

# Effect of uniform distributions of bonded and debonded fibers on the growth of the fiber/matrix interface crack in thin UD laminates with different fiber contents under transverse loading

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## Abstract

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## 1. Introduction

1. We start with a few lines devoted to the spread tow technology and thin plies: what they are, what can be done, what are the possible applications.
- 5 2. By quoting the relevant references, we report on the observation that one of the main beneficial mechanisms in thin ply is the retardation of transverse crack propagation. We then enlarge by reporting the microscopical observations by Saito, in which debonds where also observed. We observe that available microscopic observations are just a few and mainly in 2D.
- 10 3. Propagation of transverse cracks has been widely investigated both analytically and numerically
4. Initiation at the level of fiber/matrix interface is instead a less researched subject.

5. cohesive elements are a possible choice, but have some drawbacks, which  
15 makes a LEFM approach valuable
6. With regard to LEFM studies of laminates under transverse loading, models can be found in the literature about: the single fiber in infinite matrix under different mode of loading, the effect of adjacent fibers on a fiber in infinite matrix under different mode of loading, the single fiber in an  
20 equivalent composite in transverse tension, the effect of adjacent fibers on a fiber in an equivalent composite in transverse tension.
7. For initiation of transverse cracking at the fiber/matrix interface in UD laminates under transverse tension, there is thus a gap regarding: the effect of fiber volume fraction; the interaction of debonded and bonded  
25 fibers in micro-structured assemblies, i.e. no homogenization. This article addresses these two points.
8. We conclude the introduction with a summary of the article's structure.

## 2. RVE models & FE discretization

### 2.1. Introduction & Nomenclature

30 In order to investigate the interaction between debonds in UD composites, we developed different models of laminates in which the only damage present is represented by the fiber/matrix interface crack. All of these Representative Volume Elements feature regular microstructures with fibers placed according to a square-packing tiling. As the very high longitudinal modulus of UD composites and cross-ply laminates ensures that the y-strain due to loading in the  
35 x-direction is small, we consider only 2D models under the assumption of plane strain, defined in the  $x - z$  section of the laminate. Consequently, debonds are considered to be significantly longer in the fiber direction than in the arc direction. The analysis presented thus applies to long debonds, of which we are  
40 interested in understanding the mechanisms of growth along its arc direction. The UD composites are further supposed to be subjected to transverse tension, applied along the  $x$  direction in the pictures. As the models are differentiated

by the number of layers of fibers and by the spacing between debonds along the vertical and horizontal directions, the corresponding Repeating Unit Cells (RUCs) can be distinguished from each other based on the number  $n$  of fibers in the horizontal direction and  $k$  in the vertical direction. Furthermore, the upper surface can be either free or coupling can be applied. We thus introduce the common notation  $n \times k - free$  and  $n \times k - coupling$  to denote a RUC with  $n \times k$  fibers and, respectively, a free upper surface or coupling applied to it. The correspondence between specific combinations of particular choices of  $n$ ,  $k$  and upper boundary conditions and representative models of laminate are detailed in Section 2.2.

## 2.2. Models of Representative Volume Element (RVE)

The first two models feature, as shown in Fig. 1, a UD laminate with only one layer of fibers across its thickness. This is quite an extreme model from the microstructural point of view; however, it allows to focus the analysis on the interaction between debonds placed along the direction of the load. Furthermore, as the upper surface is considered free, the interaction is stronger in this case than in any other, making the predictions of this model rather conservative. In retrospective, if only 20 years ago such a model would have been considered too abstracted from the physical reality, the recent advancements in the spread tow technology make this approach appealing also for practical considerations.

In the first version of the model laminate, Fig. 1a, debonds appear in the laminate on every  $(m + 1)^{th}$  fiber on alternating sides of the partially debonded fiber. The symmetries of the model allow the use of a Repeating Unit Cell (RUC), which corresponds to the Representative Volume Element (RVE) of this microstructure, with a central debonded fiber and  $\frac{m}{2}$  fiber(s) on each side. It is highlighted by blue lines in 1a. Following the notation introduced in Section 2.1, we will refer to this model as  $(m + 1) \times 1 - free$ , where  $n = (m + 1)$ ,  $k = 1$ . In the second version of the single-layer-of-fibers model, 1b, a debond appears on each fiber on alternating sides and the corresponding RUC has only one debonded fiber. We will refer to this model as  $1 \times 1 - free$ , where  $n = k = 1$ .

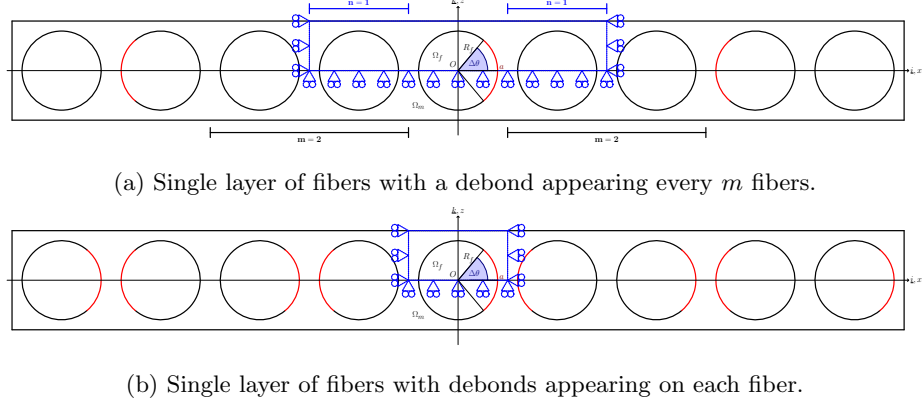


Figure 1: Models of UD laminates with a single layer of fibers and debonds repeating at different distances. The corresponding repeating element (RVE) is highlighted in blue.

