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Education and Culture

Erasmus Mundus



Outline

➤ Symbols, Models, Equations & Reference Data

➤ Results

SYMBOLS, MODELS, EQUATIONS & REFERENCE DATA

Symbols

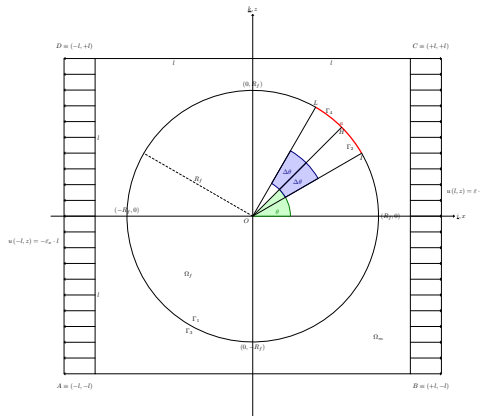
Symbol	Unit	Description
θ	[°]	Debond angular position with respect to the center of the arc defined by the debond itself
$\Delta\theta$	[°]	Debond semi-angular aperture
δ	[°]	Angle subtended by a single element at the fiber/matrix interface
VF_f	[—]	Fiber volume fraction
l	[μm]	Ply's half-length, equal to RVE's half-length (square element)
u	[μm]	Displacement along x
w	[μm]	Displacement along z

Symbols

Symbol	Unit	Description
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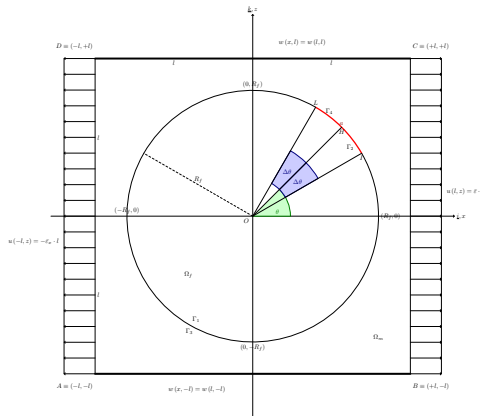
Γ_1	$[-]$	Bonded part of fiber surface
Γ_2	$[-]$	Free (debonded) part of fiber surface
Γ_3	$[-]$	Bonded part of matrix surface
Γ_4	$[-]$	Free (debonded) part of matrix surface

Reference Models



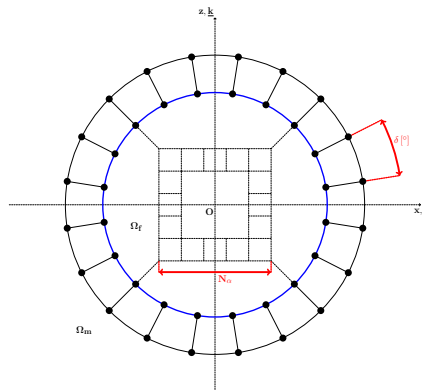
Simple RVE, BC: free.

Reference Models



Simple RVE, BC: fixed vertical displacement.

Angular discretization



Angular discretization at fiber/matrix interface: $\delta = \frac{360^\circ}{4N_\alpha}$.

Material properties

Material	E [GPa]	G [GPa]	ν [—]
Glass fiber	70,0	29,2	0,2
Epoxy	3,5	1,25	0,4

Evaluation of G_0

$$G_0 = \pi R_f \sigma_0^2 \frac{1 + k_m}{8 G_m} \quad (1)$$

$$k_m = 3 - 4\nu_m \quad (2)$$

$$\sigma_0^{undamaged} = \frac{E_m}{1 - \nu_m^2} \varepsilon_{xx} \quad (3)$$

VCCT in Forces

$$\Delta u = \left| \Delta u_{1 \text{ element before crack tip}}^{\text{matrix}} - \Delta u_{1 \text{ element before crack tip}}^{\text{fiber}} \right| \quad (4)$$

$$\Delta w = \left| \Delta w_{1 \text{ element before crack tip}}^{\text{matrix}} - \Delta w_{1 \text{ element before crack tip}}^{\text{fiber}} \right| \quad (5)$$

$$\beta = \arctan \left(\frac{z_{\text{crack tip}}^{\text{matrix, undef}}}{x_{\text{crack tip}}^{\text{matrix, undef}}} \right) \quad (6)$$

$$\Delta_r = \cos(\beta)\Delta u + \sin(\beta)\Delta w \quad \Delta_\theta = -\sin(\beta)\Delta u + \cos(\beta)\Delta w \quad (7)$$

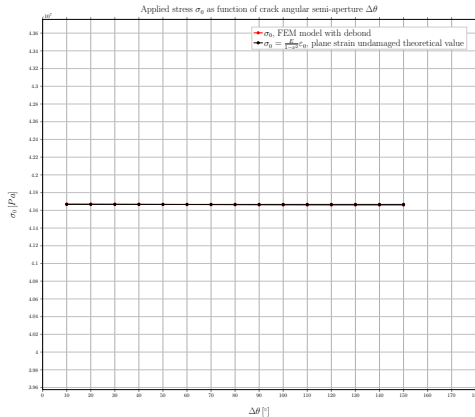
$$F_r = \cos(\beta)F_x^{\text{reaction}} + \sin(\beta)F_z^{\text{reaction}} \quad F_\theta = -\sin(\beta)F_x^{\text{reaction}} + \cos(\beta)F_z^{\text{reaction}} \quad (8)$$

$$G_I = \frac{1}{2} \frac{F_r \Delta_r}{R_f \delta} \quad G_{II} = \frac{1}{2} \frac{F_\theta \Delta_\theta}{R_f \delta} \quad b = 1.0 \leftrightarrow \Delta A = b R_f \delta \quad (9)$$

