

Energy release rate of fiber/matrix interface crack growth in cross-ply laminates under transverse loading: effect of the $0^\circ/90^\circ$ interface and of 0° layer thickness

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Abstract

Models of Representative Volume Elements (RVEs) of cross-ply laminates with different geometric configurations and damage states are studied. Debond growth is characterized by the estimation of the Mode I and Mode II Energy Release Rate (ERR) using the Virtual Crack Closure Technique (VCCT). It is found that the presence of the $0^\circ/90^\circ$ interface and the thickness of the 0° layer have no effect, apart from laminates with *ultra-thin* 90° plies where it is however modest. With the exception of cross-ply laminates with an *ultra-thin* 90° ply, no difference is found in debond ERR between a UD composite and a cross-ply laminate.

Keywords: Polymer-matrix Composites (PMCs), Fibre/matrix bond, Debonding, Finite Element Analysis (FEA)

1. Introduction

Since the development of the *spread tow* technology or “FUKUI method” [1, 2], significant efforts have been directed toward the characterization of *thin-ply* laminates [3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15] and their application to mission-critical structures in the aerospace sector [16, 17, 18, 19].

At the lamina level, the use of *thin-ply*s leads to more regular and homogeneous microstructures [9, 12]. Measurements of ply level properties (tensile and compressive modulus, Poisson’s ratio, ultimate tensile strength, tensile on-

set of damage, interlaminar shear strength) on UD specimens ($[0_m^\circ]$ and $[90_m^\circ]$)
10 revealed no remarkable difference with average properties available in the literature for the same type of fiber, nor showed any particular dependence on the ply thickness [12]. Only an increase of the ultimate compressive strength in the fiber direction was observed with very thin plies (~ 4 fiber diameters), although with very scattered values, which the authors claim to be due to the
15 fiber arrangement's increased regularity which prevents the onset of fiber microbuckling [12]. A number of researchers [4, 5, 6, 7] has reported improvements in fatigue life with the use of *thin-ply*s, which are explained as a consequence of delayed propagation of free edge delaminations and intralaminar cracks. Several researchers have analyzed the effect of *thin-ply*s on damage development
20 under static [3, 6, 7, 8, 9, 10, 11, 12], fatigue [4, 6, 7, 8, 12] and impact loadings [6, 7, 8, 12]. It seems apparent that *thin-ply* laminates possess an increased ability to delay, and in some cases even suppress, the onset and propagation of intralaminar cracks (called often transverse or matrix or micro-cracks).

The first stage in the appearance of transverse cracks is known to be the occurrence of fiber/matrix interface cracks (also referred to as debonds), which grow
25 along the fiber arc direction, then kink out of the interface and coalesce forming a transverse crack [20]. Different approaches have been applied to model the initiation and growth of debonds. The Cohesive Zone Model (CZM) has been used to mimic the propagation of debonds along fiber interfaces; coupled with
30 a failure criterion for the matrix, it has provided simulations of the growth of transverse cracks starting from a virgin material [21, 22, 23, 24]. The main advantages of this approach are the possibility to observe the development of a simulated crack path and to record a load-displacement curve to compare with experimental measurement. However, various observations cast a doubt
35 about the applicability of the CZM: the bi- (for 2D models) and tri- (in 3D) axially of the matrix stress state in the inter-fiber region that is linked with a cavitation-like failure of the polymer [25]; the locality and mode dependency of the interface failure [26]; the problematic use at the microscopic level of properties measured in UD specimens at the laminate level [22]. A second approach

40 that obviates these drawbacks is the application of Linear Elastic Fracture Me-
 chanics (LEFM) arguments to the study of debond growth. The analysis focuses
 on the evaluation of Mode I and Mode II Energy Release Rate (ERR) at the
 crack tip by means of the Virtual Crack Closure Technique (VCCT) [27] or
 the J-Integral method [28]. The stress and strain field, required for the ERR
 45 computation, can be solved by application of different methodologies such as
 analytical solutions [29], the Boundary Element Method (BEM) [30] or the Fi-
 nite Element Method (FEM) [31]. This approach presents nonetheless some
 limitations: it describes propagation of the debond and not its initiation; the
 role of friction in the contact zone is still an open issue; consensus is still lack-
 50 ing on a proper criterion for crack propagation in mixed mode. Finite fracture
 mechanics [32] is one way to address the initiation problem. Different studies
 have followed the LEFM approach and analyzed models of one or two fibers
 in an effectively infinite matrix [33, 34, 35, 36, 37] and of an hexagonal clus-
 ter of fibers in an effectively infinite homogenized UD composite [38, 31]. The
 55 problem of debond growth along the fiber-matrix interface in a cross-ply lam-
 inate has been only addressed very recently in [39, 40], where authors embed
 a single partially debonded fiber in an effectively infinite homogenized 90° ply
 bounded by homogenized 0° layers. Thus, the effect of debond-debond inter-
 action and of the relative proximity of a $0^\circ/90^\circ$ interface on debond ERR in
 60 cross-ply laminates is yet to be addressed. The present work is devoted to this
 problem. Models of Repeating Unit Cells (RUCs) are developed to represent
 laminates with different degrees of damage in the 90° ply (here only in the form
 of debonds). The number of fully bonded fibers across the thickness of the 90°
 ply is varied in order to investigate the effect of the proximity of the $0^\circ/90^\circ$
 65 interface. The thickness of the bounding 0° layers is also used as a parameter
 of the study. The stress and strain fields are solved with the Finite Element
 Method in Abaqus [41] and the debond (crack) is characterized by its Mode I
 and Mode II ERR calculated with the VCCT.

2. RVE models & FE discretization

2.1. Introduction & Nomenclature

In the present work, we investigate debond development under in-plane longitudinal tension in $[0_{m \cdot k \cdot 2L}^\circ, 90_{k \cdot 2L}^\circ, 0_{m \cdot k \cdot 2L}^\circ]$ laminates. The interaction between debonds in the presence of an interface with a stiff layer is studied with the use of different Repeating Unit Cells (RUCs) (see Figures 1 and 2 in Sec. 2.2), in
75 which only the central fiber is partially debonded. Repetition of the composite RUC occurs along the in-plane longitudinal direction (horizontal direction of the RUC in Figures 1 and 2), thus representing a cross-ply laminate with a thin or even ultra-thin 90° ply in the middle.

All the RUCs present regular microstructures with fibers placed according to a
80 square-packing configuration characterized by the repetition of the same one-fiber unit cell of size $2L \times 2L$, where L is a function of the fiber volume fraction V_f and the fiber radius according to

$$L = \frac{R_f}{2} \sqrt{\frac{\pi}{V_f}}. \quad (1)$$

Each fiber in the model has the same radius R_f , equal to $1 \mu m$. This specific value has no physical meaning per se and it has been selected for simplicity. It
85 is useful to observe that, in a linear elastic solution as the one described in the present article, the ERR is proportional to the geometrical dimensions of the model and thus re-evaluation of the ERR for fibers of any size requires just a multiplication. Furthermore, it is worth to point out that V_f is the same in the one-fiber unit and in the overall RUC, i.e. no clustering of fibers is considered.
90 The thickness of the 90° ply depends on the number k of fiber rows present across the thickness (the vertical or z direction in Figures 1 and 2) according to

$$t_{90^\circ} = k \cdot 2L. \quad (2)$$

On the other hand, the thickness of 0° layers can be assigned freely as a multiple of the 90° ply thickness as

$$t_{0^\circ} = m \cdot t_{90^\circ} \quad (3)$$

where m is an arbitrary integer. Thus, the thickness ratio m represents one
95 additional parameter for the investigation.

In the following, let us consider in-plane coordinates x and y , where x is the longitudinal direction of the cross-ply laminate under consideration and thus the transverse direction of its central 90° layer. In the presence of a load in the x -direction, the strain in the y -direction is small, due to the very small Poisson's
100 ratio of the laminate. Furthermore, debonds are considered to be significantly longer in the fiber direction than in the arc direction [42]. Therefore we use 2D models under the assumption of plane strain, defined in the $x - z$ section of the composite. The study presented in this paper thus applies to long debonds and its focus is on understanding the mechanisms of growth along their arc
105 direction. The laminates are assumed to be subject to tensile strain, which is applied in the form of a constant displacement in the x -direction along both vertical boundaries of the RUC as shown in Figure 3.

