

Effect of uniform distributions of bonded and debonded fibers on the growth of the fiber/matrix interface crack in thin UD laminates with different fiber contents under transverse loading

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Abstract

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1. Introduction

1. We start with a few lines devoted to the spread tow technology and thin plies: what they are, what can be done, what are the possible applications.
2. By quoting the relevant references, we report on the observation that one of the main beneficial mechanisms in thin ply is the retardation of transverse crack propagation. We then enlarge by reporting the microscopical observations by Saito, in which debonds were also observed. We observe that available microscopic observations are just a few and mainly in 2D.
3. Propagation of transverse cracks has been widely investigated both analytically and numerically
4. Initiation at the level of fiber/matrix interface is instead a less researched subject.

5. cohesive elements are a possible choice, but have some drawbacks, which
15 makes a LEFM approach valuable
6. With regard to LEFM studies of laminates under transverse loading, models can be found in the literature about: the single fiber in infinite matrix under different mode of loading, the effect of adjacent fibers on a fiber in infinite matrix under different mode of loading, the single fiber in an
20 equivalent composite in transverse tension, the effect of adjacent fibers on a fiber in an equivalent composite in transverse tension.
7. For initiation of transverse cracking at the fiber/matrix interface in UD laminates under transverse tension, there is thus a gap regarding: the effect of fiber volume fraction; the interaction of debonded and bonded
25 fibers in micro-structured assemblies, i.e. no homogenization. This article addresses these two points.
8. We conclude the introduction with a summary of the article's structure.

2. RVE models & FE discretization

2.1. Introduction & Nomenclature

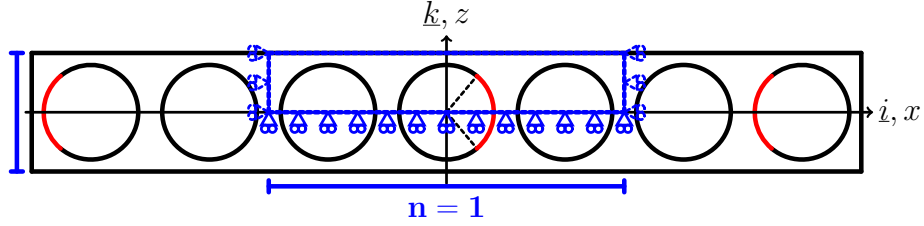
30 In this paper, we analyze debond development in unidirectional (UD) composites subjected to in-plane transverse tensile loading. The interaction between debonds in UD composites is studied developing models of different Repeating Unit Cells (RUC) of laminates where only the central fiber in the cell has a damage in the form of a fiber/matrix interface crack (debond). The composite
35 RUC may be repeating in the transverse direction only (representing an ultra-thin composite) or repeating also in the composite thickness direction, representing an infinite composite in a limiting case. Thus, the conditions at the UD composite's upper and lower boundaries are one of the parameters for the investigation. The used RUCs allow for the consideration of the composite
40 with debonds as a sequence of damaged and undamaged "rows", each "row" with only one fiber in the thickness direction. Since all of these RUCs feature regular microstructures with fibers placed according to a square-packing tiling,

they are Representative Volume Elements (RVE) of composites with a certain distribution of debonds. Introducing in-plane coordinates x and y , where x is in the transverse direction of the UD composite under consideration, the strain in the y -direction due to a load in the x -direction is small, due to the very small minor Poissons ratio of the UD composite. Additionally, debonds are considered to be significantly longer in the fiber direction than in the arc direction. Therefore, we use 2D models under the assumption of plane strain, defined in the $x - z$ section of the composite. Thus, the analysis presented applies to long debonds, with a focus on understanding the mechanisms of growth along its arc direction. The composites are subjected to transverse tensile strain, applied as a constant displacement in the x -direction along the vertical boundary of the RUC as shown in Figure 1 to 4. As the models are differentiated by the number of layers of fibers and by the spacing between debonds along the vertical and horizontal directions, the corresponding RUCs can be distinguished from each other based on the number n of fibers in the horizontal direction and k in the vertical direction. Furthermore, the horizontal surfaces can be either free or vertical displacement coupling can be applied. We thus introduce the common notation $n \times k - free$ and $n \times k - coupling$ to denote a RUC with $n \times k$ fibers and, respectively, a free upper surface or kinematic coupling applied to it. The specific combinations of particular choices of n , k , and boundary conditions are detailed in Section 2.2, together with the corresponding models of damaged composite they are representing.

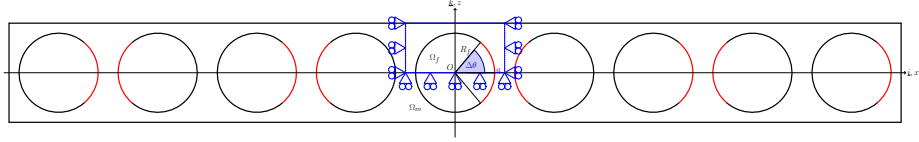
2.2. Models of Representative Volume Element (RVE)

The first two models feature, as shown in Fig. 1, an ultra-thin UD laminate with only one “row” of fibers across its thickness, $k = 1$. This is quite an extreme model from the microstructural point of view; however, it allows to focus the analysis on the interaction between debonded fibers placed along the x -direction. Furthermore, as the horizontal surfaces are considered free, the interaction is stronger in this case than in any other, making the predictions of this model rather conservative. In retrospective, if only 20 years ago such a

model would have been considered too abstracted from the physical reality, the recent advancements in the spread tow technology make this approach appealing
75 also as a limiting case for practical considerations.



(a) Single “row” of fibers with a debond appearing every m fibers.

