

Constitutive modeling for laminates with fiber/matrix interface cracks under transverse loading

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Abstract

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1. Introduction

Review damage characterization [1, 2, 3]

Shear-lag [4]

Stress-transfer [5, 6]

5 Stress-based variational [7, 8, 9]+angle ply [9]

Displacement-based variational [10]

Self-consistent approach [11]

Finite strip approach [12]

Continuum damage mechanics [13, 14, 15]

10 Discrete damage mechanics [16]

Cylindrical model [17]

Reissner mixed variational principle [18]

Development of glob-loc model [19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32]

2. Derivation of constitutive relations

15 2.1. Reference frames

Local reference frame of k -th layer: index 1 is the in-plane longitudinal or fiber or 0° -direction; index 2 is the in-plane transverse or 90° -direction; index 3 is the out-of-plane or through-the-thickness direction.

Global reference frame of laminate: index x is the in-plane longitudinal
 20 or laminate 0° direction; index y is the in-plane transverse direction; index
 z is the out-of-plane or through-the-thickness direction.

2.2. Crack density

Scalar density Normalized volume of cracks V_{an} is the ratio of cracked volume
 V_a to material volume V

$$V_{an} = \frac{V_a}{V} \quad (1)$$

25 V_a is equal to the product of total crack surface S_C and average crack
 opening u_a

$$V_{an} = \frac{S_C u_a}{V} = \frac{S_C}{V} u_a = \rho_C u_a \quad (2)$$

The ratio $\frac{S_C}{V}$ has a size of $\frac{1}{length}$ and correspond to the crack density ρ_C .
 It means: product of crack density and average crack opening is equal to
 normalized volume of cracks.

30 Applying the previous Principle to debonds, we have:

$$\begin{aligned} \rho_D &= \frac{\text{total area of debonds}}{\text{total layer volume}} = \frac{n_D w R_f \Delta \theta}{L_{lam} w t_{90^\circ}} = \frac{n_D \mathcal{W}}{L_{lam} \mathcal{W} t_{90^\circ}} R_f \Delta \theta = \frac{1}{n 2L} \frac{1}{k 2L} R_f \Delta \theta = \\ &= \frac{1}{nk 4L^2} R_f \Delta \theta = \frac{V_f}{nk \pi R_f^2} R_f \Delta \theta = \frac{V_f}{nk R_f} \frac{\Delta \theta}{\pi} \end{aligned} \quad (3)$$

Second-order tensor density

Fourth-order tensor density

2.3. Homogenization

$$\sigma_{ij}^{avg} = \frac{1}{V} \int_V \sigma_{ij} dV \quad \varepsilon_{ij}^{avg} = \frac{1}{V} \int_V \varepsilon_{ij} dV \quad (4)$$

$$\underline{\tilde{\sigma}}_k^{avg} = \underline{\tilde{Q}}_{\underline{\underline{k}}} (\underline{\tilde{\varepsilon}}_k^{avg} - \underline{\tilde{\alpha}}_k \Delta T) \quad (5)$$

$$\underline{\tilde{\sigma}}_{LAM} = \underline{\tilde{\sigma}}^{avg} = \frac{1}{V} \int_V \underline{\tilde{\sigma}} dV = \frac{1}{V} \sum_{k=1}^N \int_{V_k} \underline{\tilde{\sigma}} dV_k = \sum_{k=1}^N \underline{\tilde{\sigma}}_k^{avg} \frac{t_k}{h} \quad (6)$$

$$\varepsilon_{ij}^{avg} = \frac{1}{V} \int_V \varepsilon_{ij} dV = \frac{1}{V} \int_V \frac{1}{2} (u_{i,j} + u_{j,i}) dV = \frac{1}{V} \int_S \frac{1}{2} (u_i n_j + u_j n_i) dS \quad (7)$$

$$\begin{aligned} \varepsilon_{ij}^{avg} &= \frac{1}{V} \int_S \frac{1}{2} (u_i n_j + u_j n_i) dS = \\ &= \frac{1}{V} \int_{S_B} \frac{1}{2} (u_i n_j + u_j n_i) dS + \frac{1}{V} \int_{S_C} \frac{1}{2} (u_i n_j + u_j n_i) dS = \\ &= \varepsilon_{ij}^{applied} + \beta_{ij} \end{aligned} \quad (8)$$

$$\underline{\tilde{\varepsilon}}_k^{avg} = \underline{\tilde{\varepsilon}}_k^{applied} + \underline{\tilde{\beta}}_k = \underline{\tilde{\varepsilon}}_k^{LAM} + \underline{\tilde{\beta}}_k \quad (9)$$

$$\underline{\tilde{\sigma}}_{LAM} = \frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \left(\underline{\tilde{\varepsilon}}_k^{LAM} - \underline{\tilde{\alpha}}_k \Delta T + \underline{\tilde{\beta}}_k \right) \quad (10)$$

$$\underline{\tilde{\sigma}}_{LAM} = \underline{Q}_{eff}^{LAM} \underline{\tilde{\varepsilon}}^{LAM} \quad (11)$$

$$\underline{Q}_{eff}^{LAM} \underline{\tilde{\varepsilon}}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \right) \underline{\tilde{\varepsilon}}^{LAM} + \frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \underline{\tilde{\beta}}_k \quad (12)$$

$$\underline{Q}_{eff}^{LAM} \underline{\tilde{\varepsilon}}^{LAM} \cdot \frac{\underline{\tilde{\varepsilon}}^{LAM}}{\underline{\tilde{\varepsilon}}^{LAM} \cdot \underline{\tilde{\varepsilon}}^{LAM}} = \left(\frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \right) \underline{\tilde{\varepsilon}}^{LAM} \cdot \frac{\underline{\tilde{\varepsilon}}^{LAM}}{\underline{\tilde{\varepsilon}}^{LAM} \cdot \underline{\tilde{\varepsilon}}^{LAM}} + \left(\frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \underline{\tilde{\beta}}_k \right) \cdot \frac{\underline{\tilde{\varepsilon}}^{LAM}}{\underline{\tilde{\varepsilon}}^{LAM} \cdot \underline{\tilde{\varepsilon}}^{LAM}} \quad (13)$$