↓ RESULTS

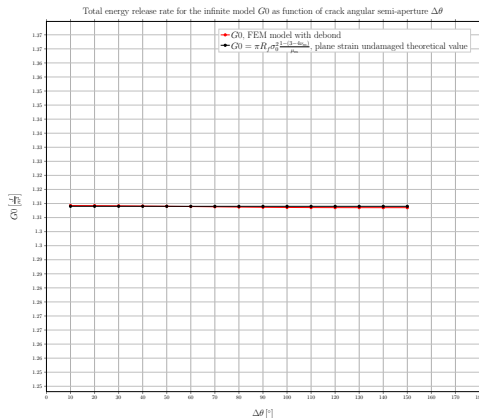
Model Data

$$\sigma_0, \delta = 1.0^\circ$$



In red small strain FEM, in black analytical plain strain value.

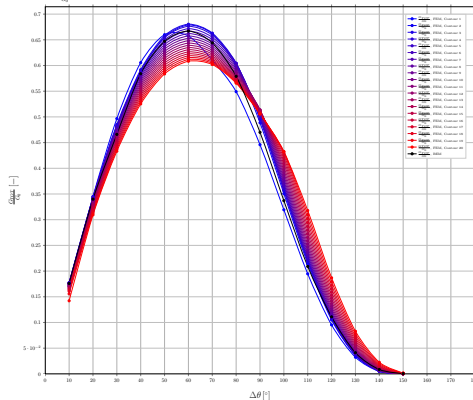
$G_0, \delta = 1.0^\circ$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 1.0^\circ$

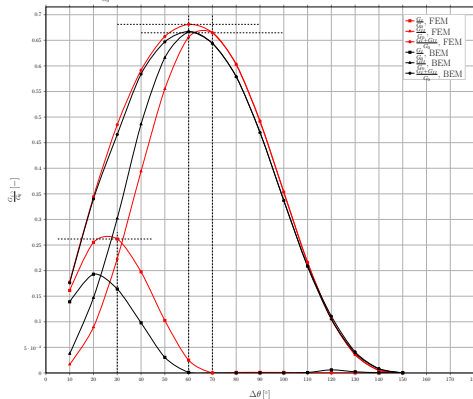
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



Fading from blue to red for contours further from the crack tip, FEM results; in black BEM results.

VCCT in forces (in-house Python routine), $\delta = 1.0^\circ$

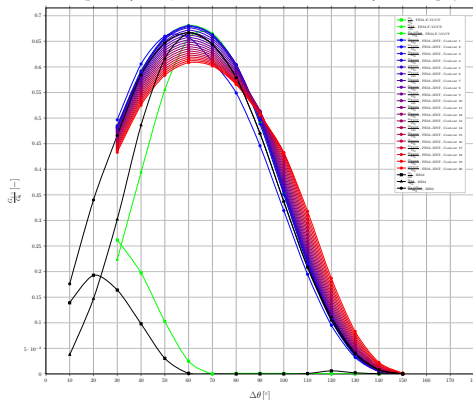
Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT post-processing routine



In green VCCT from FEM results, in black BEM results; positions of maxima highlighted by dashed lines.

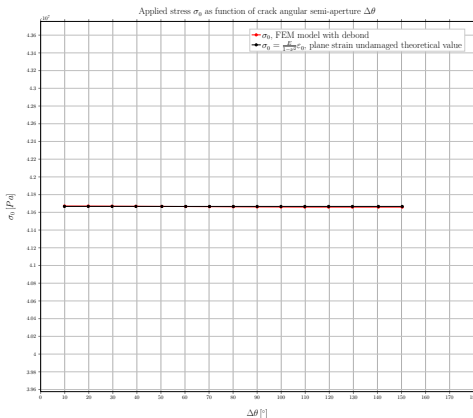
J-Integral and VCCT in forces, $\delta = 1.0^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



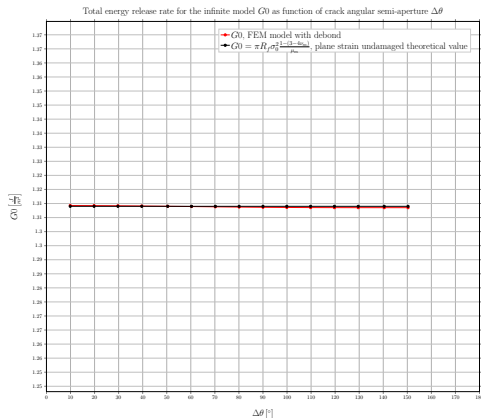
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.9^\circ$$



In red small strain FEM, in black analytical plain strain value.

