

# Computing energy release rates using the Virtual Crack Closure Technique with the Finite Element Method: analytical discussion

**Luca Di Stasio<sup>1,2,a</sup>, Janis Varna<sup>2,b</sup> and Zoubir Ayadi<sup>1,c</sup>**

<sup>1</sup>SI2M, IJL, EEIGM, Université de Lorraine, 6 Rue Bastien Lepage, F-54010 Nancy, France

<sup>2</sup>Division of Polymer Engineering, Luleå University of Technology, SE-97187 Luleå, Sweden

E-mail: <sup>a</sup>luca.di-stasio@univ-lorraine.fr, <sup>b</sup>janis.varna@ltu.se, <sup>c</sup>zoubir.ayadi@univ-lorraine.fr

**Abstract.** The effect of debond size and crack tip orientation of mode splitting in the Virtual Crack Closure Technique is analyzed by means of analytical derivations. The total energy release rate is shown to have no direct dependence on the debond angular size, but only an indirect one through the FEM solution of the crack displacement field in the crack tip neighbourhood.

## List of acronyms

|      |                                 |
|------|---------------------------------|
| VCCT | Virtual Crack Closure Technique |
| BEM  | Boundary Element Method         |
| FEM  | Finite Element Method           |

### List of symbols

|                             |                              |                                                                            |
|-----------------------------|------------------------------|----------------------------------------------------------------------------|
| $G_I$                       | $\left[\frac{J}{m^2}\right]$ | Mode I energy release rate                                                 |
| $G_{II}$                    | $\left[\frac{J}{m^2}\right]$ | Mode II energy release rate                                                |
| $G_{TOT}$                   | $\left[\frac{J}{m^2}\right]$ | Total energy release rate                                                  |
| $G_{I,r\theta}$             | $\left[\frac{J}{m^2}\right]$ | Mode I energy release rate in $r - \theta$ reference frame                 |
| $G_{II,r\theta}$            | $\left[\frac{J}{m^2}\right]$ | Mode II energy release rate in $r - \theta$ reference frame                |
| $G_{TOT,r\theta}$           | $\left[\frac{J}{m^2}\right]$ | Total energy release rate in $r - \theta$ reference frame                  |
| $\tilde{G}_{I,xy}$          | $\left[\frac{J}{m^2}\right]$ | Mode I energy release rate of equivalent crack in $x - y$ reference frame  |
| $\tilde{G}_{II,xy}$         | $\left[\frac{J}{m^2}\right]$ | Mode II energy release rate of equivalent crack in $x - y$ reference frame |
| $\tilde{G}_{TOT,xy}$        | $\left[\frac{J}{m^2}\right]$ | Total energy release rate of equivalent crack in $x - y$ reference frame   |
| $R_f$                       | $[\mu m]$                    | Fiber radius                                                               |
| $a$                         | $[\mu m]$                    | Debond size                                                                |
| $\Delta a$                  | $[\mu m]$                    | Debond increment                                                           |
| $\Delta \theta$             | $[rad]$                      | Half debond angular size                                                   |
| $\delta$                    | $[rad]$                      | Angular size of element at the interface close to the crack tip            |
| $u_{x,[A-Z]}$               | $[\mu m]$                    | Displacement along $x$ of a point labeled with a letter in [A-Z]           |
| $u_{y,[A-Z]}$               | $[\mu m]$                    | Displacement along $y$ of a point labeled with a letter in [A-Z]           |
| $u_x$                       | $[\mu m]$                    | Displacement along $x$ -direction                                          |
| $u_y$                       | $[\mu m]$                    | Displacement along $y$ -direction                                          |
| $u_r$                       | $[\mu m]$                    | Displacement along $r$ -direction                                          |
| $u_\theta$                  | $[\mu m]$                    | Displacement along $\theta$ -direction                                     |
| $F_{x,[A-Z]}$               | $[\mu m]$                    | Force along $x$ at a point labeled with a letter in [A-Z]                  |
| $F_{y,[A-Z]}$               | $[\mu m]$                    | Force along $y$ at a point labeled with a letter in [A-Z]                  |
| $F_x$                       | $[\mu m]$                    | Force along $x$ -direction                                                 |
| $F_y$                       | $[\mu m]$                    | Force along $y$ -direction                                                 |
| $F_r$                       | $[\mu m]$                    | Force along $r$ -direction                                                 |
| $F_\theta$                  | $[\mu m]$                    | Force along $\theta$ -direction                                            |
| $\underline{\underline{R}}$ | $[-]$                        | Rotation matrix                                                            |

### 1. FEM formulation with quadrilateral elements

$$\Pi(u_i) = \int_V \sigma_{ij} \varepsilon_{ij} dV + \int_V \rho \ddot{u}_i u_i dV - \int_V F_i^T u_i dV - \int_S f_i^T u_i dS \quad (1)$$

$$\Pi(u_i) = \int_V \sigma_{ij} \varepsilon_{ij} dV - \int_V F_i^T u_i dV - \int_S f_i^T u_i dS \quad (2)$$

$$\varepsilon_{ij} = \frac{1}{2} (u_{i,j} + u_{j,i}) \quad (3)$$

$$\underline{\underline{\varepsilon}}(x, y) = \underline{\underline{\tilde{B}}} \cdot \underline{u}(x, y) \quad (4)$$

$$\underline{\underline{\tilde{B}}} = \begin{bmatrix} \frac{\partial}{\partial x} & 0 \\ 0 & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial x} \end{bmatrix} \quad (5)$$

$$\underline{\underline{\sigma}} = \underline{\underline{D}} \cdot \underline{\underline{\varepsilon}} \quad (6)$$

$$\underline{\underline{\sigma}} = \begin{bmatrix} \sigma_{xx} \\ \sigma_{yy} \\ \tau_{xy} \end{bmatrix} \quad \underline{\underline{\varepsilon}} = \begin{bmatrix} \varepsilon_{xx} \\ \varepsilon_{yy} \\ \gamma_{xy} \end{bmatrix} \quad (7)$$

$$\underline{\underline{D}} = \begin{bmatrix} E_1 & E_2 & 0 \\ E_2 & E_1 & 0 \\ 0 & 0 & G \end{bmatrix} \quad \text{with } G = \frac{E}{2(1+\nu)} \text{ for an isotropic material} \quad (8)$$

$$\begin{aligned} E_1 &= \frac{E}{1-\nu^2} & E_2 &= \nu E_1 & \text{for plane stress} \\ E_1 &= \frac{E(1-\nu)}{(1+\nu)(1-2\nu)} & E_2 &= \frac{\nu E_1}{1-\nu} & \text{for plane strain} \end{aligned} \quad (9)$$

$$\begin{aligned} \Pi(\underline{u}) &= \frac{1}{2} \int_V \underline{\underline{\varepsilon}}^T \underline{\underline{D}} \cdot \underline{\underline{\varepsilon}} dV - \int_V \underline{F}^T \underline{u} dV - \int_S \underline{f}^T \underline{u} dS = \\ &= \frac{1}{2} \int_V \underline{u}^T \underline{\underline{\tilde{B}}}^T \underline{\underline{D}} \cdot \underline{\underline{\tilde{B}}} \cdot \underline{u} dV - \int_V \underline{F}^T \underline{u} dV - \int_S \underline{f}^T \underline{u} dS \end{aligned} \quad (10)$$

$$\delta \Pi(\delta \underline{u}) = 0 \quad (11)$$

$$\begin{aligned}
\delta\Pi(\delta\underline{u}) &= \Pi(\underline{u} + \delta\underline{u}) - \Pi(\underline{u}) = \\
&= \frac{1}{2} \int_V (\underline{u} + \delta\underline{u})^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot (\underline{u} + \delta\underline{u}) dV - \int_V \underline{F}^T (\underline{u} + \delta\underline{u}) dV - \int_S \underline{f}^T (\underline{u} + \delta\underline{u}) dS + \\
&- \frac{1}{2} \int_V \underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \underline{u} dV + \int_V \underline{F}^T \underline{u} dV + \int_S \underline{f}^T \underline{u} dS = \\
&= \frac{1}{2} \int_V \underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \underline{u} dV + \frac{1}{2} \int_V \delta\underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \delta\underline{u} dV \xrightarrow{\approx 0} + \\
&+ \frac{1}{2} \int_V \underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \delta\underline{u} dV + \frac{1}{2} \int_V \delta\underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \underline{u} dV + \\
&- \int_V \underline{F}^T \underline{u} dV - \int_V \underline{F}^T \delta\underline{u} dV + \\
&- \int_S \underline{f}^T \underline{u} dS - \int_S \underline{f}^T \delta\underline{u} dS + \\
&- \frac{1}{2} \int_V \underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \underline{u} dV + \int_V \underline{F}^T \underline{u} dV + \int_S \underline{f}^T \underline{u} dS = \\
&= \int_V \underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \delta\underline{u} dV - \int_V \underline{F}^T \delta\underline{u} dV - \int_S \underline{f}^T \delta\underline{u} dS
\end{aligned} \tag{12}$$

$$\int_V \delta\underline{u}^T \underline{\tilde{B}}^T \underline{D} \cdot \underline{\tilde{B}} \cdot \underline{u} dV - \int_V \delta\underline{u}^T \underline{F} dV - \int_S \delta\underline{u}^T \underline{f} dS = 0 \tag{13}$$

$$\underline{u} = \begin{bmatrix} u_x(x, y) \\ u_y(x, y) \end{bmatrix} \quad \underline{u}_N = \begin{bmatrix} u_{1,x} \\ u_{1,y} \\ u_{2,x} \\ u_{2,y} \\ u_{3,x} \\ u_{3,y} \\ u_{4,x} \\ u_{4,y} \\ u_{4,x} \\ u_{4,y} \end{bmatrix} \quad \text{or} \quad \underline{u}_N = \begin{bmatrix} u_{1,x} \\ u_{1,y} \\ u_{2,x} \\ u_{2,y} \\ u_{3,x} \\ u_{3,y} \\ u_{4,x} \\ u_{4,y} \\ u_{5,x} \\ u_{5,y} \\ u_{6,x} \\ u_{6,y} \\ u_{7,x} \\ u_{7,y} \\ u_{8,x} \\ u_{8,y} \end{bmatrix} \tag{14}$$

