# Constitutive modeling for laminates with fiber/matrix interface cracks under transverse loading

Luca Di Stasio<sup>a</sup>, Janis Varna<sup>a</sup>

<sup>a</sup>Luleå University of Technology, University Campus, SE-97187 Luleå, Sweden

#### Abstract

Keywords: Fiber Reinforced Polymer Composite (FRPC), Debonding, Finite element analysis (FEA)

#### 1. Introduction

Main ref [1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11]

## 2. Derivation of constitutive relations

#### 2.1. Reference frames

5 Local reference frame of k-th layer: index 1 is the in-plane longitudinal or fiber or 0°-direction; index 2 is the in-plane transverse or 90°-direction; index 3 is the out-of-plane or through-the-thickness direction.

Global reference frame of laminate: index x is the in-plane longitudinal or laminate 0° direction; index y is the in-plane transverse direction; index z is the out-of-plane or through-the-thickness direction.

## 2.2. Crack density

10

**Principle 1.** Normalized volume of cracks  $V_{an}$  is the ratio of cracked volume  $V_a$  to material volume V

$$V_{an} = \frac{V_a}{V} \tag{1}$$

 $V_a$  is equal to the product of total crack surface  $S_C$  and average crack opening  $u_a$ 

$$V_{an} = \frac{S_C u_a}{V} = \frac{S_C}{V} u_a = \rho_C u_a \tag{2}$$

The ratio  $\frac{S_C}{V}$  has a size of  $\frac{1}{length}$  and correspond to the crack density  $\rho_C$ . It means: product of crack density and average crack opening is equal to normalized volume of cracks.

Applying the previous Principle to debonds, we have:

$$\rho_{D} = \frac{\text{total area of debonds}}{\text{total layer volume}} = \frac{n_{D}wR_{f}\Delta\theta}{L_{lam}wt_{90^{\circ}}} = \frac{n_{D}w}{L_{lam}wt_{90^{\circ}}}R_{f}\Delta\theta = \frac{1}{n2L}\frac{1}{k2L}R_{f}\Delta\theta = \frac{1}{nk4L^{2}}R_{f}\Delta\theta = \frac{V_{f}}{nk\pi R_{f}^{2}}R_{f}\Delta\theta = \frac{V_{f}}{nkR_{f}}\frac{\Delta\theta}{\pi}$$
(3)

### 20 2.3. Homogenization

$$\sigma_{ij}^{avg} = \frac{1}{V} \int_{V} \sigma_{ij} dV \quad \varepsilon_{ij}^{avg} = \frac{1}{V} \int_{V} \varepsilon_{ij} dV \tag{4}$$

$$\underline{\tilde{\sigma}}_{k}^{avg} = \underline{\tilde{Q}}_{k} \left( \underline{\tilde{\varepsilon}}_{k}^{avg} - \underline{\tilde{\alpha}}_{k} \Delta T \right) \tag{5}$$

$$\underline{\tilde{\sigma}}_{LAM} = \underline{\tilde{\sigma}}^{avg} = \frac{1}{V} \int_{V} \underline{\tilde{\sigma}} dV = \frac{1}{V} \sum_{k=1}^{N} \int_{V_{k}} \underline{\tilde{\sigma}} dV_{k} = \sum_{k=1}^{N} \underline{\tilde{\sigma}}_{k}^{avg} \frac{t_{k}}{h}$$
 (6)

$$\varepsilon_{ij}^{avg} = \frac{1}{V} \int_{V} \varepsilon_{ij} dV = \frac{1}{V} \int_{V} \frac{1}{2} (u_{i,j} + u_{j,i}) dV = \frac{1}{V} \int_{S} \frac{1}{2} (u_{i}n_{j} + u_{j}n_{i}) dS \quad (7)$$

$$\varepsilon_{ij}^{avg} = \frac{1}{V} \int_{S} \frac{1}{2} (u_{i}n_{j} + u_{j}n_{i}) dS = 
= \frac{1}{V} \int_{S_{B}} \frac{1}{2} (u_{i}n_{j} + u_{j}n_{i}) dS + \frac{1}{V} \int_{S_{C}} \frac{1}{2} (u_{i}n_{j} + u_{j}n_{i}) dS = 
= \varepsilon_{ij}^{applied} + \beta_{ij}$$
(8)

$$\underline{\tilde{\varepsilon}}_{k}^{avg} = \underline{\tilde{\varepsilon}}_{k}^{applied} + \underline{\tilde{\beta}}_{k} = \underline{\tilde{\varepsilon}}_{k}^{LAM} + \underline{\tilde{\beta}}_{k} \tag{9}$$

$$\underline{\tilde{\sigma}}_{LAM} = \frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k \left( \underline{\tilde{\varepsilon}}_k^{LAM} - \underline{\tilde{\alpha}}_k \Delta T + \underline{\tilde{\beta}}_k \right)$$
 (10)

$$\underline{\tilde{\sigma}}_{LAM} = \underline{\underline{Q}}_{eff}^{LAM} \underline{\tilde{\varepsilon}}^{LAM} \tag{11}$$

$$\underline{\underline{Q}}_{eff}^{LAM} \underline{\tilde{\varepsilon}}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k\right) \underline{\tilde{\varepsilon}}^{LAM} + \frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k \underline{\tilde{\beta}}_k \tag{12}$$