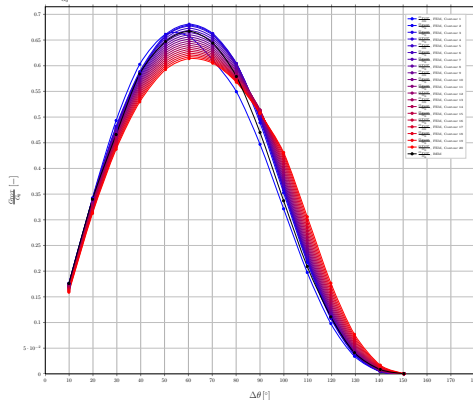
$$G_0, \delta = 0.9^\circ$$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 0.9^\circ$

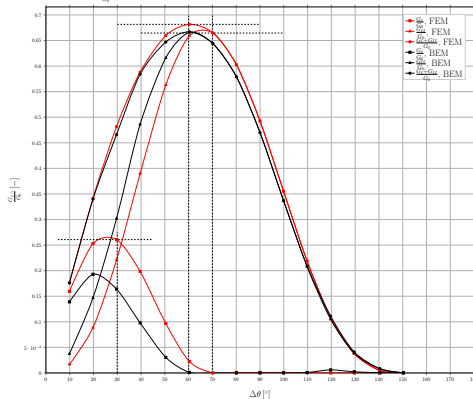
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VCCT in forces (in-house Python routine), $\delta = 0.9^\circ$

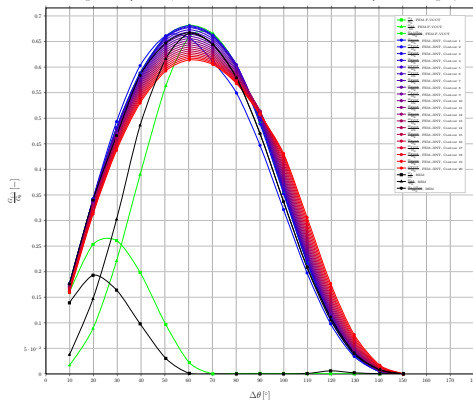
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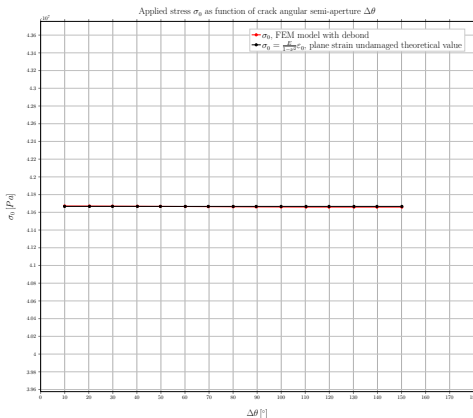
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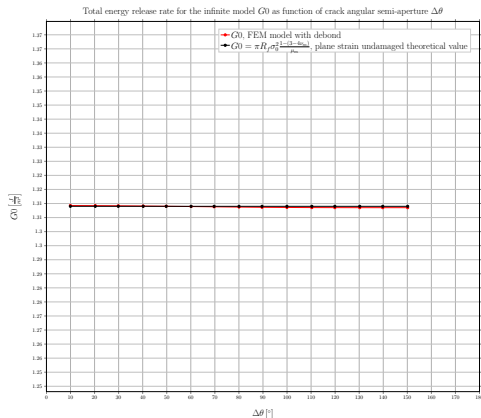
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.8^\circ$$



In red small strain FEM, in black analytical plain strain value.

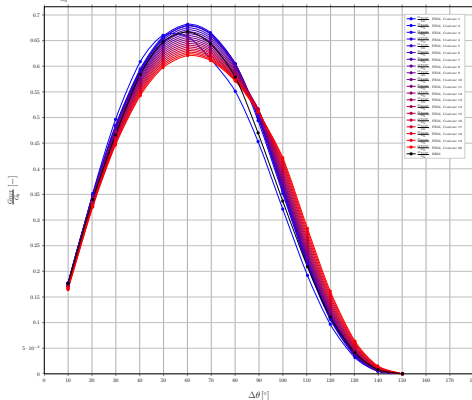
$$G_0, \delta = 0.8^\circ$$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 0.8^\circ$

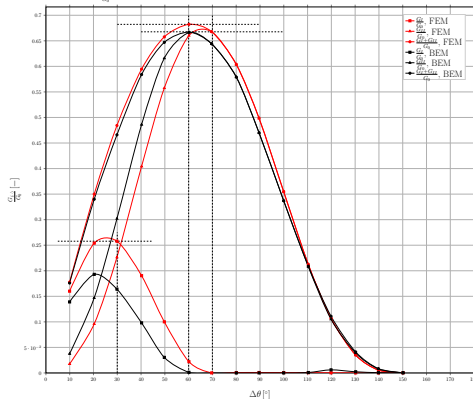
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



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VCCT in forces (in-house Python routine), $\delta = 0.8^\circ$

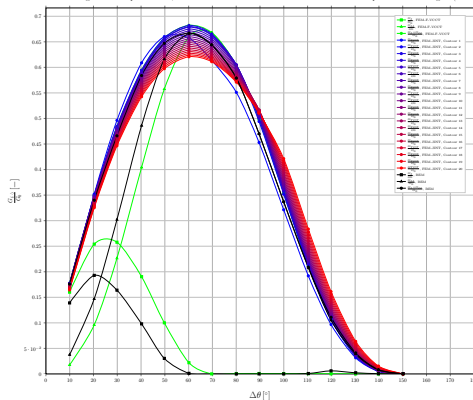
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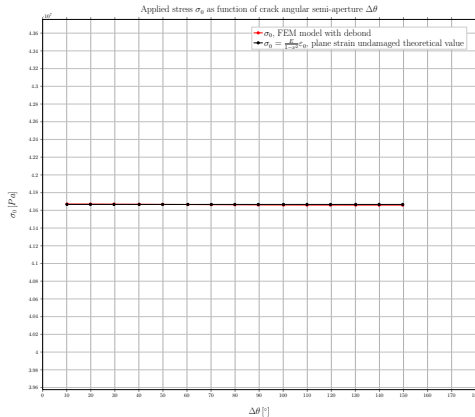
J-Integral and VCCT in forces, $\delta = 0.8^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