$$\underline{u} = \underline{\underline{N}} \cdot \underline{u}_N \tag{15}$$

$$\underline{\underline{N}} = \begin{bmatrix} N_1 & 0 & N_2 & 0 & N_3 & 0 & N_4 & 0 \\ 0 & N_1 & 0 & N_2 & 0 & N_3 & 0 & N_4 \end{bmatrix} \tag{16}$$

$$\underline{\underline{N}} = \begin{bmatrix} N_1 & 0 & N_2 & 0 & N_3 & 0 & N_4 & 0 & N_5 & 0 & N_6 & 0 & N_7 & 0 & N_8 & 0 \\ 0 & N_1 & 0 & N_2 & 0 & N_3 & 0 & N_4 & 0 & N_5 & 0 & N_6 & 0 & N_7 & 0 & N_8 \end{bmatrix} \tag{17}$$

$$\begin{cases} N_1 = N_1(\xi, \eta) \\ N_2 = N_2(\xi, \eta) \\ N_3 = N_3(\xi, \eta) \\ N_4 = N_4(\xi, \eta) \end{cases} \quad \text{with} \quad \begin{cases} \xi = \xi(x, y) \\ \eta = \eta(x, y) \end{cases} \quad \text{for isoparametric elements} \quad (18)$$

$$\underline{\underline{B}} = \underline{\underline{\tilde{B}}} \cdot \underline{\underline{N}} = \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \frac{\partial N_2}{\partial x} & 0 & \frac{\partial N_3}{\partial x} & 0 & \frac{\partial N_4}{\partial x} & 0 \\ 0 & \frac{\partial N_1}{\partial y} & 0 & \frac{\partial N_2}{\partial y} & 0 & \frac{\partial N_3}{\partial y} & 0 & \frac{\partial N_4}{\partial y} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial y} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial y} & \frac{\partial N_3}{\partial x} & \frac{\partial N_4}{\partial y} & \frac{\partial N_4}{\partial x} \end{bmatrix} \quad (19)$$

$$\begin{aligned} \underline{\underline{B}} &= \underline{\underline{\tilde{B}}} \cdot \underline{\underline{N}} = \\ &= \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \frac{\partial N_2}{\partial x} & 0 & \frac{\partial N_3}{\partial x} & 0 & \frac{\partial N_4}{\partial x} & 0 & \frac{\partial N_5}{\partial x} & 0 & \frac{\partial N_6}{\partial x} & 0 & \frac{\partial N_7}{\partial x} & 0 & \frac{\partial N_8}{\partial x} & 0 \\ 0 & \frac{\partial N_1}{\partial y} & 0 & \frac{\partial N_2}{\partial y} & 0 & \frac{\partial N_3}{\partial y} & 0 & \frac{\partial N_4}{\partial y} & 0 & \frac{\partial N_5}{\partial y} & 0 & \frac{\partial N_6}{\partial y} & 0 & \frac{\partial N_7}{\partial y} & 0 & \frac{\partial N_8}{\partial y} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial y} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial y} & \frac{\partial N_3}{\partial x} & \frac{\partial N_4}{\partial y} & \frac{\partial N_4}{\partial x} & \frac{\partial N_5}{\partial y} & \frac{\partial N_5}{\partial x} & \frac{\partial N_6}{\partial y} & \frac{\partial N_6}{\partial x} & \frac{\partial N_7}{\partial y} & \frac{\partial N_7}{\partial x} & \frac{\partial N_8}{\partial y} & \frac{\partial N_8}{\partial x} \end{bmatrix} \end{aligned} \quad (20)$$

$$\delta \underline{u} = \delta (\underline{\underline{N}} \cdot \underline{u}_N) = \underline{\underline{N}} \delta \underline{u}_N \quad (21)$$

$$\int_V \delta \underline{u}_N^T \underline{\underline{N}}^T \underline{\underline{\tilde{B}}}^T \underline{\underline{D}} \cdot \underline{\underline{\tilde{B}}} \cdot \underline{\underline{N}} \cdot \underline{u}_N dV - \int_V \delta \underline{u}_N^T \underline{\underline{N}}^T \underline{F} dV - \int_S \delta \underline{u}_N^T \underline{\underline{N}}^T \underline{f} dS = 0 \quad (22)$$

$$\delta \underline{u}_N^T \left( \int_V \underline{\underline{B}}^T \underline{\underline{D}} \cdot \underline{\underline{B}} dV \cdot \underline{u}_N - \int_V \underline{\underline{N}}^T \underline{F} dV - \int_S \underline{\underline{N}}^T \underline{f} dS \right) = 0 \quad (23)$$

$$\underline{k} \cdot \underline{u}_N = \underline{F}_N \quad \underline{k} = \int_V (\underline{\underline{B}}^T \underline{\underline{D}} \cdot \underline{\underline{B}}) dV \quad \underline{F}_N = \int_V \underline{\underline{N}}^T \underline{F} dV + \int_S \underline{\underline{N}}^T \underline{f} dS \quad (24)$$

$$\begin{cases} N_1(\xi, \eta) = \frac{1}{4}(1-\xi)(1-\eta) \\ N_2(\xi, \eta) = \frac{1}{4}(1+\xi)(1-\eta) \\ N_3(\xi, \eta) = \frac{1}{4}(1+\xi)(1+\eta) \\ N_4(\xi, \eta) = \frac{1}{4}(1-\xi)(1+\eta) \end{cases} \quad \begin{cases} N_1(\xi, \eta) = \frac{1}{4}(1-\xi)(1-\eta)(-\xi-\eta-1) \\ N_2(\xi, \eta) = \frac{1}{4}(1+\xi)(1-\eta)(\xi-\eta-1) \\ N_3(\xi, \eta) = \frac{1}{4}(1+\xi)(1+\eta)(\xi+\eta-1) \\ N_4(\xi, \eta) = \frac{1}{4}(1-\xi)(1+\eta)(-\xi+\eta-1) \\ N_5(\xi, \eta) = \frac{1}{2}(1-\xi^2)(1-\eta) \\ N_6(\xi, \eta) = \frac{1}{2}(1+\xi)(1-\eta^2) \\ N_7(\xi, \eta) = \frac{1}{2}(1-\xi^2)(1+\eta) \\ N_8(\xi, \eta) = \frac{1}{2}(1-\xi)(1-\eta^2) \end{cases} \quad (25)$$

$$\begin{cases} \frac{\partial N_1(\xi, \eta)}{\partial \xi} = -\frac{1}{4}(1-\eta) \\ \frac{\partial N_2(\xi, \eta)}{\partial \xi} = \frac{1}{4}(1-\eta) \\ \frac{\partial N_3(\xi, \eta)}{\partial \xi} = \frac{1}{4}(1+\eta) \\ \frac{\partial N_4(\xi, \eta)}{\partial \xi} = -\frac{1}{4}(1+\eta) \\ \frac{\partial N_1(\xi, \eta)}{\partial \eta} = -\frac{1}{4}(1-\xi) \\ \frac{\partial N_2(\xi, \eta)}{\partial \eta} = -\frac{1}{4}(1+\xi) \\ \frac{\partial N_3(\xi, \eta)}{\partial \eta} = \frac{1}{4}(1+\xi) \\ \frac{\partial N_4(\xi, \eta)}{\partial \eta} = \frac{1}{4}(1-\xi) \end{cases} \quad (26)$$

$$\left\{ \begin{array}{l} \frac{\partial N_1(\xi, \eta)}{\partial \xi} = \frac{1}{4} (1 - \eta) (2\xi + \eta) \\ \frac{\partial N_2(\xi, \eta)}{\partial \xi} = \frac{1}{4} (1 - \eta) (2\xi - \eta) \\ \frac{\partial N_3(\xi, \eta)}{\partial \xi} = \frac{1}{4} (1 + \eta) (2\xi + \eta) \\ \frac{\partial N_4(\xi, \eta)}{\partial \xi} = \frac{1}{4} (1 + \eta) (2\xi - \eta) \\ \frac{\partial N_5(\xi, \eta)}{\partial \xi} = -\xi (1 - \eta) \\ \frac{\partial N_6(\xi, \eta)}{\partial \xi} = \frac{1}{2} (1 - \eta^2) \\ \frac{\partial N_7(\xi, \eta)}{\partial \xi} = -\xi (1 + \eta) \\ \frac{\partial N_8(\xi, \eta)}{\partial \xi} = -\frac{1}{2} (1 - \eta^2) \\ \frac{\partial N_1(\xi, \eta)}{\partial \eta} = \frac{1}{4} (1 - \xi) (2\eta + \xi) \\ \frac{\partial N_2(\xi, \eta)}{\partial \eta} = \frac{1}{4} (1 + \xi) (2\eta - \xi) \\ \frac{\partial N_3(\xi, \eta)}{\partial \eta} = \frac{1}{4} (1 + \xi) (2\eta + \xi) \\ \frac{\partial N_4(\xi, \eta)}{\partial \eta} = \frac{1}{4} (1 - \xi) (2\eta - \xi) \\ \frac{\partial N_5(\xi, \eta)}{\partial \eta} = -\frac{1}{2} (1 - \xi^2) \\ \frac{\partial N_6(\xi, \eta)}{\partial \eta} = -\eta (1 + \xi) \\ \frac{\partial N_7(\xi, \eta)}{\partial \eta} = \frac{1}{2} (1 - \xi^2) \\ \frac{\partial N_8(\xi, \eta)}{\partial \eta} = -\eta (1 - \xi) \end{array} \right. \quad (27)$$

