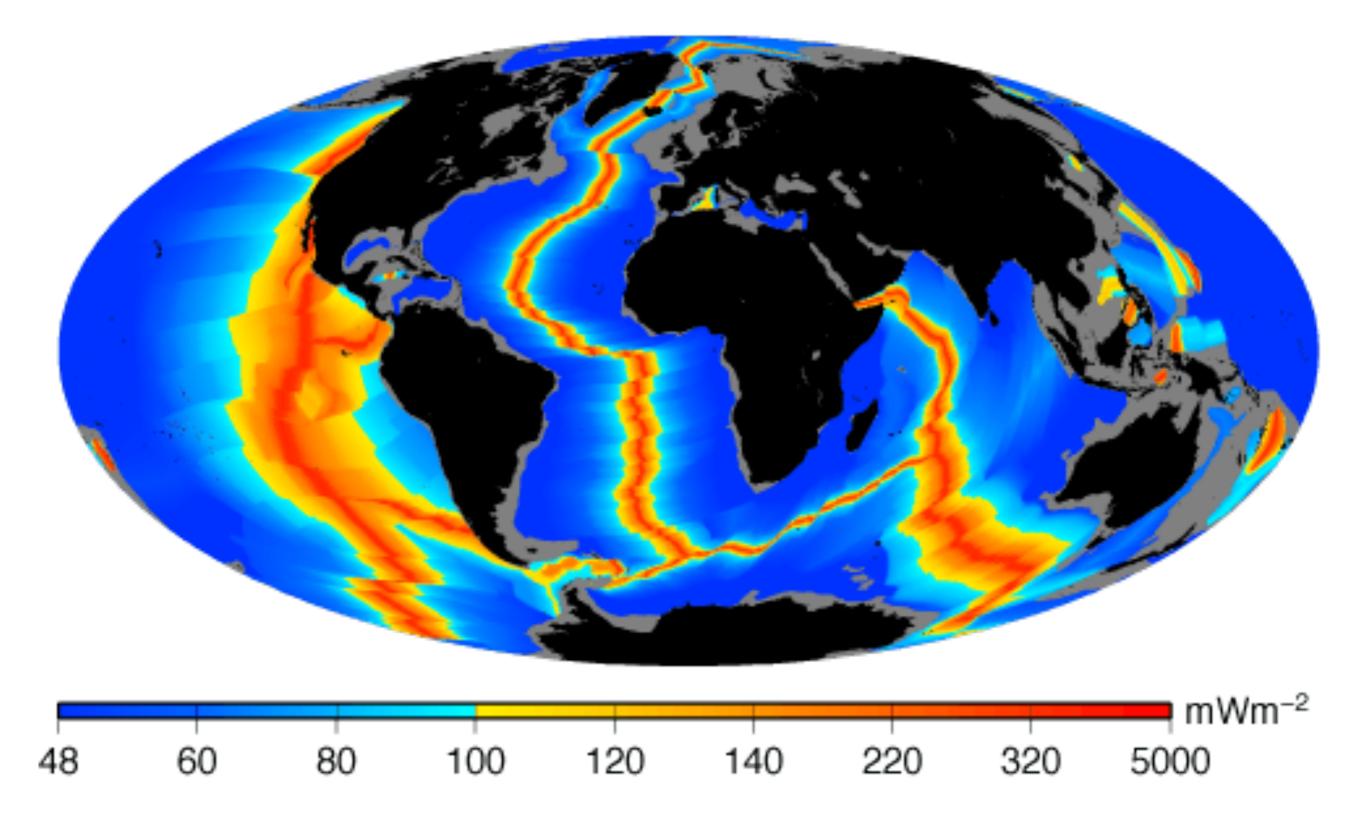


Heat transfer half-space cooling





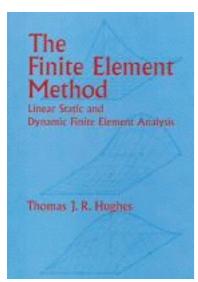
debate: half-space cooling of the Pacific plate Ritzwoller et al. (EPSL, 2004)



debate: geothermal heat transfer into the oceans Labrosse (2009)

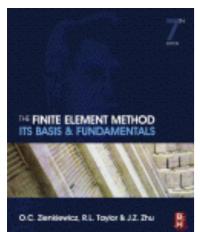
Finite-element literature

books



Thomas J.R. Hughes.