$$\underline{Q}_{eff}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \right) + \frac{1}{h} \sum_{k=1}^N t_k \underline{\tilde{Q}}_{\underline{\underline{k}}} \frac{\underline{\tilde{\beta}}_k \cdot \underline{\tilde{\varepsilon}}^{LAM}}{\underline{\tilde{\varepsilon}}^{LAM} \cdot \underline{\tilde{\varepsilon}}^{LAM}} \quad (14)$$

$$\underline{T}_{\underline{\underline{k}}} = \begin{bmatrix} \cos^2(\theta_k) & \sin^2(\theta_k) & 2 \cos(\theta_k) \sin(\theta_k) \\ \sin^2(\theta_k) & \cos^2(\theta_k) & -2 \cos(\theta_k) \sin(\theta_k) \\ -\cos(\theta_k) \sin(\theta_k) & \cos(\theta_k) \sin(\theta_k) & \cos^2(\theta_k) - \sin^2(\theta_k) \end{bmatrix} \quad (15)$$

$$\tilde{Q}_{\underline{\underline{k}}} = T_{\underline{\underline{k}}}^{-1} Q_{\underline{\underline{k}}} \left(T_{\underline{\underline{k}}}^{-1} \right)^T \quad (16)$$

$$\begin{aligned} Q_{eff}^{LAM} &= \left(\frac{1}{h} \sum_{k=1}^N t_k T_{\underline{\underline{k}}}^{-1} Q_{\underline{\underline{k}}} \left(T_{\underline{\underline{k}}}^{-1} \right)^T \right) + \frac{1}{h} \sum_{k=1}^N t_k T_{\underline{\underline{k}}}^{-1} Q_{\underline{\underline{k}}} \left(T_{\underline{\underline{k}}}^{-1} \right)^T \frac{T_{\underline{\underline{k}}}^{-1} \tilde{\beta}_{\underline{\underline{k}}} \left(T_{\underline{\underline{k}}}^{-1} \right)^T \cdot \tilde{\varepsilon}^{LAM}}{\tilde{\varepsilon}^{LAM} \cdot \tilde{\varepsilon}^{LAM}} = \\ &= \frac{1}{h} \sum_{k=1}^N t_k T_{\underline{\underline{k}}}^{-1} Q_{\underline{\underline{k}}} \left(T_{\underline{\underline{k}}}^{-1} \right)^T \left(1 + \frac{T_{\underline{\underline{k}}}^{-1} \tilde{\beta}_{\underline{\underline{k}}} \left(T_{\underline{\underline{k}}}^{-1} \right)^T \cdot \tilde{\varepsilon}^{LAM}}{\tilde{\varepsilon}^{LAM} \cdot \tilde{\varepsilon}^{LAM}} \right) \end{aligned} \quad (17)$$

$$Q_{eff,lmij}^{LAM} \tilde{\varepsilon}_{ij}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^N t_k \tilde{Q}_{k,lmij} \right) \tilde{\varepsilon}_{ij}^{LAM} + \frac{1}{h} \sum_{k=1}^N t_k \tilde{Q}_{k,lmij} \tilde{\beta}_{k,ij} \quad (18)$$

$$Q_{eff,lmij}^{LAM} \tilde{\varepsilon}_{ij}^{LAM} (\tilde{\varepsilon}_{ij}^{LAM})^{-1} = \left(\frac{1}{h} \sum_{k=1}^N t_k \tilde{Q}_{k,lmij} \right) \tilde{\varepsilon}_{ij}^{LAM} (\tilde{\varepsilon}_{ij}^{LAM})^{-1} + \frac{1}{h} \left(\sum_{k=1}^N t_k \tilde{Q}_{k,lmij} \tilde{\beta}_{k,ij} \right) (\tilde{\varepsilon}_{ij}^{LAM})^{-1} \quad (19)$$

$$Q_{eff,lmij}^{LAM} = \left(\frac{1}{h} \sum_{k=1}^N t_k \tilde{Q}_{k,lmij} \right) + \frac{1}{h} \sum_{k=1}^N t_k \left(\tilde{Q}_{k,lmij} \tilde{\beta}_{k,ij} (\tilde{\varepsilon}_{ij}^{LAM})^{-1} \right) \quad (20)$$

$$Q_{eff,lmij}^{LAM} = \frac{1}{h} \sum_{k=1}^N t_k \tilde{Q}_{k,lmij} \left(\frac{1}{2} (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) + \tilde{\beta}_{k,ij} (\tilde{\varepsilon}_{ij}^{LAM})^{-1} \right) \quad (21)$$

$$\begin{aligned} Q_{eff,lmij}^{LAM} &= \\ &= \frac{1}{h} \sum_{k=1}^N t_k T_{k,l m r s}^{-1} Q_{k,r s p q} \left(T_{\underline{\underline{k}}}^{-1} \right)_{p q i j}^T \left(\frac{1}{2} (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) + T_{k,i p}^{-1} \tilde{\beta}_{k,p q} \left(T_{\underline{\underline{k}}}^{-1} \right)_{q j}^T T_{k,l m r s}^{-1} (\tilde{\varepsilon}_{p q}^{LAM})^{-1} \left(T_{\underline{\underline{k}}}^{-1} \right)_{q j}^T \right) \end{aligned} \quad (22)$$

2.4. Exact expression of the Vakulenko-Kachanov tensor

35 In the local reference frame of k -th layer, the outer normal at crack faces has components:

$$n_1 = 0 \quad n_2 \neq 0 \quad n_3 \neq 0 \quad (23)$$

while crack face displacement has components:

$$u_1 = 0 \quad u_2 \neq 0 \quad u_3 \neq 0 \quad (24)$$

Definition of Vakulenko-Kachanov tensor:

$$\beta_{ij} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_i n_j + u_j n_i) dS \quad (25)$$