$$\underline{p} = \underline{\underline{N}} \cdot \underline{p}_N \quad (28)$$

$$\underline{p} = \begin{bmatrix} x \\ y \end{bmatrix} \quad \underline{p}_N = \begin{bmatrix} x_1 \\ y_1 \\ x_2 \\ y_2 \\ x_3 \\ y_3 \\ x_4 \\ y_4 \end{bmatrix} \quad \text{or} \quad \underline{p}_N = \begin{bmatrix} x_1 \\ y_1 \\ x_2 \\ y_2 \\ x_3 \\ y_3 \\ x_4 \\ y_4 \\ x_5 \\ y_5 \\ x_6 \\ y_6 \\ x_7 \\ y_7 \\ x_8 \\ y_8 \end{bmatrix} \quad (29)$$

$$\begin{aligned} x &= x(\xi, \eta) = N_1(\xi, \eta) x_1 + N_2(\xi, \eta) x_2 + N_3(\xi, \eta) x_3 + N_4(\xi, \eta) x_4 \\ y &= y(\xi, \eta) = N_1(\xi, \eta) y_1 + N_2(\xi, \eta) y_2 + N_3(\xi, \eta) y_3 + N_4(\xi, \eta) y_4 \end{aligned} \quad (30)$$

$$\begin{aligned} x &= x(\xi, \eta) = N_1(\xi, \eta) x_1 + N_2(\xi, \eta) x_2 + N_3(\xi, \eta) x_3 + N_4(\xi, \eta) x_4 + \\ &\quad + N_5(\xi, \eta) x_5 + N_6(\xi, \eta) x_6 + N_7(\xi, \eta) x_7 + N_8(\xi, \eta) x_8 \\ y &= y(\xi, \eta) = N_1(\xi, \eta) y_1 + N_2(\xi, \eta) y_2 + N_3(\xi, \eta) y_3 + N_4(\xi, \eta) y_4 + \\ &\quad + N_5(\xi, \eta) y_5 + N_6(\xi, \eta) y_6 + N_7(\xi, \eta) y_7 + N_8(\xi, \eta) y_8 \end{aligned} \quad (31)$$



$$\begin{aligned}
g &= \det \left( \underline{\underline{g}} \right) = \\
&= \left( \frac{\partial x}{\partial \xi} \frac{\partial x}{\partial \xi} + \frac{\partial y}{\partial \xi} \frac{\partial y}{\partial \xi} \right) \left( \frac{\partial x}{\partial \eta} \frac{\partial x}{\partial \eta} + \frac{\partial y}{\partial \eta} \frac{\partial y}{\partial \eta} \right) - \left( \frac{\partial x}{\partial \eta} \frac{\partial x}{\partial \xi} + \frac{\partial y}{\partial \eta} \frac{\partial y}{\partial \xi} \right) \left( \frac{\partial x}{\partial \xi} \frac{\partial x}{\partial \eta} + \frac{\partial y}{\partial \xi} \frac{\partial y}{\partial \eta} \right)
\end{aligned} \tag{41}$$

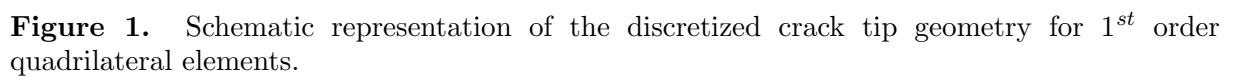
$$dV(x, y) = \sqrt{g} dV(\xi, \eta) \tag{42}$$

$$\begin{aligned}
\underline{\underline{k}}_e &= \int_{V_e(x, y)} (\underline{\underline{B}}^T \underline{\underline{D}} \cdot \underline{\underline{B}}) dV_e(x, y) = \int_{V_e(\xi, \eta)} (\underline{\underline{B}}^T \underline{\underline{D}} \cdot \underline{\underline{B}}) \sqrt{g} dV_e(\xi, \eta) \\
&= \int_{-1}^1 \int_{-1}^1 (\underline{\underline{B}}^T \underline{\underline{D}} \cdot \underline{\underline{B}}) \sqrt{g} d\xi d\eta \approx \sum_{i=1}^N \sum_{j=1}^N w_i w_j (\underline{\underline{B}}^T(\xi_i, \eta_j) \cdot \underline{\underline{D}} \cdot \underline{\underline{B}}(\xi_i, \eta_j) \sqrt{g})
\end{aligned} \tag{43}$$

$$k_e = \begin{bmatrix} k_{e|11} & k_{e|12} & k_{e|13} & k_{e|14} & k_{e|15} & k_{e|16} & k_{e|17} & k_{e|18} \\ k_{e|12} & k_{e|22} & k_{e|23} & k_{e|24} & k_{e|25} & k_{e|26} & k_{e|27} & k_{e|28} \\ k_{e|13} & k_{e|23} & k_{e|33} & k_{e|34} & k_{e|35} & k_{e|36} & k_{e|37} & k_{e|38} \\ k_{e|14} & k_{e|24} & k_{e|34} & k_{e|44} & k_{e|45} & k_{e|46} & k_{e|47} & k_{e|48} \\ k_{e|15} & k_{e|25} & k_{e|35} & k_{e|45} & k_{e|55} & k_{e|56} & k_{e|57} & k_{e|58} \\ k_{e|16} & k_{e|26} & k_{e|36} & k_{e|46} & k_{e|56} & k_{e|66} & k_{e|67} & k_{e|68} \\ k_{e|17} & k_{e|27} & k_{e|37} & k_{e|47} & k_{e|57} & k_{e|67} & k_{e|77} & k_{e|78} \\ k_{e|18} & k_{e|28} & k_{e|38} & k_{e|48} & k_{e|58} & k_{e|68} & k_{e|78} & k_{e|88} \end{bmatrix} \tag{44}$$



### 2.1. Definition of crack tip reference frame



$$\begin{bmatrix} r \\ \theta \end{bmatrix} = \underline{\underline{R}} \begin{bmatrix} x \\ y \end{bmatrix} \quad \begin{bmatrix} x \\ y \end{bmatrix} = \underline{\underline{R}}^{-1} \begin{bmatrix} r \\ \theta \end{bmatrix} \quad (46)$$

## 2.2. Calculation of displacements and reaction forces

$$\left\{ \begin{array}{l}
 (k_{e,M|11} + k_{e,M|33}) u_{x,MCT} + (k_{e,M|12} + k_{e,M|34}) u_{y,MCT} + \\
 + k_{e,M|13} u_{x,M} + k_{e,M|14} u_{y,M} + (k_{M|17} + k_{M|35}) u_{N,MC|7} + (k_{M|18} + k_{M|36}) u_{N,MC|8} + \\
 + \sum_{i=5}^6 k_{M|i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|3i} u_{N,MB|i} + k_{M|31} u_{x,NCOI} + k_{M|32} u_{y,NCOI} = 0 \\
 \\
 (k_{e,M|21} + k_{e,M|43}) u_{x,MCT} + (k_{e,M|22} + k_{e,M|44}) u_{y,MCT} + \\
 + k_{e,M|23} u_{x,M} + k_{e,M|24} u_{y,M} + (k_{M|27} + k_{M|45}) u_{N,MC|7} + (k_{M|28} + k_{M|46}) u_{N,MC|8} + \\
 + \sum_{i=5}^6 k_{M|2i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|4i} u_{N,MB|i} + k_{M|41} u_{x,NCOI} + k_{M|42} u_{y,NCOI} = 0 \\
 \\
 (k_{e,F|77} + k_{e,F|55}) u_{x,FCT} + (k_{e,F|78} + k_{e,F|56}) u_{y,FCT} + \\
 + k_{e,F|75} u_{x,F} + k_{e,F|76} u_{y,F} + (k_{F|71} + k_{F|53}) u_{N,FC|1} + (k_{F|72} + k_{F|54}) u_{N,FC|2} + \\
 + \sum_{i=2}^3 k_{F|7i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|5i} u_{N,FB|i} + k_{F|57} u_{x,NCOI} + k_{F|58} u_{y,NCOI} = 0 \\
 \\
 (k_{e,F|87} + k_{e,F|65}) u_{x,FCT} + (k_{e,F|88} + k_{e,F|66}) u_{y,FCT} + \\
 + k_{e,F|85} u_{x,F} + k_{e,F|86} u_{y,F} + (k_{F|81} + k_{F|63}) u_{N,FC|1} + (k_{F|82} + k_{F|64}) u_{N,FC|2} + \\
 + \sum_{i=2}^3 k_{F|8i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|6i} u_{N,FB|i} + k_{F|67} u_{x,NCOI} + k_{F|68} u_{y,NCOI} = 0 \\
 \\
 u_{x,FCT} - u_{x,MCT} - u_{x,DUMMY} = 0 \\
 u_{y,FCT} - u_{y,MCT} - u_{y,DUMMY} = 0 \\
 \\
 u_{x,DUMMY} = 0 \\
 u_{y,DUMMY} = 0
 \end{array} \right. \quad (47)$$