The second set of models considers instead laminates with multiple layers of fibers across the thickness: a finite number of layers in the first two models ( 2a and 2b); an infinite number in the model of Fig. 3. In the first representative laminate (Fig. 2a), all the fibers in the central layer are debonded. The UD is made by  $2p + 1$  layers of fibers across the thickness, corresponding to a RUC with  $p + 1$  fibers in the  $z$  direction. This model will be referred to in the following as  $1 \times (p + 1) - free$ , where  $n = 1, k = (p + 1)$ . In the second model (Fig. 2b), a debond appear every  $(m + 1)^{th}$  fiber in the central line of fibers in a laminate with  $2p + 1$  layers. The corresponding RUC has thus  $\frac{m}{2}$  fiber(s) on each side and  $p$  above the partially debonded fiber. We will refer to this model as  $(m + 1) \times (p + 1) - free$ , where  $n = (m + 1), k = (p + 1)$ .

Finally, the last model considers an UD composite with an infinite number of partially debonded fibers. The corresponding RUC is made by a single partially debonded fiber and kinematic coupling conditions applied to the upper boundary. This model is referred to as  $1 \times 1 - coupling$ , where  $n = k = 1$ .

### 2.3. Finite Element (FE) discretization

Each RUC is discretized using the Finite Element Method (FEM) within the Abaqus environment, a commercial FEM package [1]. The length  $l$  and height  $h$

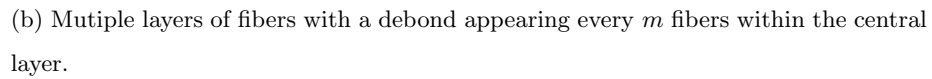
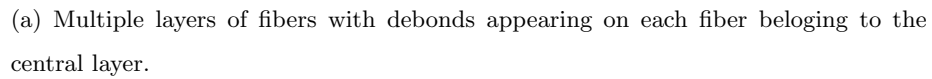


Figure 2: Models of UD laminates with different layers of fibers and debonds repeating at different distances. The corresponding repeating element (RVE) is highlighted in blue.

of the model (see Fig. 4a) are determined by number of fibers  $n$  in the horizontal direction and  $k$  across the thickness (see 2.2) according to Eq. 1:

$$l = 2nL \quad h = (2k - 1)L; \quad (1)$$

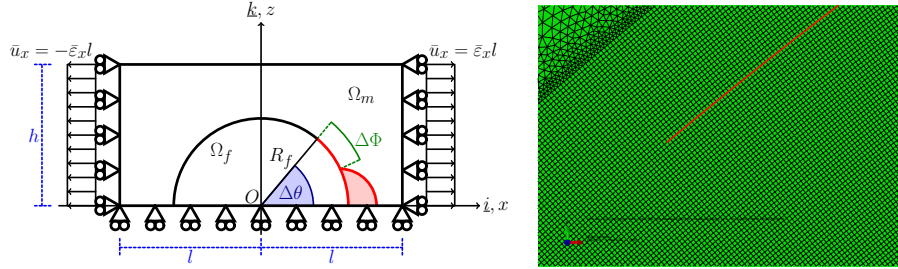
where the reference length  $L$  is defined as a function of the fiber volume fraction  $V_f$  and the fibers' radius according to



Figure 3: Model of UD laminates with an infinite number of layers of fibers and debonds appearing on each fiber. The corresponding repeating element (RVE) is highlighted in blue.

$$L = \frac{R_f}{2} \sqrt{\frac{\pi}{V_f}}. \quad (2)$$

95 The fibers' radius  $R_f$  is assumed to be the same for each fiber present in the model and equal to  $1 \mu m$ . The relationships in Eqs. 1 and 2 thus ensure that the local and global  $V_f$  are everywhere equal.



(a) Schematic of the model with its main parameters. (b) Mesh near the crack tip. Crack's faces shown in red.

Figure 4: Details and main parameters of the Finite Element model.

The debond is placed symmetrically with respect to the  $x$  axis (in red in 4a) and has an angular size of  $\Delta\theta$  (the full debond's size is thus  $2\Delta\theta$ ). For high debond's sizes ( $\geq 60^\circ - 80^\circ$ ), a region of variable size  $\Delta\Phi$  appears at the crack tip in which the crack's faces are in contact and slide on each other. Due to its appearance, frictionless contact is considered between the two crack's faces

to allow free slipping and avoid interpenetration. Symmetry with respect to the  $x$  axis is applied on the lower boundary and kinematic coupling on the left and right sides. The upper boundary is in general free, except for the model  $1 \times 1 - coupling$  (Fig. 3) which requires kinematic coupling also on the upper side. Constant transverse strain  $\bar{\varepsilon}$  equal to 1% is applied to the right and left sides by means of an imposed displacement of, respectively,  $\pm\bar{\varepsilon}l$ .

Table 1: Summary of the mechanical properties of fiber and matrix.

<b>Material</b>	$E [GPa]$	$G [GPa]$	$\nu [-]$
Glass fiber	70.0	29.2	0.2
Epoxy	3.5	1.25	0.4

The model is meshed using second order, 2D, plane strain triangular (CPE6) and rectangular (CPE8) elements. A regular mesh of quadrilateral elements with an almost unitary aspect ratio is required at the crack tip, as shown in Fig. 4b. The angular size  $\delta$  of an element in the crack tip region is always equal to  $0.05^\circ$ . The mode I, mode II and total Energy Release Rates (ERRs) represent the main output of the FEM analysis; they are evaluated using the VCCT technique [2] implemented in a custom Python routine and, for the total ERR, the J-integral [3] by application of the Abaqus built-in functionality. A glass fiber-epoxy system is considered in every model, and it is assumed that their response lies always in the linear elastic domain. The properties used are listed in Table 1.

