INVESTIGATION OF SCALING LAWS OF THE FIBER/MATRIX INTERFACE CRACK IN POLYMER COMPOSITES THROUGH FINITE ELEMENT-BASED MICROMECHANICAL MODELING

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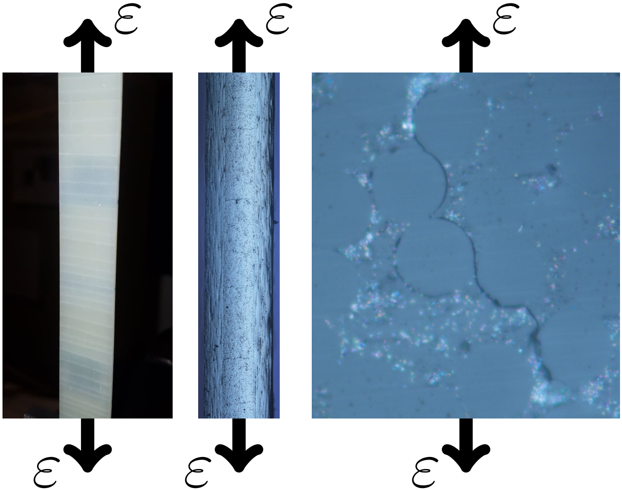
Outline

- Initiation of Transverse Cracking in Fiber Reinforced Polymer Composites (FRPCs): Microscopic Observations & Modeling
- The Fiber-Matrix Interface Crack Problem
- Analysis of the Infinite Reference Volume Element (RVE)
- Conclusions & Outlook

TRANSVERSE CRACKING IN FRPCS

Observations: From Macro to Micro



Left:
front view of $[0, 90_2]_S$, visual inspection.

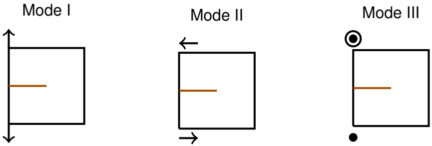
Center:
edge view of $[0, 90]_S$, optical microscope.

Right:
edge view of $[0, 90]_S$, optical microscope.

Mathematical Modeling of Fracture: Linear Elastic Fracture Mechanics (LEFM)

Fracture Mode

$I, II, III, I/II, I/III, II/III$



Variables

geometry
materials
boundary conditions
loading mode
scale

➔ Energy Release Rate G_m

$$G = \frac{\partial W}{\partial A} - \left(\frac{\partial U}{\partial A} + \frac{\partial E_k}{\partial A}\right)$$

➔ Stress Intensity Factor K_m

$$\sigma_m \sim K_m \frac{\alpha}{(x-a)^{\beta}} \quad \alpha, \beta > 0$$

➔ J-Integral J

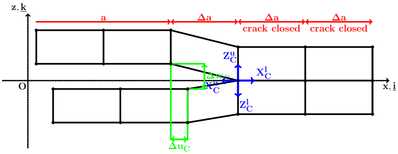
$$J = \lim_{\varepsilon \to 0} \int_{\Gamma_\varepsilon} \left(W(\Gamma)\, n_i - n_j \sigma_{jk} \frac{\partial u_k(\Gamma, x_i)}{\partial x_i} \right) d\Gamma$$

➔ Crack Opening COD & Shear Displacement $CSD_{II/III}$

$$COD = COD\,(p_1, \ldots, p_i, \ldots, p_n) \quad \text{and} \quad CSD = CSD\,(p_1, .$$

Numerical Characterization of Fracture: VCCT & J-Integral

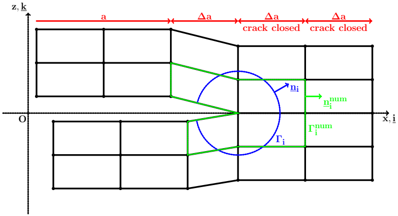
➔ Virtual Crack Closure Technique (VCCT)



$$G_I = \frac{Z_C \Delta w_C}{2B\Delta a} \quad G_{II} = \frac{X_C \Delta u_C}{2B\Delta a}$$

Krueger, 2004

➔ J-Integral

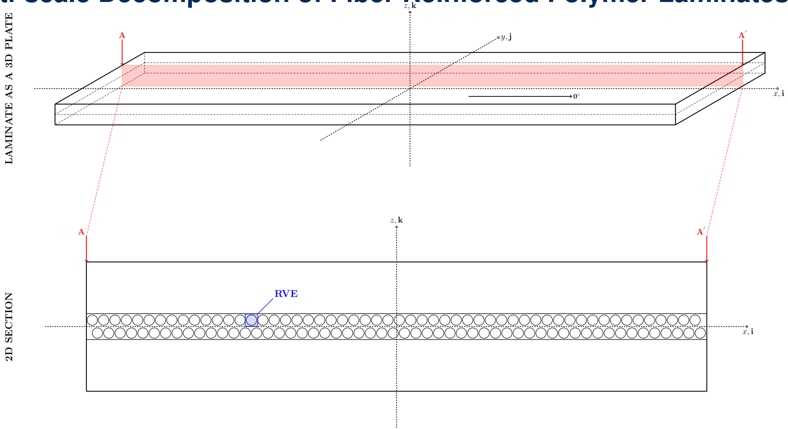


$$J_i = \lim_{\varepsilon \to 0} \int_{\Gamma_\varepsilon} \left(W(\Gamma)\, n_i - n_j \sigma_{jk} \frac{\partial u_k(\Gamma, x_i)}{\partial x_i} \right) d\Gamma$$