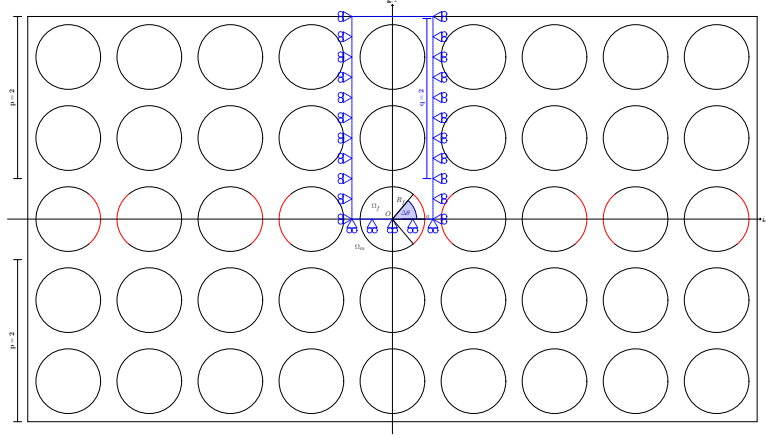


(b) Single “row” of fibers with debonds appearing on each fiber.

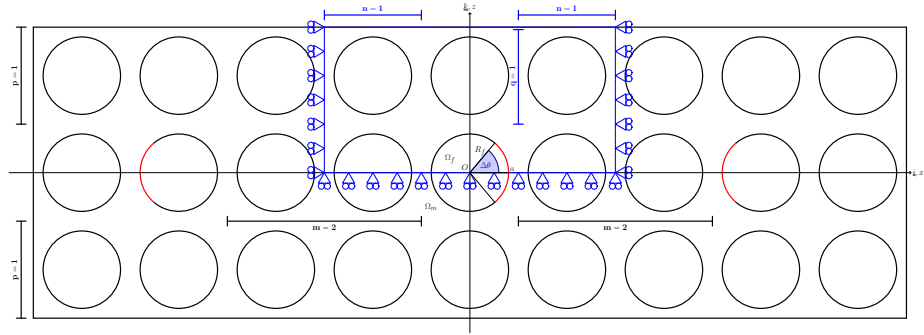
Figure 1: Models of ultra-thin UD composites with a single “row” of fibers and debonds repeating at different distances. The corresponding repeating element (RUC) is highlighted in blue, while debonds are represented in red.

In the first sub-model, Fig. 1a, every n^{th} fiber in the composite is partially debonded on alternating sides of the fiber. The symmetries of the model allow the use of the upper part of the RUC. It is highlighted by blue lines in Fig. 1 to 3. Following the notation introduced in Section 2.1, we will refer to this
80 model as $n \times 1 - free$. In the second sub-model $n = 1$, Fig. 1b, and a debond appears on each fiber on alternating sides and the corresponding RUC contains only one fiber. We will refer to this model as $1 \times 1 - free$.

The second set of models in Fig. 2 and Fig. 3 considers laminates with multiple “rows” of fibers across the thickness: a finite number of rows in the
85 first two sub-models in Fig. 2; an infinite number in the model of Fig. 3. In Fig. 2a, the RUC contains $n = 1$ fiber in the x-direction, k fibers across the thickness and the central fiber is debonded. This model will be referred to in the following as $1 \times k - free$. Thinking in terms of “rows”, in this model we



(a) Multiple “rows” of fibers with debonds appearing on each fiber belonging to the central “row”.



(b) Mutiple “rows” of fibers with a debond appearing every m fibers within the central “row”.

Figure 2: Models of UD composites with different “rows” of fibers and debonds repeating at different distances. The corresponding repeating element (RUC) is highlighted in blue, while debonds are represented in red.

have a central “row” where each fiber is debonded. This “rows” is surrounded
 90 from each side by $(k-1)/2$ “rows” with perfectly bonded fibers. In the sub-model
 in Fig. 2b, each n^{th} fiber in the central “row” is debonded and this “row” is
 surrounded by $(k-1)/2$ “rows” of undamaged fibers from each side. We will refer
 to this model as $n \times k - free$ (because the horizontal boundary of the RUC is
 free of any constraint).

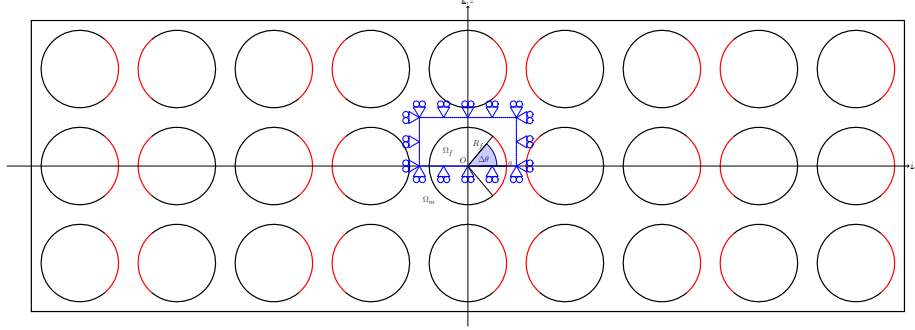


Figure 3: Model of UD composites with an infinite number of “rows” of fibers and debonds appearing on each fiber. The corresponding repeating element (RUC) is highlighted in blue, while debonds are represented in red.

95 Finally, the model in Fig. 3 considers an UD composite with an infinite number of “rows”; all of them with partially debonded fibers. As all fibers have debonds, the corresponding RUC is made of a single partially debonded fiber with kinematic coupling conditions applied to the upper boundary to assure periodicity. This model is referred to as 1×1 – *coupling*.

100 2.3. Finite Element (FE) discretization

Each RUC is discretized using the Finite Element Method (FEM) within the Abaqus environment, a commercial FEM package [1]. The length l and height h of the model are determined by number of fibers n in the horizontal direction and k across the thickness (see 2.2) according to Eq. 1:

$$l = 2nL \quad h = 2kL; \quad (1)$$

105 where the reference length L , see Fig. 4a, is defined as a function of the fiber volume fraction V_f and the fibers’ radius according to

$$L = \frac{R_f}{2} \sqrt{\frac{\pi}{V_f}}. \quad (2)$$

The fibers’ radius R_f is assumed to be the same for each fiber present in the model and equal to $1 \mu m$. The latter value is not physical and it has been

chosen for simplicity. It is worth to note at this point that, in a linear elastic
 110 solution as the one presented here, the ERR is proportional to the geometrical
 dimensions and recalculation of the ERR for fibers of any size thus requires
 a simple multiplication. Furthermore, notice that the relationships in Eqs. 1
 and 2 ensure that the local and global V_f are everywhere equal.