Expand the expression for each component and simplify based on the fact

that $u_1 = 0$:

$$\begin{aligned} \beta_{11} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_1 n_1 + u_1 n_1) dS = \frac{1}{V_k} \int_{S_C} \mu_1^0 n_1 dS = 0 \\ \beta_{22} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 n_2 + u_2 n_2) dS = \frac{1}{V_k} \int_{S_C} u_2 n_2 dS \\ \beta_{33} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 n_3 + u_3 n_3) dS = \frac{1}{V_k} \int_{S_C} u_3 n_3 dS \\ \beta_{12} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (\mu_1^0 n_2 + u_2 \mu_1^0) dS = 0 \\ \beta_{13} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (\mu_1^0 n_3 + u_3 \mu_1^0) dS = 0 \\ \beta_{23} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 n_3 + u_3 n_2) dS \\ \beta_{21} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 \mu_1^0 + \mu_1^0 n_2) dS = 0 \\ \beta_{31} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 \mu_1^0 + \mu_1^0 n_3) dS = 0 \\ \beta_{32} &= \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 n_2 + u_2 n_3) dS = \beta_{23} \end{aligned} \quad (26)$$

Only 3 independent components of the tensor β_{ij} remain: β_{22} , β_{33} and β_{23} .

Split total crack surface S_C into total matrix crack surface S_C^m and total fiber

crack surface S_C^f and remember that $n_i^f = -n_i^m$ for $i = 2, 3$

$$\begin{aligned}
\beta_{22} &= \frac{1}{V_k} \int_{S_C} u_2 n_2 dS = \frac{1}{V_k} \left[\int_{S_C^m} u_2^m n_2^m dS + \int_{S_C^f} u_2^f n_2^f dS \right] = \\
&= \frac{1}{V_k} \left[\int_{S_C^m} u_2^m n_2^m dS + \int_{S_C^f} u_2^f (-n_2^m) dS \right] \\
\beta_{33} &= \frac{1}{V_k} \int_{S_C} u_3 n_3 dS = \frac{1}{V_k} \left[\int_{S_C^m} u_3^m n_3^m dS + \int_{S_C^f} u_3^f n_3^f dS \right] = \\
&= \frac{1}{V_k} \left[\int_{S_C^m} u_3^m n_3^m dS + \int_{S_C^f} u_3^f (-n_3^m) dS \right] \\
\beta_{23} &= \frac{1}{V_k} \int_{S_C} (u_2 n_3 + u_3 n_2) dS = \\
&= \frac{1}{V_k} \left[\int_{S_C^m} (u_2^m n_3^m + u_3^m n_2^m) dS + \int_{S_C^f} (u_2^f n_3^f + u_3^f n_2^f) dS \right] = \\
&= \frac{1}{V_k} \left[\int_{S_C^m} u_2^m n_3^m dS + \int_{S_C^f} u_2^f (-n_3^m) dS + \int_{S_C^m} u_3^m n_2^m dS + \int_{S_C^f} u_3^f (-n_2^m) dS \right] \\
&\hspace{15em} (27)
\end{aligned}$$

The total matrix debonded surface S_C^m is equal to the total fiber debonded
45 surface S_C^f and equal to:

$$S_C^m = S_C^f = n_D R_f \Delta \theta \quad (28)$$

With Eq. 28, we can recast Eq. 27 as

$$\begin{aligned}
\beta_{22} &= \frac{1}{V_k} \left[n_D R_f w \int_0^{\Delta\theta} (u_2^m - u_2^f) n_2^m d\theta \right] = \\
&= \frac{1}{L_{lam} w t_{90^\circ}} \left[n_D R_f w \int_0^{\Delta\theta} (u_2^m - u_2^f) n_2^m d\theta \right] = \\
&= \frac{1}{L_{lam}} \frac{n_D R_f}{t_{90^\circ}} \left[\int_0^{\Delta\theta} (u_2^m - u_2^f) n_2^m d\theta \right] = \\
&= \rho_D \left[\frac{1}{\Delta\theta} \int_0^{\Delta\theta} (u_2^m - u_2^f) n_2^m d\theta \right] \\
\beta_{33} &= \rho_D \left[\frac{1}{\Delta\theta} \int_0^{\Delta\theta} (u_3^m - u_3^f) n_3^m d\theta \right] \\
\beta_{23} &= \rho_D \left[\frac{1}{\Delta\theta} \int_0^{\Delta\theta} (u_2^m - u_2^f) n_3^m d\theta + \frac{1}{\Delta\theta} \int_0^{\Delta\theta} (u_3^m - u_3^f) n_2^m d\theta \right]
\end{aligned} \tag{29}$$

We can express the displacement jumps at the interface as a function of the local Crack Opening Displacement (COD) and Crack Sliding Displacement (CSD) as

$$\begin{aligned}
u_2^m - u_2^f &= (u_r^m - u_r^f) \cos(\theta) - (u_\theta^m - u_\theta^f) \sin(\theta) = \\
&= COD(\theta) \cos(\theta) - CSD(\theta) \sin(\theta) \\
u_3^m - u_3^f &= (u_r^m - u_r^f) \sin(\theta) + (u_\theta^m - u_\theta^f) \cos(\theta) = \\
&= COD(\theta) \sin(\theta) + CSD(\theta) \cos(\theta)
\end{aligned} \tag{30}$$

50 where θ is the local angular coordinate at the interface. We can similarly express n_2^m and n_3^m as a function of θ :

$$\begin{aligned}
n_2^m &= \cos(\theta) - \sin(\theta) \\
n_3^m &= \sin(\theta) + \cos(\theta)
\end{aligned} \tag{31}$$