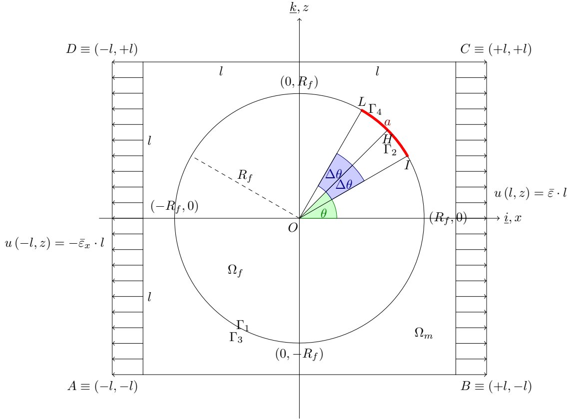
Rice, 1968

↘ The Fiber-Matrix Interface Crack Problem

Multi-scale Decomposition of Fiber Reinforced Polymer Laminates



The Fiber-Matrix Interface Crack Problem: Statement



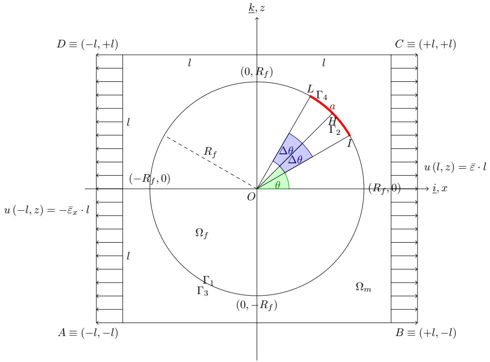
- ➔ 2D space
- ➔ Linear elastic homogeneous isotropic materials
- ➔ Mismatching elastic properties
- ➔ Plane state (strain or stress)
- ➔ Dirichlet-type BC
- ➔ Linear Fracture Mechanics
- ➔ Contact interaction
- ➔ Applied uniaxial traction
- ? SIF, ERR, mode ratio, stress and displacement distribution at the interface

The Fiber-Matrix Interface Crack Problem: Solution

Method	Domain	Natural Variable	Conjugate Variable	Dirichlet BC
Analytical (complex) functions	2D, continuous, infinite	Airy stress potential & stress	Displacement & strain	In stress
	M. Toya (1975), A Crack Along the Interface of a Circular Inclusion Embedded in an Infinite Solid [10].			
Boundary Element Method (BEM)	1D, discrete, finite	Stress, by using Green's potentials or Betti's influence functions	Displacement & strain	In stress
	F. París et al. (1996), The fiber-matrix interface crack - A numerical analysis using Boundary Elements [11].			
Finite Element Method (FEM)	2D, discrete, finite	Displacement	Stress	In displacement

ANALYSIS OF THE INFINITE RVE

The Finite Element Model



- ➔ $\theta\ [^\circ] = 0$, angular position of debond's center
- ➔ $2\Delta\theta\ [^\circ]$, debond's angular size
- ➔ $\delta\ [^\circ]$, angle subtended by an element at the fiber/matrix interface
- ➔ $VF_f\ [-]$, fiber volume fraction
- ➔ $2L\ [\mu m]$, RVE's side length
- ➔ $R_F\ [\mu m]$, fiber radius
- ➔ $\frac{L}{R_f} = \frac{1}{2}\sqrt{\frac{\pi}{VF_f}}\ [-]$, RVE's aspect ratio
- ➔ $\sigma_0\ [MPa] = \frac{E_m}{1-\nu_m^2}\varepsilon_{xx}$, reaction stress of undamaged infinite RVE
- ➔ $G_0\left[\frac{J}{m^2}\right] = \pi R_f \sigma_R^2 \frac{1+(3-4nu_m)}{8G_m}$, normalization G following Toya [10] and París [11]
- ➔ Small displacement formulation

↘ CONCLUSIONS

Conclusions & Outlook

Conclusions

- ➔ There is a limiting value of $\frac{L}{R_f}$ after which models are effectively infinite
- ➔ For models larger than this value, domain size and mesh refinement at the interface has a similar effect on the energy release rate
- ➔ The discrepancy in modes with the use of linear elements might be linked to the deformed shape of crack faces

Outlook

- ➔ Modeling extreme ply geometries, for example a ply with a single layer of fibers bounded by stiffer plies
- ➔ Investigate the effect of clusters of fibers in thin plies
- ➔ Analyzing the effect of complex stress and deformation states, thermal loads, different sets of boundary conditions

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