$$\left\{ \begin{array}{l}
 (k_{e,M|11} + k_{e,M|33}) u_{x,MCT} + (k_{e,M|12} + k_{e,M|34}) u_{y,MCT} + \\
 + k_{e,M|13} u_{x,M} + k_{e,M|14} u_{y,M} + (k_{M|17} + k_{M|35}) u_{N,MC|7} + (k_{M|18} + k_{M|36}) u_{N,MC|8} + \\
 + \sum_{i=5}^6 k_{M|i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|3i} u_{N,MB|i} + k_{M|31} u_{x,NCOI} + k_{M|32} u_{y,NCOI} = 0 \\
 \\
 (k_{e,M|21} + k_{e,M|43}) u_{x,MCT} + (k_{e,M|22} + k_{e,M|44}) u_{y,MCT} + \\
 + k_{e,M|23} u_{x,M} + k_{e,M|24} u_{y,M} + (k_{M|27} + k_{M|45}) u_{N,MC|7} + (k_{M|28} + k_{M|46}) u_{N,MC|8} + \\
 + \sum_{i=5}^6 k_{M|2i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|4i} u_{N,MB|i} + k_{M|41} u_{x,NCOI} + k_{M|42} u_{y,NCOI} = 0 \\
 \\
 (k_{e,F|77} + k_{e,F|55}) u_{x,MCT} + (k_{e,F|78} + k_{e,F|56}) u_{y,MCT} + \\
 + k_{e,F|75} u_{x,F} + k_{e,F|76} u_{y,F} + (k_{F|71} + k_{F|53}) u_{N,FC|1} + (k_{F|72} + k_{F|54}) u_{N,FC|2} + \\
 + \sum_{i=2}^3 k_{F|7i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|5i} u_{N,FB|i} + k_{F|57} u_{x,NCOI} + k_{F|58} u_{y,NCOI} = 0 \\
 \\
 (k_{e,F|87} + k_{e,F|65}) u_{x,MCT} + (k_{e,F|88} + k_{e,F|66}) u_{y,MCT} + \\
 + k_{e,F|85} u_{x,F} + k_{e,F|86} u_{y,F} + (k_{F|81} + k_{F|63}) u_{N,FC|1} + (k_{F|82} + k_{F|64}) u_{N,FC|2} + \\
 + \sum_{i=2}^3 k_{F|8i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|6i} u_{N,FB|i} + k_{F|67} u_{x,NCOI} + k_{F|68} u_{y,NCOI} = 0 \\
 \\
 u_{x,FCT} = u_{x,MCT} \\
 u_{y,FCT} = u_{y,MCT} \\
 \\
 R_{x,DUMMY} = R_{x,FCT} = -R_{x,MCT} = F_{x,CT} \\
 R_{y,DUMMY} = R_{y,FCT} = -R_{y,MCT} = F_{y,CT}
 \end{array} \right. \quad (48)$$

$$\left\{ \begin{array}{l}
(k_{e,M|11} + k_{e,M|33} + k_{e,F|77} + k_{e,F|55}) u_{x,MCT} + (k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}) u_{y,MCT} + \\
+ k_{e,M|13} u_{x,M} + k_{e,M|14} u_{y,M} + k_{e,F|75} u_{x,F} + k_{e,F|76} u_{y,F} + \\
+ (k_{M|31} + k_{F|57}) u_{x,NCOI} + (k_{M|32} + k_{F|58}) u_{y,NCOI} + \\
+ (k_{M|17} + k_{M|35}) u_{N,MC|7} + (k_{M|18} + k_{M|36}) u_{N,MC|8} + (k_{F|71} + k_{F|53}) u_{N,FC|1} + (k_{F|72} + k_{F|54}) u_{N,FC|2} + \\
+ \sum_{i=5}^6 k_{M|1i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|3i} u_{N,MB|i} + \sum_{i=2}^3 k_{F|7i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|5i} u_{N,FB|i} = 0 \\
\\
(k_{e,M|21} + k_{e,M|43} + k_{e,F|87} + k_{e,F|65}) u_{x,MCT} + (k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}) u_{y,MCT} + \\
+ k_{e,M|23} u_{x,M} + k_{e,M|24} u_{y,M} + k_{e,F|85} u_{x,F} + k_{e,F|86} u_{y,F} + \\
+ (k_{M|41} + k_{F|67}) u_{x,NCOI} + (k_{M|42} + k_{F|68}) u_{y,NCOI} + \\
+ (k_{M|27} + k_{M|45}) u_{N,MC|7} + (k_{M|28} + k_{M|46}) u_{N,MC|8} + (k_{F|81} + k_{F|63}) u_{N,FC|1} + (k_{F|82} + k_{F|64}) u_{N,FC|2} + \\
+ \sum_{i=2}^3 k_{F|8i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|6i} u_{N,FB|i} + \sum_{i=5}^6 k_{M|2i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|4i} u_{N,MB|i} = 0 \\
\\
u_{x,FCT} = u_{x,MCT} \\
u_{y,FCT} = u_{y,MCT} \\
\\
R_{x,DUMMY} = R_{x,FCT} = -R_{x,MCT} = F_{x,CT} \\
R_{y,DUMMY} = R_{y,FCT} = -R_{y,MCT} = F_{y,CT}
\end{array} \right. \quad (49)$$

$$\left\{ \begin{array}{l}
u_{y,MCT} = -\frac{k_{e,M|11} + k_{e,M|33} + k_{e,F|77} + k_{e,F|55}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} u_{x,MCT} + \\
-\frac{k_{e,M|13} u_{x,M} + k_{e,M|14} u_{y,M} + k_{e,F|75} u_{x,F} + k_{e,F|76} u_{y,F}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} + \\
-\frac{(k_{M|31} + k_{F|57}) u_{x,NCOI} + (k_{M|32} + k_{F|58}) u_{y,NCOI}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} + \\
-\frac{(k_{M|17} + k_{M|35}) u_{N,MC|7} + (k_{M|18} + k_{M|36}) u_{N,MC|8} + (k_{F|71} + k_{F|53}) u_{N,FC|1} + (k_{F|72} + k_{F|54}) u_{N,FC|2}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} + \\
-\frac{\sum_{i=5}^6 k_{M|1i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|3i} u_{N,MB|i} + \sum_{i=2}^3 k_{F|7i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|5i} u_{N,FB|i}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} = 0 \\
\\
\left[ (k_{e,M|21} + k_{e,M|43} + k_{e,F|87} + k_{e,F|65}) + \frac{k_{e,M|11} + k_{e,M|33} + k_{e,F|77} + k_{e,F|55}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} (k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}) \right] u_{x,MCT} + \\
+ \left( k_{e,M|23} - \frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} k_{e,M|13} \right) u_{x,M} + \\
+ \left( k_{e,M|24} - \frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} k_{e,M|14} \right) u_{y,M} + \\
+ \left( k_{e,F|85} - \frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} k_{e,M|75} \right) u_{x,F} + \\
+ \left( k_{e,F|86} - \frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} k_{e,M|76} \right) u_{y,F} + \\
+ \left[ (k_{M|41} + k_{F|67}) - \frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} (k_{M|31} + k_{F|57}) \right] u_{x,NCOI} + \\
+ \left[ (k_{M|42} + k_{F|68}) - \frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} (k_{M|32} + k_{F|58}) \right] u_{y,NCOI} + \\
+ (k_{M|27} + k_{M|45}) u_{N,MC|7} + (k_{M|28} + k_{M|46}) u_{N,MC|8} + (k_{F|81} + k_{F|63}) u_{N,FC|1} + (k_{F|82} + k_{F|64}) u_{N,FC|2} + \\
-\frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} [(k_{M|17} + k_{M|35}) u_{N,MC|7} + (k_{M|18} + k_{M|36}) u_{N,MC|8}] + \\
-\frac{k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}}{k_{e,M|12} + k_{e,M|34} + k_{e,F|78} + k_{e,F|56}} [(k_{F|71} + k_{F|53}) u_{N,FC|1} + (k_{F|72} + k_{F|54}) u_{N,FC|2}] + \\
+ \sum_{i=2}^3 k_{F|8i} u_{N,FC|i} + \sum_{i=1}^2 k_{F|6i} u_{N,FB|i} + \sum_{i=5}^6 k_{M|2i} u_{N,MC|i} + \sum_{i=7}^8 k_{M|4i} u_{N,MB|i} = 0 \\
\\
- (k_{e,M|22} + k_{e,M|44} + k_{e,F|88} + k_{e,F|66}) \\
u_{x,FCT} = u_{x,MCT} \\
u_{y,FCT} = u_{y,MCT} \\
\\
R_{x,DUMMY} = R_{x,FCT} = -R_{x,MCT} = F_{x,CT} \\
R_{y,DUMMY} = R_{y,FCT} = -R_{y,MCT} = F_{y,CT}
\end{array} \right. \quad (50)$$

$$u_x = u_{x,M} - u_{x,F} \quad u_y = u_{y,M} - u_{y,F} \quad (51)$$

$$u_r = \cos(\Delta\theta) u_x + \sin(\Delta\theta) u_y \quad u_\theta = -\sin(\Delta\theta) u_x + \cos(\Delta\theta) u_y \quad (52)$$

$$F_r = \cos(\Delta\theta) F_{x,CT} + \sin(\Delta\theta) F_{y,CT} \quad F_\theta = -\sin(\Delta\theta) F_{x,CT} + \cos(\Delta\theta) F_{y,CT} \quad (53)$$