#### 2.4. Validation of the model

The model is validated in Fig. 5 against the results reported in [4], obtained with the Boundary Element Method (BEM) for a single fiber with a symmetric debond placed in an infinite matrix. This situation is modeled using the *free* RVE with  $V_f = 0.0079\%$ , which corresponds to a RUC's length and height of  $\sim 100$ .

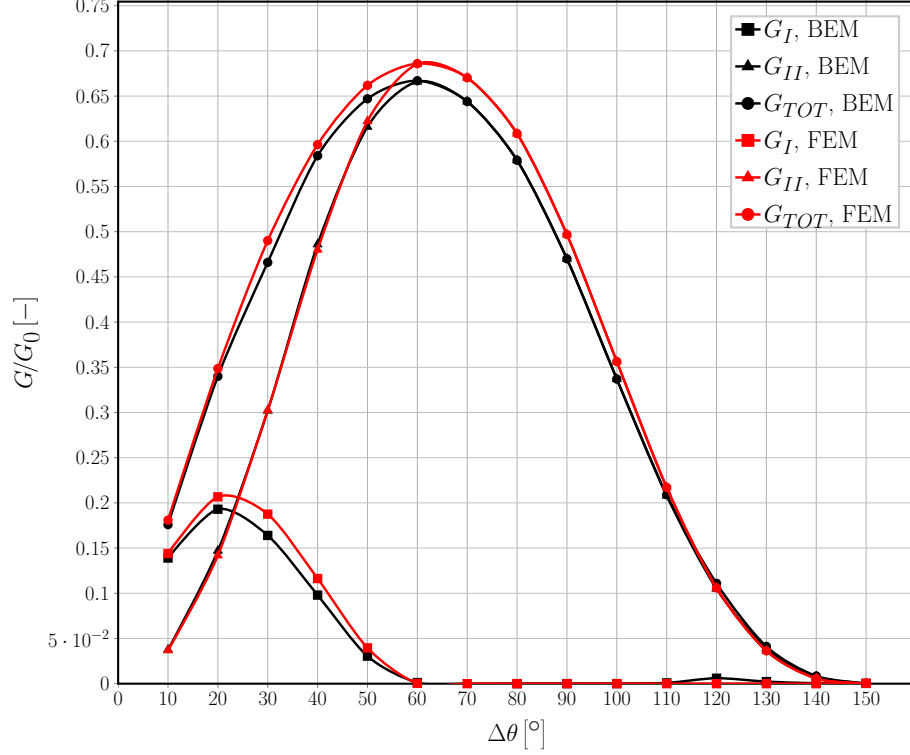


Figure 5: Validation of the single fiber model for the infinite matrix case with respect to the BEM solution in [4].

To allow for a comparison, the results are normalized following [4] with respect to a reference Energy Release Rate  $G_0$  defined as

$$G_0 = \frac{1 + k_m}{8\mu_m} \sigma_0^2 \pi R_f \quad (3)$$

where  $\mu$  is the shear modulus,  $k$  is the Kolosov's constant defined as  $3 - 4\nu$  for plane strain conditions,  $R_f$  is the fiber radius and the pedix  $m$  refers to the properties of the matrix.  $\sigma_0$  is the stress at the boundary, computed as the average of the stress extracted at each boundary node along the right side (arithmetic average as nodes are equispaced by design along both the left and right sides).



### 3. Results & Discussion

#### 3.1. Effect of Fiber Volume Fraction

As shown in Figs. 6 and 7, respectively for mode I and mode II, the fiber content has a drastic effect on the Energy Release Rate at the crack tip of the fibre/matrix interface crack. The effect of four levels of fiber volume fraction are compared, 30%, 50%, 60% and 65%, on two microstructural models: a  $11 \times 6 - free$  (a debond every 11<sup>th</sup> fiber in the central layer of an UD with 11 layers of fibers), Figs. 6a and 7a, and a  $21 \times 11 - free$  (a debond every 21<sup>th</sup> fiber in the central layer of an UD with 21 layers of fibers), Figs. 6b and 7b.

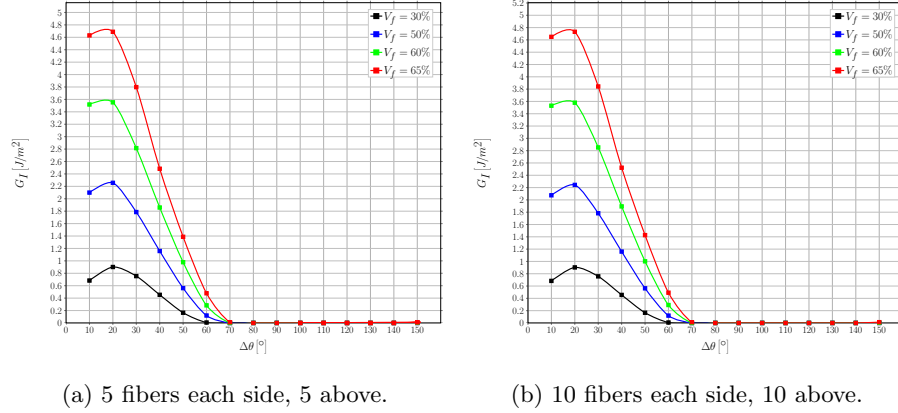


Figure 6: A view of the effect of fiber volume fraction on Mode I ERR in two exemplificative models.