$$\underline{\underline{Q}}_{eff}^{LAM} \underline{\underline{\tilde{\varepsilon}}}^{LAM} \cdot \underline{\underline{\tilde{\varepsilon}}}^{LAM} \cdot \underline{\underline{\tilde{\varepsilon}}}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k\right) \underline{\tilde{\varepsilon}}^{LAM} \cdot \underline{\underline{\tilde{\varepsilon}}}^{LAM} \cdot \underline{\underline{\tilde{\varepsilon}}}^{LAM} + \left(\frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k \underline{\tilde{\rho}}_k\right) \cdot \underline{\underline{\tilde{\varepsilon}}}^{LAM} \cdot \underline{\underline{\tilde{\varepsilon}}}^{LAM} \cdot \underline{\tilde{\varepsilon}}^{LAM}$$

$$(13)$$

$$\underline{\underline{Q}}_{eff}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k\right) + \frac{1}{h} \sum_{k=1}^{N} t_k \underline{\underline{\tilde{Q}}}_k \underline{\underline{\tilde{g}}}_k^{LAM} \cdot \underline{\underline{\tilde{g}}}^{LAM}$$
(14)

$$\underline{\underline{T}}_{k} = \begin{bmatrix}
\cos^{2}(\theta_{k}) & \sin^{2}(\theta_{k}) & 2\cos(\theta_{k})\sin(\theta_{k}) \\
\sin^{2}(\theta_{k}) & \cos^{2}(\theta_{k}) & -2\cos(\theta_{k})\sin(\theta_{k}) \\
-\cos(\theta_{k})\sin(\theta_{k}) & \cos(\theta_{k})\sin(\theta_{k}) & \cos^{2}(\theta_{k}) - \sin^{2}(\theta_{k})
\end{bmatrix}$$
(15)

$$\underline{\underline{\tilde{Q}}}_{k} = \underline{\underline{T}}_{k}^{-1} \underline{\underline{Q}}_{k} \left(\underline{\underline{T}}_{k}^{-1}\right)^{T} \tag{16}$$

$$\underline{\underline{Q}}_{eff}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^{N} t_{k} \underline{\underline{T}}_{k}^{-1} \underline{\underline{Q}}_{k} \left(\underline{\underline{T}}_{k}^{-1}\right)^{T}\right) + \frac{1}{h} \sum_{k=1}^{N} t_{k} \underline{\underline{T}}_{k}^{-1} \underline{\underline{Q}}_{k} \left(\underline{\underline{T}}_{k}^{-1}\right)^{T} \underline{\underline{\hat{\beta}}}_{k} \cdot \underline{\underline{\hat{\varepsilon}}}^{LAM} = \\
= \frac{1}{h} \sum_{k=1}^{N} t_{k} \underline{\underline{T}}_{k}^{-1} \underline{\underline{Q}}_{k} \left(\underline{\underline{T}}_{k}^{-1}\right)^{T} \left(1 + \underline{\underline{\hat{\beta}}}_{k} \cdot \underline{\underline{\hat{\varepsilon}}}^{LAM}\right) \tag{17}$$

$$Q_{eff,lmij}^{LAM} \tilde{\varepsilon}_{ij}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^{N} t_k \tilde{Q}_{k,lmij}\right) \tilde{\varepsilon}_{ij}^{LAM} + \frac{1}{h} \sum_{k=1}^{N} t_k \tilde{Q}_{k,lmij} \tilde{\beta}_{k,ij}$$
(18)

### 2.4. Vakulenko-Kachanov tensor

In the local reference frame of k-th layer, the outer normal at crack faces has components:

$$n_1 = 0 \quad n_2 \neq 0 \quad n_3 \neq 0 \tag{19}$$

while crack face displacement has components:

$$u_1 = 0 \quad u_2 \neq 0 \quad u_3 \neq 0 \tag{20}$$

Definition of Vakulenko-Kachanov tensor:

$$\beta_{ij} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_i n_j + u_j n_i) dS$$
 (21)

Expand the expression for each component and simplify based on the fact that  $u_1 = 0$ :

$$\beta_{11} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_1 n_1 + u_1 n_1) dS = \frac{1}{V_k} \int_{S_C} \mathcal{U}_1 \cdot 0 n_1 dS = 0$$

$$\beta_{22} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 n_2 + u_2 n_2) dS = \frac{1}{V_k} \int_{S_C} u_2 n_2 dS$$

$$\beta_{33} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 n_3 + u_3 n_3) dS = \frac{1}{V_k} \int_{S_C} u_3 n_3 dS$$

$$\beta_{12} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (\mathcal{U}_1 \cdot 0 n_2 + u_2 \mathcal{U}_1 \cdot 0) dS = 0$$

$$\beta_{13} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (\mathcal{U}_1 \cdot 0 n_3 + u_3 \mathcal{U}_1 \cdot 0) dS = 0$$

$$\beta_{23} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 n_3 + u_3 n_2) dS$$

$$\beta_{21} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 \mathcal{U}_1 \cdot 0 + \mathcal{U}_1 \cdot 0 n_2) dS = 0$$

$$\beta_{31} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 \mathcal{U}_1 \cdot 0 + \mathcal{U}_1 \cdot 0 n_3) dS = 0$$

$$\beta_{32} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 n_2 + u_2 n_3) dS = \beta_{23}$$