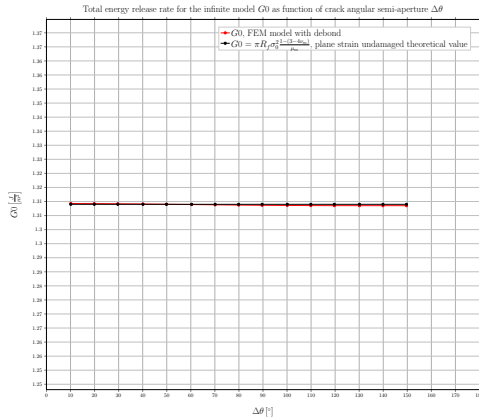
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.7^\circ$$



In red small strain FEM, in black analytical plain strain value.

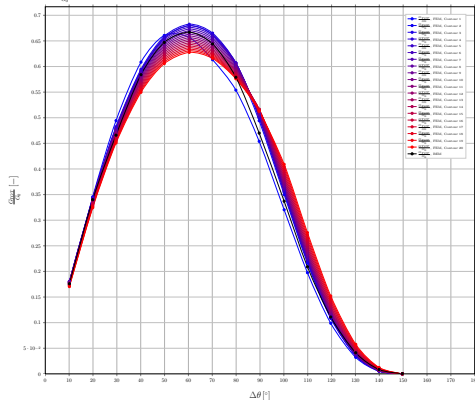
$$G_0, \delta = 0.7^\circ$$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 0.7^\circ$

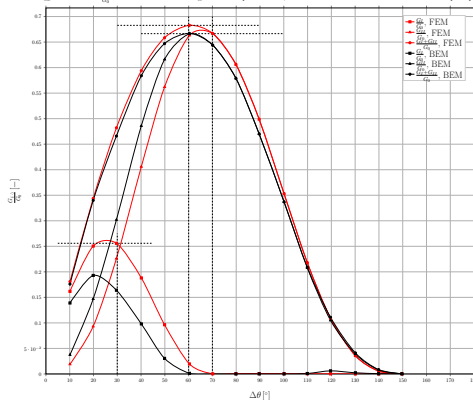
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



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VCCT in forces (in-house Python routine), $\delta = 0.7^\circ$

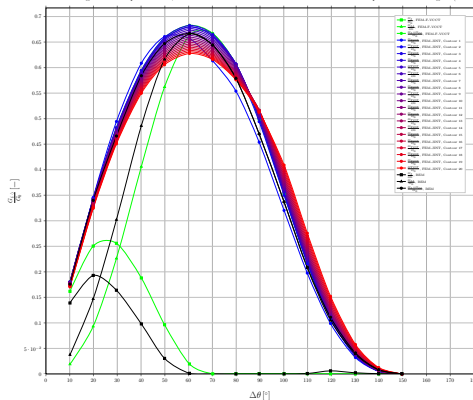
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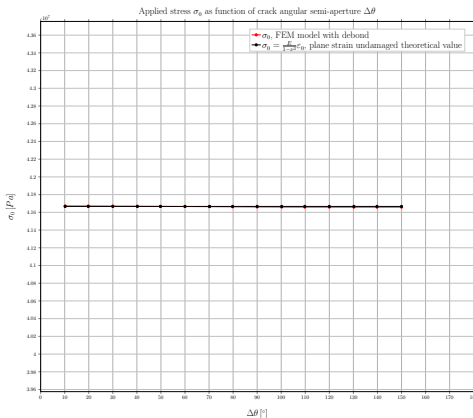
J-Integral and VCCT in forces, $\delta = 0.7^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



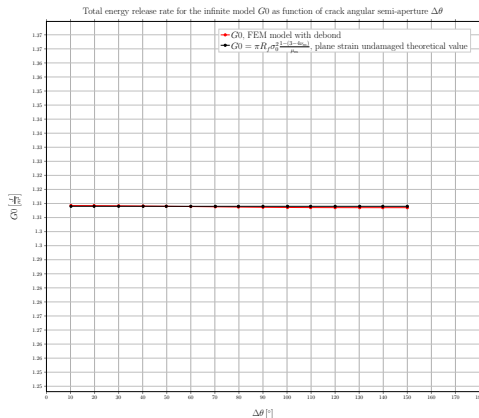
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.6^\circ$$



In red small strain FEM, in black analytical plain strain value.

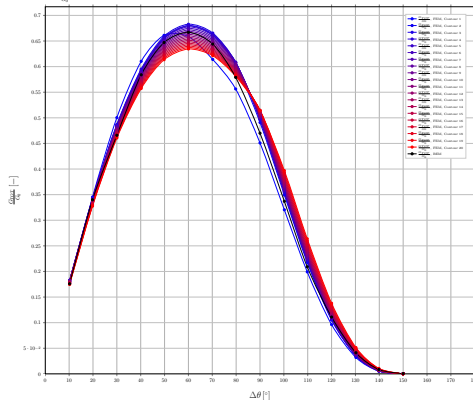
$$G_0, \delta = 0.6^\circ$$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 0.6^\circ$

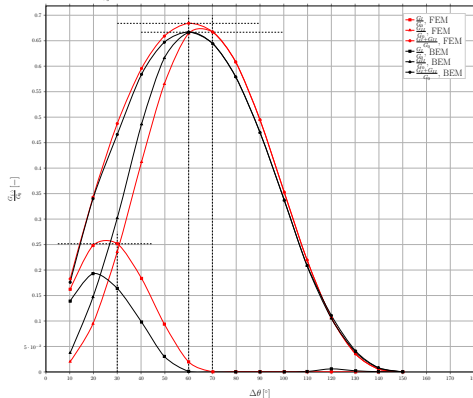
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



Fading from blue to red for contours further from the crack tip, FEM results; in black BEM results.