Thus, Eq. 29 becomes

$$\begin{aligned}
& \beta_{22} = \\
& = \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} [COD(\theta) (\cos^2(\theta) - \cos(\theta) \sin(\theta)) - CSD(\theta) (\sin(\theta) \cos(\theta) - \sin^2(\theta))] d\theta = \\
& = \rho_D \frac{1}{2\Delta\theta} \int_0^{\Delta\theta} [COD(\theta) (1 + \cos(2\theta) - \sin(2\theta)) + CSD(\theta) (1 - \cos(2\theta) - \sin(2\theta))] d\theta = \\
& = \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} (1 - \sin(2\theta)) + \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta \\
& \beta_{33} = \\
& = \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} [COD(\theta) (\sin(\theta) \cos(\theta) + \sin^2(\theta)) + CSD(\theta) (\cos^2(\theta) + \cos(\theta) \sin(\theta))] d\theta = \\
& = \rho_D \frac{1}{2\Delta\theta} \int_0^{\Delta\theta} [COD(\theta) (1 + \sin(2\theta) - \cos(2\theta)) + CSD(\theta) (1 + \sin(2\theta) + \cos(2\theta))] d\theta = \\
& = \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} (1 + \sin(2\theta)) - \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta \\
& \beta_{23} = \\
& = \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} COD(\theta) (2 \sin(\theta) \cos(\theta) + \cos^2(\theta) - \sin^2(\theta)) + \\
& \quad - \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} CSD(\theta) (\sin^2(\theta) - \cos^2(\theta) + 2 \cos(\theta) \sin(\theta)) d\theta = \\
& = \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} 2 \left[\frac{COD(\theta) + CSD(\theta)}{2} \cos(2\theta) + \frac{COD(\theta) - CSD(\theta)}{2} \sin(2\theta) \right] d\theta \\
& \hspace{15em} (32)
\end{aligned}$$

2.5. Analytical modeling of $COD(\theta)$ and $CSD(\theta)$

The Crack Opening Displacement (COD) and Crack Sliding Displacement
55 (CSD) are in general a function of θ , the angular coordinate along the crack
which varies between 0 and $\Delta\theta$. Without making any approximation, the Crack
Opening Displacement (COD) and Crack Sliding Displacement (CSD) can be
expressed as the sum of their average value and a term, respectively $\delta COD(\theta)$

and $\delta CSD(\theta)$, that represents the variation of the function from its average:

$$\begin{aligned} COD(\theta) &= COD_{avg} + \delta COD(\theta) \\ CSD(\theta) &= CSD_{avg} + \delta CSD(\theta). \end{aligned} \quad (33)$$

60 By defining $\Delta\Psi$

$$\Delta\Psi = \min(\Delta\theta, \Delta\Phi), \quad (34)$$

we introduce at this point an approximation and assume that the functions $\delta COD(\theta)$ and $\delta CSD(\theta)$ can be expressed as the product of the maximum value of the displacement and a function, respectively $f\left(\theta - \frac{\Delta\Psi}{2}\right)$ and $g\left(\theta - \frac{\Delta\theta}{2}\right)$:

$$\begin{aligned} COD(\theta) &= COD_{avg} + \delta COD(\theta) = COD_{avg} + COD_{max} f\left(\theta - \frac{\Delta\Psi}{2}\right) \\ CSD(\theta) &= CSD_{avg} + \delta CSD(\theta) = CSD_{avg} + CSD_{max} g\left(\theta - \frac{\Delta\theta}{2}\right), \end{aligned} \quad (35)$$

where $f\left(\theta - \frac{\Delta\Psi}{2}\right)$ and $g\left(\theta - \frac{\Delta\theta}{2}\right)$ are assumed to be odd functions over their
65 respective integration domain $[0, \Delta\Psi]$ and $[0, \Delta\theta]$

$$\int_0^{\Delta\theta} f\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = 0 \quad \int_0^{\Delta\theta} g\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = 0. \quad (36)$$

We assume the two functions $f\left(\theta - \frac{\Delta\Psi}{2}\right)$ and $g\left(\theta - \frac{\Delta\theta}{2}\right)$ to be two odd polynomials of degree $2n - 1$:

$$\begin{aligned} f\left(\theta - \frac{\Delta\Psi}{2}\right) &= \begin{cases} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} & 0 \leq \theta \leq \Delta\Psi \\ 0 & otherwise \end{cases} \\ g\left(\theta - \frac{\Delta\theta}{2}\right) &= \begin{cases} \sum_{k=0}^{n-1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} & 0 \leq \theta \leq \Delta\theta \\ 0 & otherwise \end{cases} \end{aligned} \quad (37)$$

which satisfy by construction the conditions expressed in Equation 36. The coefficients a_{2k+1} and b_{2k+1} are determined by imposing that

$$\begin{aligned} COD(\Delta\Psi) &= 0 \\ CSD(\Delta\theta) &= 0. \end{aligned} \quad (38)$$

70 The explicit construction of the polynomials $f\left(\theta - \frac{\Delta\Psi}{2}\right)$ and $g\left(\theta - \frac{\Delta\theta}{2}\right)$ for $n = 1, 2, 3$ (or degree $2n - 1 = 1, 3, 5$) is reported in Appendix A. We recall the expressions of the non-zero components of the Vakulenko-Kachanov tensor

$$\begin{aligned}
\beta_{22} &= \\
&= \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} (1 - \sin(2\theta)) + \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta \\
\beta_{33} &= \\
&= \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} (1 + \sin(2\theta)) - \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta \\
\beta_{23} &= \\
&= \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} 2 \left[\frac{COD(\theta) + CSD(\theta)}{2} \cos(2\theta) + \frac{COD(\theta) - CSD(\theta)}{2} \sin(2\theta) \right] d\theta
\end{aligned} \tag{39}$$

and proceed to the integration of the different summands:

1.

