Stiffness reduction in UD and cross-ply laminates due to fiber/matrix interface cracks

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Abstract

Keywords: Fiber Reinforced Polymer Composite (FRPC), Debonding, Finite element analysis (FEA)

1. Introduction

Main ref [1]

2. Derivation of constitutive relations

2.1. Reference frames

5 Local reference frame of k-th layer: index 1 is the in-plane longitudinal or fiber or 0°-direction; index 2 is the in-plane transverse or 90°-direction; index 3 is the out-of-plane or through-the-thickness direction.

Global reference frame of laminate: index x is the in-plane longitudinal or laminate 0° direction; index y is the in-plane transverse direction; index z is the out-of-plane or through-the-thickness direction.

2.2. Crack density

Principle 1. Normalized volume of cracks V_{an} is the ratio of cracked volume V_a to material volume V

$$V_{an} = \frac{V_a}{V} \tag{1}$$

 V_a is equal to the product of total crack surface S_C and average crack opening u_a

$$V_{an} = \frac{S_C u_a}{V} = \frac{S_C}{V} u_a = \rho_C u_a \tag{2}$$

The ratio $\frac{S_C}{V}$ has a size of $\frac{1}{length}$ and correspond to the crack density ρ_C . It means: product of crack density and average crack opening is equal to normalized volume of cracks.

Applying the previous Principle to debonds, we have:

$$\rho_{D} = \frac{\text{total area of debonds}}{\text{total layer volume}} = \frac{n_{D}wR_{f}\Delta\theta}{L_{lam}wt_{90^{\circ}}} = \frac{n_{D}w}{L_{lam}wt_{90^{\circ}}}R_{f}\Delta\theta = \frac{1}{n2L}\frac{1}{k2L}R_{f}\Delta\theta = \frac{1}{nk4L^{2}}R_{f}\Delta\theta = \frac{V_{f}}{nk\pi R_{f}^{2}}R_{f}\Delta\theta = \frac{V_{f}}{nkR_{f}}\frac{\Delta\theta}{\pi}$$
(3)

2.3. Vakulenko-Kachanov tensor

In the local reference frame of k-th layer, the outer normal at crack faces has components:

$$n_1 = 0 \quad n_2 \neq 0 \quad n_3 \neq 0$$
 (4)

while crack face displacement has components:

$$u_1 = 0 \quad u_2 \neq 0 \quad u_3 \neq 0$$
 (5)

Definition of Vakulenko-Kachanov tensor:

$$\beta_{ij} = \frac{1}{V_k} \int_{SC} \frac{1}{2} (u_i n_j + u_j n_i) dS$$
 (6)

Expand the expression for each component and simplify based on the fact that $u_1 = 0$:

$$\beta_{11} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_1 n_1 + u_1 n_1) dS = \frac{1}{V_k} \int_{S_C} u_1^{-1} n_1 dS = 0$$

$$\beta_{22} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 n_2 + u_2 n_2) dS = \frac{1}{V_k} \int_{S_C} u_2 n_2 dS$$

$$\beta_{33} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 n_3 + u_3 n_3) dS = \frac{1}{V_k} \int_{S_C} u_3 n_3 dS$$

$$\beta_{12} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_1^{-1} n_2 + u_2 u_1^{-1}) dS = 0$$

$$\beta_{13} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_1^{-1} n_3 + u_3 u_1^{-1}) dS = 0$$

$$\beta_{23} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 n_3 + u_3 n_2) dS$$

$$\beta_{21} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_2 u_1^{-1} + u_1^{-1} n_2) dS = 0$$

$$\beta_{31} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 u_1^{-1} + u_1^{-1} n_3) dS = 0$$

$$\beta_{32} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 u_1^{-1} + u_1^{-1} n_3) dS = 0$$

$$\beta_{32} = \frac{1}{V_k} \int_{S_C} \frac{1}{2} (u_3 n_2 + u_2 n_3) dS = \beta_{23}$$