Comparison of Fig. 6a with 6b, and of Fig. 7a with 7b, indicates that there exists a specific effect of the fiber content, independent of the microstructure. For mode I, Fig. 6, the maximum value of the ERR is increased by  $\sim 5.2$  times when  $V_f$  changes from 30% to 65% in both models. The debond's size for which the peak value occurs remains unchanged at  $20^\circ$ , but for 60% and 65% the value at  $10^\circ$  and at  $20^\circ$  are almost identical, approximately creating a plateau and thus making the growth of small debonds ( $\leq 20^\circ$ ) in mode I unstable. Furthermore, increasing the fiber volume fraction delays the onset of the contact zone, which corresponds in 6 to the first value of  $\Delta\theta$  for which  $G_I$  is equal to zero. For

$V_f = 30\%$ , the contact zone first appears for a debond of  $60^\circ$ , similarly to what happens in the single fiber in infinite matrix model (Fig. 5). For higher fiber contents, the contact zone's onset is delayed to a debond's size equal to  $70^\circ$ .

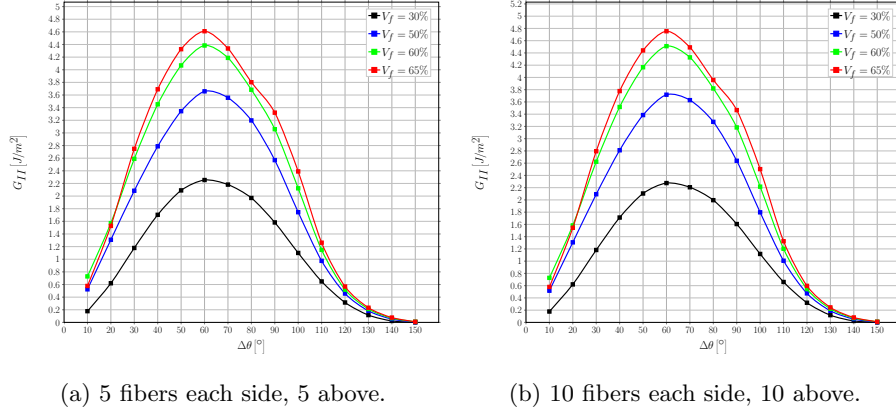


Figure 7: A view of the effect of fiber volume fraction on Mode II ERR in two exemplificative models.

For mode II, Fig. 6, the maximum value of the ERR is increased by  $\sim 2.1$  times when  $V_f$  changes from 30% to 65% in both models. The effect is thus similar to mode I, but with a significantly lower magnitude. As for mode I, the debond's size for which the peak value occurs remains unchanged, at  $60^\circ$  for mode II. The shape of the curve remains instead unchanged, thus no effect on the stability of mode II with respect to debond's size can be observed. It is worthwhile to notice, however, that the ratio of mode II to mode I peak values is  $\frac{\max(G_{II})}{\max(G_I)} \sim \frac{2.2}{0.9} \sim 2.4$  for  $V_f = 30\%$ , while it is  $\sim \frac{4.7}{4.7} \sim 1$  for  $V_f = 65\%$  in both models. Given that the peaks occur at different debond's sizes, for which the value of the other ERR is very small or even close to zero, this means that the increase in fiber content creates a long range of very close values of total ERR, and thus has a global destabilizing effect on the debond's growth.

The general increasing trends observed in Figs. 6 and 7 are related to the fact that, given that the global and local  $V_f$  are everywhere identical in the models presented, an increase in fiber content corresponds to a decrease in the average distance between fibers. Thus, the relaxation of the stress and strain fields in the

matrix domain occurs over smaller lengths causing higher values at the crack tip. The difference in relative magnification between mode I and mode II and the delay in the contact zone's onset are instead due to the interplay between two different mechanisms, both caused by the ordered microstructural arrangement of the model. In the models considered, a fully bonded fiber is always placed  
175 along the horizontal direction, aligned with the partially debonded fiber and exactly in front of the debond. By increasing  $V_f$ , the former moves closer to the latter and this causes a magnification of the x-strain at the crack tip. For small debonds ( $\leq 20^\circ - 30^\circ$ ), the crack tip is approximately normal to the x-direction  
180 and thus an increase in  $\varepsilon_x$  causes an increase in  $G_I$ . On the other hand, for large debonds ( $\geq 70^\circ - 80^\circ$ ) the crack growth is almost aligned with the x-axis, thus a magnification in the x-strain translates into an increase of mode II ERR. However, this increasing effect on  $G_{II}$  is counteracted by the presence of a fully bonded fiber along the vertical direction, aligned with the partially debonded  
185 one. As fibers are more rigid than the surrounding matrix, the presence of the former will restrain horizontal displacements, thus hampering strong increases in  $G_{II}$  for large debonds. Furthermore, due to the mismatch in the Poisson's ratios, the fully bonded fiber placed above generates an upward-directed component of the vertical displacement field in the matrix, which tends to open the debond  
190 and causes the delay in the contact zone's onset. The interplay between these mechanisms is governed by the average inter-fiber distance and, in turn, by the fiber volume fraction.