Only 3 independent components of the tensor  $\beta_{ij}$  remain:  $\beta_{22}$ ,  $\beta_{33}$  and  $\beta_{23}$ . Split total crack surface  $S_C$  into total matrix crack surface  $S_C^m$  and total fiber crack surface  $S_C^f$  and remember that  $n_i^f = -n_i^m$  for i = 2, 3

$$\beta_{22} = \frac{1}{V_k} \int_{S_C} u_2 n_2 dS = \frac{1}{V_k} \left[ \int_{S_C^m} u_2^m n_2^m dS + \int_{S_C^f} u_2^f n_2^f dS \right] =$$

$$= \frac{1}{V_k} \left[ \int_{S_C^m} u_2^m n_2^m dS + \int_{S_C^f} u_2^f (-n_2^m) dS \right]$$

$$\beta_{33} = \frac{1}{V_k} \int_{S_C} u_3 n_3 dS = \frac{1}{V_k} \left[ \int_{S_C^m} u_3^m n_3^m dS + \int_{S_C^f} u_3^f n_3^f dS \right] =$$

$$= \frac{1}{V_k} \left[ \int_{S_C^m} u_3^m n_3^m dS + \int_{S_C^f} u_3^f (-n_3^m) dS \right]$$

$$\beta_{23} = \frac{1}{V_k} \int_{S_C} (u_2 n_3 + u_3 n_2) dS =$$

$$= \frac{1}{V_k} \left[ \int_{S_C^m} (u_2^m n_3^m + u_3^m n_2^m) dS + \int_{S_C^f} \left( u_2^f n_3^f + u_3^f n_2^f \right) dS \right] =$$

$$= \frac{1}{V_k} \left[ \int_{S_C^m} u_2^m n_3^m dS + \int_{S_C^f} u_2^f (-n_3^m) dS + \int_{S_C^m} u_3^m n_2^m dS + \int_{S_C^f} u_3^f (-n_2^m) dS \right]$$

$$(23)$$

The total matrix debonded surface  $S_C^m$  is equal to the total fiber debonded surface  $S_C^f$  and equal to:

$$S_C^m = S_C^f = n_D R_f \Delta \theta \tag{24}$$

With Eq. 24, we can recast Eq. 23 as

$$\beta_{22} = \frac{1}{V_k} \left[ n_D R_f w \int_0^{\Delta \theta} \left( u_2^m - u_2^f \right) n_2^m d\theta \right] =$$

$$= \frac{1}{L_{lam} w t_{90^{\circ}}} \left[ n_D R_f w \int_0^{\Delta \theta} \left( u_2^m - u_2^f \right) n_2^m d\theta \right] =$$

$$= \frac{1}{L_{lam}} \frac{n_D R_f}{t_{90^{\circ}}} \left[ \int_0^{\Delta \theta} \left( u_2^m - u_2^f \right) n_2^m d\theta \right] =$$

$$= \rho_D \left[ \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left( u_2^m - u_2^f \right) n_2^m d\theta \right]$$

$$\beta_{33} = \rho_D \left[ \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left( u_3^m - u_3^f \right) n_3^m d\theta \right]$$

$$\beta_{23} = \rho_D \left[ \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left( u_2^m - u_2^f \right) n_3^m d\theta + \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left( u_3^m - u_3^f \right) n_2^m d\theta \right]$$

We can express the displacement jumps at the interface as a function of
the local Crack Opening Displacement (COD) and Crack Sliding Displacement
(CSD) as

$$u_{2}^{m} - u_{2}^{f} = \left(u_{r}^{m} - u_{r}^{f}\right)\cos\left(\theta\right) - \left(u_{\theta}^{m} - u_{\theta}^{f}\right)\sin\left(\theta\right) =$$

$$= COD\left(\theta\right)\cos\left(\theta\right) - CSD\left(\theta\right)\sin\left(\theta\right)$$

$$u_{3}^{m} - u_{3}^{f} = \left(u_{r}^{m} - u_{r}^{f}\right)\sin\left(\theta\right) + \left(u_{\theta}^{m} - u_{\theta}^{f}\right)\cos\left(\theta\right) =$$

$$= COD\left(\theta\right)\sin\left(\theta\right) + CSD\left(\theta\right)\cos\left(\theta\right)$$

$$(26)$$

where  $\theta$  is the local angular coordinate at the interface. We can similarly express  $n_2^m$  and  $n_3^m$  as a function of  $\theta$ :

$$n_2^m = \cos(\theta) - \sin(\theta)$$

$$n_3^m = \sin(\theta) + \cos(\theta)$$
(27)