We assume damage to be present only in the central “row” of fibers of the 90° layer in the form of multiple debonds appearing at different regular intervals
110 along the loading (horizontal) direction. The number of fibers n present in the horizontal direction of the RUC (Figures 1 and 2) controls the distance, in terms of fully bonded fibers, between consecutive debonds: if the RUC has n fibers in the horizontal direction, two consecutive debonds are separated by $n - 1$ undamaged fibers. The RUCs considered are thus Representative Volume
115 Elements (RVEs) of cross-ply laminates with a certain distribution of debonds in the middle 90° layer.

In summary, the models are differentiated by: first, the spacing between debonds along the horizontal direction in the 90° layer, which corresponds to the number n of fibers in the RUC's horizontal direction; second, the thickness of the middle
120 90° ply measured in terms of the number k of fiber rows in the vertical direction; third, the factor m which provides the thickness of 0° layers as a multiple of

the 90° ply thickness. It thus seems natural to introduce a common notation for the RUCs as $n \times k - m \cdot t_{90^\circ}$.

An additional family of RUCs is considered to study the effect of equivalent
125 boundary conditions, which is constituted by only one partially debonded fiber. Homogenized 0° layers are not present. The application of coupling of horizontal displacements u_x along the right and left sides allows for repetition along the horizontal direction. When the upper boundary of the RUC is left free, we define the $1 \times 1 - free$ model. If coupling of the vertical displacements u_z is
130 applied to the upper boundary, we define instead the $1 \times 1 - coupling$ model. In the case a linear distribution of the horizontal displacement u_x is applied to the upper boundary, the model is referred to as $1 \times 1 - H$. Finally, when the linear distribution of the horizontal displacement u_x is superimposed to the condition of coupling of the vertical displacements u_z on the upper boundary, we have
135 the $1 \times 1 - coupling + H$. Further details about this family of RUCs and the corresponding laminate RVE can be found in [43].

2.2. Description of modelled Representative Volume Elements (RVEs)

The first family of Representative Volume Elements (RVEs) is represented in Figure 1. It represents a set of $[0_{m \cdot k \cdot 2L}^\circ, 90_{k \cdot 2L}^\circ, 0_{m \cdot k \cdot 2L}^\circ]$ laminates with an
140 ultra-thin 90° layer, constituted by a single row of fibers across the thickness. Debonds appear at regular intervals measured in terms of number $n - 1$ of fully bonded fibers present between them, which in turn correspond to the number of fibers along the horizontal direction of the RVE as highlighted in Fig. 1. They are thus the $n \times 1 - m \cdot t_{90^\circ}$ models, where $m = 1, 10$ and n is an integer
145 ≥ 1 ($n = 1$ corresponds to the case of a debond appearing on all the fibers in the central 90° layer). These models are geometrically extreme, but allow to focus on the interaction between debonds and the inter-ply $0^\circ/90^\circ$ interface. Furthermore, the *spread tow* technology is today capable of producing cross-ply laminates with the central 90° layer thickness only 4–5 times the fiber diameter,
150 as shown for example in [9], which may in future give practical relevance even to such extreme case.

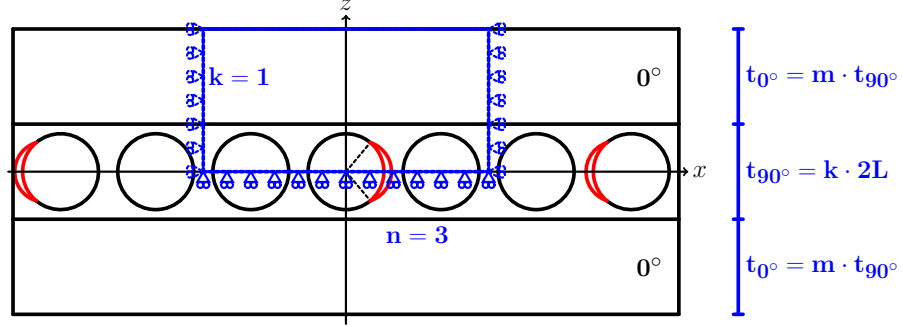


Figure 1: Models of $[0_{m \cdot k \cdot 2L}^{\circ}, 90_{k \cdot 2L}^{\circ}, 0_{m \cdot k \cdot 2L}^{\circ}]$ laminates with an ultra-thin 90° layer, where the 90° ply is made up by a single “row” of fibers. Debonds are repeating at different distances, measured in terms of the number $n-1$ of fully bonded fibers appearing between two consecutive debonds. $2L$ is the thickness of one-fiber row.

The second set of models considers instead cross-ply laminates with a central 90° ply of variable thickness, measured in terms of number k of fiber rows “stacked” in the vertical direction in Figure 2. Once again, debonds appear in the central row only at regular intervals measured in terms of number $n-1$ of fully bonded fibers present between them, as highlighted in Fig. 2. These models are thus the $n \times k - m \cdot t_{90^{\circ}}$ models, where $m = 1, 10$, $k > 1$ and n is an integer ≥ 1 ($n = 1$ corresponds to the case of a debond appearing on all fibers of the central fiber row in the 90° layer).

By increasing the number n of fibers in the horizontal direction in the RUC, decreasing levels of damage (debonds spaced further apart and the interaction between debonds becomes less important) are considered to be present in the laminate. By increasing the number k of fiber rows, the thickness of the 90° layer is increased and the effect of the relative proximity of the inter-ply $0^{\circ}/90^{\circ}$ interface can thus be studied. Finally, by increasing the factor m , the thickness of the 0° layers is increased for a given thickness of the 90° , which allows the investigation of the 0° ply-block effect [44].

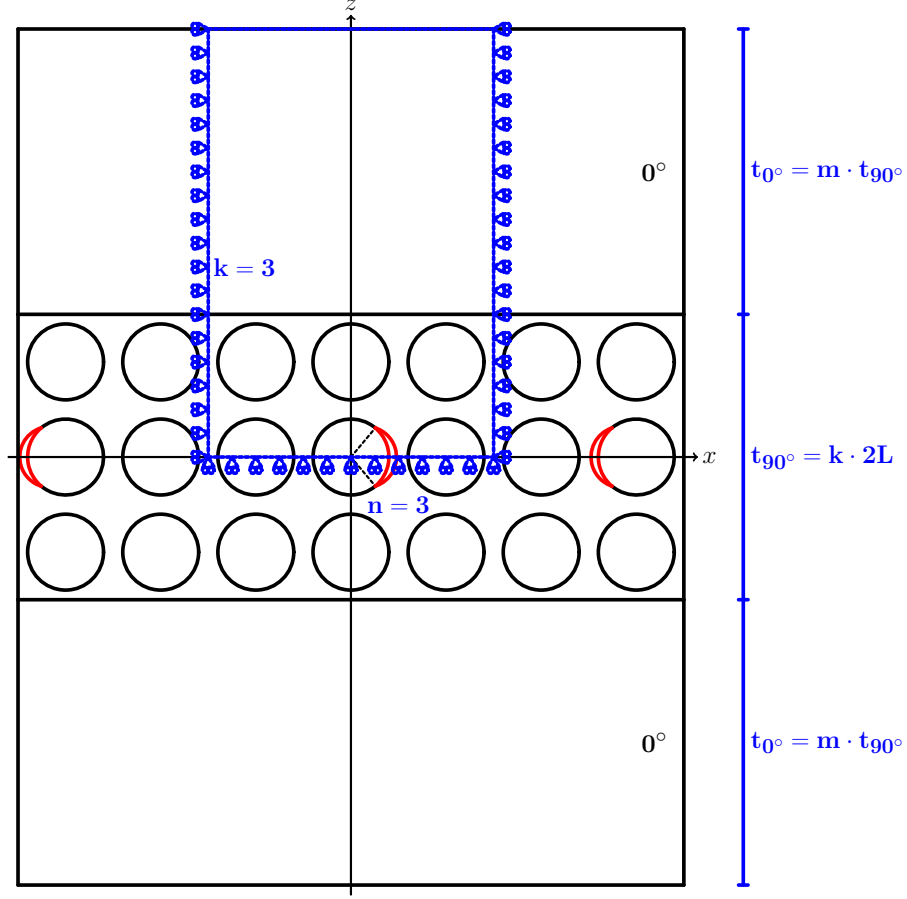


Figure 2: Models of $[0_{m \cdot k \cdot 2L}^\circ, 90_{k \cdot 2L}^\circ, 0_{m \cdot k \cdot 2L}^\circ]$ laminates with a 90° layer of variable thickness, determined by the number k of “rows” of fibers along the vertical direction. Debonds are repeating at different distances along the horizontal direction, measured in terms of the number $n - 1$ of fully bonded fibers appearing between two consecutive debonds. $2L$ is the thickness of one-fiber row.