### 3.2. Interaction between debonds in UD laminates with a single layer of fibers

The interaction of debonds appearing at regular intervals in UD composites with a single layer of fibers is studied for mode I (Fig. 8) and mode II (Fig. 9)  
195 and fiber content equal to 30% (Figs. 8a and 9a) and 60% (Figs. 8b and 9b). The models treated are  $3 \times 1 - free$ ,  $5 \times 1 - free$ ,  $7 \times 1 - free$ ,  $11 \times 1 - free$ ,  $21 \times 1 - free$ ,  $101 \times 1 - free$  and  $201 \times 1 - free$ , corresponding respectively to a debond every  $3^{rd}$ ,  $5^{th}$ ,  $7^{th}$ ,  $11^{th}$ ,  $21^{st}$ ,  $101^{st}$  and  $201^{st}$  fiber (Fig. 1a). Given  
200 that the upper surface of the UD is left free, the interaction is stronger than in

any other case and the results of this section are thus the most conservative in terms of debond's growth. From both 8 and 9, it can be seen that the presence of a debond decreases the strain magnification effect discussed in Sec. 3.1 and thus reduces the value of the ERR.

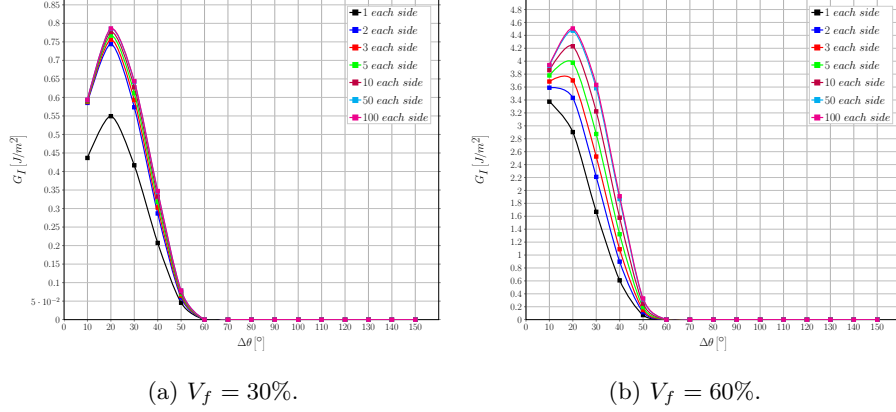


Figure 8: Effect of the interaction between debonds appearing at regular intervals on Mode I ERR in an UD with a single layer of fibers at different levels of fiber volume fraction  $V_f$ .

For mode I, the presence of a free surface, and inversely the absence of a fully bonded fiber along the vertical direction, implies the absence of the counteracting upward-oriented vertical component of the displacement field due to the mismatch in Poisson's ratios. This in turn translates into the constancy of the value of  $\Delta\theta$  corresponding to contact zone's onset, always equal to  $60^\circ$ . For  $V_f = 30\%$ , mode I is reduced going from a debond placed every 5<sup>th</sup> fiber to every 3<sup>th</sup> fiber. Larger spacing does not seem to have a sizable effect. Similarly, at 60% no difference can be seen between the case of a debond placed every 101<sup>th</sup> and every 201<sup>th</sup> fiber. These observations suggest the existence of characteristic distance dependent on the fiber volume fraction which governs the interaction between debonds.

Without constraint on the upper surface, the strain magnification effect creates larger displacements in the x-direction, which increase mode II for larger debonds. When debonds are far apart, the series of rigid elements (constituted by fully bonded fibers and their surrounding matrix) creates higher x-strains,

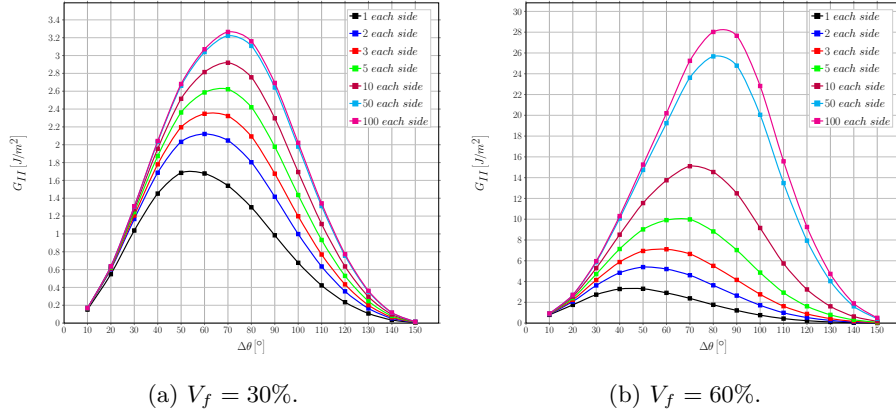


Figure 9: Effect of the interaction between debonds appearing at regular intervals on Mode II ERR in a single-ply laminate with a single layer of fibers at different levels of fiber volume fraction  $V_f$ .

220 which in turn generates higher tangential displacements at the crack tip for larger debonds. Conversely, when debonds are closer, the strain concentration is reduced and the tangential component at the crack tip decreases for large  $\Delta\theta$ . This is the mechanism behind the change in the value of  $\Delta\theta$  for which the peak of  $G_{II}$  occurs: from  $70^\circ$  to  $50^\circ$  at 30%, and from  $80^\circ$  to  $40^\circ$  at 60% going

225 from the higher to the smaller spacing of debonds. Differently from mode I, the presence of a characteristic distance is harder to establish. For  $V_f = 30\%$  (Fig. 9a), it seems reasonable to establish it at around 100 fully bonded fibers between each debond. For  $V_f = 60\%$  (Fig. 9b), the difference between models  $101 \times 1 - free$  and  $201 \times 1 - free$  is still sizable, thus preventing the establish-

230 ment of such characteristic distance. It is possible to observe, however, that the change between  $101 \times 1 - free$  and  $201 \times 1 - free$  is significantly smaller than between  $21 \times 1 - free$  and  $101 \times 1 - free$  ( $2 \left[ \frac{J}{m^2} \right]$  vs  $11 \left[ \frac{J}{m^2} \right]$ ), thus suggesting the existence of the characteristic distance outside the range studied.