Only 3 independent components of the tensor β_{ij} remain: β_{22} , β_{33} and β_{23} . Split total crack surface S_C into total matrix crack surface S_C^m and total fiber crack surface S_C^f and remember that $n_i^f = -n_i^m$ for i=2,3

$$\beta_{22} = \frac{1}{V_k} \int_{S_C} u_2 n_2 dS = \frac{1}{V_k} \left[\int_{S_C^m} u_2^m n_2^m dS + \int_{S_C^f} u_2^f n_2^f dS \right] =$$

$$= \frac{1}{V_k} \left[\int_{S_C^m} u_2^m n_2^m dS + \int_{S_C^f} u_2^f (-n_2^m) dS \right]$$

$$\beta_{33} = \frac{1}{V_k} \int_{S_C} u_3 n_3 dS = \frac{1}{V_k} \left[\int_{S_C^m} u_3^m n_3^m dS + \int_{S_C^f} u_3^f n_3^f dS \right] =$$

$$= \frac{1}{V_k} \left[\int_{S_C^m} u_3^m n_3^m dS + \int_{S_C^f} u_3^f (-n_3^m) dS \right]$$

$$\beta_{23} = \frac{1}{V_k} \int_{S_C} (u_2 n_3 + u_3 n_2) dS =$$

$$= \frac{1}{V_k} \left[\int_{S_C^m} (u_2^m n_3^m + u_3^m n_2^m) dS + \int_{S_C^f} \left(u_2^f n_3^f + u_3^f n_2^f \right) dS \right] =$$

$$= \frac{1}{V_k} \left[\int_{S_C^m} u_2^m n_3^m dS + \int_{S_C^f} u_2^f (-n_3^m) dS + \int_{S_C^m} u_3^m n_2^m dS + \int_{S_C^f} u_3^f (-n_2^m) dS \right]$$

$$(8)$$

The total matrix debonded surface S_C^m is equal to the total fiber debonded surface S_C^f and equal to:

$$S_C^m = S_C^f = n_D R_f \Delta \theta \tag{9}$$

With Eq. 9, we can recast Eq. 8 as

$$\beta_{22} = \frac{1}{V_k} \left[n_D R_f w \int_0^{\Delta \theta} \left(u_2^m - u_2^f \right) n_2^m d\theta \right] = \\
= \frac{1}{L_{lam} w t_{90^\circ}} \left[n_D R_f w \int_0^{\Delta \theta} \left(u_2^m - u_2^f \right) n_2^m d\theta \right] = \\
= \frac{1}{L_{lam}} \frac{n_D R_f}{t_{90^\circ}} \left[\int_0^{\Delta \theta} \left(u_2^m - u_2^f \right) n_2^m d\theta \right] = \\
= \rho_D \left[\frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left(u_2^m - u_2^f \right) n_2^m d\theta \right] = \\
= \rho_D \left[\frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left(u_3^m - u_3^f \right) n_3^m d\theta \right] \\
\beta_{23} = \rho_D \left[\frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left(u_2^m - u_2^f \right) n_3^m d\theta + \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left(u_3^m - u_3^f \right) n_2^m d\theta \right]$$
(10)

We can express the displacement jumps at the interface as a function of the local Crack Opening Displacement (COD) and Crack Sliding Displacement (CSD) as

$$u_{2}^{m} - u_{2}^{f} = \left(u_{r}^{m} - u_{r}^{f}\right)\cos\left(\theta\right) - \left(u_{\theta}^{m} - u_{\theta}^{f}\right)\sin\left(\theta\right) =$$

$$= COD\left(\theta\right)\cos\left(\theta\right) - CSD\left(\theta\right)\sin\left(\theta\right)$$

$$u_{3}^{m} - u_{3}^{f} = \left(u_{r}^{m} - u_{r}^{f}\right)\sin\left(\theta\right) + \left(u_{\theta}^{m} - u_{\theta}^{f}\right)\cos\left(\theta\right) =$$

$$= COD\left(\theta\right)\sin\left(\theta\right) + CSD\left(\theta\right)\cos\left(\theta\right)$$

$$(11)$$

where θ is the local angular coordinate at the interface. We can similarly express n_2^m and n_3^m as a function of θ :

$$n_2^m = \cos(\theta) - \sin(\theta)$$

$$n_3^m = \sin(\theta) + \cos(\theta)$$
(12)

