

# Finite Element solution of the fiber/matrix interface crack problem: convergence properties and mode mixity of the Virtual Crack Closure Technique

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## Abstract

*Priority: 3*

*Target journal(s): Engineering Fracture Mechanics, Theoretical and Applied Fracture Mechanics, International Journal of Fracture*

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## 1. Introduction

Bi-material interfaces represent the basic load transfer mechanism at the heart of Fiber Reinforced Polymer Composite (FRPC) materials. They are present at the macroscale, in the form of adhesive joints; at the mesoscale, as  
5 interfaces between layers with different orientations; at the microscale, as fiber-matrix interfaces. Bi-material interfaces have for long attracted the attention of researchers in Fracture Mechanics [1, 2], due to their hidden complexity. The problem was first addressed in the 1950's by Williams [3], who derived through a linear elastic asymptotic analysis the stress distribution around an  
10 *open* crack (with crack faces nowhere in contact for any size of the crack) between two infinite half-planes of dissimilar materials and found the existence of a strong oscillatory behavior in the stress singularity at the crack tip of the form

$$r^{-\frac{1}{2}} \sin(\varepsilon \log r) \quad \text{with} \quad \varepsilon = \frac{1}{2\pi} \log \left( \frac{1-\beta}{1+\beta} \right); \quad (1)$$

in which  $\beta$  is one of the two parameters introduced by Dundurs [4] to characterize bi-material interfaces:

$$\beta = \frac{\mu_2(\kappa_1 - 1) - \mu_1(\kappa_2 - 1)}{\mu_2(\kappa_1 + 1) + \mu_1(\kappa_2 + 1)} \quad (2)$$

15 where  $\kappa = 3 - 4\nu$  in plane strain and  $\kappa = \frac{3-4\nu}{1+\nu}$  in plane stress,  $\mu$  is the shear modulus,  $\nu$  Poisson's coefficient, and indexes 1, 2 refer to the two bulk materials joined at the interface. Defining  $a$  as the length of the crack, it was found that the size of the oscillatory region is in the order of  $10^{-6}a$  [5]. Given the oscillatory behaviour of the crack tip singularity of the stress field of Eq. 1, 20 the definition of Stress Intensity Factor (SIF)  $\lim_{r \rightarrow 0} \sqrt{2\pi r} \sigma$  ceases to be valid as it returns logarithmically infinite terms [1]. Furthermore, it implies that the Mode mixity problem at the crack tip is ill-posed.

It was furthermore observed, always in the context of Linear Elastic Fracture Mechanics (LEFM), that an interpenetration zone exists close to the crack tip [6, 25 7] with a length in the order of  $10^{-4}$  [6]. Following conclusions firstly proposed in [7], the presence of a *contact zone* in the crack tip neighborhood, of a length to be determined from the solution of the elastic problem, was introduced in [8] and shown to provide a physically consistent solution to the straight bi-material interface crack problem.

30 The curved bi-material interface crack, more often referred to as the fiber-matrix interface due to its relevance in FRPCs, was first treated by Perlman and Sih [9], who provided the analytical solution of stress and displacement fields for a circular inclusion with an arbitrary number of cracks. Building on their work, Toya [10] particularized the solution for an inclusion with a single interface crack 35 (or debond) and provided the expression of the Energy Release Rate (ERR) at the crack tip.

## 2. Vectorial formulation of the Virtual Crack Closure Technique (VCCT)

## 3. Formulation of the ERR with respect to the FEM solution's variables

## 40 4. Convergence analysis

### 4.1. Analytical considerations

### 4.2. Numerical results

## 5. Conclusions & Outlook

## Acknowledgements

45 Luca Di Stasio gratefully acknowledges the support of the European School of Materials (EUSMAT) through the DocMASE Doctoral Programme and the European Commission through the Erasmus Mundus Programme.

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