### 3.3. Influence of layers of fully bonded fibers on debond's growth in a line of debonded fibers located at mid-thickness

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The effect of the presence of layers of fully bonded fibers on debond's growth in a line of partially debonded fibers located at mid-thickness in UD composites is studied for mode I (Fig. 10) and mode II (Fig. 11) and fiber content equal to 30% (Figs. 10a and 11a) and 60% (Figs. 10b and 11b). The models treated are  
 240  $1 \times 2 - free$ ,  $1 \times 3 - free$ ,  $1 \times 4 - free$ ,  $1 \times 6 - free$ ,  $1 \times 11 - free$ ,  $1 \times 51 - free$  and  $1 \times 101 - free$ , corresponding to a UD composite with respectively 3, 5, 7, 11, 21, 101 and 201 layers of fibers (Fig. 2a).

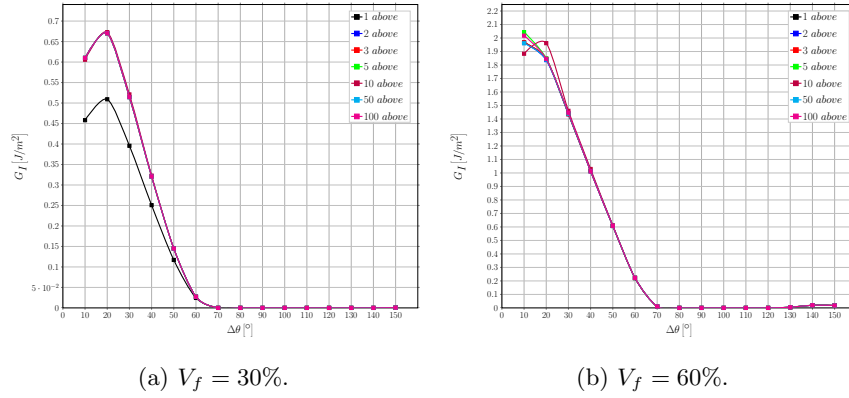


Figure 10: Influence of layers of fully bonded fibers on debond's growth in Mode I ERR in a centrally located line of debonded fibers at different levels of fiber volume fraction  $V_f$ .

The results shown strengthen the considerations made in Sec. 3.1. It can in fact be seen in Fig. 10 that the presence of fully bonded fibers across the  
 245 thickness delays the onset of the contact zone to a debond of  $70^\circ$  in size, due to the introduction of an additional upward-directed component of the vertical displacement which translates into an opening displacement at the debond's tip.

The results of both mode I and mode II show how the introduction of an increasing number of fully bonded fibers doesn't change the ERR calculated at the crack tip. The effect of the  $V_f$  can be observed at low fiber content (Figs. 10a  
 250 and 11a), while for high fiber content the smaller model with only fiber above the partially debonded one is already representative.

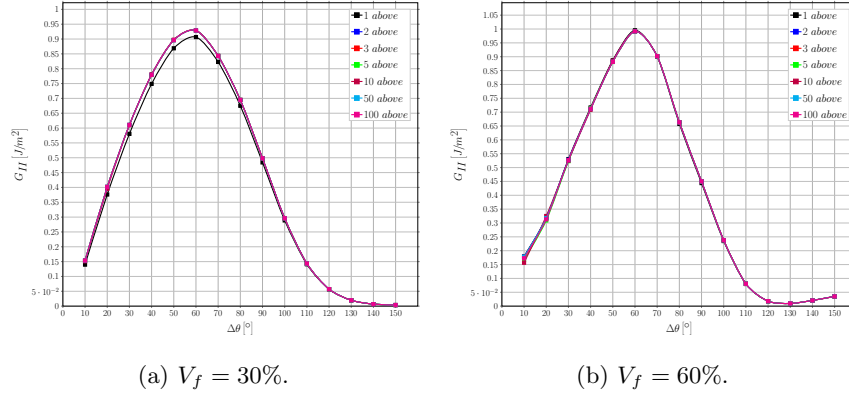


Figure 11: Influence of layers of fully bonded fibers on debond's growth in Mode II ERR in a centrally located line of debonded fibers at different levels of fiber volume fraction  $V_f$ .

### 3.4. Interaction between debonds in UD laminates with multiple layers of fibers

The interaction of debonds appearing at regular intervals in UD composites with multiple layers of fibers is investigated for mode I (Fig. ??) and mode II (Fig. 13) and fiber content equal to 30% (Figs. 12a and 13a) and 60% (Figs. 12b and 13b). The models treated are  $3 \times 2 - free$ ,  $5 \times 1 - free$ ,  $5 \times 2 - free$ ,  $11 \times 1 - free$ ,  $11 \times 6 - free$ ,  $21 \times 1 - free$ ,  $21 \times 11 - free$ ,  $101 \times 1 - free$ ,  $101 \times 6 - free$ ,  $201 \times 1 - free$  and  $201 \times 6 - free$  (Fig. 2b).