VCCT in forces (in-house Python routine), $\delta = 0.6^\circ$

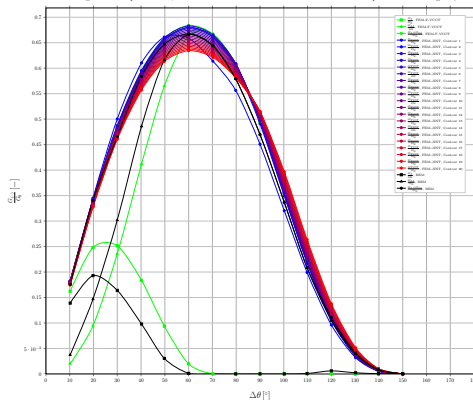
Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT post-processing routine



In green VCCT from FEM results, in black BEM results; positions of maxima highlighted by dashed lines.

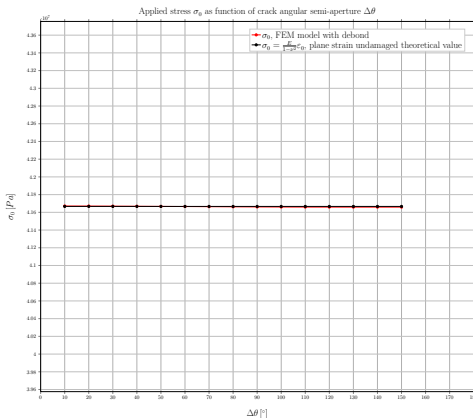
J-Integral and VCCT in forces, $\delta = 0.6^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



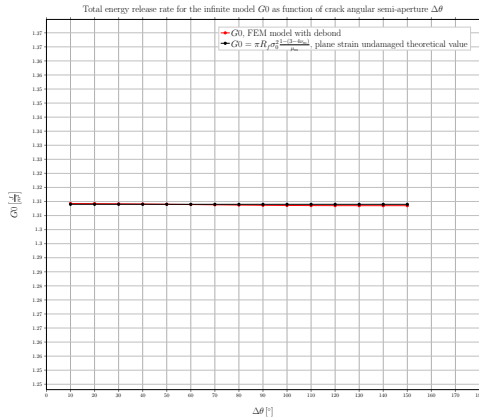
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.5^\circ$$



In red small strain FEM, in black analytical plain strain value.

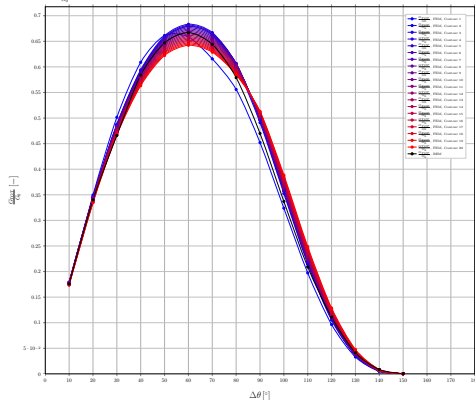
$$G_0, \delta = 0.5^\circ$$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 0.5^\circ$

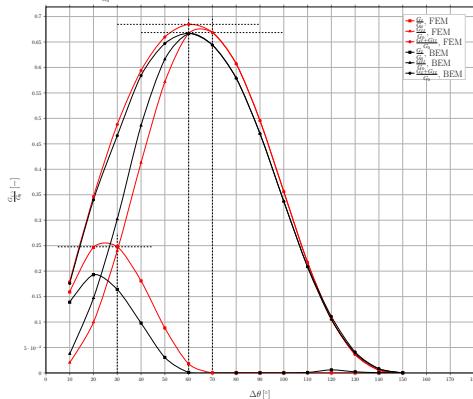
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



Fading from blue to red for contours further from the crack tip, FEM results; in black BEM results.

VCCT in forces (in-house Python routine), $\delta = 0.5^\circ$

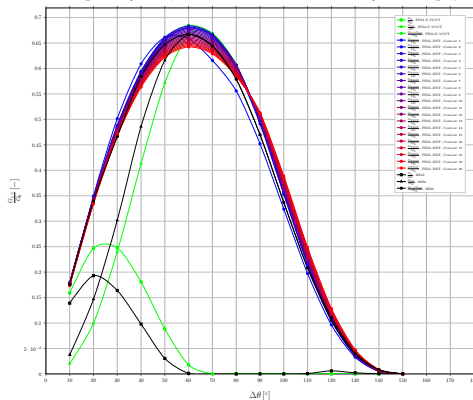
Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT post-processing routine



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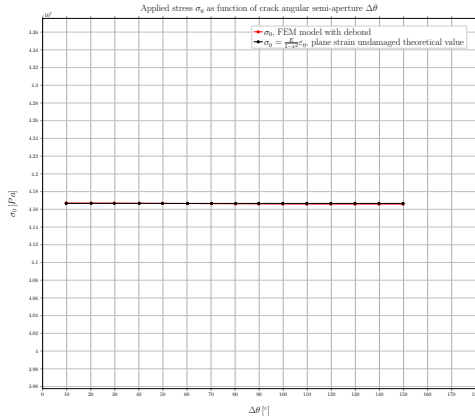
J-Integral and VCCT in forces, $\delta = 0.5^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