Thus, Eq. 25 becomes

$$\begin{split} \beta_{22} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[ COD\left(\theta\right) \left( \cos^2\left(\theta\right) - \cos\left(\theta\right) \sin\left(\theta\right) \right) - CSD\left(\theta\right) \left( \sin\left(\theta\right) \cos\left(\theta\right) - \sin^2\left(\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{2\Delta \theta} \int_0^{\Delta \theta} \left[ COD\left(\theta\right) \left( 1 + \cos\left(2\theta\right) - \sin\left(2\theta\right) \right) + CSD\left(\theta\right) \left( 1 - \cos\left(2\theta\right) - \sin\left(2\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[ \frac{COD\left(\theta\right) + CSD\left(\theta\right)}{2} \left( 1 - \sin\left(2\theta\right) \right) + \frac{COD\left(\theta\right) - CSD\left(\theta\right)}{2} \cos\left(2\theta\right) \right] d\theta \\ \beta_{33} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[ COD\left(\theta\right) \left( \sin\left(\theta\right) \cos\left(\theta\right) + \sin^2\left(\theta\right) \right) + CSD\left(\theta\right) \left( \cos^2\left(\theta\right) + \cos\left(\theta\right) \sin\left(\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{2\Delta \theta} \int_0^{\Delta \theta} \left[ COD\left(\theta\right) \left( 1 + \sin\left(2\theta\right) - \cos\left(2\theta\right) \right) + CSD\left(\theta\right) \left( 1 + \sin\left(2\theta\right) + \cos\left(2\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[ \frac{COD\left(\theta\right) + CSD\left(\theta\right)}{2} \left( 1 + \sin\left(2\theta\right) \right) - \frac{COD\left(\theta\right) - CSD\left(\theta\right)}{2} \cos\left(2\theta\right) \right] d\theta \\ \beta_{23} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} COD\left(\theta\right) \left( 2\sin\left(\theta\right) \cos\left(\theta\right) + \cos^2\left(\theta\right) - \sin^2\left(\theta\right) \right) + \\ &- \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} CSD\left(\theta\right) \left( \sin^2\left(\theta\right) - \cos^2\left(\theta\right) + 2\cos\left(\theta\right) \sin\left(\theta\right) \right) d\theta = \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} 2 \left[ \frac{COD\left(\theta\right) + CSD\left(\theta\right)}{2} \cos\left(2\theta\right) + \frac{COD\left(\theta\right) - CSD\left(\theta\right)}{2} \sin\left(2\theta\right) \right] d\theta \\ \left( 28 \right) \end{split}$$

# <sup>40</sup> 2.5. Analytical modeling of $COD(\theta)$ and $CSD(\theta)$

The Crack Opening Displacement (COD) and Crack Sliding Displacement (CSD) are in general a function of  $\theta$ , the angular coordinate along the crack which varies between 0 and  $\Delta\theta$ . Without making any approximation, the Crack Opening Displacement (COD) and Crack Sliding Displacement (CSD) can be expressed as the sum of their average value and a term, respectively  $\delta COD(\theta)$ 

and  $\delta CSD(\theta)$ , that represents the variation of the function from its average:

$$COD(\theta) = COD_{avg} + \delta COD(\theta)$$

$$CSD(\theta) = CSD_{avg} + \delta CSD(\theta).$$
(29)

By defining  $\Delta\Psi$ 

$$\Delta\Psi = \min\left(\Delta\theta, \Delta\Phi\right),\tag{30}$$

we introduce at this point an approximation and assume that the functions  $\delta COD\left(\theta\right)$  and  $\delta CSD\left(\theta\right)$  can be expressed as the product of the maximum value of the displacement and a function, respectively  $f\left(\theta - \frac{\Delta\Psi}{2}\right)$  and  $g\left(\theta - \frac{\Delta\theta}{2}\right)$ :

$$COD(\theta) = COD_{avg} + \delta COD(\theta) = COD_{avg} + COD_{max} f\left(\theta - \frac{\Delta \Psi}{2}\right)$$

$$CSD(\theta) = CSD_{avg} + \delta CSD(\theta) = CSD_{avg} + CSD_{max} g\left(\theta - \frac{\Delta \theta}{2}\right),$$
(31)

where  $f\left(\theta - \frac{\Delta\Psi}{2}\right)$  and  $g\left(\theta - \frac{\Delta\theta}{2}\right)$  are assumed to be odd functions over their respective integration domain  $[0, \Delta\Psi]$  and  $[0, \Delta\theta]$ 

$$\int_{0}^{\Delta\theta} f\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = 0 \quad \int_{0}^{\Delta\theta} g\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = 0. \tag{32}$$

We assume the two functions  $f\left(\theta - \frac{\Delta\Psi}{2}\right)$  and  $g\left(\theta - \frac{\Delta\theta}{2}\right)$  to be two odd polynomials of degree 2n-1:

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \begin{cases} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} & 0 \le \theta \le \Delta\Psi \\ 0 & otherwise \end{cases}$$

$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \begin{cases} \sum_{k=0}^{n-1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} & 0 \le \theta \le \Delta\theta \\ 0 & otherwise \end{cases}$$

$$(33)$$

which satisfy by construction the conditions expressed in Equation 32. The coefficients  $a_{2k+1}$  and  $b_{2k+1}$  are determined by imposing that

$$COD(\Delta \Psi) = 0$$

$$CSD(\Delta \theta) = 0.$$
(34)

The explicit construction of the polynomials  $f\left(\theta-\frac{\Delta\Psi}{2}\right)$  and  $g\left(\theta-\frac{\Delta\theta}{2}\right)$  for n=1,2,3 (or degree 2n-1=1,3,5) is reported in Appendix A.

We recall the expressions of the non-zero components of the Vakulenko-Kachanov

50 tensor

$$\beta_{22} = \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left[ \frac{COD(\theta) + CSD(\theta)}{2} \left( 1 - \sin(2\theta) \right) + \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta$$

$$\beta_{33} = \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left[ \frac{COD(\theta) + CSD(\theta)}{2} \left( 1 + \sin(2\theta) \right) - \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta$$

$$\beta_{23} = \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} 2 \left[ \frac{COD(\theta) + CSD(\theta)}{2} \cos(2\theta) + \frac{COD(\theta) - CSD(\theta)}{2} \sin(2\theta) \right] d\theta$$

$$(35)$$

and proceed to the integration of the different summands:

1.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD(\theta) d\theta =$$

$$= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left( COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left( \theta - \frac{\Delta\Psi}{2} \right)^{2k+1} \right) d\theta =$$

$$= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD_{avg} d\theta +$$

$$+ \frac{1}{\Delta\theta} \int_{0}^{\Delta\Psi} COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left( \theta - \frac{\Delta\Psi}{2} \right)^{2k+1} d\theta +$$

$$+ \frac{1}{\Delta\theta} \int_{\Delta\Psi}^{\Delta\theta} COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left( \theta - \frac{\Delta\Psi}{2} \right)^{2k+1} d\theta =$$

$$= \frac{1}{\Delta\theta} \left[ COD_{avg} \theta \right]_{0}^{\Delta\theta} + \frac{1}{\Delta\theta} \left[ COD_{max} \sum_{k=0}^{n-1} \frac{a_{2k+1}}{2(k+1)} \left( \theta - \frac{\Delta\Psi}{2} \right)^{2(k+1)} \right]_{0}^{\Delta\Psi} =$$

$$= COD_{avg} + COD_{max} \sum_{k=0}^{n-1} \frac{a_{2k+1}}{2(k+1)\Delta\theta} \left( \left( \frac{\Delta\Psi}{2} \right)^{2(k+1)} - \left( -\frac{\Delta\Psi}{2} \right)^{2(k+1)} \right) =$$

$$= COD_{avg}$$

$$(36)$$

2.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} CSD\left(\theta\right) d\theta = CSD_{avg} \tag{37}$$

3.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD(\theta) \sin(2\theta) d\theta =$$

$$= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left( COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \theta^{2k+1} \right) \sin(2\theta) d\theta =$$

$$= -\frac{1}{2\Delta\theta} COD_{avg} \left[ \cos(2\theta) \right]_{0}^{\Delta\theta} +$$

$$+ \frac{1}{\Delta\theta} \left[ COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin(\frac{1+mod(i,2)}{2}\pi - 2\theta) \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \theta^{k-i} \right) \right]_{0}^{\Delta\Psi} =$$

$$= \frac{1-\cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} +$$

$$+ \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin(\frac{1+mod(i,2)}{2}\pi - 2\Delta\Psi) \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)$$
(38)

$$\begin{split} &\frac{1}{\Delta\theta}\int_{0}^{\Delta\theta}CSD\left(\theta\right)\sin\left(2\theta\right)d\theta = \\ &= \frac{1}{\Delta\theta}\int_{0}^{\Delta\theta}\left(CSD_{avg} + CSD_{max}\sum_{k=0}^{n-1}b_{2k+1}\theta^{2k+1}\right)\sin\left(2\theta\right)d\theta = \\ &= -\frac{1}{2\Delta\theta}CSD_{avg}\left[\cos\left(2\theta\right)\right]\bigg|_{0}^{\Delta\theta} + \\ &+ \frac{1}{\Delta\theta}\left[CSD_{max}\sum_{i=0}^{2n-1}\left(-\frac{1}{2}\right)^{i+1}\sin(\frac{1+mod\left(i,2\right)}{2}\pi - 2\theta)\left(\sum_{k=i}^{2n-1}b_{k}\frac{k!}{(k-i)!}\theta^{k-i}\right)\right]\bigg|_{0}^{\Delta\Psi} = \\ &= \frac{1-\cos\left(2\Delta\theta\right)}{2\Delta\theta}CSD_{avg} + \\ &+ \frac{1}{\Delta\theta}CSD_{max}\sum_{i=0}^{2n-1}\left(-\frac{1}{2}\right)^{i+1}\sin(\frac{1+mod\left(i,2\right)}{2}\pi - 2\Delta\Psi)\left(\sum_{k=i}^{2n-1}b_{k}\frac{k!}{(k-i)!}\Delta\Psi^{k-i}\right) \end{split}$$

5.

$$\begin{split} &\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD\left(\theta\right) \cos\left(2\theta\right) d\theta = \\ &= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left( COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \theta^{2k+1} \right) \cos\left(2\theta\right) d\theta = \\ &= \frac{1}{2\Delta\theta} COD_{avg} \left[ \sin\left(2\theta\right) \right] \Big|_{0}^{\Delta\theta} + \\ &+ \frac{1}{\Delta\theta} \left[ COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin\left( \frac{1 + mod\left(i+1,2\right)}{2} \pi - 2\theta \right) \left( \sum_{k=i}^{2n-1} a_{k} \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \Big|_{0}^{\Delta\Psi} = \\ &= \frac{\sin\left(2\Delta\theta\right)}{2\Delta\theta} COD_{avg} + \\ &+ \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin\left( \frac{1 + mod\left(i+1,2\right)}{2} \pi - 2\Delta\Psi \right) \left( \sum_{k=i}^{2n-1} a_{k} \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right) \end{split} \tag{40}$$

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} CSD(\theta) \cos(2\theta) d\theta = 
= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left( CSD_{avg} + CSD_{max} \sum_{k=0}^{n-1} b_{2k+1} \theta^{2k+1} \right) \cos(2\theta) d\theta = 
= -\frac{1}{2\Delta\theta} CSD_{avg} \left[ \cos(2\theta) \right]_{0}^{\Delta\theta} + 
+ \frac{1}{\Delta\theta} \left[ CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin(\frac{1 + mod(i+1,2)}{2}\pi - 2\theta) \left( \sum_{k=i}^{2n-1} b_{k} \frac{k!}{(k-i)!} \theta^{k-i} \right) \right]_{0}^{\Delta\Psi} = 
= \frac{\sin(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + 
+ \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin(\frac{1 + mod(i+1,2)}{2}\pi - 2\Delta\Psi) \left( \sum_{k=i}^{2n-1} b_{k} \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)$$
(41)