Comparing with the results in Sec. 3.2, it can be observed how the presence of fully bonded fibers across the thickness has a restraining effect on the ERR, that counteracts the magnification due to an increasing number of fully bonded fibers in the horizontal direction. The interplay is further modulated by the fiber content. For mode I, at low fiber content the contact zone onset starts at  $60^\circ$ , while it is delayed to debonds of  $70^\circ$  for  $V_f = 60\%$ . Convergence can also be observed: at 30% fiber volume fraction, the  $5 \times 2 - free$  model can already be considered representative of further spaced debonds in arbitrarily thick UD; at 60%, the  $21 \times 2 - free$  model can be considered representative of laminates with 3 layers of fibers and the  $11 \times 6 - free$  of thicker UD. A less definite situation characterizes instead mode II. An increase in the value of ERR can be observed for any additional fully bonded fiber present in the horizontal direction, while

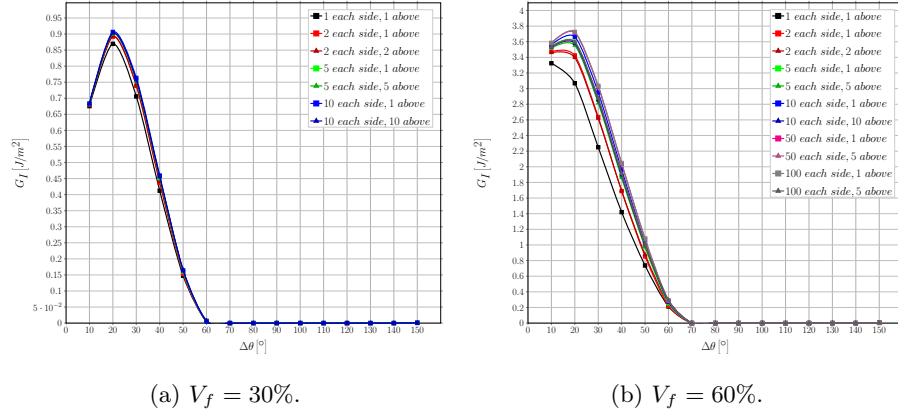


Figure 12: Effect of the interaction between debonds appearing at regular intervals on Mode I ERR in a single-ply laminate with multiple layers of fibers at different levels of fiber volume fraction  $V_f$ .

a change due to the number of fibers across the thickness can be observed only between 1 and  $> 1$ .

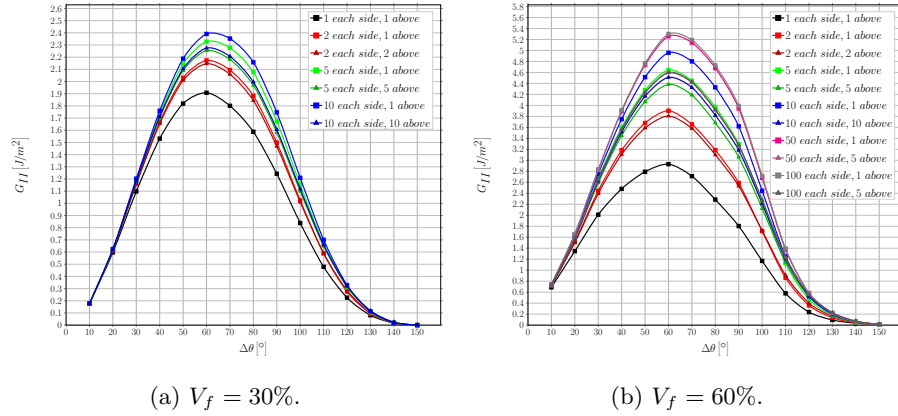


Figure 13: Effect of the interaction between debonds appearing at regular intervals on Mode II ERR in a single-ply laminate with multiple layers of fibers at different levels of fiber volume fraction  $V_f$ .

It seems to be apparent that the interaction of debonds is strongly affected by the presence of fully bonded fiber between them: the further apart debonds are, the higher the Energy Release Rate. The presence of layers of fully bonded



fibers has instead a suppressing effect and there exists a limit value of layers after which no sizeable change is measurable. Such limit value seems however to depend on the spacing of debonds in the horizontal direction. Increasing the fiber content leads in general to more drastic changes in the ERR.

### 3.5. Comparison with the single fiber model with equivalent boundary conditions

The comparison of the single fiber models with the corresponding multi-fiber models (Figs. 14, 15, 14 and 15) show that the former provide in general the lowest estimation of the ERR and correspond to the most damaged state of the laminate, i.e. the state in which the greatest number of debonds is present. The  $1 \times 1 - free$  or simply free model (Figs. 14 and 15), which represents a UD with a single layer of partially debonded fibers, agrees with the results of Sec. 3.2 and constitutes the extreme case for UD with a single layer of fibers, i.e. the case in which all the fibers are partially debonded.

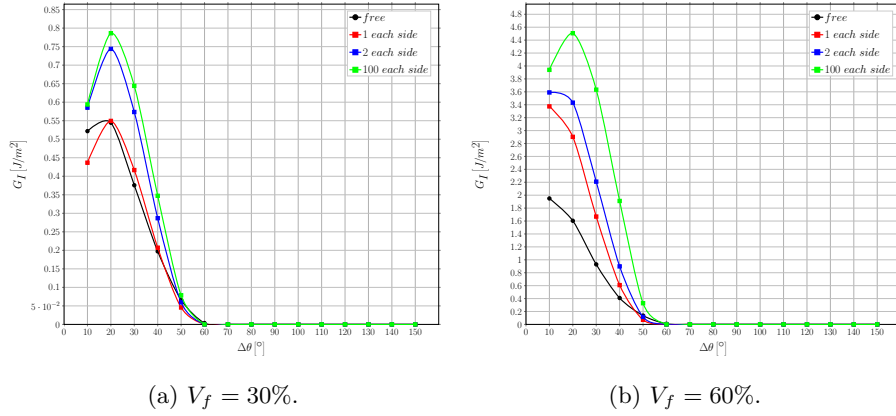


Figure 14: Comparison of Mode I ERR between the single fiber model with free upper boundary and the multiple fibers model with fibers only on the side at different levels of fiber volume fraction  $V_f$ .