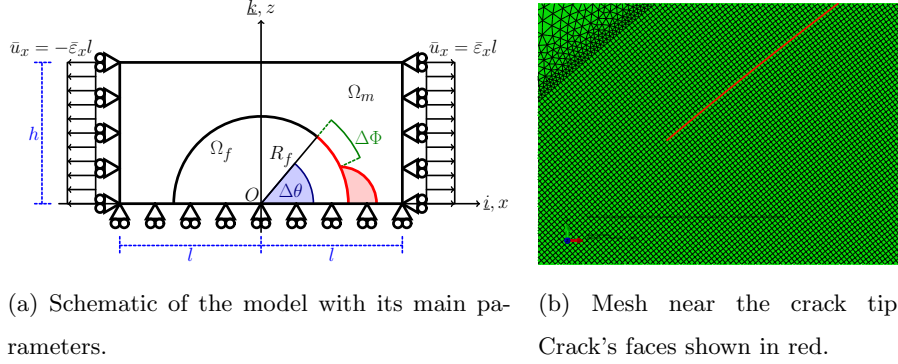


Figure 4: Details and main parameters of the Finite Element model.

The debond is placed symmetrically with respect to the x axis (in red in 4a)
 115 and has an angular size of $\Delta\theta$ (the full debond's size is thus $2\Delta\theta$). For large
 debond's sizes ($\geq 60^\circ - 80^\circ$), a region of variable size $\Delta\Phi$ appears at the crack
 tip in which the crack's faces are in contact and slide on each other. Due to
 its appearance, frictionless contact is considered between the two crack's faces
 to allow free sliding and avoid interpenetration. Symmetry with respect to
 120 the x axis is applied on the lower boundary and kinematic coupling on the x -
 displacement along the left and right sides. The upper boundary is in general
 free, except for the model $1 \times 1 - coupling$ (Fig. 3) which requires kinematic
 coupling of vertical displacements also on the upper side. Constant transverse
 strain $\bar{\epsilon}$ equal to 1% is applied to the right and left sides by means of an imposed
 125 x -displacement of, respectively, $\pm\bar{\epsilon}l$.

The model is meshed using second order, 2D, plane strain triangular (CPE6)
 and rectangular (CPE8) elements. A regular mesh of quadrilateral elements
 with an almost unitary aspect ratio is required at the crack tip, as shown in

Table 1: Summary of the mechanical properties of fiber and matrix.

Material	E [GPa]	G [GPa]	ν [-]
Glass fiber	70.0	29.2	0.2
Epoxy	3.5	1.25	0.4

Fig. 4b. The angular size δ of an element in the crack tip region is always equal to 0.05° . The Mode I, Mode II and total Energy Release Rates (ERRs) (respectively referred to as G_I , G_{II} and G_{TOT}) represent the main output of the FEM analysis; they are evaluated using the VCCT technique [2] implemented in a custom Python routine and, for the total ERR, the J-integral [3] by application of the Abaqus built-in functionality. A glass fiber-epoxy system is considered in every model, and it is assumed that their response lies always in the linear elastic domain. The properties used are listed in Table 1.

2.4. Validation of the model

The model is validated in Fig. 5 against the results reported in [4], obtained with the Boundary Element Method (BEM) for a single fiber with a symmetric debond placed in an infinite matrix. This situation is modeled using the *free* RVE with $V_f = 0.0079\%$, which corresponds to a RUC's length and height of ~ 100 .

To allow for a comparison, the results are normalized following [4] with respect to a reference Energy Release Rate G_0 defined as

$$G_0 = \frac{1 + k_m}{8\mu_m} \sigma_0^2 \pi R_f \quad (3)$$

where μ is the shear modulus, k is the Kolosov's constant defined as $3 - 4\nu$ for plane strain conditions, R_f is the fiber radius and the index m refers to the properties of the matrix. σ_0 is the stress at the boundary, computed as the average of the stress extracted at each boundary node along the right side (arithmetic average as nodes are equispaced by design along both the left and right sides). The agreement is good: the difference between the BEM solution,