Thus, Eq. 10 becomes

$$\begin{split} \beta_{22} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[COD\left(\theta\right) \left(\cos^2\left(\theta\right) - \cos\left(\theta\right) \sin\left(\theta\right) \right) - CSD\left(\theta\right) \left(\sin\left(\theta\right) \cos\left(\theta\right) - \sin^2\left(\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{2\Delta \theta} \int_0^{\Delta \theta} \left[COD\left(\theta\right) \left(1 + \cos\left(2\theta\right) - \sin\left(2\theta\right) \right) + CSD\left(\theta\right) \left(1 - \cos\left(2\theta\right) - \sin\left(2\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[\frac{COD\left(\theta\right) + CSD\left(\theta\right)}{2} \left(1 - \sin\left(2\theta\right) \right) + \frac{COD\left(\theta\right) - CSD\left(\theta\right)}{2} \cos\left(2\theta\right) \right] d\theta \\ \beta_{33} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[COD\left(\theta\right) \left(\sin\left(\theta\right) \cos\left(\theta\right) + \sin^2\left(\theta\right) \right) + CSD\left(\theta\right) \left(\cos^2\left(\theta\right) + \cos\left(\theta\right) \sin\left(\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{2\Delta \theta} \int_0^{\Delta \theta} \left[COD\left(\theta\right) \left(1 + \sin\left(2\theta\right) - \cos\left(2\theta\right) \right) + CSD\left(\theta\right) \left(1 + \sin\left(2\theta\right) + \cos\left(2\theta\right) \right) \right] d\theta = \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} \left[\frac{COD\left(\theta\right) + CSD\left(\theta\right)}{2} \left(1 + \sin\left(2\theta\right) \right) - \frac{COD\left(\theta\right) - CSD\left(\theta\right)}{2} \cos\left(2\theta\right) \right] d\theta \\ \beta_{23} &= \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} COD\left(\theta\right) \left(2\sin\left(\theta\right) \cos\left(\theta\right) + \cos^2\left(\theta\right) - \sin^2\left(\theta\right) \right) + \\ &- \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} CSD\left(\theta\right) \left(\sin^2\left(\theta\right) - \cos^2\left(\theta\right) + 2\cos\left(\theta\right) \sin\left(\theta\right) \right) d\theta = \\ &= \rho_D \frac{1}{\Delta \theta} \int_0^{\Delta \theta} 2 \left[\frac{COD\left(\theta\right) + CSD\left(\theta\right)}{2} \cos\left(2\theta\right) + \frac{COD\left(\theta\right) - CSD\left(\theta\right)}{2} \sin\left(2\theta\right) \right] d\theta \\ (13) \end{split}$$

2.4. Analytical modeling of $COD(\theta)$ and $CSD(\theta)$

The Crack Opening Displacement (COD) and Crack Sliding Displacement (CSD) are in general a function of θ , the angular coordinate along the crack which varies between 0 and $\Delta\theta$. Without making any approximation, the Crack Opening Displacement (COD) and Crack Sliding Displacement (CSD) can be expressed as the sum of their average value and a term, respectively $\delta COD(\theta)$

and $\delta CSD(\theta)$, that represents the variation of the function from its average:

$$COD(\theta) = COD_{avg} + \delta COD(\theta)$$

$$CSD(\theta) = CSD_{avg} + \delta CSD(\theta).$$
(14)

By defining $\Delta\Psi$

$$\Delta\Psi = \min\left(\Delta\theta, \Delta\Phi\right),\tag{15}$$

we introduce at this point an approximation and assume that the functions $\delta COD\left(\theta\right)$ and $\delta CSD\left(\theta\right)$ can be expressed as the product of the maximum value of the displacement and a function, respectively $f\left(\theta-\frac{\Delta\Psi}{2}\right)$ and $g\left(\theta-\frac{\Delta\theta}{2}\right)$:

$$COD(\theta) = COD_{avg} + \delta COD(\theta) = COD_{avg} + COD_{max} f\left(\theta - \frac{\Delta \Psi}{2}\right)$$

$$CSD(\theta) = CSD_{avg} + \delta CSD(\theta) = CSD_{avg} + CSD_{max} g\left(\theta - \frac{\Delta \theta}{2}\right),$$
(16)

where $f\left(\theta - \frac{\Delta\Psi}{2}\right)$ and $g\left(\theta - \frac{\Delta\theta}{2}\right)$ are assumed to be odd functions over their respective integration domain $[0, \Delta\Psi]$ and $[0, \Delta\theta]$

$$\int_{0}^{\Delta\theta} f\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = 0 \quad \int_{0}^{\Delta\theta} g\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = 0. \tag{17}$$

We assume the two functions $f\left(\theta - \frac{\Delta\Psi}{2}\right)$ and $g\left(\theta - \frac{\Delta\theta}{2}\right)$ to be two odd polynomials of degree 2n-1:

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \begin{cases} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} & 0 \le \theta \le \Delta\Psi \\ 0 & otherwise \end{cases}$$

$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \begin{cases} \sum_{k=0}^{n-1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} & 0 \le \theta \le \Delta\theta \\ 0 & otherwise \end{cases}$$

$$(18)$$

which satisfy by construction the conditions expressed in Equation 17. The coefficients a_{2k+1} and b_{2k+1} are determined by imposing that

$$COD(\Delta \Psi) = 0$$

$$CSD(\Delta \theta) = 0.$$
(19)

The explicit construction of the polynomials $f\left(\theta-\frac{\Delta\Psi}{2}\right)$ and $g\left(\theta-\frac{\Delta\theta}{2}\right)$ for n=1,2,3 (or degree 2n-1=1,3,5) is reported in Appendix A.

We recall the expressions of the non-zero components of the Vakulenko-Kachanov tensor

$$\beta_{22} = \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} \left(1 - \sin(2\theta) \right) + \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta$$

$$\beta_{33} = \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left[\frac{COD(\theta) + CSD(\theta)}{2} \left(1 + \sin(2\theta) \right) - \frac{COD(\theta) - CSD(\theta)}{2} \cos(2\theta) \right] d\theta$$

$$\beta_{23} = \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} 2 \left[\frac{COD(\theta) + CSD(\theta)}{2} \cos(2\theta) + \frac{COD(\theta) - CSD(\theta)}{2} \sin(2\theta) \right] d\theta$$

$$(20)$$

and proceed to the integration of the different summands:

1.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD(\theta) d\theta =$$

$$= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left(COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} \right) d\theta =$$

$$= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD_{avg} d\theta +$$

$$+ \frac{1}{\Delta\theta} \int_{0}^{\Delta\Psi} COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} d\theta +$$

$$+ \frac{1}{\Delta\theta} \int_{\Delta\Psi}^{\Delta\theta} COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2k+1} d\theta =$$

$$= \frac{1}{\Delta\theta} \left[COD_{avg} \theta \right] \Big|_{0}^{\Delta\theta} + \frac{1}{\Delta\theta} \left[COD_{max} \sum_{k=0}^{n-1} \frac{a_{2k+1}}{2(k+1)} \left(\theta - \frac{\Delta\Psi}{2} \right)^{2(k+1)} \right] \Big|_{0}^{\Delta\Psi} =$$

$$= COD_{avg} + COD_{max} \sum_{k=0}^{n-1} \frac{a_{2k+1}}{2(k+1)\Delta\theta} \left(\left(\frac{\Delta\Psi}{2} \right)^{2(k+1)} - \left(-\frac{\Delta\Psi}{2} \right)^{2(k+1)} \right) =$$

$$= COD_{avg}$$
(21)

2.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} CSD\left(\theta\right) d\theta = CSD_{avg} \tag{22}$$

3.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD(\theta) \sin(2\theta) d\theta =$$

$$= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left(COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \theta^{2k+1} \right) \sin(2\theta) d\theta =$$

$$= -\frac{1}{2\Delta\theta} COD_{avg} \left[\cos(2\theta) \right]_{0}^{\Delta\theta} +$$

$$+ \frac{1}{\Delta\theta} \left[COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i+1} \sin(\frac{1+mod(i,2)}{2}\pi - 2\theta) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \theta^{k-i} \right) \right]_{0}^{\Delta\Psi} =$$

$$= \frac{1-\cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} +$$

$$+ \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i+1} \sin(\frac{1+mod(i,2)}{2}\pi - 2\Delta\Psi) \left(\sum_{k=i}^{2n-1} a_k \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)$$
(23)