The  $1 \times 1 - coupling$  or coupling model (Figs. 16 and 17) underestimates consistently the ERR in mode I and mode II when compared with  $n \times k - free$  models, as it represents an infinitely thick UD with all the fibers partially debonded. When compared with the  $1 \times k - free$  model, it shows interestingly

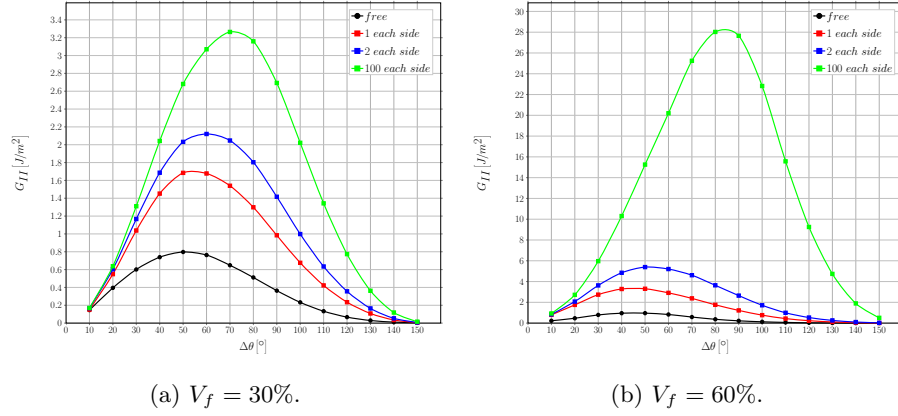


Figure 15: Comparison of Mode II ERR between the single fiber model with free upper boundary and the multiple fibers model with fibers only on the side at different levels of fiber volume fraction  $V_f$ .

a good agreement, especially in mode I (Fig. 16a).

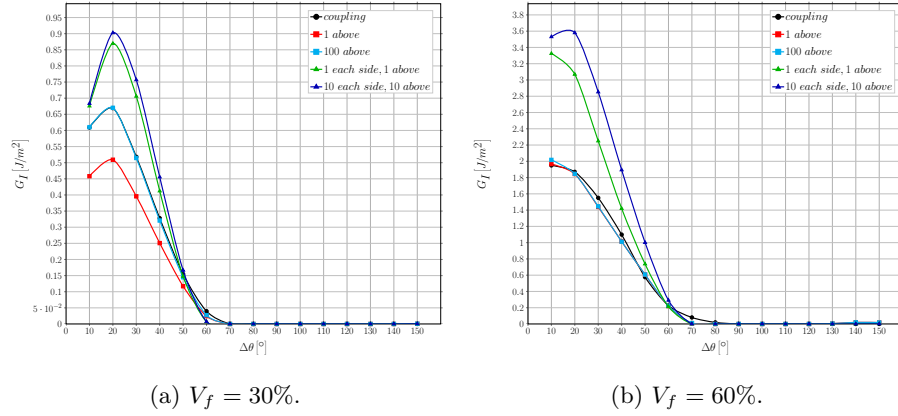


Figure 16: Comparison of Mode I ERR between the single fiber model with coupling conditions along the upper boundary and the multiple fibers model with fibers above and both above and on the side at different levels of fiber volume fraction  $V_f$ .

295 In mode II, it shows a sizeable difference in the range  $50^\circ - 90^\circ$ , while its results coincide with those of the  $1 \times k$ -free model for other values of  $\Delta\theta$ . These observations point to the evidence that debonds' interaction has a significant effect in the loading direction and not in the transverse one. The lower estimates

of  $G_{II}$  in the range  $50^\circ - 90^\circ$  are due to the presence of a debond of the same  
 size in the fiber just above the central one (modeled by the coupling boundary  
 condition), which leaves the strip of matrix between the two fibers free to deform  
 away from both fibers due to Poisson's effect and thus favors mode I and reduces  
 mode II. This translates in the lower estimates in Fig. 17 and to the delay in  
 the appearance of the contact zone, particularly evident in Fig. 16b.

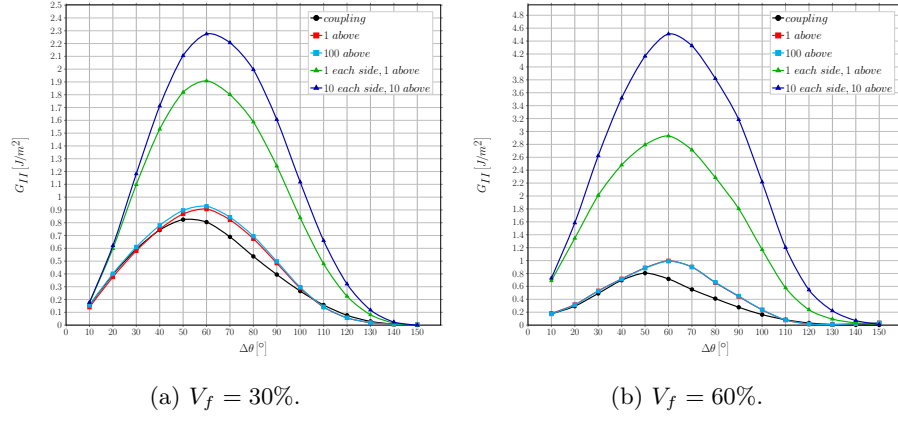


Figure 17: Comparison of Mode II ERR between the single fiber model with coupling conditions along the upper boundary and the multiple fibers model with fibers above and both above and on the side at different levels of fiber volume fraction  $V_f$ .

## 4. Conclusions & Outlook

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