2.3. Finite Element (FE) discretization

The RUCs are discretized and solved with the Finite Element Method (FEM) using the commercial FEM package Abaqus [41]. The total length l and height h of a RUC are determined by the number of fibers n in the horizontal direction, the number of fiber rows k across the thickness and the thickness ratio m (see Sec. 2.2) according to Eq. 4:

$\bar{\varepsilon}_x$ equal to 1%.

Table 1: Summary of mechanical properties of fiber, matrix and UD layer.

Material	V_f [%]	E_L [GPa]	E_T [GPa]	G_{LT} [GPa]	ν_{LT} [-]	ν_{TT} [-]
Glass fiber	-	70.0	70.0	29.2	0.2	0.2
Epoxy	-	3.5	3.5	1.25	0.4	0.4
UD	60.0	43.442	13.714	4.315	0.273	0.465

The FEM model is discretized using second order, 2D, plane strain triangular (CPE6) and rectangular (CPE8) elements. In the crack tip neighborhood, a refined regular mesh of quadrilateral elements with almost unitary aspect ratio is needed to ensure a correct evaluation of the ERR. The angular size δ of an element in this refined region close to the crack tip is by design equal to 0.05° . The crack faces are modeled as element-based surfaces with a frictionless small-sliding contact pair interaction. The Mode I, Mode II and total Energy Release Rates (ERRs) (respectively G_I , G_{II} and G_{TOT}) represent the main result of the numerical analysis. They are computed using the VCCT [27] implemented in a custom Python routine. Glass fiber and epoxy are considered throughout this article, and it is assumed that their response always lies in the linear elastic domain. The effective UD properties are computed using Hashin's Concentric Cylinder Assembly model [45] with the self-consistency scheme for the out-of-plane shear modulus of Christensen [46]. The properties used are listed in Table 1. The model was validated with respect to BEM results of [47, 36]; considerations about the order of accuracy can be found in [43].

3. Results & Discussion

3.1. Effect of the proximity of the $0^\circ/90^\circ$ interface and of the thickness of the 0° layer on debond ERR

We first focus our attention on the model $1 \times 1 - m \cdot t_{90^\circ}$, which represents a particular case of the family $n \times 1 - m \cdot t_{90^\circ}$. It corresponds to a cross-ply

laminate in which the central 90° ply is constituted by only one fiber row, in
 which each fiber possesses a debond appearing on alternating sides. The model
 thus represents an extreme idealization, in the sense that: first, the central 90°
 layer is the thinniest that can be conceived; second, a very particular damage
 state is present for which every fiber is partially debonded from the surrounding
 matrix. The first condition allows us to investigate the direct effect of the
 proximity of the $0^\circ/90^\circ$ interface on debond ERR. The second condition implies
 that we are analyzing the most severe damage state that can occur in the 90°
 ply when considering debonds as the only mechanism of damage. As pointed
 out in a previous work [43], the presence of fully bonded fibers close to the
 partially debonded one causes a magnification of the x -strain in the matrix
 region between the debonded fiber and the closest undamaged one. This increase
 in the value of the strain leads in turn to higher values of Energy Release Rate.
 Given that we are considering a 90° ply with all fibers partially debonded, we
 are neglecting such magnification effect and focusing only on the presence of
 the $0^\circ/90^\circ$ interface and on the thickness of the 0° layer, by considering the
 ratio $m = \frac{t_{0^\circ}}{t_{90^\circ}}$ of ply thicknesses as a free parameter. We will later analyze
 in Sec. 3.2 the effect of the combined presence of fully bonded fibers and the
 $0^\circ/90^\circ$ interface.

In Figures 4 and 5 respectively the Mode I and Mode II ERR are shown
 for models $1 \times 1 - m \cdot t_{90^\circ}$ with $m = 1, 10, 50, 100$ and models $1 \times 1 - free$,
 $1 \times 1 - coupling$ and $1 \times 1 - H + V$. It is worth to remind us of the laminate
 RVE that correspond to these last three models: model $1 \times 1 - free$ represents
 a one-fiber-row UD composite with all the fibers partially debonded; model
 $1 \times 1 - coupling$ corresponds to a UD laminate with an infinite number of fiber
 rows and all the fibers partially debonded; model $1 \times 1 - H + V$ represents a
 cross-ply laminate with one-fiber-row central 90° ply and the 0° ply replaced
 by boundary conditions at the interface not allowing interface bending and
 with an applied uniform strain not affected by fibers and debonds in the 90°
 ply. Observing Figure 4, it is possible to notice that the values of G_I for the
 $1 \times 1 - free$ and the $1 \times 1 - coupling$ model represent respectively a lower and an

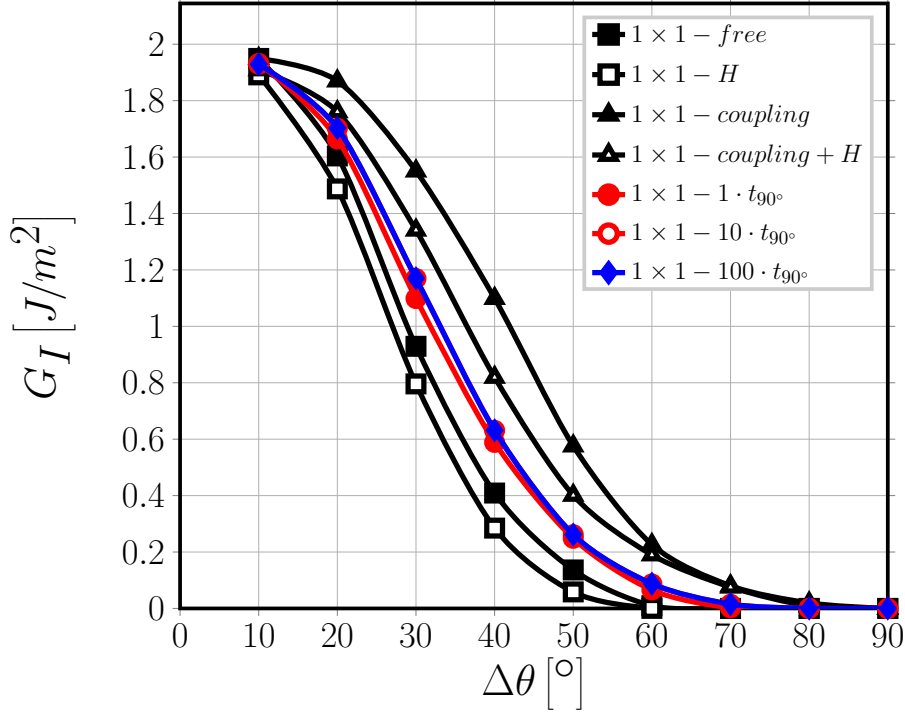


Figure 4: Effect of the proximity of the $0^\circ/90^\circ$ interface and of the thickness of the 0° layer on Mode I ERR: models $1 \times 1 - free$, $1 \times 1 - coupling$, $1 \times 1 - H + V$ and $1 \times 1 - m \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

upper bound for all the other RVEs. The $1 \times 1 - H + V$ model is as well an upper
 240 bound for the $1 \times 1 - m \cdot t_{90^\circ}$ RVEs; however its values of G_I are lower than
 those of the $1 \times 1 - coupling$ model due to the applied uniform x -strain at the
 interface, which prevents the crack to open as much as in the $1 \times 1 - coupling$
 case. The same observation holds for the size of the debond at contact zone
 onset, i.e. when $G_I = 0$: the lower bound is provided by the $1 \times 1 - free$
 245 model ($\Delta\theta \sim 60^\circ$), while the contact zone onset for models $1 \times 1 - coupling$ and
 $1 \times 1 - H + V$ represents the upper bound ($\sim 80^\circ$). All $1 \times 1 - m \cdot t_{90^\circ}$ RVEs lie
 in between these two bounds for any thickness of the 0° ply, with contact zone
 onset occurring at a debond size of $\sim 70^\circ$.