$$\begin{aligned}
& \frac{1}{\Delta\theta} \int_0^{\Delta\theta} COD(\theta) d\theta = \\
& = \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left(COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} \right) d\theta = \\
& = \frac{1}{\Delta\theta} \int_0^{\Delta\theta} COD_{avg} d\theta + \\
& + \frac{1}{\Delta\theta} \int_0^{\Delta\Psi} COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} d\theta + \\
& + \frac{1}{\Delta\theta} \int_{\Delta\Psi}^{\Delta\theta} COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} d\theta = \\
& = \frac{1}{\Delta\theta} [COD_{avg}\theta] \Big|_0^{\Delta\theta} + \frac{1}{\Delta\theta} \left[COD_{max} \sum_{k=0}^{n-1} \frac{a_{2k+1}}{2(k+1)} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2(k+1)} \right] \Big|_0^{\Delta\Psi} = \\
& = COD_{avg} + COD_{max} \sum_{k=0}^{n-1} \frac{a_{2k+1}}{2(k+1)\Delta\theta} \left(\left(\frac{\Delta\Psi}{2} \right)^{2(k+1)} - \left(-\frac{\Delta\Psi}{2} \right)^{2(k+1)} \right) = \\
& = COD_{avg}
\end{aligned} \tag{40}$$

2.

$$\frac{1}{\Delta\theta} \int_0^{\Delta\theta} CSD(\theta) d\theta = CSD_{avg} \tag{41}$$

3.

$$\begin{aligned}
& \frac{1}{\Delta\theta} \int_0^{\Delta\theta} COD(\theta) \sin(2\theta) d\theta = \\
& = \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left(COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \theta^{2k+1} \right) \sin(2\theta) d\theta = \\
& = -\frac{1}{2\Delta\theta} COD_{avg} [\cos(2\theta)] \Big|_0^{\Delta\theta} + \\
& + \frac{1}{\Delta\theta} \left[COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i+1} \sin\left(\frac{1+\text{mod}(i,2)}{2} \pi - 2\theta \right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \Big|_0^{\Delta\Psi} = \\
& = \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} + \\
& + \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i+1} \sin\left(\frac{1+\text{mod}(i,2)}{2} \pi - 2\Delta\Psi \right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)
\end{aligned} \tag{42}$$

4.

$$\begin{aligned}
& \frac{1}{\Delta\theta} \int_0^{\Delta\theta} CSD(\theta) \sin(2\theta) d\theta = \\
& = \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left(CSD_{avg} + CSD_{max} \sum_{k=0}^{n-1} b_{2k+1} \theta^{2k+1} \right) \sin(2\theta) d\theta = \\
& = -\frac{1}{2\Delta\theta} CSD_{avg} [\cos(2\theta)] \Big|_0^{\Delta\theta} + \\
& + \frac{1}{\Delta\theta} \left[CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i+1} \sin\left(\frac{1+\text{mod}(i,2)}{2}\pi - 2\theta\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \Big|_0^{\Delta\theta} = \\
& = \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
& + \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i+1} \sin\left(\frac{1+\text{mod}(i,2)}{2}\pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)
\end{aligned} \tag{43}$$

5.

$$\begin{aligned}
& \frac{1}{\Delta\theta} \int_0^{\Delta\theta} COD(\theta) \cos(2\theta) d\theta = \\
& = \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left(COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \theta^{2k+1} \right) \cos(2\theta) d\theta = \\
& = \frac{1}{2\Delta\theta} COD_{avg} [\sin(2\theta)] \Big|_0^{\Delta\theta} + \\
& + \frac{1}{\Delta\theta} \left[COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^i \sin\left(\frac{1+\text{mod}(i+1,2)}{2}\pi - 2\theta\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \Big|_0^{\Delta\theta} = \\
& = \frac{\sin(2\Delta\theta)}{2\Delta\theta} COD_{avg} + \\
& + \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^i \sin\left(\frac{1+\text{mod}(i+1,2)}{2}\pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)
\end{aligned} \tag{44}$$

6.

$$\begin{aligned}
& \frac{1}{\Delta\theta} \int_0^{\Delta\theta} CSD(\theta) \cos(2\theta) d\theta = \\
& = \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left(CSD_{avg} + CSD_{max} \sum_{k=0}^{n-1} b_{2k+1} \theta^{2k+1} \right) \cos(2\theta) d\theta = \\
& = -\frac{1}{2\Delta\theta} CSD_{avg} [\cos(2\theta)] \Big|_0^{\Delta\theta} + \\
& + \frac{1}{\Delta\theta} \left[CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\theta \right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \Big|_0^{\Delta\theta} = \\
& = \frac{\sin(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
& + \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\theta \right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\theta^{k-i} \right) \\
& \hspace{15em} (45)
\end{aligned}$$

75 Finally we can compute the expressions of the components of the Vakulenko-Kachanov tensor:

1. β_{22}

$$\begin{aligned}
\beta_{22} &= \\
&= \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} (1 - \sin(2\theta)) + \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta \\
&= \frac{\rho_D}{2} (COD_{avg} + CSD_{avg}) + \\
&\quad - \frac{\rho_D}{2} \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} - \frac{\rho_D}{2} \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
&\quad - \frac{\rho_D}{2} \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&\quad - \frac{\rho_D}{2} \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&\quad + \frac{\rho_D}{2} \frac{\sin(2\Delta\theta)}{2\Delta\theta} COD_{avg} + \\
&\quad + \frac{\rho_D}{2} \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&\quad - \frac{\rho_D}{2} \frac{\sin(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
&\quad - \frac{\rho_D}{2} \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) = \\
&= \frac{\rho_D}{2} COD_{avg} \left(1 - \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} + \frac{\sin(2\Delta\theta)}{2\Delta\theta}\right) + \\
&\quad + \frac{\rho_D}{2} CSD_{avg} \left(1 - \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} - \frac{\sin(2\Delta\theta)}{2\Delta\theta}\right) + \\
&\quad + \frac{\rho_D}{2} COD_{max} \frac{1}{\Delta\theta} \sum_{i=0}^{2n-1} \left(\left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) - \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) \right) \cdot \\
&\quad \cdot \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&\quad - \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta\theta} \sum_{i=0}^{2n-1} \left(\left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) + \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) \right) \cdot \\
&\quad \cdot \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right)
\end{aligned} \tag{46}$$