### 2.3. Calculation of energy release rates

$$\begin{aligned} G_{I,r\theta} &= \frac{1}{2} \frac{F_r u_r}{R_f \delta} = \\ &= \frac{1}{2 R_f \delta} (\cos(\Delta\theta) F_x + \sin(\Delta\theta) F_y) (\cos(\Delta\theta) u_x + \sin(\Delta\theta) u_y) = \\ &= \frac{1}{2 R_f \delta} (\cos^2(\Delta\theta) F_x u_x + (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_y) \end{aligned} \quad (54)$$

$$\begin{aligned} G_{II,r\theta} &= \frac{1}{2} \frac{F_\theta u_\theta}{R_f \delta} = \\ &= \frac{1}{2 R_f \delta} (-\sin(\Delta\theta) F_x + \cos(\Delta\theta) F_y) (-\sin(\Delta\theta) u_x + \cos(\Delta\theta) u_y) = \\ &= \frac{1}{2 R_f \delta} (\sin^2(\Delta\theta) F_x u_x - (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_y u_y) \end{aligned} \quad (55)$$

$$\begin{aligned} G_{TOT,r\theta} &= G_{I,r\theta} + G_{II,r\theta} = \\ &= \frac{1}{2 R_f \delta} (\cos^2(\Delta\theta) F_x u_x + (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_y) + \\ &\quad + \frac{1}{2 R_f \delta} (\sin^2(\Delta\theta) F_x u_x - (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_y u_y) = \\ &= \frac{1}{2 R_f \delta} \left( \begin{array}{c} \xrightarrow{1} \\ (\cos^2(\Delta\theta) + \sin^2(\Delta\theta)) \quad F_x u_x \end{array} \right) + \\ &\quad + \frac{1}{2 R_f \delta} \left( \begin{array}{c} \xrightarrow{0} \\ ((F_x u_y + F_y u_x) - (F_x u_y + F_y u_x)) \quad \cos(\Delta\theta) \sin(\Delta\theta) \end{array} \right) + \\ &\quad + \frac{1}{2 R_f \delta} \left( \begin{array}{c} \xrightarrow{1} \\ (\cos^2(\Delta\theta) + \sin^2(\Delta\theta)) \quad F_y u_y \end{array} \right) = \\ &= \frac{1}{2} \frac{F_x u_x}{R_f \delta} + \frac{1}{2} \frac{F_y u_y}{R_f \delta} = \\ &= \tilde{G}_{I,xy} + \tilde{G}_{II,xy} = \tilde{G}_{TOT,xy} \end{aligned} \quad (56)$$

$$\begin{aligned} G_{I,r\theta} &= \frac{1}{2 R_f \delta} (\cos^2(\Delta\theta) F_x u_x + (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_y) = \\ &= \cos^2(\Delta\theta) \frac{F_x u_x}{2 R_f \delta} + \left( \frac{F_x u_y}{2 R_f \delta} + \frac{F_y u_x}{2 R_f \delta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) \frac{F_y u_y}{2 R_f \delta} = \\ &= \cos^2(\Delta\theta) \tilde{G}_{I,xy} + \left( \tilde{G}_{I,xy} \frac{u_y}{u_x} + \tilde{G}_{II,xy} \frac{u_x}{u_y} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) \tilde{G}_{II,xy} \end{aligned} \quad (57)$$

$$\begin{aligned}
G_{II,r\theta} &= \frac{1}{2R_f\delta} \left( \sin^2(\Delta\theta) F_x u_x - (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_y u_y \right) = \\
&= \sin^2(\Delta\theta) \frac{F_x u_x}{2R_f\delta} - \left( \frac{F_x u_y}{2R_f\delta} + \frac{F_y u_x}{2R_f\delta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) \frac{F_y u_y}{2R_f\delta} = \\
&= \sin^2(\Delta\theta) \tilde{G}_{I,xy} - \left( \tilde{G}_{I,xy} \frac{u_y}{u_x} + \tilde{G}_{II,xy} \frac{u_x}{u_y} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) \tilde{G}_{II,xy}
\end{aligned} \tag{58}$$

2.4. Sensitivity analysis of the FEM solution

$$F_x \sim k_x u_x \quad F_y \sim k_y u_y \tag{59}$$

$$\begin{aligned}
G_{I,r\theta} &\sim \frac{1}{2R_f\delta} \cos^2(\Delta\theta) k_x u_x^2(\Delta\theta) + \\
&\quad + \frac{1}{2R_f\delta} (k_x + k_y) u_x(\Delta\theta) u_y(\Delta\theta) \cos(\Delta\theta) \sin(\Delta\theta) + \\
&\quad + \frac{1}{2R_f\delta} \sin^2(\Delta\theta) k_y u_y^2(\Delta\theta)
\end{aligned} \tag{60}$$

$$\begin{aligned}
G_{II,r\theta} &\sim \frac{1}{2R_f\delta} \sin^2(\Delta\theta) k_x u_x^2(\Delta\theta) + \\
&\quad - \frac{1}{2R_f\delta} (k_x + k_y) u_x(\Delta\theta) u_y(\Delta\theta) \cos(\Delta\theta) \sin(\Delta\theta) + \\
&\quad + \frac{1}{2R_f\delta} \cos^2(\Delta\theta) k_y u_y^2(\Delta\theta)
\end{aligned} \tag{61}$$

$$G_{TOT,r\theta} \sim \frac{1}{2R_f\delta} (k_x u_x^2(\Delta\theta) + k_y u_y^2(\Delta\theta)) \tag{62}$$

$$\begin{aligned}
\frac{\partial G_{I,r\theta}}{\partial \Delta\theta} &\sim \frac{1}{R_f\delta} \cos^2(\Delta\theta) k_x u_x(\Delta\theta) \frac{\partial u_x(\Delta\theta)}{\partial \Delta\theta} + \\
&\quad + \frac{1}{2R_f\delta} (k_x + k_y) \left( \frac{\partial u_x(\Delta\theta)}{\partial \Delta\theta} u_y(\Delta\theta) + u_x(\Delta\theta) \frac{\partial u_y(\Delta\theta)}{\partial \Delta\theta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \\
&\quad + \frac{1}{R_f\delta} \sin^2(\Delta\theta) k_y u_y(\Delta\theta) \frac{\partial u_y(\Delta\theta)}{\partial \Delta\theta} + \\
&\quad + \frac{1}{2R_f\delta} (k_y u_y^2(\Delta\theta) - k_x u_x^2(\Delta\theta)) \sin(2\Delta\theta) + \\
&\quad + \frac{1}{2R_f\delta} (k_x u_x(\Delta\theta) u_y(\Delta\theta) + k_y u_y(\Delta\theta) u_x(\Delta\theta)) \cos(2\Delta\theta)
\end{aligned} \tag{63}$$

$$\begin{aligned}
\frac{\partial G_{II,r\theta}}{\partial \Delta\theta} \sim & \frac{1}{R_f \delta} \sin^2(\Delta\theta) k_x u_x(\Delta\theta) \frac{\partial u_x(\Delta\theta)}{\partial \Delta\theta} + \\
& - \frac{1}{2R_f \delta} (k_x + k_y) \left( \frac{\partial u_x(\Delta\theta)}{\partial \Delta\theta} u_y(\Delta\theta) + u_x(\Delta\theta) \frac{\partial u_y(\Delta\theta)}{\partial \Delta\theta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \\
& + \frac{1}{R_f \delta} \cos^2(\Delta\theta) k_y u_y(\Delta\theta) \frac{\partial u_y(\Delta\theta)}{\partial \Delta\theta} + \\
& + \frac{1}{2R_f \delta} (k_x u_x^2(\Delta\theta) - k_y u_y^2(\Delta\theta)) \sin(2\Delta\theta) + \\
& - \frac{1}{2R_f \delta} (k_x u_x(\Delta\theta) u_y(\Delta\theta) + k_y u_y(\Delta\theta) u_x(\Delta\theta)) \cos(2\Delta\theta)
\end{aligned} \tag{64}$$

$$\frac{\partial G_{TOT,r\theta}}{\partial \Delta\theta} \sim \frac{1}{R_f \delta} \left( k_x u_x(\Delta\theta) \frac{\partial u_x(\Delta\theta)}{\partial \Delta\theta} + k_y u_y(\Delta\theta) \frac{\partial u_y(\Delta\theta)}{\partial \Delta\theta} \right) \tag{65}$$

## 2.5. Discretization error

$$u_r = \cos(\Delta\theta - \delta) u_x + \sin(\Delta\theta - \delta) u_y \quad u_\theta = -\sin(\Delta\theta - \delta) u_x + \cos(\Delta\theta - \delta) u_y \tag{66}$$

$$F_r = \cos(\Delta\theta) F_{x,CT} + \sin(\Delta\theta) F_{y,CT} \quad F_\theta = -\sin(\Delta\theta) F_{x,CT} + \cos(\Delta\theta) F_{y,CT} \tag{67}$$

$$\begin{aligned}
\tilde{G}_{I,r\theta} &= \frac{1}{2} \frac{F_r u_r}{R_f \delta} = \\
&= \frac{1}{2R_f \delta} (\cos(\Delta\theta) F_x + \sin(\Delta\theta) F_y) (\cos(\Delta\theta - \delta) u_x + \sin(\Delta\theta - \delta) u_y) = \\
&= \frac{1}{2R_f \delta} (\cos(\Delta\theta) F_x + \sin(\Delta\theta) F_y) (\cos(\Delta\theta) u_x + \sin(\Delta\theta) u_y) \cos(\delta) + \\
&\quad + \frac{1}{2R_f \delta} (\cos(\Delta\theta) F_x + \sin(\Delta\theta) F_y) (\sin(\Delta\theta) u_x - \cos(\Delta\theta) u_y) \sin(\delta) = \\
&= \frac{1}{2R_f \delta} (\cos^2(\Delta\theta) F_x u_x + (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_y) \cos(\delta) + \\
&\quad + \frac{1}{2R_f \delta} (-\cos^2(\Delta\theta) F_x u_y + (F_x u_x - F_y u_y) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_x) \sin(\delta) = \\
&= G_{I,r\theta} \cos(\delta) + \\
&\quad + \frac{1}{2R_f \delta} (-\cos^2(\Delta\theta) F_x u_y + (F_x u_x - F_y u_y) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_x) \sin(\delta)
\end{aligned} \tag{68}$$

$$\begin{aligned}
\lim_{\delta \rightarrow 0} \tilde{G}_{I,r\theta} &= \lim_{\delta \rightarrow 0} G_{I,r\theta} \cos(\delta) + \\
&+ \lim_{\delta \rightarrow 0} \frac{1}{2R_f\delta} \left( -\cos^2(\Delta\theta) F_x u_y + (F_x u_x - F_y u_y) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_x \right) \sin(\delta) = \\
&= G_{I,r\theta} + \\
&+ \frac{1}{2R_f} \left( -\cos^2(\Delta\theta) F_x u_y + (F_x u_x - F_y u_y) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_x \right) \lim_{\delta \rightarrow 0} \frac{\sin(\delta)}{\delta} \\
&= G_{I,r\theta} \cos(\delta) + \frac{1}{2R_f} \left( -\cos^2(\Delta\theta) F_x u_y + (F_x u_x - F_y u_y) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_y u_x \right)
\end{aligned} \tag{69}$$

$$\begin{aligned}
G_{II,r\theta} &= \frac{1}{2} \frac{F_\theta u_\theta}{R_f \delta} = \\
&= \frac{1}{2R_f \delta} \left( -\sin(\Delta\theta) F_x + \cos(\Delta\theta) F_y \right) \left( -\sin(\Delta\theta - \delta) u_x + \cos(\Delta\theta - \delta) u_y \right) = \\
&= \frac{1}{2R_f \delta} \left( \sin^2(\Delta\theta) F_x u_x - (F_x u_y + F_y u_x) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_y u_y \right)
\end{aligned} \tag{70}$$