For Mode II (see Fig. 5), the ERR for the cases with a 0° layer of finite thick-

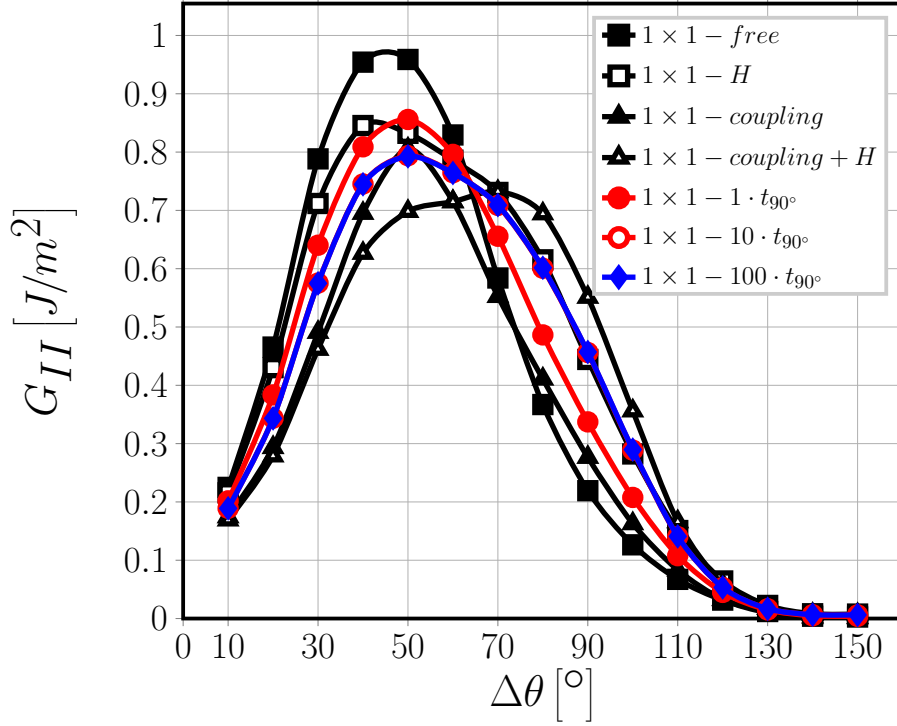


Figure 5: Effect of the proximity of the $0^\circ/90^\circ$ interface and of the thickness of the 0° layer on Mode II ERR: models $1 \times 1 - free$, $1 \times 1 - coupling$, $1 \times 1 - H + V$ and $1 \times 1 - m \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

ness always lies between the values provided by the $1 \times 1 - free$ and $1 \times 1 - H + V$ model: for open debonds ($\Delta\theta < 60^\circ - 70^\circ$), when $G_I \neq 0$ and there is no contact zone, $1 \times 1 - free$ provides the upper bound while $1 \times 1 - H + V$ the lower bound; for close debonds ($\Delta\theta > 60^\circ - 70^\circ$), when $G_I = 0$ and a contact zone is present, the situation is reversed. An effect of the thickness of the 0° layer on Mode II ERR can be noticed in Fig. 5 when the ratio $m = \frac{t_{0^\circ}}{t_{90^\circ}}$ is increased from 1 to 10. The change between the two follows the same pattern described previously: when the thickness of the 0° ply is increased, Mode II decreases for open debonds and increases for closed debonds, in line with the bound switch. These results help to shed light on the effect of the $0^\circ/90^\circ$ interface on debond ERR. The presence of the stiff homogenized 0° layer causes the matrix placed

relatively far from the fiber (close to the interface) to contract much less than
 it would do in the presence of a free surface due to its relatively high Poisson's
 ratio. Furthermore, the presence of the $0^\circ/90^\circ$ interface induces a more
 homogeneous x -displacement field all over the matrix domain. This causes a
 265 concurrent increase of G_I and decrease of G_{II} for small debonds, where the
 crack opening displacement component at the crack tip (responsible for Mode
 I) is mostly due to the global x -displacement field (which increases in the presence
 of the $0^\circ/90^\circ$ interface) while the crack sliding displacement component at
 the crack tip (responsible for Mode II) is for small debonds linked to the global
 270 vertical displacement field due to Poisson's effect (which is lower in the presence
 of a 0° layer instead of a free surface thanks to the stiffness of the former).
 This causes also the delay in the onset of the contact zone. For large debonds
 instead, after the onset of the contact zone, the situation reverses: the magnitude
 increase of the global x -displacement field leads to an increase in the crack
 275 sliding displacement component at the crack tip and thus in Mode II ERR. By
 comparing the results for Mode II of models $1 \times 1 - free$, $1 \times 1 - H + V$ and
 $1 \times 1 - m \cdot t_{90^\circ}$ with $m = 1, 10, 50, 100$ (Fig. 5), it can be argued that the effect
 of the 0° ply thickness is related to its local bending stiffness. In the presence
 a free surface, the matrix in the 90° ply contracts significantly more than the
 280 fibers due to the mismatch in Poisson's ratios, thus leading to higher y -strains
 in the inter-fibers regions than above the fibers. This in turn results in a very
 curved surface, roughly following the fibers' curvature. In the presence of a 0°
 layer, such deformation is prevented by its bending stiffness. A relatively thin
 0° layer ($\frac{t_{0^\circ}}{t_{90^\circ}} = 1$) possesses a lower bending stiffness and thus matrix deformation
 285 is able to bend the interface, which translates into a G_{II} profile closer
 to the $1 \times 1 - free$ model. For thicker 0° layers, the increased bending stiffness
 prevents the curvature of the interface and Mode II ERR becomes closer to the
 $1 \times 1 - H + V$ model, in which the interface is forced to remain straight by the
 applied boundary conditions.

290 3.2. Effect of the proximity of the $0^\circ/90^\circ$ interface on debond-debond interaction
in a single fiber row 90° ply

We turn now our attention to the model $n \times 1 - 1 \cdot t_{90^\circ}$, which corresponds to a cross-ply laminate in which the central 90° ply is constituted by only one fiber row where multiple partially debonded fibers are present, located at a distance of $n - 1$ fully bonded fibers from each other, and debonds appear on alternating sides of consecutive damaged fibers (see Figure 1). This class of models allows
295 to study the effect of the presence of the 0° layer on debond-debond interaction and, particularly, crack shielding [48, 43].

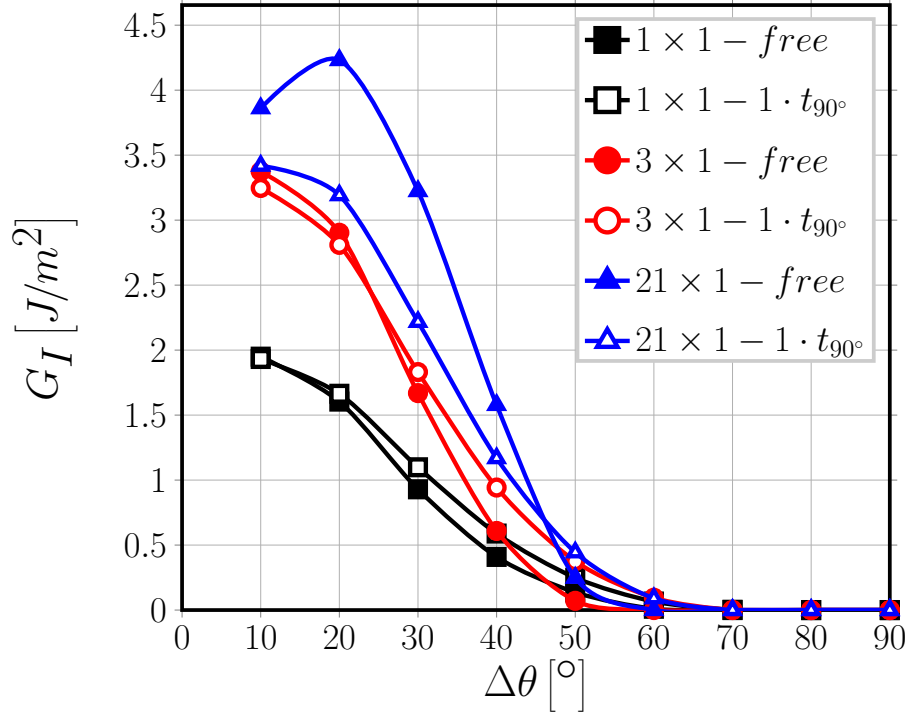


Figure 6: Effect of the presence of the 0° layer on debond-debond interaction for Mode I ERR: models $n \times 1 - free$ and $n \times 1 - 1 \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