2. β_{33}

$$\begin{aligned}
\beta_{33} &= \\
&= \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} (1 + \sin(2\theta)) - \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta = \\
&= \frac{\rho_D}{2} (COD_{avg} + CSD_{avg}) + \\
&+ \frac{\rho_D}{2} \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} + \frac{\rho_D}{2} \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
&+ \frac{\rho_D}{2} \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&+ \frac{\rho_D}{2} \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&- \frac{\rho_D}{2} \frac{\sin(2\Delta\theta)}{2\Delta\theta} COD_{avg} + \\
&- \frac{\rho_D}{2} \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&+ \frac{\rho_D}{2} \frac{\sin(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
&+ \frac{\rho_D}{2} \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) = \\
&= \frac{\rho_D}{2} COD_{avg} \left(1 + \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} - \frac{\sin(2\Delta\theta)}{2\Delta\theta}\right) + \\
&+ \frac{\rho_D}{2} CSD_{avg} \left(1 - \frac{1 + \cos(2\Delta\theta)}{2\Delta\theta} + \frac{\sin(2\Delta\theta)}{2\Delta\theta}\right) + \\
&+ \frac{\rho_D}{2} COD_{max} \frac{1}{\Delta\theta} \sum_{i=0}^{2n-1} \left(\left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right) - \left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right)\right) \cdot \\
&\quad \cdot \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta\theta} \sum_{i=0}^{2n-1} \left(\left(-\frac{1}{2}\right)^i \sin\left(\frac{1 + \text{mod}(i+1, 2)}{2} \pi - 2\Delta\Psi\right) + \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi\right)\right) \cdot \\
&\quad \cdot \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right)
\end{aligned} \tag{47}$$

3. β_{23}

$$\begin{aligned}
\beta_{23} &= \\
&= \rho_D \frac{1}{\Delta\theta} \int_0^{\Delta\theta} 2 \left[\frac{COD(\theta) + CSD(\theta)}{2} \cos(2\theta) + \frac{COD(\theta) - CSD(\theta)}{2} \sin(2\theta) \right] d\theta = \\
&= \frac{\rho_D}{2} \frac{\sin(2\Delta\theta)}{2\Delta\theta} COD_{avg} + \\
&+ \frac{\rho_D}{2} \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^i \sin\left(\frac{1+mod(i+1,2)}{2}\pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&+ \frac{\rho_D}{2} \frac{\sin(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
&+ \frac{\rho_D}{2} \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^i \sin\left(\frac{1+mod(i+1,2)}{2}\pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&+ \frac{\rho_D}{2} \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} - \frac{\rho_D}{2} \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} CSD_{avg} + \\
&+ \frac{\rho_D}{2} \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1+mod(i,2)}{2}\pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&- \frac{\rho_D}{2} \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1+mod(i,2)}{2}\pi - 2\Delta\Psi\right) \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) = \\
&= \frac{\rho_D}{2} COD_{avg} \left(\frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} + \frac{\sin(2\Delta\theta)}{2\Delta\theta}\right) + \\
&- \frac{\rho_D}{2} CSD_{avg} \left(\frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} - \frac{\sin(2\Delta\theta)}{2\Delta\theta}\right) + \\
&+ \frac{\rho_D}{2} COD_{max} \frac{1}{\Delta\theta} \sum_{i=0}^{2n-1} \left(\left(-\frac{1}{2}\right)^i \sin\left(\frac{1+mod(i+1,2)}{2}\pi - 2\Delta\Psi\right) + \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1+mod(i,2)}{2}\pi - 2\Delta\Psi\right)\right) \cdot \\
&\quad \cdot \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right) + \\
&+ \frac{\rho_D}{2} CSD_{max} \frac{1}{\Delta\theta} \sum_{i=0}^{2n-1} \left(\left(-\frac{1}{2}\right)^i \sin\left(\frac{1+mod(i+1,2)}{2}\pi - 2\Delta\Psi\right) - \left(-\frac{1}{2}\right)^{i+1} \sin\left(\frac{1+mod(i,2)}{2}\pi - 2\Delta\Psi\right)\right) \cdot \\
&\quad \cdot \left(\sum_{k=i}^{2n-1} b_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i}\right)
\end{aligned} \tag{48}$$

80 2.6. *Application to UD composite*

2.7. *Application to $[0_{mk}^\circ, 90_k^\circ, 0_{mk}^\circ]$ laminate*

3. Computations with the Finite Element Method (FEM)

3.1. *Models of Representative Volume Element (RVE)*

3.2. *Details of FEM implementation*

85 4. Results and discussion

5. Conclusions

References

- [1] R. Talreja, Damage characterization, in: *Fatigue of Composite Materials*, Elsevier, 1991, pp. 79–103. doi:10.1016/b978-0-444-70507-5.50007-x.
- 90 [2] J. A. Nairn, Matrix microcracking in composites, in: *Comprehensive Composite Materials*, Elsevier, 2000, pp. 403–432. doi:10.1016/b0-08-042993-9/00069-3.
- [3] J.-M. Berthelot, Transverse cracking and delamination in cross-ply glass-fiber and carbon-fiber reinforced plastic laminates: Static and fatigue loading, *Applied Mechanics Reviews* 56 (1) (2003) 111–147. doi:10.1115/1.1519557.
- 95 [4] K. W. Garrett, J. E. Bailey, Multiple transverse fracture in 90° cross-ply laminates of a glass fibre-reinforced polyester, *Journal of Materials Science* 12 (1) (1977) 157–168. doi:10.1007/bf00738481.
- 100 [5] C. Henaff-Gardin, M. Lafarie-Frenot, D. Gamby, Doubly periodic matrix cracking in composite laminates part 1: General in-plane loading, *Composite Structures* 36 (1-2) (1996) 113–130. doi:10.1016/s0263-8223(96)00071-2.