Finally we can compute the expressions of the components of the Vakulenko-Kachanov tensor:

1.  $\beta_{22}$ 

$$\begin{split} \beta_{22} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_{0}^{\Delta \theta} \left[ \frac{COD(\theta) + CSD(\theta)}{2} \left( 1 - \sin{(2\theta)} \right) + \frac{COD(\theta) - CSD(\theta)}{2} \cos{(2\theta)} \right] d\theta \\ &= \frac{\rho_D}{2} \left[ COD_{avg} + CSD_{avg} \right] + \\ &- \frac{\rho_D}{2} \frac{1 - \cos{(2\Delta \theta)}}{2\Delta \theta} COD_{avg} - \frac{\rho_D}{2} \frac{1 - \cos{(2\Delta \theta)}}{2\Delta \theta} CSD_{avg} + \\ &- \frac{\rho_D}{2} \frac{1}{\Delta \theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin{(\frac{1 + mod(i, 2)}{2}\pi - 2\Delta \Psi)} \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} \frac{1}{\Delta \theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin{(\frac{1 + mod(i, 2)}{2}\pi - 2\Delta \Psi)} \left( \sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} \frac{\sin{(2\Delta \theta)}}{2\Delta \theta} COD_{avg} + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin{(\frac{1 + mod(i+1, 2)}{2}\pi - 2\Delta \Psi)} \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} \frac{\sin{(2\Delta \theta)}}{2\Delta \theta} CSD_{avg} + \\ &- \frac{\rho_D}{2} \frac{1}{\Delta \theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin{(\frac{1 + mod(i+1, 2)}{2}\pi - 2\Delta \Psi)} \left( \sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) = \\ &= \frac{\rho_D}{2} COD_{avg} \left( 1 - \frac{1 - \cos{(2\Delta \theta)}}{2\Delta \theta} + \frac{\sin{(2\Delta \theta)}}{2\Delta \theta} \right) + \\ &+ \frac{\rho_D}{2} CSD_{avg} \left( 1 - \frac{1 - \cos{(2\Delta \theta)}}{2\Delta \theta} - \frac{\sin{(2\Delta \theta)}}{2\Delta \theta} \right) + \\ &+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^{i} \sin{(\frac{1 + mod(i+1, 2)}{2}\pi - 2\Delta \Psi)} - \left( -\frac{1}{2} \right)^{i+1} \sin{(\frac{1 + mod(i, 2)}{2}\pi - 2\Delta \Psi)} \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^{i} \sin{(\frac{1 + mod(i+1, 2)}{2}\pi - 2\Delta \Psi)} + \left( -\frac{1}{2} \right)^{i+1} \sin{(\frac{1 + mod(i, 2)}{2}\pi - 2\Delta \Psi)} \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^{i} \sin{(\frac{1 + mod(i+1, 2)}{2}\pi - 2\Delta \Psi)} + \left( -\frac{1}{2} \right)^{i+1} \sin{(\frac{1 + mod(i, 2)}{2}\pi - 2\Delta \Psi)} \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_$$

65 2.  $\beta_{33}$ 

$$\begin{split} &\beta_{33} = \\ &= \rho_D \frac{1}{\Delta \theta} \int_{0}^{\Delta \theta} \left[ \frac{COD(\theta) + CSD(\theta)}{2} \left( 1 + \sin{(2\theta)} \right) - \frac{COD(\theta) - CSD(\theta)}{2} \cos{(2\theta)} \right] d\theta = \\ &= \frac{\rho_D}{2} \left( COD_{avg} + CSD_{avg} \right) + \\ &+ \frac{\rho_D}{2} \frac{1 - \cos{(2\Delta\theta)}}{2\Delta \theta} COD_{avg} + \frac{\rho_D}{2} \frac{1 - \cos{(2\Delta\theta)}}{2\Delta \theta} CSD_{avg} + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i, 2)}{2} \pi - 2\Delta \Psi \right)} \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i, 2)}{2} \pi - 2\Delta \Psi \right)} \left( \sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} \frac{\sin{(2\Delta\theta)}}{2\Delta \theta} COD_{avg} + \\ &- \frac{\rho_D}{2} \frac{1}{\Delta \theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin{\left( \frac{1 + mod(i+1, 2)}{2} \pi - 2\Delta \Psi \right)} \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} \frac{\sin{(2\Delta\theta)}}{2\Delta \theta} CSD_{avg} + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i} \sin{\left( \frac{1 + mod(i+1, 2)}{2} \pi - 2\Delta \Psi \right)} \left( \sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) = \\ &= \frac{\rho_D}{2} COD_{avg} \left( 1 + \frac{1 - \cos{(2\Delta\theta)}}{2\Delta \theta} - \frac{\sin{(2\Delta\theta)}}{2\Delta \theta} \right) + \\ &+ \frac{\rho_D}{2} CSD_{avg} \left( 1 - \frac{1 + \cos{(2\Delta\theta)}}{2\Delta \theta} + \frac{\sin{(2\Delta\theta)}}{2\Delta \theta} \right) + \\ &+ \frac{\rho_D}{2} COD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i, 2)}{2} \pi - 2\Delta \Psi \right)} - \left( -\frac{1}{2} \right)^{i} \sin{\left( \frac{1 + mod(i+1, 2)}{2} \pi - 2\Delta \Psi \right)} \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i+1, 2)}{2} \pi - 2\Delta \Psi \right)} - \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i, 2)}{2} \pi - 2\Delta \Psi \right)} \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i+1, 2)}{2} \pi - 2\Delta \Psi \right)} - \left( -\frac{1}{2} \right)^{i+1} \sin{\left( \frac{1 + mod(i, 2)}{2} \pi - 2\Delta \Psi \right)} \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2$$