In the presence of a free surface, both Mode I and Mode II ERR increase
300 rapidly when the number of fully bonded fibers placed between two consecutive partially debonded one is increased ($n \times 1 - free$ models in Figures 6

and 7). The presence of fully bonded fibers causes an increase in the local x -strain in the debond neighborhood, which leads to greater crack opening and sliding displacements and thus higher ERR (strain magnification [43]). The same mechanism can be described from the opposite point of view: increasing the number of debonds present in the 90° ply reduces the stress concentration in the inter-fibers regions and thus results in lower values of the ERR (crack shielding [48, 43]). From Figures 6 and 7 it seems apparent that the strain magnification effect is present in cross-ply laminates as well, albeit strongly reduced by the presence of the $0^\circ/90^\circ$ interface. This effect is less evident when debonds are close to each other ($1 \times 1 - 1 \cdot t_{90^\circ}$ and $3 \times 1 - 1 \cdot t_{90^\circ}$), i.e. in the case of more severe damage states.

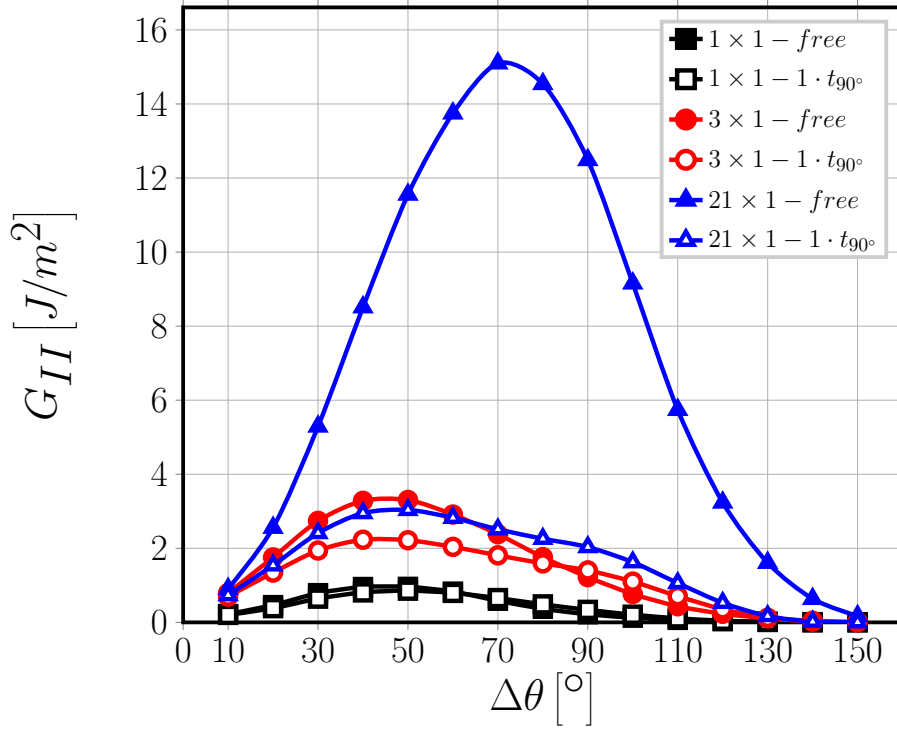


Figure 7: Effect of the presence of the 0° layer on debond-debond interaction for Mode II ERR: models $n \times 1 - free$ and $n \times 1 - 1 \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

3.3. Effect of the presence of fiber rows with no damage on the debond-0°/90° interface interaction

315 After having investigated the effect of the proximity of the 0°/90° interface and of the thickness of the 0° layer on debond ERR and on debond-debond interaction, we address in this section the effect of the presence of fiber rows with only fully bonded fibers inside on the interaction between debonds and the 0°/90° interface. In other words, we are separating the debond from the
320 interface by inserting rows of fully bonded fibers in between, thus increasing the distance to the interface. To this end, we study the models $1 \times k - 1 \cdot t_{90^\circ}$, which represent a cross-ply laminate with the central 90° ply made of k fiber rows and where all the fibers in the central row are partially debonded. The absence of fully bonded fibers in the central row prevents the occurrence of
325 strain magnification or crack shielding (see Sec. 3.2), thus allowing to focus on the effect of the distance of the 0°/90° interface (measured in terms of rows of fully bonded fibers).

Figures 8 and 9 thus show the effect on ERR of the presence of the 0° ply in the case of non-interacting debonds (no strain magnification or crack shielding).
330 If the distance between the 0°/90° interface and the debond is at least one fully bonded fiber, the presence of the 0° ply does not influence debond ERR and no measurable difference can be observed between models $1 \times k - free$ and $1 \times k - 1 \cdot t_{90^\circ}$ for $k \geq 1$.

However, the situation changes when fully bonded fibers are present between
335 consecutive partially debonded fibers, as shown in Figures 10 and 11. For Mode I ERR (Fig. 10), the presence of one row of fully bonded fibers already prevents the 0° ply from having any measurable effect on debond ERR: no difference can be seen between results for models $n \times k - free$ and models $n \times k - 1 \cdot t_{90^\circ}$. Thus, the effect of strain magnification on G_I (Sec. 3.2) in cross-ply laminates follows
340 the same pattern as in UD composites. A more noticeable effect of the presence of the 0° ply can be observed for Mode II (Fig. 11): it causes a reduction in the ERR, particularly when debonds are far apart (models $21 \times 3 - free$ and

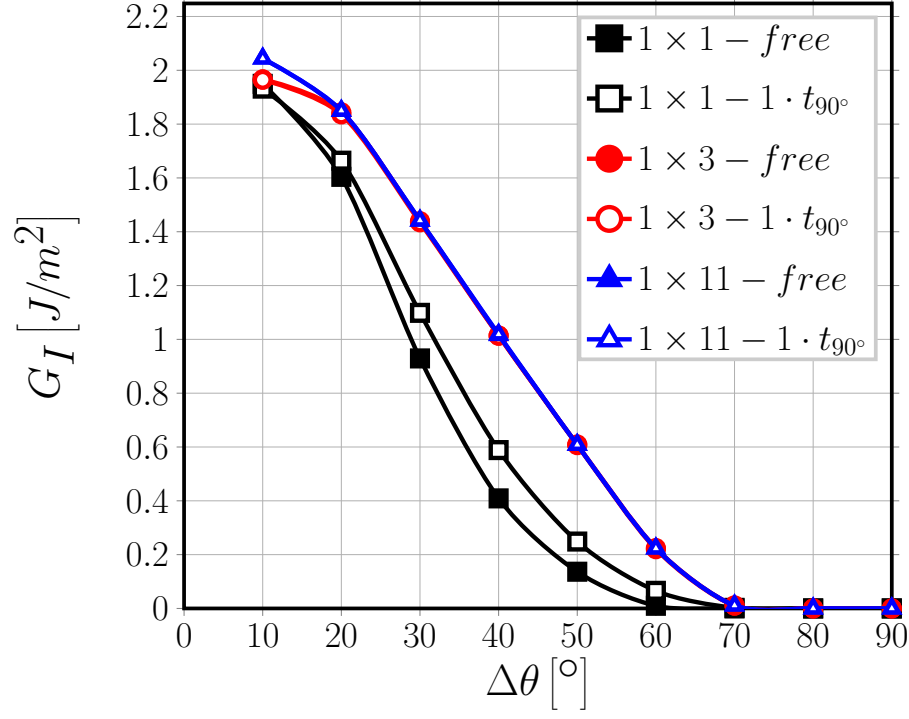


Figure 8: Effect of the presence of undamaged fiber rows in the 90° layer on debond- $0^\circ/90^\circ$ interface interaction for Mode I ERR: models $1 \times k - free$ and $1 \times k - 1 \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

$21 \times 3 - 1 \cdot t_{90^\circ}$), thus mitigating the strain magnification effect for Mode II.