The Finite Element Method: linear static and dynamic finite element analysis, Mineola, N.Y.: Dover, 2000.

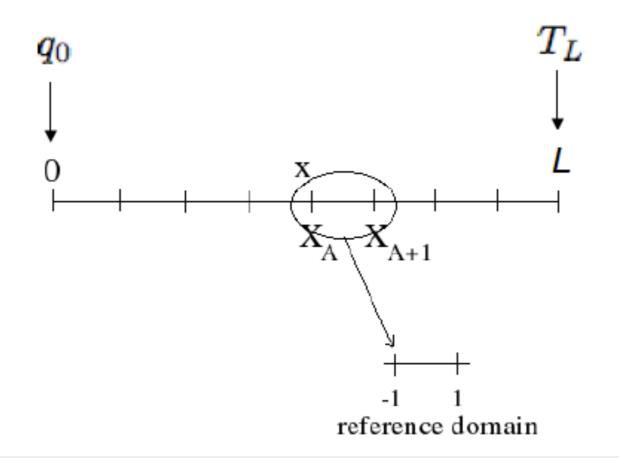


O. C. Zienkiewicz, R. L. Taylor and J. Z. Zhu. **The Finite Element Method:** its basis and fundamentals,

ISBN: 978-1-85617-633-0.

Strong form: $\rho c_p \partial_t T - \partial_x (\kappa \partial_x T) = f$

Boundary conditions:
$$\left\{ \begin{array}{lcl} T(L,t) & = & T_L \\ -\kappa \partial_x T(0,t) & = & q_0 \\ T(x,0) & = & T_0(x) \end{array} \right.$$



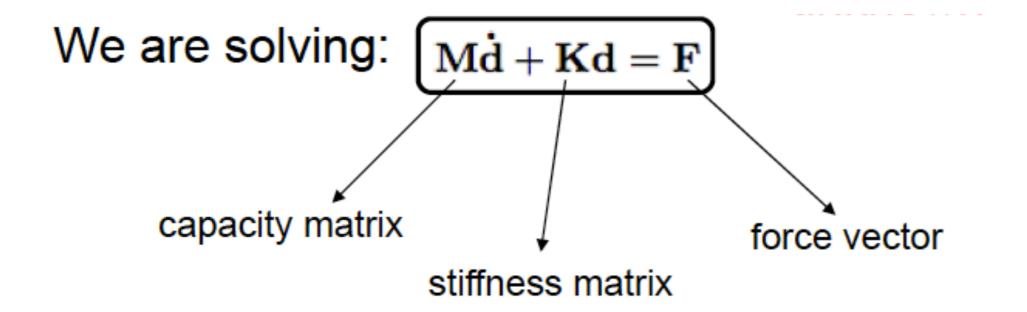
$$\text{Weak form: } \int_0^L \rho c_p w \partial_t T \mathrm{d}x = -\int_0^L \kappa \partial_x w \partial_x T \mathrm{d}x + q_0 w(0) + \int_0^L w f \mathrm{d}x$$

Test function and temperature field expanded on some basis functions:

$$w(x) = \sum_{A=1}^{N} c_A N_A(x)$$

$$T(x) = \sum_{A=1}^{N_{el}} d_A N_A(x) + T_1 N_{n+1}(x)$$

$$\text{Weak form: } \int_0^L \rho c_p w \partial_t T \mathrm{d}x = -\int_0^L \kappa \partial_x w \partial_x T \mathrm{d}x + q_0 w(0) + \int_0^L w f \mathrm{d}x$$