- [6] L. McCartney, Theory of stress transfer in a $0^\circ - 90^\circ - 0^\circ$ cross-ply laminate
 105 containing a parallel array of transverse cracks, *Journal of the Mechanics
 and Physics of Solids* 40 (1) (1992) 27–68. doi:10.1016/0022-5096(92)
 90226-r.
- [7] Z. Hashin, Analysis of cracked laminates: a variational approach, *Me-
 110 chanics of Materials* 4 (2) (1985) 121–136. doi:10.1016/0167-6636(85)
 90011-0.
- [8] Z. Hashin, Analysis of orthogonally cracked laminates under tension, *Jour-
 nal of Applied Mechanics* 54 (4) (1987) 872–879. doi:10.1115/1.3173131.
- [9] V. Vinogradov, Z. Hashin, Variational analysis of cracked angle-ply lam-
 inates, *Composites Science and Technology* 70 (4) (2010) 638–646. doi:
 115 10.1016/j.compscitech.2009.12.018.
- [10] J.-M. Berthelot, P. Leblond, A. E. Mahi, J.-F. L. Corre, Transverse crack-
 ing of cross-ply laminates: Part 1. analysis, *Composites Part A: Ap-
 plied Science and Manufacturing* 27 (10) (1996) 989–1001. doi:10.1016/
 1359-835x(96)80002-a.
- 120 [11] N. Laws, G. Dvorak, M. Hejazi, Stiffness changes in unidirectional compos-
 ites caused by crack systems, *Mechanics of Materials* 2 (2) (1983) 123–137.
 doi:10.1016/0167-6636(83)90032-7.
- [12] S. Li, S. Reid, P. Soden, A finite strip analysis of cracked laminates, *Me-
 125 chanics of Materials* 18 (4) (1994) 289–311. doi:10.1016/0167-6636(94)
 90041-8.
- [13] D. Allen, C. Harris, S. Groves, A thermomechanical constitutive theory
 for elastic composites with distributed damage—II. application to ma-
 trix cracking in laminated composites, *International Journal of Solids
 and Structures* 23 (9) (1987) 1319–1338. doi:10.1016/0020-7683(87)
 130 90108-9.

- [14] P. Ladeveze, A damage mechanics for composites materials, in: *Integration of Theory and Applications in Applied Mechanics*, Springer Netherlands, 1990, pp. 13–24. doi:10.1007/978-94-009-2125-2_2.
- [15] C. V. Singh, R. Talreja, Analysis of multiple off-axis ply cracks in composite laminates, *International Journal of Solids and Structures* 45 (16) (2008) 4574–4589. doi:10.1016/j.ijsolstr.2008.04.004.
- [16] E. Barbero, G. Sgambitterra, A. Adumitroaie, X. Martinez, A discrete constitutive model for transverse and shear damage of symmetric laminates with arbitrary stacking sequence, *Composite Structures* 93 (2) (2011) 1021–1030. doi:10.1016/j.compstruct.2010.06.011.
- [17] G. Schoeppner, N. Pagano, Stress fields and energy release rates in cross-ply laminates, *International Journal of Solids and Structures* 35 (11) (1998) 1025–1055. doi:10.1016/s0020-7683(97)00107-8.
- [18] J. Reddy, *Energy Principles and Variational Methods in Applied Mechanics*, Wiley, 2002.
- [19] P. Gudmundson, S. Östlund, First order analysis of stiffness reduction due to matrix cracking, *Journal of Composite Materials* 26 (7) (1992) 1009–1030. doi:10.1177/002199839202600704.
- [20] P. Gudmundson, S. Östlund, Numerical verification of a procedure for calculation of elastic constants in microcracking composite laminates, *Journal of Composite Materials* 26 (17) (1992) 2480–2492. doi:10.1177/002199839202601701.
URL <https://doi.org/10.1177/002199839202601701>
- [21] P. Gudmundson, Z. Weilin, An analytic model for thermoelastic properties of composite laminates containing transverse matrix cracks, *International Journal of Solids and Structures* 30 (23) (1993) 3211–3231. doi:10.1016/0020-7683(93)90110-s.

- [22] P. Lundmark, J. Varna, Modeling thermo-mechanical properties of damaged laminates, *Key Engineering Materials* 251-252 (2003) 381–388. doi:10.4028/www.scientific.net/kem.251-252.381.
- [23] P. Lundmark, J. Varna, Crack face sliding effect on stiffness of laminates with ply cracks, *Composites Science and Technology* 66 (10) (2006) 1444–1454. doi:10.1016/j.compscitech.2005.08.016.
- [24] J. Varna, Modelling mechanical performance of damaged laminates, *Journal of Composite Materials* 47 (20-21) (2012) 2443–2474. doi:10.1177/0021998312469241.
- [25] M. S. Loukil, J. Varna, Z. Ayadi, Applicability of solutions for periodic intralaminar crack distributions to non-uniformly damaged laminates, *Journal of Composite Materials* 47 (3) (2012) 287–301. doi:10.1177/0021998312440126.
- [26] M. S. Loukil, W. Hussain, A. Kirti, A. Pupurs, J. Varna, Thermoelastic constants of symmetric laminates with cracks in 90-layer: application of simple models, *Plastics, Rubber and Composites* 42 (4) (2013) 157–166. doi:10.1179/1743289811y.00000000064.
- [27] M. S. Loukil, J. Varna, Z. Ayadi, Engineering expressions for thermo-elastic constants of laminates with high density of transverse cracks, *Composites Part A: Applied Science and Manufacturing* 48 (2013) 37–46. doi:10.1016/j.compositesa.2012.12.012.
- [28] J. Varna, M. S. Loukil, Effective transverse modulus of a damaged layer: Potential for predicting symmetric laminate stiffness degradation, *Journal of Composite Materials* 51 (14) (2016) 1945–1959. doi:10.1177/0021998316658965.
- [29] A. Pupurs, J. Varna, M. Loukil, H. B. Kahla, D. Mattsson, Effective stiffness concept in bending modeling of laminates with damage in surface 90-

- 185 layers, Composites Part A: Applied Science and Manufacturing 82 (2016)
244–252. doi:10.1016/j.compositesa.2015.11.012.
- [30] J. Varna, 2.10 crack separation based models for microcracking, in:
P. W. Beaumont, C. H. Zweben (Eds.), Comprehensive Composite
Materials II, Elsevier, Oxford, 2018, pp. 192 – 220. doi:10.1016/
190 B978-0-12-803581-8.09910-0.
- [31] M. S. Loukil, J. Varna, Effective shear modulus of a damaged ply in lami-
nate stiffness analysis: Determination and validation, Journal of Composite
Materials (2019) 002199831987436doi:10.1177/0021998319874369.
- [32] M. S. Loukil, J. Varna, Crack face sliding displacement (CSD) as an input in
195 exact GLOB-LOC expressions for in-plane elastic constants of symmetric
damaged laminates, International Journal of Damage Mechanics (2019)
105678951986600doi:10.1177/1056789519866000.