In [39, 40], the authors investigate the existence of a ply-thickness effect
 345 on the fiber-matrix interface crack using two models with respectively an isolated and two neighboring debonded fibers embedded in a homogenized 90° ply bounded by homogenized 0° layers. They select the thickness of the 0° layer as reference and model a $[0_p, 90_{r,p}]_S$ laminate. The thickness of the 90° ply, measured relatively to the thickness of the 0° layer through the factor r , represents
 350 the main parameter of the study, varying from $r = 3$ (thick 90° ply, > 100 fiber diameters) to $r = 0.1$ (ultra-thin 90° ply, $\sim 4 - 5$ fiber diameters). No measurable ply-thickness effect is observed. The results presented in this article confirm their observation and provide a micromechanical explanation (see Sec. 3.1). We

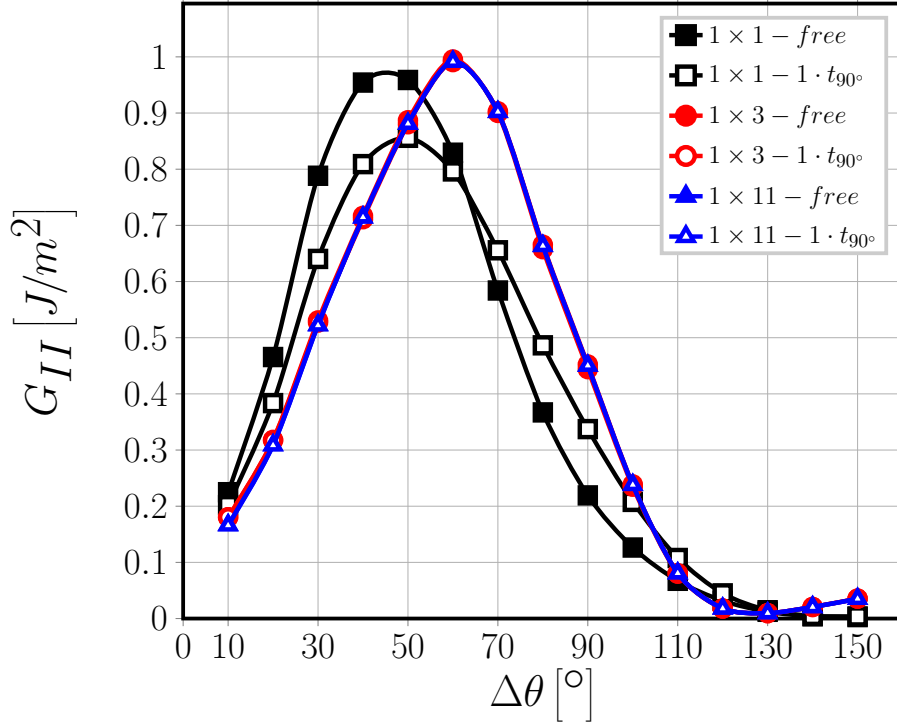


Figure 9: Effect of the presence of undamaged fiber rows in the 90° layer on debond- $0^\circ/90^\circ$ interface interaction for Mode II ERR: models $1 \times k - free$ and $1 \times k - 1 \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

have also shown that extremely thin 90° plies (1 – 5 fiber diameters thick) are
 355 on the other hand subject to the strain magnification effect when fully bonded
 fibers appear between consecutive aligned debonds. The only effect of the 0° ply
 is to reduce the magnification of ERR, which nonetheless takes place. However,
 this mechanism is not peculiar only of cross-ply laminates, but it can be ob-
 served in UD composites as well [43]. The results proposed in this paper could
 360 provide a possible mechanical description of the observations presented in [9].
 The authors conducted *in-situ* observations of edge micro-cracks with an optical
 microscope on $[0_2^\circ, 90_n^\circ, 0_2^\circ]$ carbon fiber-epoxy laminates with $n = 1, 2, 4$, corre-
 sponding to a 90° ply thickness of respectively $40 [\mu m]$ ($\sim 6 - 8$ fiber diameters),
 $80 [\mu m]$ ($\sim 12 - 16$ fiber diameters) and $160 [\mu m]$ ($\sim 24 - 32$ fiber diameters).

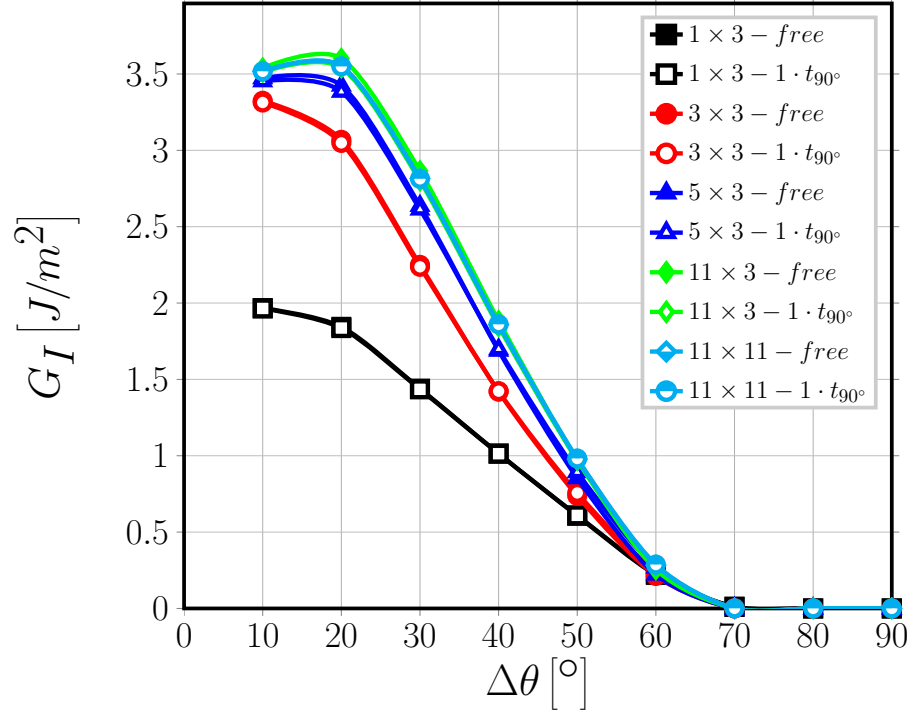


Figure 10: Effect of the presence of undamaged fiber rows in the 90° layer on debond- $0^\circ/90^\circ$ interface interaction for Mode I ERR: models $n \times k - free$ and $n \times k - 1 \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

For $n = 1$, i.e. the case of a very thin 90° ply, isolated debonds appear at a lower value of the applied strain than in thicker plies (at 0.4% vs 0.7%) while coalescence of debonds is suppressed and no transverse crack can be observed even at a strain of 1.5%. It has been shown in this work that in thin 90° plies, i.e. with < 10 fibers across the thickness, a relevant strain magnification effect can be observed when debonds are far from each other and separated by fully bonded, which causes an increase in ERR. This in turn makes the growth of debonds more likely to occur at lower levels of strain than in thick plies (the ERR is proportional to ε^2 in LEFM), which would explain the observations reported in [9].