Global level:

$$M_{AB} = (N_A, \rho c_p N_B)$$
$$= \int_0^L \rho c_p N_A N_B dx$$

$$K_{AB} = a(N_A, N_B) = \int_0^L \kappa \partial_x N_A \partial_x N_B dx$$

and

$$F_{A} = (N_{A}, f) + N_{A}(0)q_{0} - a(N_{A}, N_{n+1})T_{L}$$

$$= \int_{0}^{L} N_{A}f dx + N_{A}(0)q_{0} - \int_{0}^{L} \partial_{x}N_{A}\partial_{x}N_{n+1}dx$$

Global level:
$$M_{AB}=\int_0^L \rho c_p N_A N_B \mathrm{d}x$$

$$K_{AB}=\int_0^L \kappa \partial_x N_A \partial_x N_B \mathrm{d}x$$

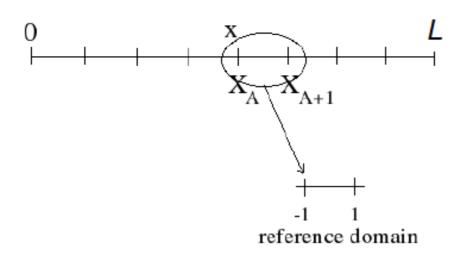
$$F_A=\int_0^L N_A f \mathrm{d}x + N_A(0) q_0 - \int_0^L \partial_x N_A \partial_x N_{n+1} \mathrm{d}x$$

$$\rightarrow$$
 $\mathbf{M}\dot{\mathbf{d}} + \mathbf{K}\mathbf{d} = \mathbf{F}$ where $\dot{\mathbf{d}} = \partial_{\mathbf{t}}\mathbf{d}$

mapping using Jacobian:

$$\int_0^1 g(x) dx = \sum_{\Omega_e} \int_{\Omega_e} g(x) dx = \sum_{\Omega_e} \int_{-1}^1 g(x(\xi)) J d\xi$$

Local level: Consider the mapping $\xi : [X_A, X_{A+1}] \to [\xi_1, \xi_2]$, such that



$$\begin{cases} \xi(X_A) &= \xi_1 = -1 \\ \xi(X_{A+1}) &= \xi_2 = 1 \end{cases}$$

=> Linear shape functions:

$$N_a(\xi) = \frac{1}{2}(1 + \xi_a \xi)$$
 a=1,2

Local (element) resolution:

$$N_a(\xi) = \frac{1}{2}(1 + \xi_a \xi)$$
 a=1,2

Capacity matrix:

$$m_{ab}^e = (N_a,
ho c_p N_b) = \int_{\Omega_e}
ho c_p N_a N_b \mathrm{d}x$$

Change of variables (reference domain)

$$m_{ab}^e = rac{h_e}{2} \int_{-1}^1
ho c_p N_a N_b \mathrm{d} \xi$$

$$m^e = rac{
ho c_p h_e}{6} \left(egin{array}{cc} 2 & 1 \ 1 & 2 \end{array}
ight)$$

Local (element) resolution:

$$N_a(\xi) = \frac{1}{2}(1 + \xi_a \xi)$$
 a=1,2

Stiffness matrix:

$$k_{ab}^e = a(N_a, \kappa N_b) = \int_{\Omega_e} \kappa \partial_x N_a \partial_x N_b \mathrm{d}x$$

 ♣ Change of variables (reference domain)

$$k_{ab}^e = \frac{2}{h_e} \int_{-1}^1 \kappa \partial_{\xi} N_a \partial_{\xi} N_b \mathrm{d}\xi$$

Matricial form

$$k^e = \frac{\kappa}{h_e} \left(\begin{array}{cc} 1 & -1 \\ -1 & 1 \end{array} \right)$$

Local (element) resolution:

$$N_a(\xi) = \frac{1}{2}(1 + \xi_a \xi)$$
 a=1,2

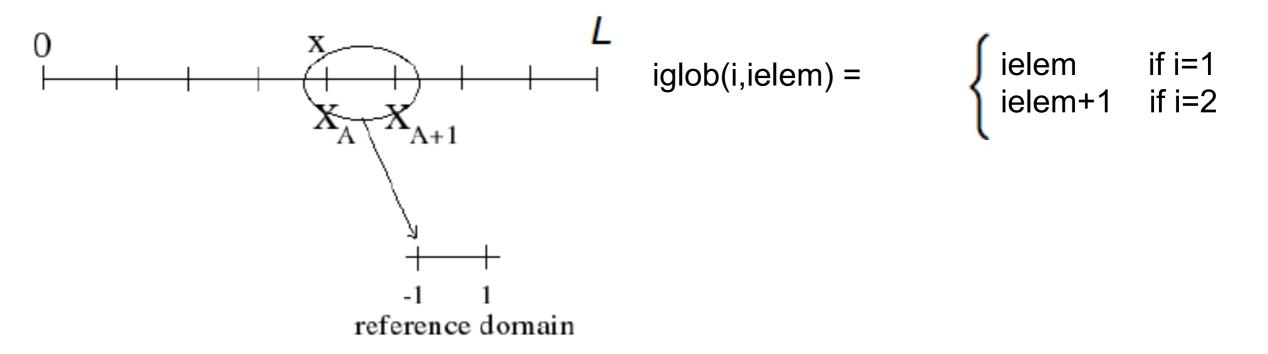
Force vector:
$$f_a^e = \int_{\Omega_e} N_A f \mathrm{d}x + \left\{ \begin{array}{ll} \delta_{a1} q_0 & \text{for } e=1 \\ -k_{a2}^e T_L & \text{for } e=N_{el} \\ 0 & \text{else} \end{array} \right.$$

 ♣ Change of variables (reference domain)

$$f_a^e = \frac{h_e}{2} \int_{-1}^1 N_a f d\xi + \text{boundary terms}$$

$$f^e = \frac{h_e}{6} \left(\begin{array}{c} 2f_1 + f_2 \\ f_1 + 2f_2 \end{array} \right) + \text{boundary terms}$$

Assembling: back to global level



code example:

```
do ielem = 1, nelem
    do i = 1,2
        u(iglobe(i,ielem)) = u(iglobe(i,ielem)) + u_local(i,ielem)
    end
end
```

Time scheme: Predictor-Corrector algorithm

Predictor:

$$d_{n+1} = d_n + (1-\alpha)\Delta t \dot{d}_n$$

 $\dot{d}_{n+1} = 0$ (initialization at the beginning of each time step)

Solve:

$$rhs = F - M\dot{d}_{n+1} - Kd_{n+1}$$

 $\delta\dot{d}_{n+1} = M^{-1}rhs$

Corrector:

$$d_{n+1} = d_{n+1} + \alpha \Delta t \dot{d}_{n+1}
 \dot{d}_{n+1} = \dot{d}_{n+1} + \delta \dot{d}_{n+1}$$

where Δt is the time step.

$$\begin{cases} \alpha = 0 & \text{forward differences} \\ \alpha = 1/2 & \text{midpoint rule} \\ \alpha = 1 & \text{backward differences} \end{cases}$$