$$\begin{split} &\frac{1}{\Delta\theta}\int_{0}^{\Delta\theta}CSD\left(\theta\right)\sin\left(2\theta\right)d\theta = \\ &= \frac{1}{\Delta\theta}\int_{0}^{\Delta\theta}\left(CSD_{avg} + CSD_{max}\sum_{k=0}^{n-1}b_{2k+1}\theta^{2k+1}\right)\sin\left(2\theta\right)d\theta = \\ &= -\frac{1}{2\Delta\theta}CSD_{avg}\left[\cos\left(2\theta\right)\right]\bigg|_{0}^{\Delta\theta} + \\ &+ \frac{1}{\Delta\theta}\left[CSD_{max}\sum_{i=0}^{2n-1}\left(-\frac{1}{2}\right)^{i+1}\sin(\frac{1+mod\left(i,2\right)}{2}\pi - 2\theta)\left(\sum_{k=i}^{2n-1}b_{k}\frac{k!}{(k-i)!}\theta^{k-i}\right)\right]\bigg|_{0}^{\Delta\Psi} = \\ &= \frac{1-\cos\left(2\Delta\theta\right)}{2\Delta\theta}CSD_{avg} + \\ &+ \frac{1}{\Delta\theta}CSD_{max}\sum_{i=0}^{2n-1}\left(-\frac{1}{2}\right)^{i+1}\sin(\frac{1+mod\left(i,2\right)}{2}\pi - 2\Delta\Psi)\left(\sum_{k=i}^{2n-1}b_{k}\frac{k!}{(k-i)!}\Delta\Psi^{k-i}\right) \end{split}$$

5.

$$\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} COD(\theta) \cos(2\theta) d\theta =
= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left(COD_{avg} + COD_{max} \sum_{k=0}^{n-1} a_{2k+1} \theta^{2k+1} \right) \cos(2\theta) d\theta =
= \frac{1}{2\Delta\theta} COD_{avg} \left[\sin(2\theta) \right] \Big|_{0}^{\Delta\theta} +
+ \frac{1}{\Delta\theta} \left[COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i} \sin(\frac{1 + mod(i+1,2)}{2} \pi - 2\theta) \left(\sum_{k=i}^{2n-1} a_{k} \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \Big|_{0}^{\Delta\Psi} =
= \frac{1 - \cos(2\Delta\theta)}{2\Delta\theta} COD_{avg} +
+ \frac{1}{\Delta\theta} COD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i} \sin(\frac{1 + mod(i+1,2)}{2} \pi - 2\Delta\Psi) \left(\sum_{k=i}^{2n-1} a_{k} \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right)$$
(25)

6.

$$\begin{split} &\frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} CSD\left(\theta\right) \cos\left(2\theta\right) d\theta = \\ &= \frac{1}{\Delta\theta} \int_{0}^{\Delta\theta} \left(CSD_{avg} + CSD_{max} \sum_{k=0}^{n-1} b_{2k+1} \theta^{2k+1} \right) \cos\left(2\theta\right) d\theta = \\ &= -\frac{1}{2\Delta\theta} CSD_{avg} \left[\cos\left(2\theta\right) \right] \bigg|_{0}^{\Delta\theta} + \\ &+ \frac{1}{\Delta\theta} \left[CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i} \sin\left(\frac{1 + mod\left(i+1,2\right)}{2} \pi - 2\theta \right) \left(\sum_{k=i}^{2n-1} b_{k} \frac{k!}{(k-i)!} \theta^{k-i} \right) \right] \bigg|_{0}^{\Delta\Psi} = \\ &= \frac{1 - \cos\left(2\Delta\theta\right)}{2\Delta\theta} CSD_{avg} + \\ &+ \frac{1}{\Delta\theta} CSD_{max} \sum_{i=0}^{2n-1} \left(-\frac{1}{2} \right)^{i} \sin\left(\frac{1 + mod\left(i+1,2\right)}{2} \pi - 2\Delta\Psi \right) \left(\sum_{k=i}^{2n-1} b_{k} \frac{k!}{(k-i)!} \Delta\Psi^{k-i} \right) \end{split}$$

References

[1] J. Varna, 2.10 crack separation based models for microcracking, in: P. W. Beaumont, C. H. Zweben (Eds.), Comprehensive Composite Materials II, Elsevier, Oxford, 2018, pp. 192 – 220. doi:https://doi.org/10.1016/B978-0-12-803581-8.09910-0.

