Effect of uniform distributions of bonded and debonded fibers on the growth of the fiber/matrix interface crack in UD laminates with different fiber contents under transverse loading

Luca Di Stasio^{a,b}, Janis Varna^b, Zoubir Ayadi^a

^a Université de Lorraine, EEIGM, IJL, 6 Rue Bastien Lepage, F-54010 Nancy, France ^bLuleå University of Technology, University Campus, SE-97187 Luleå, Sweden

Abstract

Priority: 1

Type: long article

Target journal(s): Composites Part B: Engineering, Composites Part A: Applied Science and Manufacturing, Composite Science and Technology, Composite Structures, Journal of Composite Materials, Composite Communications

- (a) A debonded fiber every 2 fully (b) Central debonded fiber with 1 fiber bonded ones. each side.
- (c) A debonded fiber every 4 fully (d) Central debonded fiber with 2 bonded ones. fibers each side.
- (e) A debonded fiber every 6 fully (f) Central debonded fiber with 3 fibers bonded ones. each side.

Figure 1: Models of single-ply laminates with a single layer of fibers and debonds repeating at different distances (left column), and corresponding Representative Volume Elements (right column) with symmetry applied on the lower boundary line. The interface crack is represented in red.

- (a) 3 layers with a central line of (b) Central debonded fiber with 1 fiber debonded fibers. above.
- (c) 5 layers with a central line of (d) Central debonded fiber with 2 debonded fibers. fibers above.
- (e) 7 layers with a central line of (f) Central debonded fiber with 3 fibers debonded fibers.

 above.

Figure 2: Models of single-ply laminates with multiple layers of fibers and a central line of debonded fibers (left column), and corresponding Representative Volume Elements (right column) with symmetry applied on the lower boundary line. The interface crack is represented in red.

- (a) 3 layers with a debonded fiber every
- 2 fully bonded ones in the central line of fibers.
- (c) 3 layers with a debonded fiber every 4 fully bonded ones in the central line of fibers.
- (e) 5 layers with a debonded fiber every 4 fully bonded ones in the central line of fibers.
- (g) 3 layers with a debonded fiber every 6 fully bonded ones in the central line of fibers.

- (b) Central debonded fiber with 1 fiber on each side and 1 above.
- (d) Central debonded fiber with 2 fibers on each side and 1 above.
- (f) Central debonded fiber with 2 fibers on each side and 2 above.
- (h) Central debonded fiber with 3 fibers on each side and 1 above.

Figure 3: Models of single-ply laminates with multiple layers of fibers with debonds repeating at different distances in the central line of fibers (left column), and corresponding Representative Volume Elements (right column) with symmetry applied on the lower boundary line.

- (a) Single layer of debonded fibers.
- (c) Infinite number of layers of debonded fibers.
- (b) Element with a single debonded fiber and free boundary on top.
- (d) Element with a single debonded fiber and coupling of vertical displacements along the upper boundary.

Figure 4: Models of single-ply laminates with all the fibers debonded (left column), and corresponding Representative Volume Elements (right column) with symmetry applied on the lower boundary line.

- main parameters.
- (a) Schematic of the model with its (b) Detail of the mesh in the crack tip's neighborhood.

Figure 5: Details and main parameters of the Finite Element model.

Figure 6: Validation of the single fiber model for the infinite matrix case with respect to the BEM solution in [].

(a) Single fiber model with coupling of vertical displacements along the upper ary on top.

(b) Single fiber model with coupling of vertical displacements along the upper boundary.

(c) 1 fiber each side.

(d) 1 fiber above.

(f) 5 fibers above.

(g) 10 fibers each side.

(h) 10 fibers above.

(i) 1 fiber each side, 1 above.

(j) 3 fibers each side, 1 above.

(k) 2 fibers each side, 2 above.

(l) 5 fibers each side, 2 above.

Figure 7: A view of the effect of fiber volume fraction on Mode I ERR across different models.

(a) Single fiber model with coupling of vertical displacements along the upper boundary.

(c) 1 fiber each side.

(d) 1 fiber above.

(e) 5 fibers each side.

(f) 5 fibers above.

(g) 10 fibers each side.

(h) 10 fibers above.

(i) 1 fiber each side, 1 above.

(j) 3 fibers each side, 1 above.

(k) 2 fibers each side, 2 above.

(l) 5 fibers each side, 2 above.

Figure 8: A view of the effect of fiber volume fraction on Mode II ERR across different models.

1. Introduction

2. RVE models & FE discretization

- 2.1. Models of Representative Volume Element(RVE)
- 2.2. Finite Element (FE) discretization
- 5 2.3. Validation of the model

3. Results & Discussion 4

- 3.1. Effect of Fiber Volume Fraction
- 3.2. Interaction between debonds in UD laminates with a single layer of fibers
- 3.3. Influence of layers of fully bonded fibers on debond's growth in a centrally located line of debonded fibers

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 9: Effect of the interaction between debonds appearing at regular intervals on Mode I ERR in a single-ply laminate with a single layer of fibers at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 10: Effect of the interaction between debonds appearing at regular intervals on Mode II ERR in a single-ply laminate with a single layer of fibers at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 11: Influence of layers of fully bonded fibers on debond's growth in Mode I ERR in a centrally located line of debonded fibers at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 12: Influence of layers of fully bonded fibers on debond's growth in Mode II ERR in a centrally located line of debonded fibers at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 13: Effect of the interaction between debonds appearing at regular intervals on Mode I ERR in a single-ply laminate with multiple layers of fibers at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 14: Effect of the interaction between debonds appearing at regular intervals on Mode II ERR in a single-ply laminate with multiple layers of fibers at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 15: Comparison of Mode I ERR between the single fiber model with free upper boundary and the multiple fibers model with fibers only on the side at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 16: Comparison of Mode II ERR between the single fiber model with free upper boundary and the multiple fibers model with fibers only on the side at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 17: Comparison of Mode I ERR between the single fiber model with coupling conditions along the upper boundary and the multiple fibers model with fibers above and both above and on the side at different levels of fiber volume fraction V_f .

(a)
$$V_f = 30\%$$
. (b) $V_f = 50\%$.

(c)
$$V_f = 60\%$$
. (d) $V_f = 65\%$.

Figure 18: Comparison of Mode II ERR between the single fiber model with coupling conditions along the upper boundary and the multiple fibers model with fibers above and both above and on the side at different levels of fiber volume fraction V_f .