3.  $\beta_{23}$ 

$$\begin{split} \beta_{23} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} 2 \left[ \frac{COD(\theta) + CSD(\theta)}{2} \cos(2\theta) + \frac{COD(\theta) - CSD(\theta)}{2} \sin(2\theta) \right] d\theta = \\ &= \frac{\rho_D}{2} \frac{\sin(2\Delta \theta)}{2\Delta \theta} COD_{avg} + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^i \sin\left( \frac{1 + mod(i+1,2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} \frac{\sin(2\Delta \theta)}{2\Delta \theta} CSD_{avg} + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^i \sin\left( \frac{1 + mod(i+1,2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} \frac{1 - \cos(2\Delta \theta)}{2\Delta \theta} COD_{avg} - \frac{\rho_D}{2} \frac{1 - \cos(2\Delta \theta)}{2\Delta \theta} CSD_{avg} + \\ &+ \frac{\rho_D}{2} \frac{1}{\Delta \theta} COD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin\left( \frac{1 + mod(i,2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} \frac{1}{\Delta \theta} CSD_{max} \sum_{i=0}^{2n-1} \left( -\frac{1}{2} \right)^{i+1} \sin\left( \frac{1 + mod(i,2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &- \frac{\rho_D}{2} CSD_{avg} \left( \frac{1 - \cos(2\Delta \theta)}{2\Delta \theta} + \frac{\sin(2\Delta \theta)}{2\Delta \theta} \right) + \\ &- \frac{\rho_D}{2} CSD_{avg} \left( \frac{1 - \cos(2\Delta \theta)}{2\Delta \theta} - \frac{\sin(2\Delta \theta)}{2\Delta \theta} \right) + \\ &+ \frac{\rho_D}{2} COD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^i \sin\left( \frac{1 + mod(i+1,2)}{2} \pi - 2\Delta \Psi \right) + \left( -\frac{1}{2} \right)^{i+1} \sin\left( \frac{1 + mod(i,2)}{2} \pi - 2\Delta \Psi \right) \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^i \sin\left( \frac{1 + mod(i+1,2)}{2} \pi - 2\Delta \Psi \right) - \left( -\frac{1}{2} \right)^{i+1} \sin\left( \frac{1 + mod(i,2)}{2} \pi - 2\Delta \Psi \right) \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta \theta} \sum_{i=0}^{2n-1} \left( \left( -\frac{1}{2} \right)^i \sin\left( \frac{1 + mod(i+1,2)}{2} \pi - 2\Delta \Psi \right) - \left( -\frac{1}{2} \right)^{i+1} \sin\left( \frac{1 + mod(i,2)}{2} \pi - 2\Delta \Psi \right) \right) \cdot \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta \Psi^{k-i} \right) + \\ &\cdot \left( \sum_{k=i}^{2n-1} a_$$

- 2.6. Application to UD composite
- 2.7. Application to  $[0_{mk}^{\circ}, 90_{k}^{\circ}, 0_{mk}^{\circ}]$  laminate
- 3. Computations with the Finite Element Method (FEM)
- 3.1. Models of Representative Volume Element (RVE)
  - 3.2. Details of FEM implementation
  - 4. Results and discussion
  - 5. Conclusions

#### References

85

90

- [1] P. Lundmark, J. Varna, Modeling thermo-mechanical properties of damaged laminates, Key Engineering Materials 251-252 (2003) 381-388. doi: 10.4028/www.scientific.net/kem.251-252.381.
  - [2] P. Lundmark, J. Varna, Crack face sliding effect on stiffness of laminates with ply cracks, Composites Science and Technology 66 (10) (2006) 1444– 1454. doi:10.1016/j.compscitech.2005.08.016.
  - [3] J. Varna, Modelling mechanical performance of damaged laminates, Journal of Composite Materials 47 (20-21) (2012) 2443–2474. doi:10.1177/0021998312469241.
  - [4] M. S. Loukil, J. Varna, Z. Ayadi, Applicability of solutions for periodic intralaminar crack distributions to non-uniformly damaged laminates, Journal of Composite Materials 47 (3) (2012) 287–301. doi:10.1177/0021998312440126.
    - [5] M. S. Loukil, W. Hussain, A. Kirti, A. Pupurs, J. Varna, Thermoelastic constants of symmetric laminates with cracks in 90-layer: application of simple models, Plastics, Rubber and Composites 42 (4) (2013) 157–166. doi:10.1179/1743289811y.0000000064.