2.6. Contact region

$$u_r = 0 \tag{71}$$

$$\cos(\Delta\theta) u_x + \sin(\Delta\theta) u_y = 0 \tag{72}$$

$$u_y = -\frac{u_x}{\tan(\Delta\theta)} \tag{73}$$

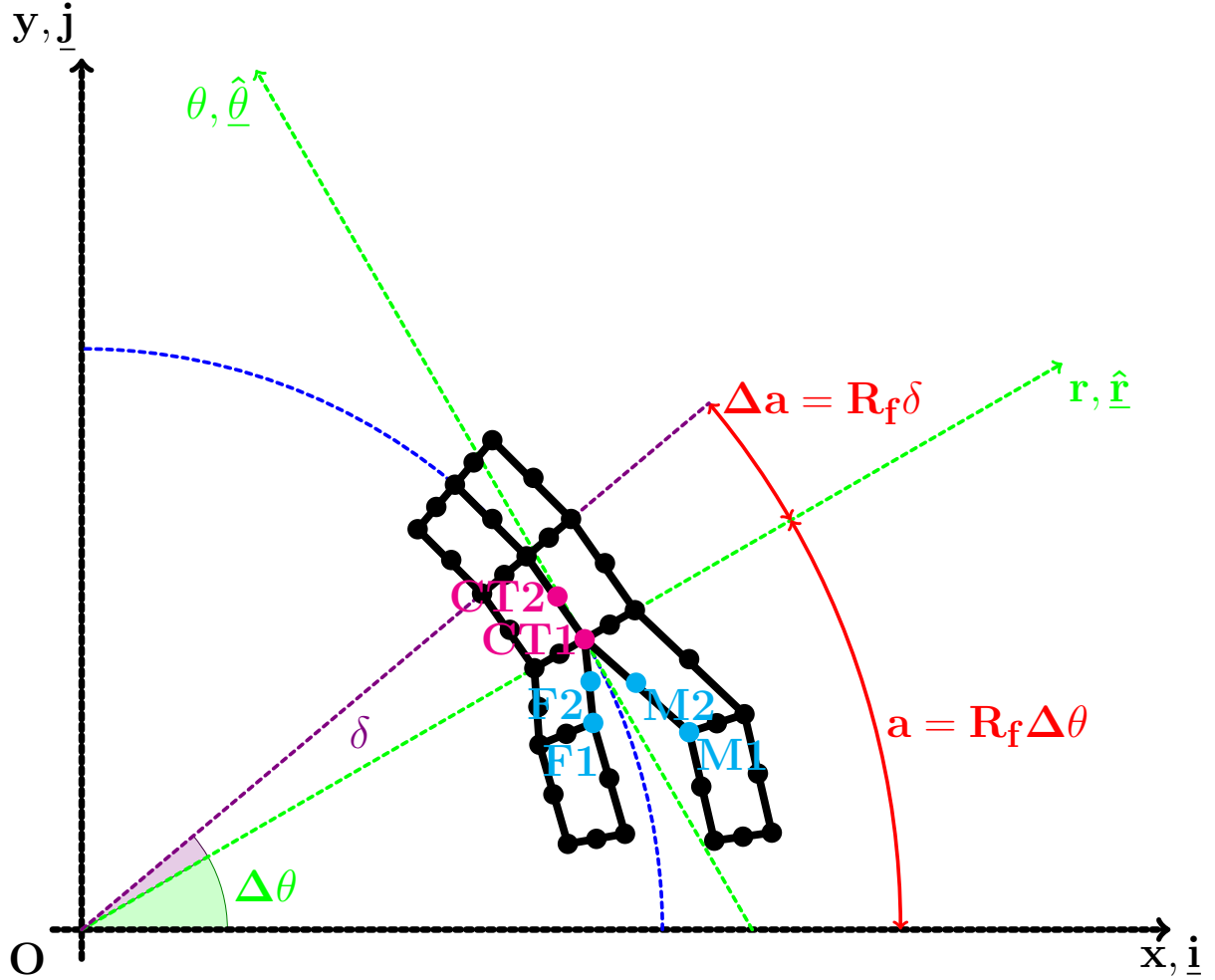
$$\begin{aligned}
u_\theta &= -\sin(\Delta\theta) u_x - \frac{\cos^2(\Delta\theta)}{\sin(\Delta\theta)} u_x = \\
&= -\frac{u_x}{\sin(\Delta\theta)}
\end{aligned} \tag{74}$$

$$F_r = \cos(\Delta\theta) F_{x,CT} + \sin(\Delta\theta) F_{y,CT} \quad F_\theta = -\sin(\Delta\theta) F_{x,CT} + \cos(\Delta\theta) F_{y,CT} \tag{75}$$

$$G_{I,r\theta} = \frac{1}{2} \frac{F_r u_r}{R_f \delta} = 0 \tag{76}$$

$$\begin{aligned}
G_{II,r\theta} &= \frac{1}{2} \frac{F_\theta u_\theta}{R_f \delta} = \\
&= \frac{1}{2R_f \delta} \left( -\sin(\Delta\theta) F_x + \cos(\Delta\theta) F_y \right) \left( -\frac{u_x}{\sin(\Delta\theta)} \right) = \\
&= \frac{1}{2R_f \delta} \left( F_x u_x - \frac{F_y u_x}{\tan(\Delta\theta)} \right) \\
&= \frac{1}{2R_f \delta} \left( F_x - \frac{F_y}{\tan(\Delta\theta)} \right) u_x
\end{aligned} \tag{77}$$

### 3.1. Definition of crack tip reference frame



**Figure 2.** Schematic representation of the discretized crack tip geometry for  $2^{nd}$  order quadrilateral elements.

$$\underline{\underline{R}} = \begin{bmatrix} \cos(\Delta\theta) & \sin(\Delta\theta) \\ -\sin(\Delta\theta) & \cos(\Delta\theta) \end{bmatrix} \quad \underline{\underline{R}}^{-1} = \underline{\underline{R}}^T = \begin{bmatrix} \cos(\Delta\theta) & -\sin(\Delta\theta) \\ \sin(\Delta\theta) & \cos(\Delta\theta) \end{bmatrix} \quad (78)$$

$$\begin{bmatrix} r \\ \theta \end{bmatrix} = \underline{\underline{R}} \begin{bmatrix} x \\ y \end{bmatrix} \quad \begin{bmatrix} x \\ y \end{bmatrix} = \underline{\underline{R}}^{-1} \begin{bmatrix} r \\ \theta \end{bmatrix} \quad (79)$$

### 3.2. Calculation of displacements and reaction forces

$$\begin{aligned} u_{x,1} &= u_{x,M1} - u_{x,F1} & u_{y,1} &= u_{y,M1} - u_{y,F1} \\ u_{x,2} &= u_{x,M2} - u_{x,F2} & u_{y,2} &= u_{y,M2} - u_{y,F2} \end{aligned} \quad (80)$$

$$\begin{aligned} u_{r,1} &= \cos(\Delta\theta) u_{x,1} + \sin(\Delta\theta) u_{y,1} & u_{\theta,1} &= -\sin(\Delta\theta) u_{x,1} + \cos(\Delta\theta) u_{y,1} \\ u_{r,2} &= \cos(\Delta\theta) u_{x,2} + \sin(\Delta\theta) u_{y,2} & u_{\theta,2} &= -\sin(\Delta\theta) u_{x,2} + \cos(\Delta\theta) u_{y,2} \end{aligned} \quad (81)$$



$$\begin{aligned}
F_{r,1} &= \cos(\Delta\theta) F_{x,1} + \sin(\Delta\theta) F_{y,1} & F_{\theta,1} &= -\sin(\Delta\theta) F_{x,1} + \cos(\Delta\theta) F_{y,1} \\
F_{r,2} &= \cos(\Delta\theta) F_{x,2} + \sin(\Delta\theta) F_{y,2} & F_{\theta,2} &= -\sin(\Delta\theta) F_{x,2} + \cos(\Delta\theta) F_{y,2}
\end{aligned} \tag{82}$$