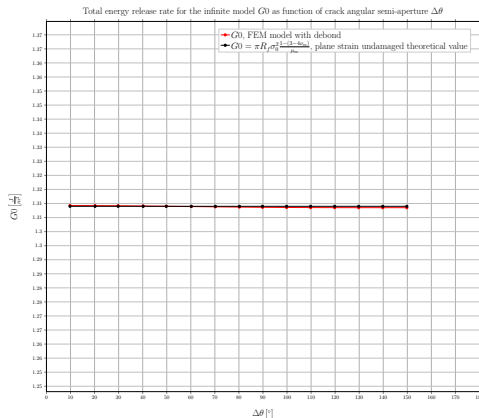
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.4^\circ$$



In red small strain FEM, in black analytical plain strain value.

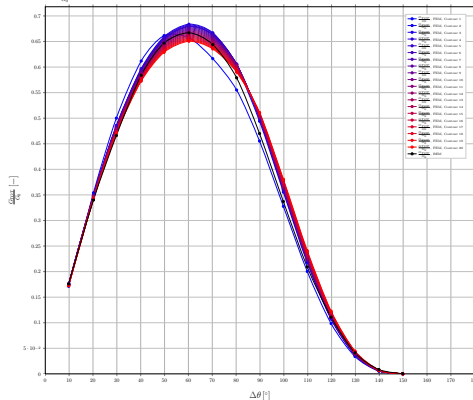
$$G_0, \delta = 0.4^\circ$$



In red small strain FEM, in black analytical plain strain value.

J-Integral (Abaqus built-in routine), $\delta = 0.4^\circ$

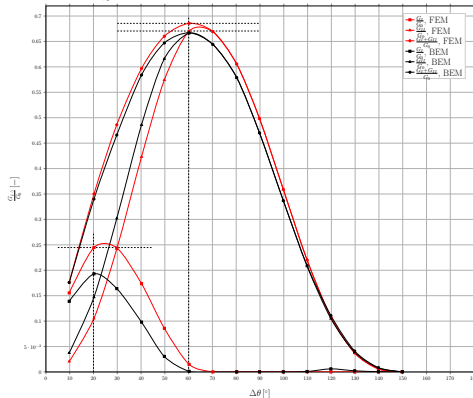
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



Fading from blue to red for contours further from the crack tip, FEM results; in black BEM results.

VCCT in forces (in-house Python routine), $\delta = 0.4^\circ$

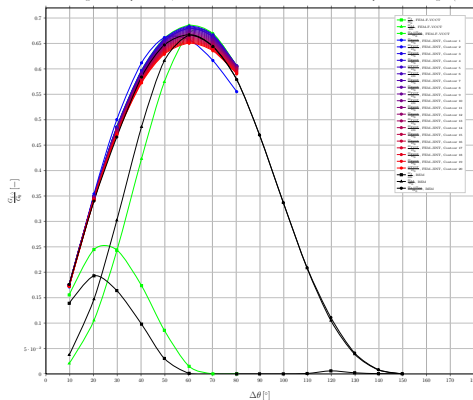
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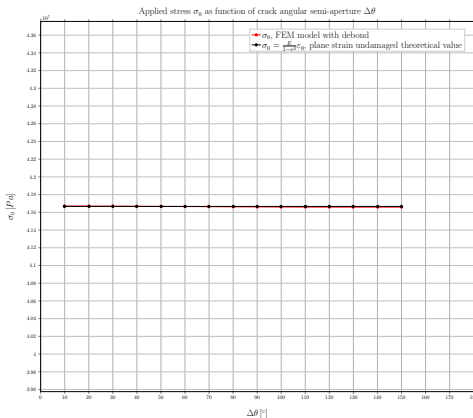
J-Integral and VCCT in forces, $\delta = 0.4^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



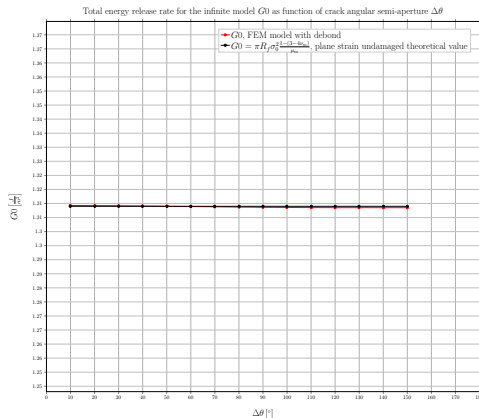
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.3^\circ$$



In red small strain FEM, in black analytical plain strain value.

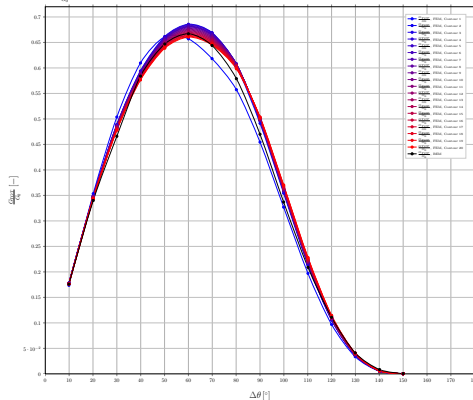
$$G_0, \delta = 0.3^\circ$$



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J-Integral (Abaqus built-in routine), $\delta = 0.3^\circ$

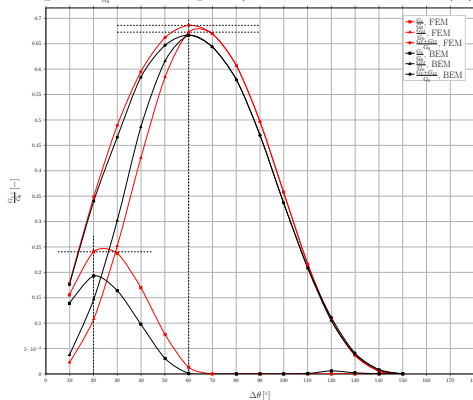
Normalized total energy release rate $\frac{G_{tot}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with Abaqus built-in J-Integral post-processing routine (*CONTOUR INTEGRAL)



Fading from blue to red for contours further from the crack tip, FEM results; in black BEM results.