Appendix A. Explicit expressions for $f(\theta)$ and $g(\theta)$

In the following, recall that

$$\Delta\Psi = \min(\Delta\theta, \Delta\Phi). \quad (\text{A.1})$$

$\mathbf{n} = \mathbf{1}$

$$\begin{aligned} f\left(\theta - \frac{\Delta\Psi}{2}\right) &= \sum_{k=0}^0 a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} = a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) \\ g\left(\theta - \frac{\Delta\theta}{2}\right) &= \sum_{k=0}^0 b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} = b_1 \left(\theta - \frac{\Delta\theta}{2}\right) \end{aligned} \quad (\text{A.2})$$

$$\begin{aligned} \int_0^{\Delta\Psi} f\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta &= \int_0^{\Delta\Psi} a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = \left[\frac{a_1}{2} \theta^2 - a_1 \frac{\Delta\Psi}{2} \theta \right] \Big|_0^{\Delta\Psi} = 0 \quad \forall a_1 \\ \int_0^{\Delta\theta} g\left(\theta - \frac{\Delta\theta}{2}\right) d\theta &= \int_0^{\Delta\theta} b_1 \left(\theta - \frac{\Delta\theta}{2}\right) d\theta = \left[\frac{b_1}{2} \theta^2 - b_1 \frac{\Delta\theta}{2} \theta \right] \Big|_0^{\Delta\theta} = 0 \quad \forall b_1 \end{aligned} \quad (\text{A.3})$$

$$\begin{aligned}
COD_{avg} + COD_{max} a_1 \left(\Delta\Psi - \frac{\Delta\Psi}{2} \right) &= 0 \rightarrow a_1 = -\frac{2}{\Delta\Psi} \frac{COD_{avg}}{COD_{max}} \\
CSD_{avg} + CSD_{max} b_1 \left(\Delta\theta - \frac{\Delta\theta}{2} \right) &= 0 \rightarrow b_1 = -\frac{2}{\Delta\theta} \frac{CSD_{avg}}{CSD_{max}}
\end{aligned} \tag{A.4}$$

$$\begin{aligned}
&\sum_{i=0}^1 \left(-\frac{1}{2} \right)^{i+1} \sin \left(\frac{1 + \text{mod}(i, 2)}{2} \pi - 2\Delta\Psi \right) \left(\sum_{k=0}^{1-i} a_k (1 - (k+1))! \Delta\Psi^k \right) = \\
&= \left(-\frac{1}{2} \right)^1 \sin \left(\frac{1 + \text{mod}(0, 2)}{2} \pi - 2\Delta\Psi \right) \left(\sum_{k=0}^1 a_k (1 - (k+1))! \Delta\Psi^k \right) + \\
&+ \left(-\frac{1}{2} \right)^2 \sin \left(\frac{1 + \text{mod}(1, 2)}{2} \pi - 2\Delta\Psi \right) \left(\sum_{k=0}^0 a_k (1 - (k+1))! \Delta\Psi^k \right) = \\
&= -\frac{1}{2} \cos(2\Delta\Psi) \left(\sum_{k=0}^1 a_k (1 - (k+1))! \Delta\Psi^k \right) + \\
&+ \frac{1}{4} \sin(2\Delta\Psi) \left(\sum_{k=0}^0 a_k (1 - (k+1))! \Delta\Psi^k \right) = \\
&= -\frac{1}{2} \cos(2\Delta\Psi) (a_0 + a_1 (n - (k+1))! \Delta\Psi^k) + \\
&+ \frac{1}{4} \sin(2\Delta\Psi) \left(\sum_{k=0}^0 a_k (n - (k+1))! \Delta\Psi^k \right) =
\end{aligned} \tag{A.5}$$

n = 2

$$\begin{aligned}
f \left(\theta - \frac{\Delta\Psi}{2} \right) &= \sum_{k=0}^1 a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} = a_1 \left(\theta - \frac{\Delta\Psi}{2} \right) + a_3 \left(\theta - \frac{\Delta\Psi}{2} \right)^3 \\
g \left(\theta - \frac{\Delta\theta}{2} \right) &= \sum_{k=0}^1 b_{2k+1} \left(\theta - \frac{\Delta\theta}{2} \right)^{2k+1} = b_1 \left(\theta - \frac{\Delta\theta}{2} \right) + b_3 \left(\theta - \frac{\Delta\theta}{2} \right)^3
\end{aligned} \tag{A.6}$$

n = 3

$$\begin{aligned}
f\left(\theta - \frac{\Delta\Psi}{2}\right) &= \sum_{k=0}^2 a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} = \\
&= a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) + a_3 \left(\theta - \frac{\Delta\Psi}{2}\right)^3 + a_5 \left(\theta - \frac{\Delta\Psi}{2}\right)^5 \\
g\left(\theta - \frac{\Delta\theta}{2}\right) &= \sum_{k=0}^1 b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} = \\
&= b_1 \left(\theta - \frac{\Delta\theta}{2}\right) + b_3 \left(\theta - \frac{\Delta\theta}{2}\right)^3 + b_5 \left(\theta - \frac{\Delta\theta}{2}\right)^5
\end{aligned} \tag{A.7}$$