FEM solution: initial, simple harmonic function

$$\rho c_p \partial_t T - \partial_x (\kappa \partial_x T) = f = 0$$

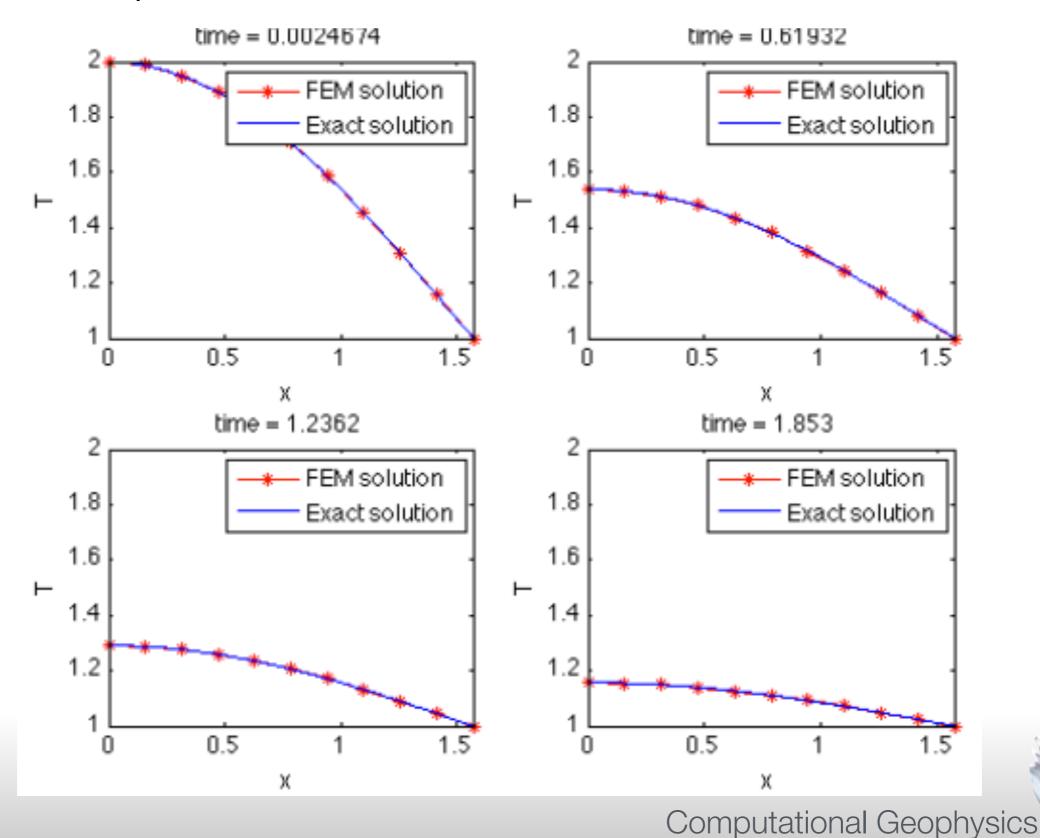
Boundary conditions:

$$\begin{cases} T(L,t) &= T_L = 1 \\ -\kappa \partial_x T(0,t) &= q_0 = 0 \\ T(x,0) &= T_0(x) = 1 + \cos(x) & \text{in [0,L] and } L = \frac{\pi}{2} \end{cases}$$

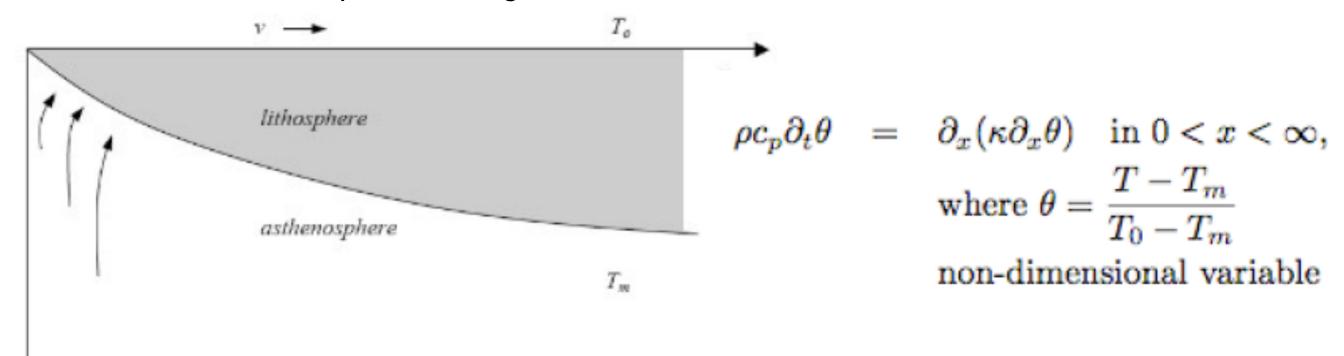
has exact solution:

$$T(x,t) = 1 + e^{-t}\cos(x)$$

FEM solution: simple harmonic function



FEM solution: half-space cooling



Boundary conditions:

$$T(0,t) = T_0$$
 (surface temperature)
 $T(x \to \infty, t) \to T_m$
 $T(x,0) = T_m$ (initial temperature)

has exact solution:

$$\theta = \operatorname{erfc} \frac{x}{2\sqrt{rac{\kappa}{
ho c_p} t}}$$



FEM solution: half-space cooling