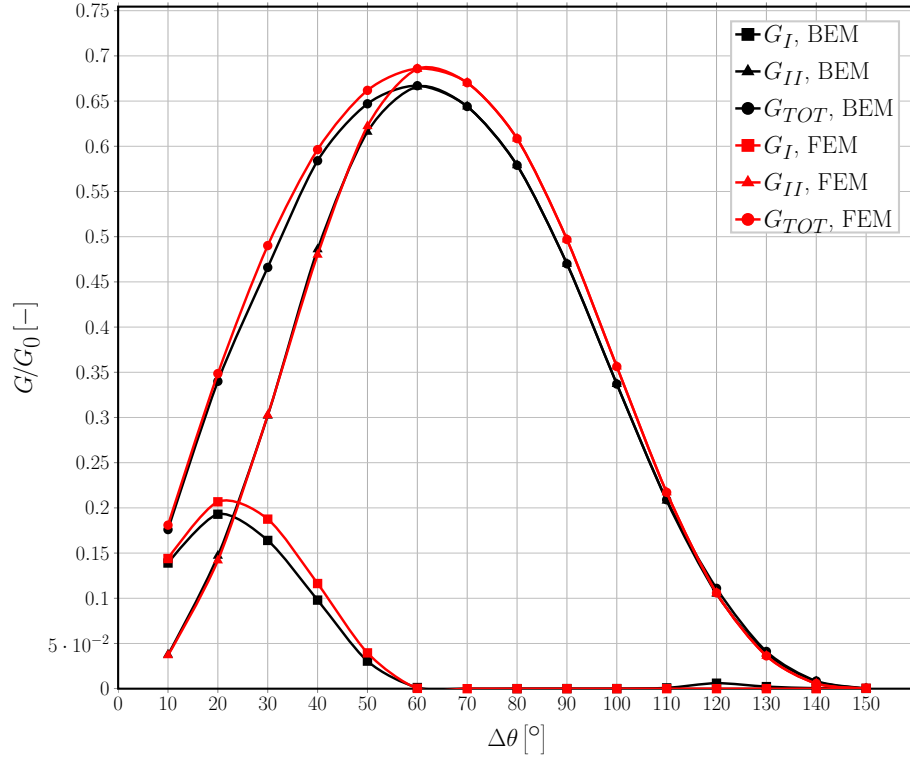


Figure 5: Validation of the single fiber model for the infinite matrix case with respect to the BEM solution in [4].

which is considered more accurate, and the FEM solution does not exceed 5%. The ERRs' maxima are in the same positions and the size of the contact zone is the same. Nevertheless, an analysis of phenomena leading to less than 5% differences in ERR would not be reliable and, therefore, it is not recommended.

155 3. Results & Discussion

3.1. Effect of Fiber Volume Fraction

As shown in Figs. 6 and 7, respectively for Mode I and Mode II, the fiber content has a drastic effect on the Energy Release Rate at the tip of the fibre/matrix interface crack. The effect of four levels of fiber volume fraction are compared, 30%, 50%, 60% and 65%, on two microstructural models: a 11×11 – free

(every 11th fiber in the central fiber “row” is partially debonded and, on the top of this “row”, we have 5 undamaged fiber “rows”), Figs. 6a and 7a, and a 21×21 – *free* (every 21th fiber in the central fiber “row” is partially debonded and, on the top of this “row”, we have 10 undamaged fiber “rows”), Figs. 6b and 7b.

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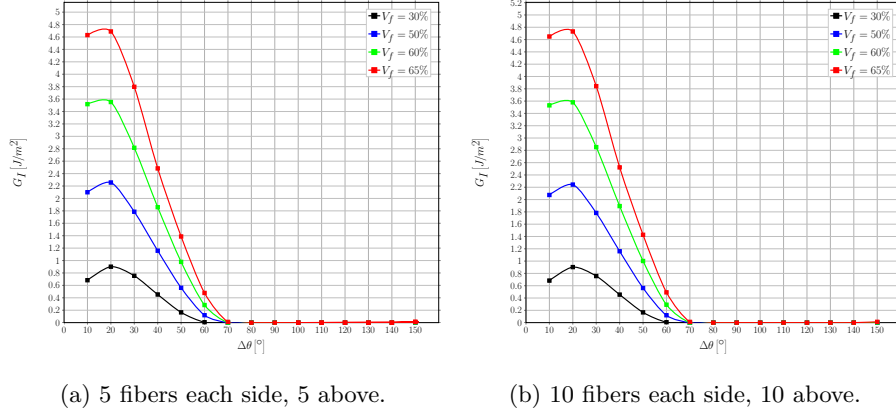


Figure 6: A view of the effect of fiber volume fraction on Mode I ERR in two exemplificative models.

Comparing Fig. 6a with 6b, and Fig. 7a with 7b, we can observe that the ERRs’ values are very similar for RUCs with 11 – 11 and 21 – 21 fibers, though they are slightly higher for the larger RUC where the next debonded fiber and the free surface are further away from the debonded fiber. From these results we conclude that both RUCs are large enough to represent a single debonded fiber in an infinite array of bonded fibers. Obviously, there exists a specific effect of the fiber content. For Mode I, Fig. 6, the maximum value of the ERR increases by ~ 5.2 times when V_f changes from 30% to 65%. The debond’s angular size for which the peak value occurs remains unchanged at 20° , but for $V_f = 60\%$ and 65% the Mode I ERR at 10° and at 20° are rather similar, approximately creating a plateau. Furthermore, increasing the fiber volume fraction delays the onset of the contact zone, which corresponds in Fig. 6 to the first value of $\Delta\theta$ for which G_I is equal to zero. For $V_f = 30\%$, the contact zone first appears for a debond of 60° , similarly to what happens in the single fiber in infinite matrix

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180 model (Fig. 5). For higher fiber contents, the contact zone's onset is delayed to a debond's size approximately equal to 70° .

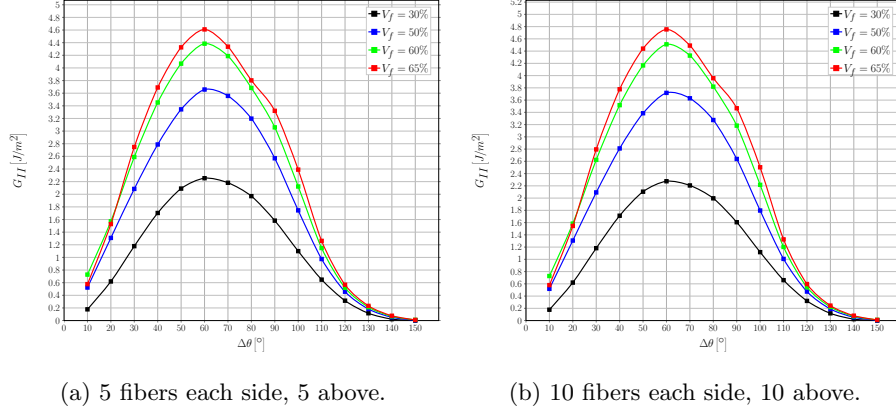


Figure 7: A view of the effect of fiber volume fraction on Mode II ERR in two exemplificative models.