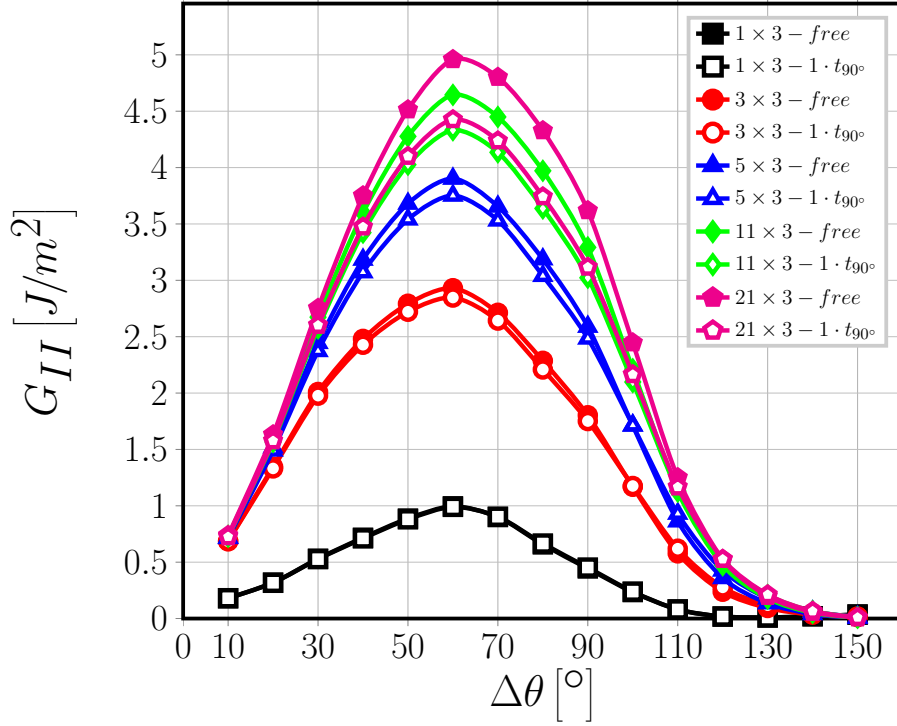


Figure 11: Effect of the presence of undamaged fiber rows in the 90° layer on debond- $0^\circ/90^\circ$ interface interaction for Mode II ERR: models $n \times k - free$ and $n \times k - 1 \cdot t_{90^\circ}$. $V_f = 60\%$, $\varepsilon_x = 1\%$.

4. Conclusions

Different models of Repeating Unit Cell, representing different cross-ply laminates, have been studied in order to study the effect of the presence of the 0° layer and of its thickness on debond Energy Release Rate and on crack shielding. It has been found that the presence of the 0° ply does not significantly alter the trends in ERR observed for the same 90° ply thickness and damage configuration in UD models [43], albeit reducing in general the estimated values of G_I and G_{II} . Furthermore, it has been observed that the influence of the 0° layer is strongly mitigated by the presence of rows of undamaged fibers between the debond and the $0^\circ/90^\circ$ interface. Already the presence of only 1 row of fully bonded fibers between respectively the upper and lower 0° layer and the

central fiber row with partially debonded fibers causes the Mode I and Mode II ERR to adhere closely to the UD results. The observations presented provide an important insight: it appears that the behavior of the fiber/matrix interface crack is affected strongly only by very close perturbation of the elastic fields. *Thin* and *ultra-thin* plies present a peculiar behavior in terms of debond growth because their reduced thickness brings the $0^\circ/90^\circ$ interface close enough for the debonds to feel the perturbation in the elastic fields. Otherwise, it seems that no difference can be found in the mechanism of debond growth between a UD composite and a cross-ply laminate.

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References

- [1] K. Kawabe, New spreading technology for carbon fiber tow and its application to composite materials, *Sen'i Gakkaishi* 64 (8) (2008) 262–267. doi:10.2115/fiber.64.p_262.
- [2] K. Kawabe, H. Sasayama, S. Tomoda, New carbon fiber tow-spread technology and applications to advanced composite materials, *SAMPE Journal* 45 (2) (2008) 6–17.
- [3] H. Sasayama, K. Kawabe, S. Tomoda, I. Ohsawa, K. Kageyama, N. Ogata, Effect of lamina thickness on first ply failure in multidirectionally laminated composites, in: *Proceedings of the 8th Japan SAMPE Symposium*, SAMPE, 2003.
- [4] K. Yamaguchi, H. Hahn, The improved ply cracking resistance of thinly laminates, in: *Proceedings of the 15th International Conference on Composite Materials (ICCM-15)*, SAMPE, 2005.

- 415 [5] S. Tsai, S. Sihh, R. Kim, Thin ply composites, in: Proceedings of 46th AIAA/ASME/AHS/ASC Structures, Structural Dynamics & Materials Conference, 2005.
- [6] S. Sihh, R. Kim, K. Kawabe, S. Tsai, Experimental studies of thin-ply laminated composites, *Composites Science and Technology* 67 (6) (2007) 996–1008. doi:10.1016/j.compscitech.2006.06.008.
- 420 [7] T. Yokozeki, Y. Aoki, T. Ogasawara, Experimental characterization of strength and damage resistance properties of thin-ply carbon fiber/toughened epoxy laminates, *Composite Structures* 82 (3) (2008) 382–389. doi:10.1016/j.compstruct.2007.01.015.
- 425 [8] T. Yokozeki, A. Kuroda, A. Yoshimura, T. Ogasawara, T. Aoki, Damage characterization in thin-ply composite laminates under out-of-plane transverse loadings, *Composite Structures* 93 (1) (2010) 49–57. doi:10.1016/j.compstruct.2010.06.016.
- [9] H. Saito, H. Takeuchi, I. Kimpara, Experimental evaluation of the damage growth restraining in 90 layer of thin-ply cfrp cross-ply laminates, *Advanced Composite Materials* 21 (1) (2012) 57–66. doi:10.1163/156855112X629522.
- 430 [10] A. Arteiro, G. Catalanotti, J. Xavier, P. Camanho, Notched response of non-crimp fabric thin-ply laminates, *Composites Science and Technology* 79 (2013) 97–114. doi:10.1016/j.compscitech.2013.02.001.
- 435 [11] A. Arteiro, G. Catalanotti, J. Xavier, P. Camanho, Large damage capability of non-crimp fabric thin-ply laminates, *Composites Part A: Applied Science and Manufacturing* 63 (2014) 110–122. doi:10.1016/j.compositesa.2014.04.002.
- [12] R. Amacher, J. Cugnoni, J. Botsis, L. Sorensen, W. Smith, C. Dransfeld, Thin ply composites: Experimental characterization and modeling of size-

- 440 effects, *Composites Science and Technology* 101 (2014) 121–132. doi:10.1016/j.compscitech.2014.06.027.
- [13] G. Guillet, A. Turon, J. Costa, J. Renart, P. Linde, J. Mayugo, Damage occurrence at edges of non-crimp-fabric thin-ply laminates under off-axis uniaxial loading, *Composites Science and Technology* 98 (2014) 44–50. doi:10.1016/j.compscitech.2014.04.014.
- 445 [14] C. Huang, S. Ju, M. He, Q. Zheng, Y. He, J. Xiao, J. Zhang, D. Jiang, Identification of failure modes of composite thin-ply laminates containing circular hole under tension by acoustic emission signals, *Composite Structures* 206 (2018) 70–79. doi:10.1016/j.compstruct.2018.08.019.
- [15] J. Cugnoni, R. Amacher, S. Kohler, J. Brunner, E. Kramer, C. Dransfeld, W. Smith, K. Scobbie, L. Sorensen, J. Botsis, Towards aerospace grade thin-ply composites: Effect of ply thickness, fibre, matrix and interlayer toughening on strength and damage tolerance, *Composites Science and Technology* 168 (2018) 467–477. doi:10.1016/j.compscitech.2018.08.037.
- 455 [16] J.-B. Moon, M.-G. Kim, C.-G. Kim, S. Bhowmik, Improvement of tensile properties of CFRP composites under LEO space environment by applying MWNTs and thin-ply, *Composites Part A: Applied Science and Manufacturing* 42 (6) (2011) 694–701. doi:10.1016/j.compositesa.2011.02.011.
- 460 [17] Y. H. N. Kim, S. Ko, W.-S. Lay, J. Tian, P. Chang, S. U. Thielk, H.-J. Bang, J. Yang, Effects of shallow biangle, thin-ply laminates on structural performance of composite wings, *AIAA Journal* 55 (6) (2017) 2086–2092. doi:10.2514/1.j055465.
- [18] A. Kopp, S. Stappert, D. Mattsson, K. Olofsson, E. Marklund, G. Kurth, E. Mooij, E. Roorda, The aurora space launcher concept, *CEAS Space Journal* 10 (2) (2017) 167–187. doi:10.1007/s12567-017-0184-2.
- 465