VCCT in forces (in-house Python routine), $\delta = 0.3^\circ$

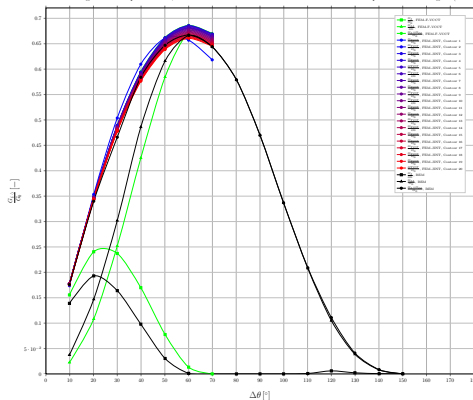
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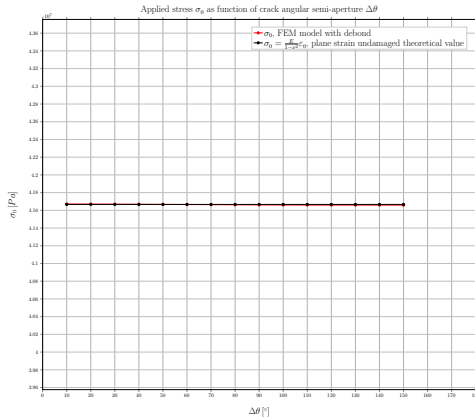
J-Integral and VCCT in forces, $\delta = 0.3^\circ$

Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT and Abaqus built-in J-Integral (*CONTOUR INTEGRAL) post-processing routines



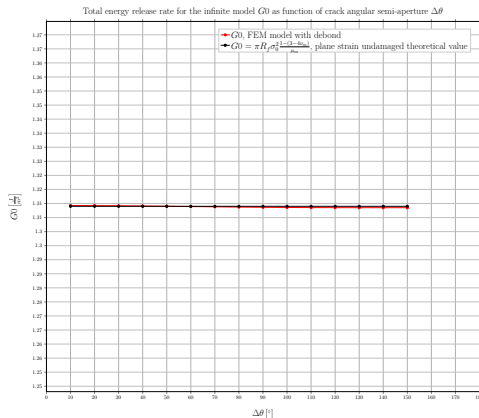
Fading from blue to red for contours further from the crack tip, J-Integral from FEM results; in green VCCT from FEM results; in black BEM results.

$$\sigma_0, \delta = 0.2^\circ$$



In red small strain FEM, in black analytical plain strain value.

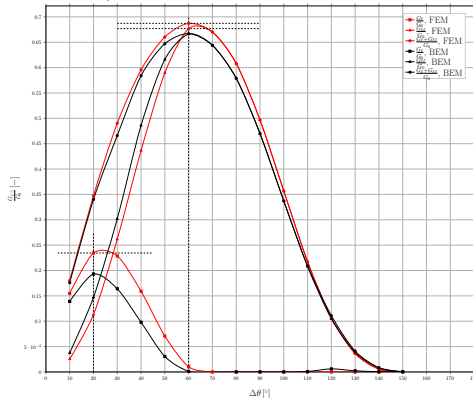
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In red small strain FEM, in black analytical plain strain value.

VCCT in forces (in-house Python routine), $\delta = 0.2^\circ$

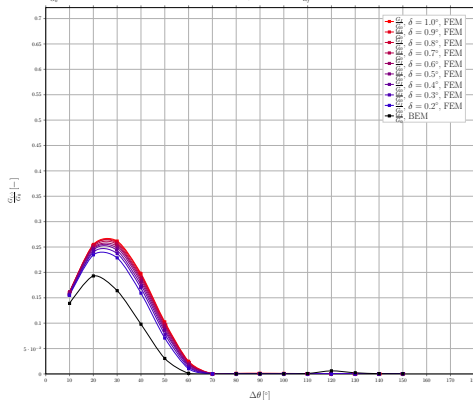
Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, calculated with in-house force-based VCCT post-processing routine



In green VCCT from FEM results, in black BEM results; positions of maxima highlighted by dashed lines.

G_I , VCCT in forces

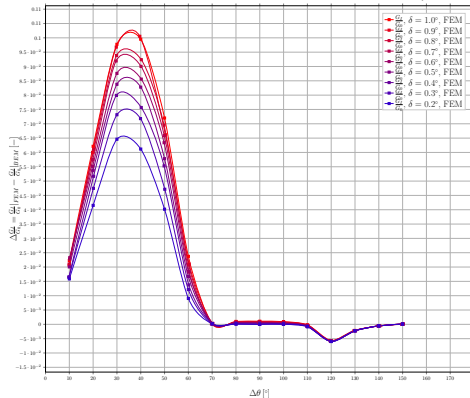
Normalized energy release rate $\frac{G_I}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, $VF_I = 7.9 \cdot 10^{-5}$, $\frac{G_I}{G_0} \sim 100$ calculated with in-house force-based VCCT post-processing routine



Fading from red to blue for decreasing size of elements at the interface, VCCT from FEM results; in black BEM results.