- [6] M. S. Loukil, J. Varna, Z. Ayadi, Engineering expressions for thermo-elastic constants of laminates with high density of transverse cracks, Composites Part A: Applied Science and Manufacturing 48 (2013) 37–46. doi:10. 1016/j.compositesa.2012.12.012.
- [7] J. Varna, M. S. Loukil, Effective transverse modulus of a damaged layer: Potential for predicting symmetric laminate stiffness degradation, Journal of Composite Materials 51 (14) (2016) 1945–1959. doi:10.1177/0021998316658965.
- [8] A. Pupurs, J. Varna, M. Loukil, H. B. Kahla, D. Mattsson, Effective stiffness concept in bending modeling of laminates with damage in surface 90-layers, Composites Part A: Applied Science and Manufacturing 82 (2016) 244–252. doi:10.1016/j.compositesa.2015.11.012.
- [9] J. Varna, 2.10 crack separation based models for microcracking, in:
   P. W. Beaumont, C. H. Zweben (Eds.), Comprehensive Composite Materials II, Elsevier, Oxford, 2018, pp. 192 220. doi:10.1016/B978-0-12-803581-8.09910-0.
  - [10] M. S. Loukil, J. Varna, Effective shear modulus of a damaged ply in laminate stiffness analysis: Determination and validation, Journal of Composite Materials (2019) 002199831987436doi:10.1177/0021998319874369.
  - [11] M. S. Loukil, J. Varna, Crack face sliding displacement (CSD) as an input in exact GLOB-LOC expressions for in-plane elastic constants of symmetric damaged laminates, International Journal of Damage Mechanics (2019) 105678951986600doi:10.1177/1056789519866000.

# Appendix A. Explicit expressions for $f\left( heta ight)$ and $g\left( heta ight)$

In the following, recall that

95

110

$$\Delta\Psi = \min\left(\Delta\theta, \Delta\Phi\right). \tag{A.1}$$

n = 1

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \sum_{k=0}^{0} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} = a_1 \left(\theta - \frac{\Delta\Psi}{2}\right)$$
$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \sum_{k=0}^{0} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} = b_1 \left(\theta - \frac{\Delta\theta}{2}\right)$$
(A.2)

$$\int_{0}^{\Delta\Psi} f\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = \int_{0}^{\Delta\Psi} a_{1}\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = \left[\frac{a_{1}}{2}\theta^{2} - a_{1}\frac{\Delta\Psi}{2}\theta\right] \Big|_{0}^{\Delta\Psi} = 0 \quad \forall a_{1}$$

$$\int_{0}^{\Delta\theta} g\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = \int_{0}^{\Delta\theta} b_{1}\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = \left[\frac{b_{1}}{2}\theta^{2} - b_{1}\frac{\Delta\theta}{2}\theta\right] \Big|_{0}^{\Delta\theta} = 0 \quad \forall b_{1}$$
(A.3)

$$\begin{split} COD_{avg} + COD_{max} a_1 \left( \Delta \Psi - \frac{\Delta \Psi}{2} \right) &= 0 \rightarrow a_1 = -\frac{2}{\Delta \Psi} \frac{COD_{avg}}{COD_{max}} \\ CSD_{avg} + CSD_{max} b_1 \left( \Delta \theta - \frac{\Delta \theta}{2} \right) &= 0 \rightarrow b_1 = -\frac{2}{\Delta \theta} \frac{CSD_{avg}}{CSD_{max}} \end{split} \tag{A.4}$$

$$\begin{split} &\sum_{i=0}^{1} \left( -\frac{1}{2} \right)^{i+1} \sin \left( \frac{1 + mod (i, 2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=0}^{1-i} a_k \left( 1 - (k+1) \right) ! \Delta \Psi^k \right) = \\ &= \left( -\frac{1}{2} \right)^{1} \sin \left( \frac{1 + mod (0, 2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=0}^{1} a_k \left( 1 - (k+1) \right) ! \Delta \Psi^k \right) + \\ &+ \left( -\frac{1}{2} \right)^{2} \sin \left( \frac{1 + mod (1, 2)}{2} \pi - 2\Delta \Psi \right) \left( \sum_{k=0}^{0} a_k \left( 1 - (k+1) \right) ! \Delta \Psi^k \right) = \\ &= -\frac{1}{2} \cos \left( 2\Delta \Psi \right) \left( \sum_{k=0}^{1} a_k \left( 1 - (k+1) \right) ! \Delta \Psi^k \right) + \\ &+ \frac{1}{4} \sin \left( 2\Delta \Psi \right) \left( \sum_{k=0}^{0} a_k \left( 1 - (k+1) \right) ! \Delta \Psi^k \right) = \\ &= -\frac{1}{2} \cos \left( 2\Delta \Psi \right) \left( a_0 + a_1 \left( n - (k+1) \right) ! \Delta \Psi^k \right) + \\ &+ \frac{1}{4} \sin \left( 2\Delta \Psi \right) \left( \sum_{k=0}^{0} a_k \left( n - (k+1) \right) ! \Delta \Psi^k \right) = \end{split}$$

$$(A.5)$$

n = 2

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \sum_{k=0}^{1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} = a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) + a_3 \left(\theta - \frac{\Delta\Psi}{2}\right)^3$$
$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \sum_{k=0}^{1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} = b_1 \left(\theta - \frac{\Delta\theta}{2}\right) + b_3 \left(\theta - \frac{\Delta\theta}{2}\right)^3 \tag{A.6}$$

n = 3

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \sum_{k=0}^{2} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} =$$

$$= a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) + a_3 \left(\theta - \frac{\Delta\Psi}{2}\right)^3 + a_5 \left(\theta - \frac{\Delta\Psi}{2}\right)^5$$

$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \sum_{k=0}^{1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} =$$

$$= b_1 \left(\theta - \frac{\Delta\theta}{2}\right) + b_3 \left(\theta - \frac{\Delta\theta}{2}\right)^3 + b_5 \left(\theta - \frac{\Delta\theta}{2}\right)^5$$
(A.7)