For Mode II, Fig. 6, the maximum value of the ERR is increased by ~ 2.1 times when V_f changes from 30% to 65% in both models. The effect is thus similar to Mode I, but with a significantly lower magnitude. As for Mode I, the debond's size for which the peak value occurs remains unchanged, at 60° for Mode II. The shape of the curve remains instead unchanged, thus no effect on the stability of Mode II with respect to debond's size can be observed. It is worthwhile to notice, however, that the ratio of Mode II to Mode I peak values is $\frac{\max(G_{II})}{\max(G_I)} \sim \frac{2.2}{0.9} \sim 2.4$ for $V_f = 30\%$, while it is $\sim \frac{4.7}{4.7} \sim 1$ for $V_f = 65\%$ in both models. Given that the peaks occur at different debond's sizes, for which the value of the other ERR is very small or even close to zero, this means that the increase in fiber content creates a long range of very close values of total ERR, and thus has a global destabilizing effect on the debond's growth.

The general increasing trends observed in Figs. 6 and 7 are related to the fact that, given that the global and local V_f are everywhere identical in the models presented, an increase in fiber content corresponds to a decrease in the average distance between fibers. Thus, the relaxation of the stress and strain fields in the matrix domain occurs over smaller lengths causing higher values at the crack tip.

The difference in relative magnification between Mode I and Mode II and the
 200 delay in the contact zone's onset are instead due to the interplay between two
 different mechanisms, both caused by the ordered microstructural arrangement
 of the model. In the models considered, a fully bonded fiber is always placed
 along the horizontal direction, aligned with the partially debonded fiber and
 exactly in front of the debond. By increasing V_f , the former moves closer to the
 205 latter and this causes a magnification of the x-strain at the crack tip. For small
 debonds ($\leq 20^\circ - 30^\circ$), the crack tip is approximately normal to the x-direction
 and thus an increase in ε_x causes an increase in G_I . On the other hand, for
 large debonds ($\geq 70^\circ - 80^\circ$) the crack growth is almost aligned with the x-axis,
 thus a magnification in the x-strain translates into an increase of Mode II ERR.
 210 However, this increasing effect on G_{II} is counteracted by the presence of a fully
 bonded fiber along the vertical direction, aligned with the partially debonded
 one. As fibers are more rigid than the surrounding matrix, the presence of the
 former will restrain horizontal displacements, thus hampering strong increases in
 G_{II} for large debonds. Furthermore, due to the mismatch in the Poisson's ratios,
 215 the fully bonded fiber placed above generates an upward-directed component of
 the vertical displacement field in the matrix, which tends to open the debond
 and causes the delay in the contact zone's onset. The interplay between these
 mechanisms is governed by the average inter-fiber distance and, in turn, by the
 fiber volume fraction.

220 3.2. Interaction between debonds in UD laminates with a single layer of fibers

The interaction of debonds appearing at regular intervals in UD composites
 with a single layer of fibers is studied for Mode I (Fig. 8) and Mode II (Fig. 9)
 and fiber content equal to 30% (Figs. 8a and 9a) and 60% (Figs. 8b and 9b).
 The models treated are $3 \times 1 - free$, $5 \times 1 - free$, $7 \times 1 - free$, $11 \times 1 - free$,
 225 $21 \times 1 - free$, $101 \times 1 - free$ and $201 \times 1 - free$, corresponding respectively to
 a debond every 3^{rd} , 5^{th} , 7^{th} , 11^{th} , 21^{st} , 101^{st} and 201^{st} fiber (Fig. 1a). Given
 that the upper surface of the UD is left free, the interaction is stronger than in
 any other case and the results of this section are thus the most conservative in

terms of debond's growth. From both 8 and 9, it can be seen that the presence
of a debond decreases the strain magnification effect discussed in Sec. 3.1 and
thus reduces the value of the ERR.

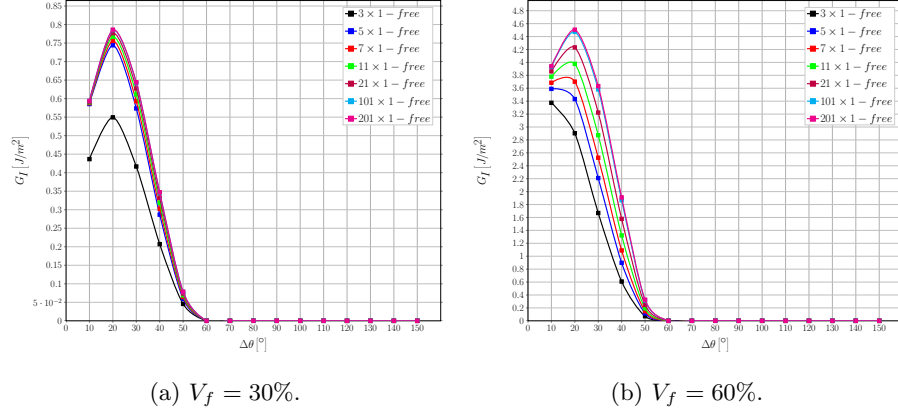


Figure 8: Effect of the interaction between debonds appearing at regular intervals on Mode I ERR in an UD with a single layer of fibers at different levels of fiber volume fraction V_f .

For Mode I, the presence of a free surface, and inversely the absence of
a fully bonded fiber along the vertical direction, implies the absence of the
counteracting upward-oriented vertical component of the displacement field due
to the mismatch in Poisson's ratios. This in turn translates into the constancy
of the value of $\Delta\theta$ corresponding to contact zone's onset, always equal to 60° .
For $V_f = 30\%$, Mode I is reduced going from a debond placed every 5^{th} fiber to
every 3^{th} fiber. Larger spacing does not seem to have a sizable effect. Similarly,
at 60% no difference can be seen between the case of a debond placed every 101^{th}
and every 201^{th} fiber. These observations suggest the existence of characteristic
distance dependent on the fiber volume fraction which governs the interaction
between debonds.