- [19] D. A. McCarville, J. C. Guzman, A. K. Dillon, J. R. Jackson, J. O. Birkland, 3.5 Design, Manufacture and Test of Cryotank Components, Elsevier, 2018, pp. 153–179. doi:10.1016/b978-0-12-803581-8.09958-6.
- 470 [20] J. E. Bailey, A. Parvizi, On fibre debonding effects and the mechanism of transverse-ply failure in cross-ply laminates of glass fibre/thermoset composites, *Journal of Materials Science* 16 (3) (1981) 649–659. doi:10.1007/bf02402782.
- 475 [21] V. Kushch, S. Shmegeera, P. Brøndsted, L. Mishnaevsky, Numerical simulation of progressive debonding in fiber reinforced composite under transverse loading, *International Journal of Engineering Science* 49 (1) (2011) 17–29. doi:10.1016/j.ijengsci.2010.06.020.
- 480 [22] L. P. Canal, C. González, J. Segurado, J. LLorca, Intraply fracture of fiber-reinforced composites: Microscopic mechanisms and modeling, *Composites Science and Technology* 72 (11) (2012) 1223–1232. doi:10.1016/j.compscitech.2012.04.008.
- 485 [23] L. Bouhala, A. Makradi, S. Belouettar, H. Kiefer-Kamal, P. Frères, Modelling of failure in long fibres reinforced composites by x-FEM and cohesive zone model, *Composites Part B: Engineering* 55 (2013) 352–361. doi:10.1016/j.compositesb.2012.12.013.
- [24] M. Herráez, D. Mora, F. Naya, C. S. Lopes, C. González, J. LLorca, Transverse cracking of cross-ply laminates: A computational micromechanics perspective, *Composites Science and Technology* 110 (2015) 196–204. doi:10.1016/j.compscitech.2015.02.008.
- 490 [25] L. E. Asp, L. A. Berglund, P. Gudmundson, Effects of a composite-like stress state on the fracture of epoxies, *Composites Science and Technology* 53 (1) (1995) 27–37. doi:10.1016/0266-3538(94)00075-1.
- [26] V. Mantič, Interface crack onset at a circular cylindrical inclusion under a remote transverse tension. application of a coupled stress and energy

- 495 criterion, *International Journal of Solids and Structures* 46 (6) (2009) 1287–1304. doi:10.1016/j.ijsolstr.2008.10.036.
- [27] R. Krueger, Virtual crack closure technique: History, approach, and applications, *Applied Mechanics Reviews* 57 (2) (2004) 109. doi:10.1115/1.1595677.
- 500 [28] J. R. Rice, A path independent integral and the approximate analysis of strain concentration by notches and cracks, *Journal of Applied Mechanics* 35 (2) (1968) 379. doi:10.1115/1.3601206.
- [29] M. Toya, A crack along the interface of a circular inclusion embedded in an infinite solid, *Journal of the Mechanics and Physics of Solids* 22 (5) (1974) 325–348. doi:10.1016/0022-5096(74)90002-7.
- 505 [30] F. París, J. C. Caño, J. Varna, The fiber-matrix interface crack — a numerical analysis using boundary elements, *International Journal of Fracture* 82 (1) (1996) 11–29. doi:10.1007/bf00017861.
- [31] L. Zhuang, A. Pupurs, J. Varna, R. Talreja, Z. Ayadi, Effects of inter-fiber spacing on fiber-matrix debond crack growth in unidirectional composites under transverse loading, *Composites Part A: Applied Science and Manufacturing* 109 (2018) 463–471. doi:10.1016/j.compositesa.2018.03.031.
- 510 [32] M. Muñoz-Reja, L. Távara, V. Mantič, P. Cornetti, Crack onset and propagation at fibre-matrix elastic interfaces under biaxial loading using finite fracture mechanics, *Composites Part A: Applied Science and Manufacturing* 82 (2016) 267–278. doi:10.1016/j.compositesa.2015.09.023.
- 515 [33] E. Correa, V. Mantič, F. París, Effect of thermal residual stresses on matrix failure under transverse tension at micromechanical level: A numerical and experimental analysis, *Composites Science and Technology* 71 (5) (2011) 622–629. doi:10.1016/j.compscitech.2010.12.027.
- 520

- [34] E. Correa, F. París, V. Mantič, Effect of the presence of a secondary transverse load on the inter-fibre failure under tension, *Engineering Fracture Mechanics* 103 (2013) 174–189. doi:10.1016/j.engfracmech.2013.02.026.
- 525 [35] E. Correa, F. París, V. Mantič, Effect of a secondary transverse load on the inter-fibre failure under compression, *Composites Part B: Engineering* 65 (2014) 57–68. doi:10.1016/j.compositesb.2014.01.005.
- [36] C. Sandino, E. Correa, F. París, Numerical analysis of the influence of a nearby fibre on the interface crack growth in composites under transverse tensile load, *Engineering Fracture Mechanics* 168 (2016) 58–75. doi:10.1016/j.engfracmech.2016.01.022.
- 530 [37] C. Sandino, E. Correa, F. París, Interface crack growth under transverse compression: nearby fibre effect, in: *Proceeding of the 18th European Conference on Composite Materials (ECCM-18)*, 2018.
- 535 [38] J. Varna, L. Q. Zhuang, A. Pupurs, Z. Ayadi, Growth and interaction of debonds in local clusters of fibers in unidirectional composites during transverse loading, *Key Engineering Materials* 754 (2017) 63–66. doi:10.4028/www.scientific.net/kem.754.63.
- [39] M. Velasco, E. Graciani, L. Távara, E. Correa, F. París, BEM multiscale modelling involving micromechanical damage in fibrous composites, *Engineering Analysis with Boundary Elements* 93 (2018) 1–9. doi:10.1016/j.enganabound.2018.03.012.
- 540 [40] F. París, M. L. Velasco, E. Correa, Micromechanical study on the influence of scale effect in the first stage of damage in composites, *Composites Science and Technology* 160 (2018) 1–8. doi:10.1016/j.compscitech.2018.03.004.
- 545 [41] Simulia, Providence, RI, USA, ABAQUS/Standard User’s Manual, Version 6.12 (2012).

- [42] H. Zhang, M. Ericson, J. Varna, L. Berglund, Transverse single-fibre test
550 for interfacial debonding in composites: 1. experimental observations, Com-
posites Part A: Applied Science and Manufacturing 28 (4) (1997) 309–315.
doi:10.1016/s1359-835x(96)00123-6.
- [43] L. Di Stasio, J. Varna, Z. Ayadi, Energy release rate of the fiber/matrix
555 interface crack in UD composites under transverse loading: effect of the
fiber volume fraction and of the distance to the free surface and to non-
adjacent debonds, Theoretical and Applied Fracture Mechanics (2019)
102251doi:10.1016/j.tafmec.2019.102251.
- [44] R. Teixeira, S. Pinho, P. Robinson, Thickness-dependence of the translam-
inar fracture toughness: Experimental study using thin-ply composites,
560 Composites Part A: Applied Science and Manufacturing 90 (2016) 33–44.
doi:10.1016/j.compositesa.2016.05.031.
- [45] Z. Hashin, Analysis of composite materials—a survey, Journal of Applied
Mechanics 50 (3) (1983) 481. doi:10.1115/1.3167081.
- [46] R. Christensen, K. Lo, Solutions for effective shear properties in three phase
565 sphere and cylinder models, Journal of the Mechanics and Physics of Solids
27 (4) (1979) 315–330. doi:10.1016/0022-5096(79)90032-2.
- [47] F. París, E. Correa, V. Mantič, Kinking of transversal interface cracks
between fiber and matrix, Journal of Applied Mechanics 74 (4) (2007) 703.
doi:10.1115/1.2711220.
- [48] I. García, V. Mantič, E. Graciani, Debonding at the fibre–matrix interface
570 under remote transverse tension. one debond or two symmetric debonds?,
European Journal of Mechanics - A/Solids 53 (2015) 75–88. doi:10.1016/
j.euromechsol.2015.02.007.