### 3.3. Calculation of energy release rates

$$\begin{aligned}
G_{I,r\theta} &= \frac{1}{2R_f\delta} (F_{r,1}u_{r,1} + F_{r,2}u_{r,2}) = \\
&= \frac{1}{2R_f\delta} (\cos(\Delta\theta) F_{x,1} + \sin(\Delta\theta) F_{y,1}) (\cos(\Delta\theta) u_{x,1} + \sin(\Delta\theta) u_{y,1}) + \\
&\quad + \frac{1}{2R_f\delta} (\cos(\Delta\theta) F_{x,2} + \sin(\Delta\theta) F_{y,2}) (\cos(\Delta\theta) u_{x,2} + \sin(\Delta\theta) u_{y,2}) + \\
&= \frac{1}{2R_f\delta} (\cos^2(\Delta\theta) F_{x,1}u_{x,1} + (F_{x,1}u_{y,1} + F_{y,1}u_{x,1}) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_{y,1}u_{y,1}) + \\
&\quad + \frac{1}{2R_f\delta} (\cos^2(\Delta\theta) F_{x,2}u_{x,2} + (F_{x,2}u_{y,2} + F_{y,2}u_{x,2}) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_{y,2}u_{y,2})
\end{aligned} \tag{83}$$

$$\begin{aligned}
G_{II,r\theta} &= \frac{1}{2R_f\delta} (F_{\theta,1}u_{\theta,1} + F_{\theta,2}u_{\theta,2}) = \\
&= \frac{1}{2R_f\delta} (-\sin(\Delta\theta) F_{x,1} + \cos(\Delta\theta) F_{y,1}) (-\sin(\Delta\theta) u_{x,1} + \cos(\Delta\theta) u_{y,1}) + \\
&\quad + \frac{1}{2R_f\delta} (-\sin(\Delta\theta) F_{x,2} + \cos(\Delta\theta) F_{y,2}) (-\sin(\Delta\theta) u_{x,2} + \cos(\Delta\theta) u_{y,2}) = \\
&= \frac{1}{2R_f\delta} (\sin^2(\Delta\theta) F_{x,1}u_{x,1} - (F_{x,1}u_{y,1} + F_{y,1}u_{x,1}) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_{y,1}u_{y,1}) + \\
&\quad + \frac{1}{2R_f\delta} (\sin^2(\Delta\theta) F_{x,2}u_{x,2} - (F_{x,2}u_{y,2} + F_{y,2}u_{x,2}) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_{y,2}u_{y,2})
\end{aligned} \tag{84}$$

$$\begin{aligned}
G_{TOT,r\theta} &= G_{I,r\theta} + G_{II,r\theta} = \\
&= \frac{1}{2R_f\delta} \left( \cos^2(\Delta\theta) F_{x,1}u_{x,1} + (F_{x,1}u_{y,1} + F_{y,1}u_{x,1}) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_{y,1}u_{y,1} \right) + \\
&\quad + \frac{1}{2R_f\delta} \left( \cos^2(\Delta\theta) F_{x,2}u_{x,2} + (F_{x,2}u_{y,2} + F_{y,2}u_{x,2}) \cos(\Delta\theta) \sin(\Delta\theta) + \sin^2(\Delta\theta) F_{y,2}u_{y,2} \right) + \\
&\quad + \frac{1}{2R_f\delta} \left( \sin^2(\Delta\theta) F_{x,1}u_{x,1} - (F_{x,1}u_{y,1} + F_{y,1}u_{x,1}) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_{y,1}u_{y,1} \right) + \\
&\quad + \frac{1}{2R_f\delta} \left( \sin^2(\Delta\theta) F_{x,2}u_{x,2} - (F_{x,2}u_{y,2} + F_{y,2}u_{x,2}) \cos(\Delta\theta) \sin(\Delta\theta) + \cos^2(\Delta\theta) F_{y,2}u_{y,2} \right) = \\
&= \frac{1}{2R_f\delta} \cos^2(\Delta\theta) (F_{x,1}u_{x,1} + F_{x,2}u_{x,2} + F_{y,1}u_{y,1} + F_{y,2}u_{y,2}) + \\
&\quad + \frac{1}{2R_f\delta} ((F_{x,1}u_{y,1} + F_{x,1}u_{y,1}) + (F_{y,2}u_{x,2} + F_{y,2}u_{x,2})) \cos(\Delta\theta) \sin(\Delta\theta) + \\
&\quad + \frac{1}{2R_f\delta} \sin^2(\Delta\theta) (F_{x,1}u_{x,1} + F_{x,2}u_{x,2} + F_{y,1}u_{y,1} + F_{y,2}u_{y,2}) + \\
&\quad - \frac{1}{2R_f\delta} ((F_{x,1}u_{y,1} + F_{x,1}u_{y,1}) + (F_{y,2}u_{x,2} + F_{y,2}u_{x,2})) \cos(\Delta\theta) \sin(\Delta\theta) = \\
&= \frac{1}{2R_f\delta} \left( \begin{array}{c} \nearrow 1 \\ (\cos^2(\Delta\theta) + \sin^2(\Delta\theta)) \quad (F_{x,1}u_{x,1} + F_{x,2}u_{x,2}) \end{array} \right) + \\
&\quad + \frac{1}{2R_f\delta} \begin{array}{c} \nearrow 0 \\ ((F_{x,1}u_{y,1} + F_{x,1}u_{y,1}) - (F_{x,1}u_{y,1} + F_{x,1}u_{y,1})) \quad \cos(\Delta\theta) \sin(\Delta\theta) + \end{array} \\
&\quad + \frac{1}{2R_f\delta} \begin{array}{c} \nearrow 0 \\ ((F_{y,2}u_{x,2} + F_{y,2}u_{x,2}) - (F_{y,2}u_{x,2} + F_{y,2}u_{x,2})) \quad \cos(\Delta\theta) \sin(\Delta\theta) + \end{array} \\
&\quad + \frac{1}{2R_f\delta} \left( \begin{array}{c} \nearrow 1 \\ (\cos^2(\Delta\theta) + \sin^2(\Delta\theta)) \quad (F_{y,1}u_{y,1} + F_{y,2}u_{y,2}) \end{array} \right) = \\
&= \frac{1}{2} \frac{F_{x,1}u_{x,1} + F_{x,2}u_{x,2}}{R_f\delta} + \frac{1}{2} \frac{F_{y,1}u_{y,1} + F_{y,2}u_{y,2}}{R_f\delta} = \\
&= \tilde{G}_{I,xy} + \tilde{G}_{II,xy} = \tilde{G}_{TOT,xy}
\end{aligned}$$

$$\begin{aligned}
G_{I,r\theta} &= \cos^2(\Delta\theta) \frac{F_{x,1}u_{x,1} + F_{x,2}u_{x,2}}{2R_f\delta} + \\
&+ \frac{F_{x,1}u_{y,1} + F_{y,1}u_{x,1} + F_{x,2}u_{y,2} + F_{y,2}u_{x,2}}{2R_f\delta} \cos(\Delta\theta) \sin(\Delta\theta) + \\
&+ \sin^2(\Delta\theta) \frac{F_{y,1}u_{y,1} + F_{y,2}u_{y,2}}{2R_f\delta} = \\
&= \cos^2(\Delta\theta) \tilde{G}_{I,xy} + \sin^2(\Delta\theta) \tilde{G}_{II,xy} + \\
&+ \frac{F_{x,1}u_{y,1} + F_{y,1}u_{x,1} + F_{x,2}u_{y,2} + F_{y,2}u_{x,2}}{2R_f\delta} \cos(\Delta\theta) \sin(\Delta\theta)
\end{aligned} \tag{86}$$

$$\begin{aligned}
G_{II,r\theta} &= \sin^2(\Delta\theta) \frac{F_{x,1}u_{x,1} + F_{x,2}u_{x,2}}{2R_f\delta} + \\
&- \frac{F_{x,1}u_{y,1} + F_{y,1}u_{x,1} + F_{x,2}u_{y,2} + F_{y,2}u_{x,2}}{2R_f\delta} \cos(\Delta\theta) \sin(\Delta\theta) + \\
&+ \cos^2(\Delta\theta) \frac{F_{y,1}u_{y,1} + F_{y,2}u_{y,2}}{2R_f\delta} = \\
&= \sin^2(\Delta\theta) \tilde{G}_{I,xy} + \cos^2(\Delta\theta) \tilde{G}_{II,xy} + \\
&- \frac{F_{x,1}u_{y,1} + F_{y,1}u_{x,1} + F_{x,2}u_{y,2} + F_{y,2}u_{x,2}}{2R_f\delta} \cos(\Delta\theta) \sin(\Delta\theta)
\end{aligned} \tag{87}$$

### 3.4. Sensitivity analysis of the FEM solution

$$\begin{aligned}
F_{x,1} &\sim k_{x,1}u_{x,1} & F_{y,1} &\sim k_{y,1}u_{y,1} \\
F_{x,2} &\sim k_{x,2}u_{x,2} & F_{y,2} &\sim k_{y,2}u_{y,2}
\end{aligned} \tag{88}$$

$$\begin{aligned}
G_{I,r\theta} &\sim \frac{1}{2R_f\delta} \cos^2(\Delta\theta) (k_{x,1}u_{x,1}^2 + k_{x,2}u_{x,2}^2) + \\
&+ \frac{1}{2R_f\delta} \cos(\Delta\theta) \sin(\Delta\theta) (k_{x,1}u_{x,1}u_{y,1} + k_{y,1}u_{y,1}u_{x,1} + k_{x,2}u_{x,2}u_{y,2} + k_{y,2}u_{y,2}u_{x,2}) + \\
&+ \frac{1}{2R_f\delta} \sin^2(\Delta\theta) (k_{y,1}u_{y,1}^2 + k_{y,2}u_{y,2}^2)
\end{aligned} \tag{89}$$

$$\begin{aligned}
G_{II,r\theta} &\sim \frac{1}{2R_f\delta} \sin^2(\Delta\theta) (k_{x,1}u_{x,1}^2 + k_{x,2}u_{x,2}^2) + \\
&- \frac{1}{2R_f\delta} \cos(\Delta\theta) \sin(\Delta\theta) (k_{x,1}u_{x,1}u_{y,1} + k_{y,1}u_{y,1}u_{x,1} + k_{x,2}u_{x,2}u_{y,2} + k_{y,2}u_{y,2}u_{x,2}) + \\
&+ \frac{1}{2R_f\delta} \cos^2(\Delta\theta) (k_{y,1}u_{y,1}^2 + k_{y,2}u_{y,2}^2)
\end{aligned} \tag{90}$$

$$G_{TOT,r\theta} \sim \frac{1}{2R_f\delta} ((k_{x,1}u_{x,1}^2(\Delta\theta) + k_{x,2}u_{x,2}^2(\Delta\theta)) + (k_{y,1}u_{y,1}^2(\Delta\theta) + k_{y,2}u_{y,2}^2(\Delta\theta))) \tag{91}$$