G_I Error with respect to BEM, VCCT in forces

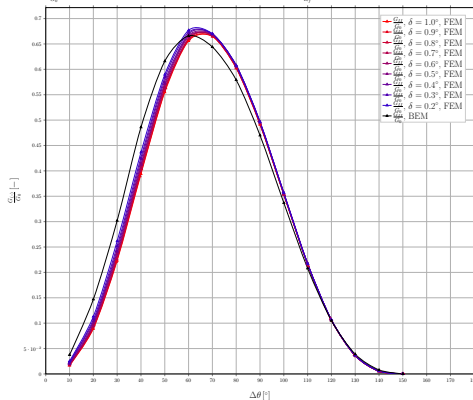
Error of normalized energy release rate with respect to BEM results $\Delta \frac{\bar{G}_I}{\bar{G}_I} = \frac{\bar{G}_I}{\bar{G}_I} |_{FEM} - \frac{\bar{G}_I}{\bar{G}_I} |_{BEM}$ as function of crack angular semi-aperture $\Delta\theta$, $V/F_I = 7.9 \cdot 10^{-5}$, $\frac{L}{R_I} \sim 100$ calculated with in-house force-based VCCT post-processing routine



Fading from red to blue for decreasing size of elements at the interface, VCCT from FEM results.

G_{II} , VCCT in forces

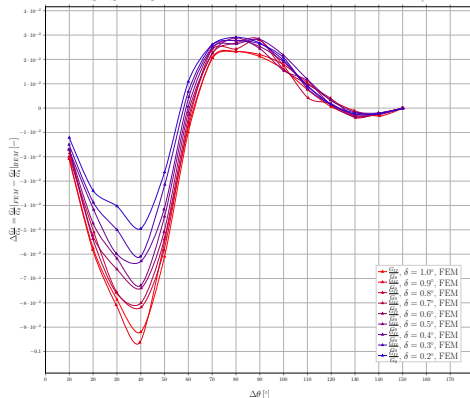
Normalized energy release rate $\frac{G_{II}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, $VF_I = 7.9 \cdot 10^{-5}$, $\frac{G_0}{E_f} \sim 100$ calculated with in-house force-based VCCT post-processing routine



Fading from red to blue for decreasing size of elements at the interface, VCCT from FEM results; in black BEM results.

G_{II} Error with respect to BEM, VCCT in forces

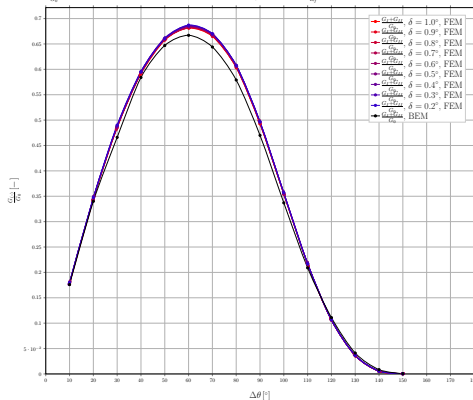
Error of normalized energy release rate with respect to BEM results $\Delta \frac{\bar{G}_0}{G_0} = \frac{\bar{G}_0}{G_0}|_{FEM} - \frac{\bar{G}_0}{G_0}|_{BEM}$ as function of crack angular semi-aperture $\Delta\theta$, $V/F_I = 7.9 \cdot 10^{-5}$, $\frac{L}{R_I} \sim 100$ calculated with in-house force-based VCCT post-processing routine



Fading from red to blue for decreasing size of elements at the interface, VCCT from FEM results.

G_{TOT} , VCCT in forces

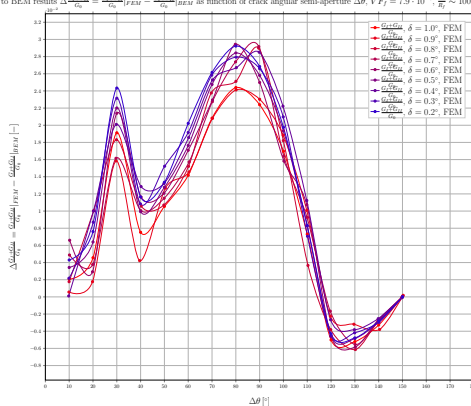
Normalized energy release rate $\frac{G_{TOT}}{G_0}$ as function of crack angular semi-aperture $\Delta\theta$, $V/F_I = 7.9 \cdot 10^{-5}$, $\frac{a}{R_I} \sim 100$ calculated with in-house force-based VCCT post-processing routine



Fading from red to blue for decreasing size of elements at the interface, VCCT from FEM results; in black BEM results.

G_{TOT} Error with respect to BEM, VCCT in forces

Error of normalized energy release rate with respect to BEM results $\Delta \frac{G_{tot}}{G_0} = \frac{G_{tot}}{G_0} |_{FEM} - \frac{G_{tot}}{G_0} |_{BEM}$ as function of crack angular semi-aperture $\Delta\theta$, $VF_7 = 7.9 \cdot 10^{-5}$, $\frac{L}{B_I} \sim 100$ calculated with in-house force-based VCCT post-processing



Fading from red to blue for decreasing size of elements at the interface, VCCT from FEM results.