Appendix A. Explicit expressions for $f(\theta)$ and $g(\theta)$

In the following, recall that

$$\Delta\Psi = \min\left(\Delta\theta, \Delta\Phi\right). \tag{A.1}$$

n = 1

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \sum_{k=0}^{0} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} = a_1 \left(\theta - \frac{\Delta\Psi}{2}\right)$$
$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \sum_{k=0}^{0} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} = b_1 \left(\theta - \frac{\Delta\theta}{2}\right)$$
(A.2)

$$\int_{0}^{\Delta\Psi} f\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = \int_{0}^{\Delta\Psi} a_{1}\left(\theta - \frac{\Delta\Psi}{2}\right) d\theta = \left[\frac{a_{1}}{2}\theta^{2} - a_{1}\frac{\Delta\Psi}{2}\theta\right] \Big|_{0}^{\Delta\Psi} = 0 \quad \forall a_{1}$$

$$\int_{0}^{\Delta\theta} g\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = \int_{0}^{\Delta\theta} b_{1}\left(\theta - \frac{\Delta\theta}{2}\right) d\theta = \left[\frac{b_{1}}{2}\theta^{2} - b_{1}\frac{\Delta\theta}{2}\theta\right] \Big|_{0}^{\Delta\theta} = 0 \quad \forall b_{1}$$
(A.3)

$$COD_{avg} + COD_{max}a_1 \left(\Delta \Psi - \frac{\Delta \Psi}{2}\right) = 0 \rightarrow a_1 = -\frac{2}{\Delta \Psi} \frac{COD_{avg}}{COD_{max}}$$

$$CSD_{avg} + CSD_{max}b_1 \left(\Delta \theta - \frac{\Delta \theta}{2}\right) = 0 \rightarrow b_1 = -\frac{2}{\Delta \theta} \frac{CSD_{avg}}{CSD_{max}}$$
(A.4)

$$\begin{split} &\sum_{i=0}^{1} \left(-\frac{1}{2} \right)^{i+1} \sin \left(\frac{1 + mod (i, 2)}{2} \pi - 2\Delta \Psi \right) \left(\sum_{k=0}^{1-i} a_k \left(1 - (k+1) \right) ! \Delta \Psi^k \right) = \\ &= \left(-\frac{1}{2} \right)^{1} \sin \left(\frac{1 + mod (0, 2)}{2} \pi - 2\Delta \Psi \right) \left(\sum_{k=0}^{1} a_k \left(1 - (k+1) \right) ! \Delta \Psi^k \right) + \\ &+ \left(-\frac{1}{2} \right)^{2} \sin \left(\frac{1 + mod (1, 2)}{2} \pi - 2\Delta \Psi \right) \left(\sum_{k=0}^{0} a_k \left(1 - (k+1) \right) ! \Delta \Psi^k \right) = \\ &= -\frac{1}{2} \cos \left(2\Delta \Psi \right) \left(\sum_{k=0}^{1} a_k \left(1 - (k+1) \right) ! \Delta \Psi^k \right) + \\ &+ \frac{1}{4} \sin \left(2\Delta \Psi \right) \left(\sum_{k=0}^{0} a_k \left(1 - (k+1) \right) ! \Delta \Psi^k \right) = \\ &= -\frac{1}{2} \cos \left(2\Delta \Psi \right) \left(a_0 + a_1 \left(n - (k+1) \right) ! \Delta \Psi^k \right) + \\ &+ \frac{1}{4} \sin \left(2\Delta \Psi \right) \left(\sum_{k=0}^{0} a_k \left(n - (k+1) \right) ! \Delta \Psi^k \right) = \end{split}$$

$$(A.5)$$

n = 2

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \sum_{k=0}^{1} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} = a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) + a_3 \left(\theta - \frac{\Delta\Psi}{2}\right)^3$$
$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \sum_{k=0}^{1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} = b_1 \left(\theta - \frac{\Delta\theta}{2}\right) + b_3 \left(\theta - \frac{\Delta\theta}{2}\right)^3 \tag{A.6}$$

n = 3

$$f\left(\theta - \frac{\Delta\Psi}{2}\right) = \sum_{k=0}^{2} a_{2k+1} \left(\theta - \frac{\Delta\Psi}{2}\right)^{2k+1} =$$

$$= a_1 \left(\theta - \frac{\Delta\Psi}{2}\right) + a_3 \left(\theta - \frac{\Delta\Psi}{2}\right)^3 + a_5 \left(\theta - \frac{\Delta\Psi}{2}\right)^5$$

$$g\left(\theta - \frac{\Delta\theta}{2}\right) = \sum_{k=0}^{1} b_{2k+1} \left(\theta - \frac{\Delta\theta}{2}\right)^{2k+1} =$$

$$= b_1 \left(\theta - \frac{\Delta\theta}{2}\right) + b_3 \left(\theta - \frac{\Delta\theta}{2}\right)^3 + b_5 \left(\theta - \frac{\Delta\theta}{2}\right)^5$$
(A.7)