$$\begin{aligned}
\frac{\partial G_{I,r\theta}}{\partial \Delta\theta} \sim & \frac{1}{R_f\delta} \cos^2(\Delta\theta) \left( k_{x,1} u_{x,1}(\Delta\theta) \frac{\partial u_{x,1}(\Delta\theta)}{\partial \Delta\theta} + k_{x,2} u_{x,2}(\Delta\theta) \frac{\partial u_{x,2}(\Delta\theta)}{\partial \Delta\theta} \right) + \\
& + \frac{1}{2R_f\delta} (k_{x,1} + k_{y,1}) \left( \frac{\partial u_{x,1}(\Delta\theta)}{\partial \Delta\theta} u_{y,1}(\Delta\theta) + u_{x,1}(\Delta\theta) \frac{\partial u_{y,1}(\Delta\theta)}{\partial \Delta\theta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \\
& + \frac{1}{2R_f\delta} (k_{x,2} + k_{y,2}) \left( \frac{\partial u_{x,2}(\Delta\theta)}{\partial \Delta\theta} u_{y,2}(\Delta\theta) + u_{x,2}(\Delta\theta) \frac{\partial u_{y,2}(\Delta\theta)}{\partial \Delta\theta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \\
& + \frac{1}{R_f\delta} \sin^2(\Delta\theta) \left( k_{y,1} u_{y,1}(\Delta\theta) \frac{\partial u_{y,1}(\Delta\theta)}{\partial \Delta\theta} + k_{y,2} u_{y,2}(\Delta\theta) \frac{\partial u_{y,2}(\Delta\theta)}{\partial \Delta\theta} \right) + \\
& + \frac{1}{2R_f\delta} ((k_{y,1} u_{y,1}^2 + k_{y,2} u_{y,2}^2) - (k_{x,1} u_{x,1}^2 + k_{x,2} u_{x,2}^2)) \sin(2\Delta\theta) + \\
& + \frac{1}{2R_f\delta} ((k_{x,1} + k_{y,1}) u_{x,1} u_{y,1} + (k_{x,2} + k_{y,2}) u_{x,2} u_{y,2}) \cos(2\Delta\theta)
\end{aligned} \tag{92}$$

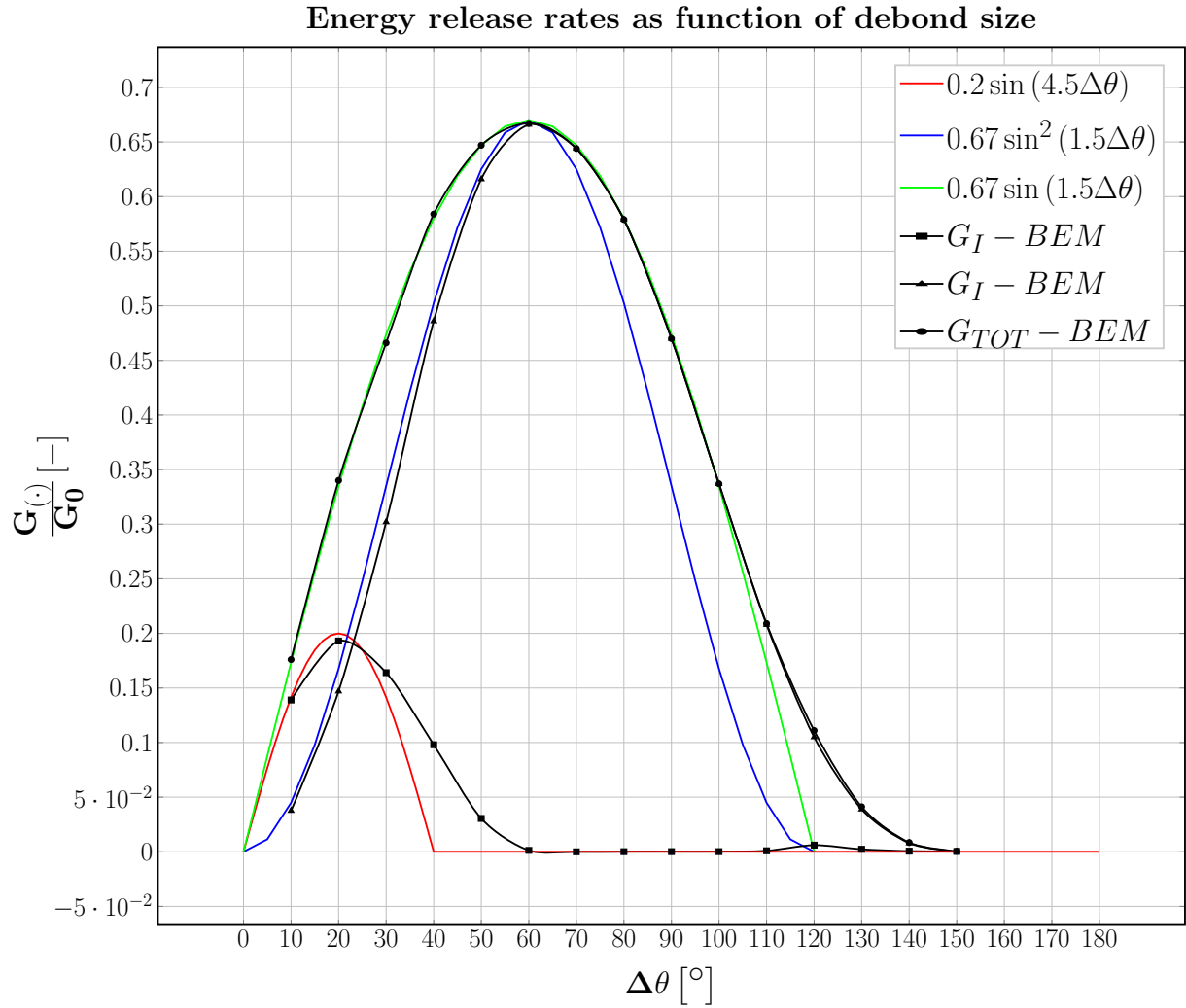
$$\begin{aligned}
\frac{\partial G_{II,r\theta}}{\partial \Delta\theta} \sim & \frac{1}{R_f\delta} \sin^2(\Delta\theta) \left( k_{x,1} u_{x,1}(\Delta\theta) \frac{\partial u_{x,1}(\Delta\theta)}{\partial \Delta\theta} + k_{x,2} u_{x,2}(\Delta\theta) \frac{\partial u_{x,2}(\Delta\theta)}{\partial \Delta\theta} \right) + \\
& - \frac{1}{2R_f\delta} (k_{x,1} + k_{y,1}) \left( \frac{\partial u_{x,1}(\Delta\theta)}{\partial \Delta\theta} u_{y,1}(\Delta\theta) + u_{x,1}(\Delta\theta) \frac{\partial u_{y,1}(\Delta\theta)}{\partial \Delta\theta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \\
& - \frac{1}{2R_f\delta} (k_{x,2} + k_{y,2}) \left( \frac{\partial u_{x,2}(\Delta\theta)}{\partial \Delta\theta} u_{y,2}(\Delta\theta) + u_{x,2}(\Delta\theta) \frac{\partial u_{y,2}(\Delta\theta)}{\partial \Delta\theta} \right) \cos(\Delta\theta) \sin(\Delta\theta) + \\
& + \frac{1}{R_f\delta} \cos^2(\Delta\theta) \left( k_{y,1} u_{y,1}(\Delta\theta) \frac{\partial u_{y,1}(\Delta\theta)}{\partial \Delta\theta} + k_{y,2} u_{y,2}(\Delta\theta) \frac{\partial u_{y,2}(\Delta\theta)}{\partial \Delta\theta} \right) + \\
& + \frac{1}{2R_f\delta} ((k_{x,1} u_{x,1}^2 + k_{x,2} u_{x,2}^2) - (k_{y,1} u_{y,1}^2 + k_{y,2} u_{y,2}^2)) \sin(2\Delta\theta) + \\
& - \frac{1}{2R_f\delta} ((k_{x,1} + k_{y,1}) u_{x,1} u_{y,1} + (k_{x,2} + k_{y,2}) u_{x,2} u_{y,2}) \cos(2\Delta\theta)
\end{aligned} \tag{93}$$

$$G_{TOT,r\theta} \sim \frac{1}{R_f\delta} \left( \left( k_{x,1} u_{x,1} \frac{\partial u_{x,1}}{\partial \Delta\theta} + k_{x,2} u_{x,2} \frac{\partial u_{x,2}}{\partial \Delta\theta} \right) + \left( k_{y,1} u_{y,1} \frac{\partial u_{y,1}}{\partial \Delta\theta} + k_{y,2} u_{y,2} \frac{\partial u_{y,2}}{\partial \Delta\theta} \right) \right) \tag{94}$$

#### 4. Trigonometric interpolation

By inspecting the results of the previous sections, an interpolation of the BEM results is performed manually by trial and error. The following procedure is followed:

- (i) a basis function is selected;
- (ii) the frequency of the trigonometric basis function is calculated based on the position of the maximum value;
- (iii) the amplitude is calculated based on the maximum value.



**Figure 3.** Interpolation of BEM results by manual trial and error.

The good agreement suggests that trigonometric functions are very good candidates for energy release rate data interpolation. The effect of different parameters can thus modeled as the functional variation of frequency (period) and amplitude of the trigonometric basis functions.

#### References

- [1] Griffiths R. 1994 Stiffness matrix of the four-node quadrilateral element in closed form *Int. J. Numer. Meth. Eng.* **57** (2) 109–143

- [2] Krueger R. 2004 Virtual crack closure technique: History, approach, and applications *Appl. Mech. Rev.* **57** (2) 109–143
- [3] ABAQUS 2016 ABAQUS 2016 Analysis User's Manual *Online Documentation Help: Dassault Systèmes*
- [4] Rice J. R. 1968 A Path Independent Integral and the Approximate Analysis of Strain Concentration by Notches and Cracks *J. Appl. Mech.* **35** 379–386