Without constraint on the upper surface, the strain magnification effect cre-
ates larger displacements in the x-direction, which increase Mode II for larger
debonds. When debonds are far apart, the series of rigid elements (constituted
by fully bonded fibers and their surrounding matrix) creates higher x-strains,
which in turn generates higher tangential displacements at the crack tip for

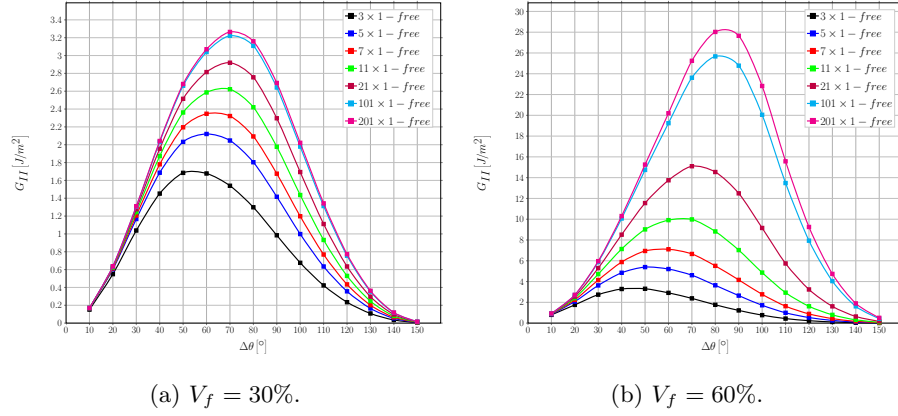


Figure 9: Effect of the interaction between debonds appearing at regular intervals on Mode II ERR in a single-ply laminate with a single layer of fibers at different levels of fiber volume fraction V_f .

larger debonds. Conversely, when debonds are closer, the strain concentration is reduced and the tangential component at the crack tip decreases for large $\Delta\theta$. This is the mechanism behind the change in the value of $\Delta\theta$ for which the peak of G_{II} occurs: from 70° to 50° at 30%, and from 80° to 40° at 60% going from the higher to the smaller spacing of debonds. Differently from Mode I, the presence of a characteristic distance is harder to establish. For $V_f = 30\%$ (Fig. 9a), it seems reasonable to establish it at around 100 fully bonded fibers between each debond. For $V_f = 60\%$ (Fig. 9b), the difference between models $101 \times 1 - free$ and $201 \times 1 - free$ is still sizable, thus preventing the establishment of such characteristic distance. It is possible to observe, however, that the change between $101 \times 1 - free$ and $201 \times 1 - free$ is significantly smaller than between $21 \times 1 - free$ and $101 \times 1 - free$ ($2 \left[\frac{J}{m^2} \right]$ vs $11 \left[\frac{J}{m^2} \right]$), thus suggesting the existence of the characteristic distance outside the range studied.

3.3. Influence of layers of fully bonded fibers on debond's growth in a line of debonded fibers located at mid-thickness

The effect of the presence of layers of fully bonded fibers on debond's growth in a line of partially debonded fibers located at mid-thickness in UD composites

is studied for Mode I (Fig. 10) and Mode II (Fig. 11) and fiber content equal to 30% (Figs. 10a and 11a) and 60% (Figs. 10b and 11b). The models treated are $1 \times 2 - free$, $1 \times 3 - free$, $1 \times 4 - free$, $1 \times 6 - free$, $1 \times 11 - free$, $1 \times 51 - free$ and $1 \times 101 - free$, corresponding to a UD composite with respectively 3, 5, 7, 11, 21, 101 and 201 layers of fibers (Fig. 2a).

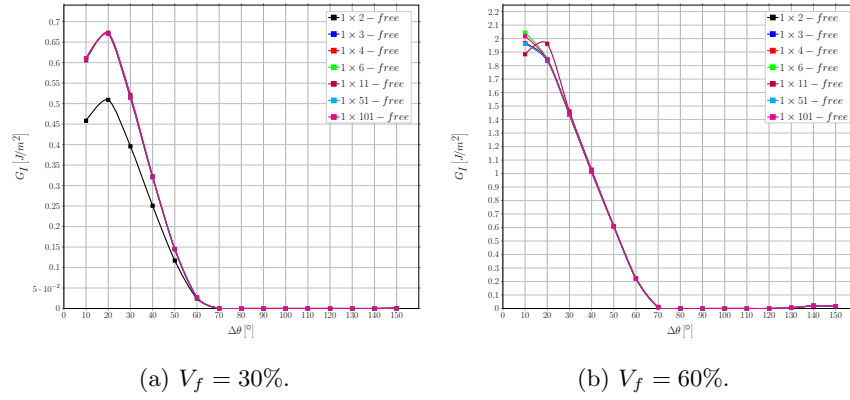


Figure 10: Influence of layers of fully bonded fibers on debond's growth in Mode I ERR in a centrally located line of debonded fibers at different levels of fiber volume fraction V_f .

The results shown strengthen the considerations made in Sec. 3.1. It can in fact be seen in Fig. 10 that the presence of fully bonded fibers across the thickness delays the onset of the contact zone to a debond of 70° in size, due to the introduction of an additional upward-directed component of the vertical displacement which translates into an opening displacement at the debond's tip.

The results of both Mode I and Mode II show how the introduction of an increasing number of fully bonded fibers doesn't change the ERR calculated at the crack tip. The effect of the V_f can be observed at low fiber content (Figs. 10a and 11a), while for high fiber content the smaller model with only fiber above the partially debonded one is already representative.

3.4. Interaction between debonds in UD laminates with multiple layers of fibers

The interaction of debonds appearing at regular intervals in UD composites with multiple layers of fibers is investigated for Mode I (Fig. ??) and Mode II

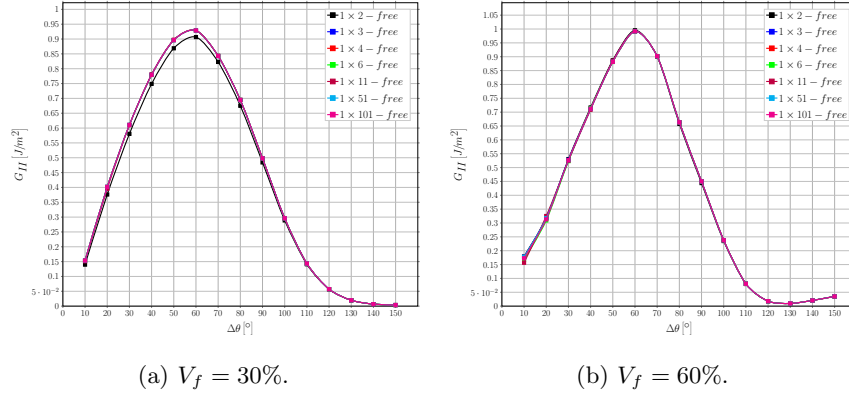


Figure 11: Influence of layers of fully bonded fibers on debond's growth in Mode II ERR in a centrally located line of debonded fibers at different levels of fiber volume fraction V_f .

(Fig. 13) and fiber content equal to 30% (Figs. 12a and 13a) and 60% (Figs. 12b and 13b). The models treated are $3 \times 2 - free$, $5 \times 1 - free$, $5 \times 2 - free$, $11 \times 1 - free$, $11 \times 6 - free$, $21 \times 1 - free$, $21 \times 11 - free$, $101 \times 1 - free$, $101 \times 6 - free$, $201 \times 1 - free$ and $201 \times 6 - free$ (Fig. 2b).

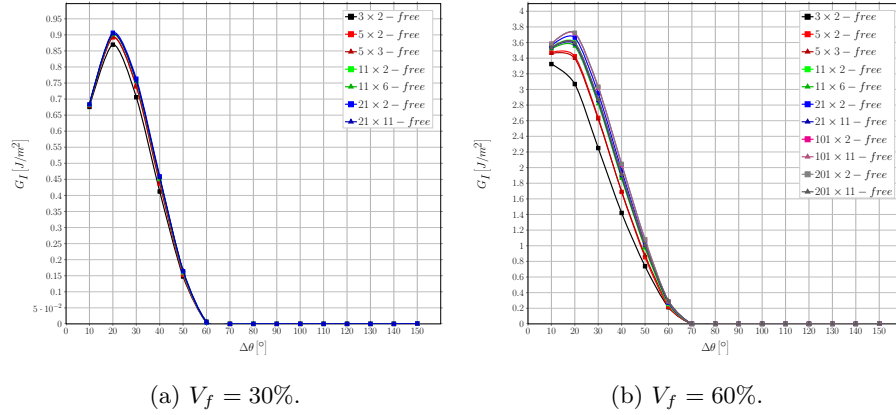


Figure 12: Effect of the interaction between debonds appearing at regular intervals on Mode I ERR in a single-ply laminate with multiple layers of fibers at different levels of fiber volume fraction V_f .

Comparing with the results in Sec. 3.2, it can be observed how the presence of fully bonded fibers across the thickness has a restraining effect on the ERR,

that counteracts the magnification due to an increasing number of fully bonded
 290 fibers in the horizontal direction. The interplay is further modulated by the
 fiber content. For Mode I, at low fiber content the contact zone onset starts at
 60°, while it is delayed to debonds of 70° for $V_f = 60\%$. Convergence can also
 be observed: at 30% fiber volume fraction, the $5 \times 2 - free$ model can already be
 considered representative of further spaced debonds in arbitrarily thick UD; at
 295 60%, the $21 \times 2 - free$ model can be considered representative of laminates with
 3 layers of fibers and the $11 \times 6 - free$ of thicker UD. A less definite situation
 characterizes instead Mode II. An increase in the value of ERR can be observed
 for any additional fully bonded fiber present in the horizontal direction, while
 a change due to the number of fibers across the thickness can be observed only
 300 between 1 and > 1 .

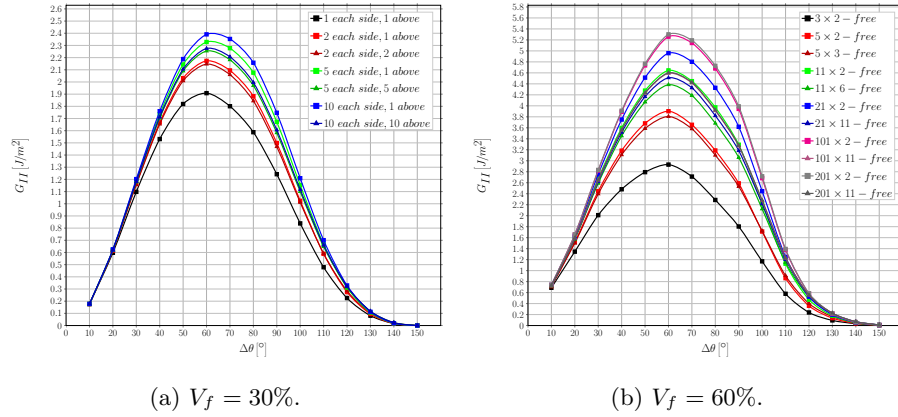


Figure 13: Effect of the interaction between debonds appearing at regular intervals on Mode II ERR in a single-ply laminate with multiple layers of fibers at different levels of fiber volume fraction V_f .

It seems to be apparent that the interaction of debonds is strongly affected
 by the presence of fully bonded fiber between them: the further apart debonds
 are, the higher the Energy Release Rate. The presence of layers of fully bonded
 fibers has instead a suppressing effect and there exists a limit value of layers
 305 after which no sizeable change is measurable. Such limit value seems however
 to depend on the spacing of debonds in the horizontal direction. Increasing the

fiber content leads in general to more drastic changes in the ERR.

3.5. Comparison with the single fiber model with equivalent boundary conditions

The comparison of the single fiber models with the corresponding multi-fiber
 310 models (Figs. 14, 15, 14 and 15) show that the former provide in general the
 lowest estimation of the ERR and correspond to the most damaged state of the
 laminate, i.e. the state in which the greatest number of debonds is present. The
 $1 \times 1 - free$ or simply free model (Figs. 14 and 15), which represents a UD with
 a single layer of partially debonded fibers, agrees with the results of Sec. 3.2
 315 and constitutes the extreme case for UD with a single layer of fibers, i.e. the
 case in which all the fibers are partially debonded.

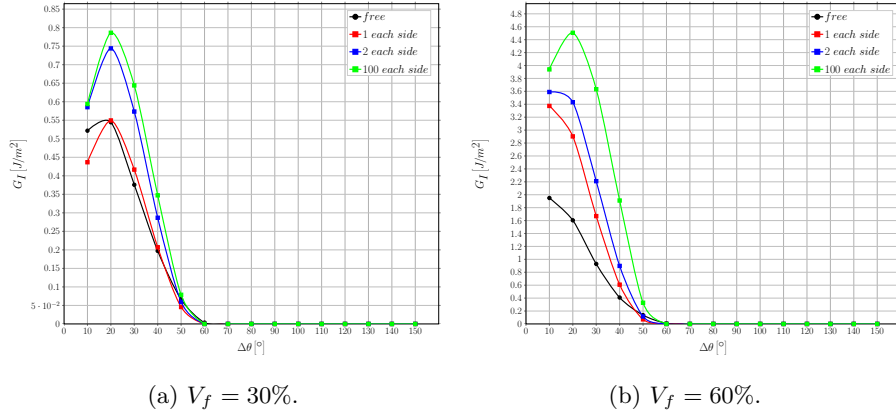


Figure 14: Comparison of Mode I ERR between the single fiber model with free upper boundary and the multiple fibers model with fibers only on the side at different levels of fiber volume fraction V_f .

The $1 \times 1 - coupling$ or coupling model (Figs. 16 and 17) underestimates
 consistently the ERR in Mode I and Mode II when compared with $n \times k -$
 $free$ models, as it represents an infinitely thick UD with all the fibers partially
 320 debonded. When compared with the $1 \times k - free$ model, it shows interestingly
 a good agreement, especially in Mode I (Fig. 16a).

In Mode II, it shows a sizeable difference in the range $50^\circ - 90^\circ$, while its
 results coincide with those of the $1 \times k - free$ model for other values of $\Delta\theta$. These

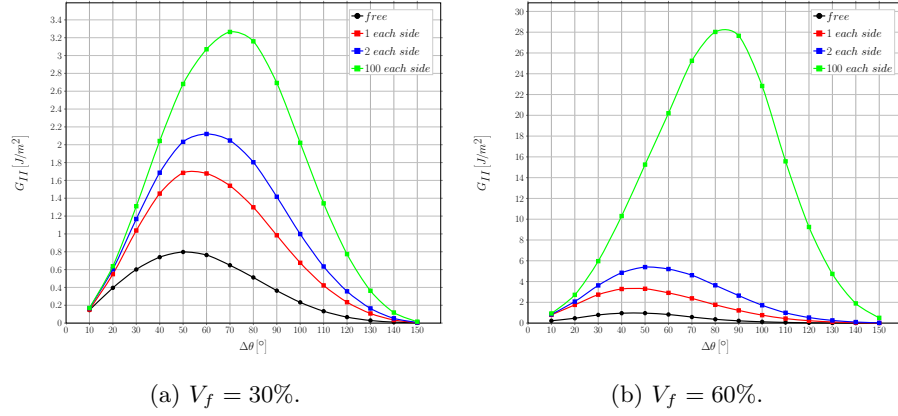


Figure 15: Comparison of Mode II ERR between the single fiber model with free upper boundary and the multiple fibers model with fibers only on the side at different levels of fiber volume fraction V_f .

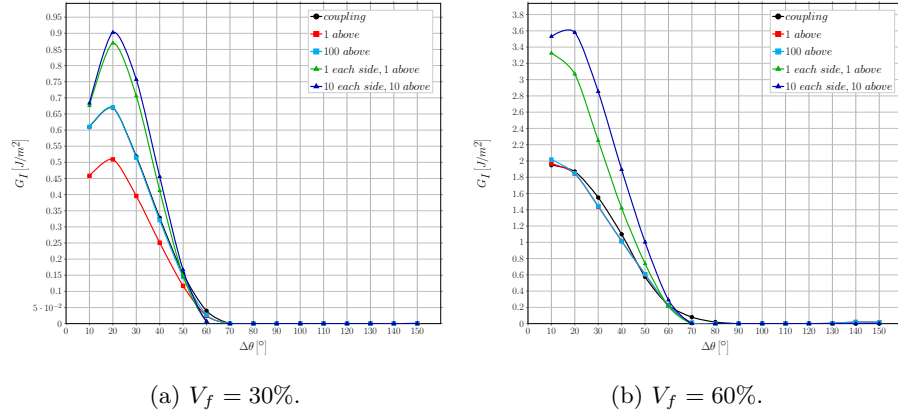


Figure 16: Comparison of Mode I ERR between the single fiber model with coupling conditions along the upper boundary and the multiple fibers model with fibers above and both above and on the side at different levels of fiber volume fraction V_f .

observations point to the evidence that debonds' interaction has a significant effect in the loading direction and not in the transverse one. The lower estimates of G_{II} in the range $50^\circ - 90^\circ$ are due to the presence of a debond of the same size in the fiber just above the central one (modeled by the coupling boundary condition), which leaves the strip of matrix between the two fibers free to deform away from both fibers due to Poisson's effect and thus favors Mode I and reduces

330 Mode II. This translates in the lower estimates in Fig. 17 and to the delay in the appearance of the contact zone, particularly evident in Fig. 16b.

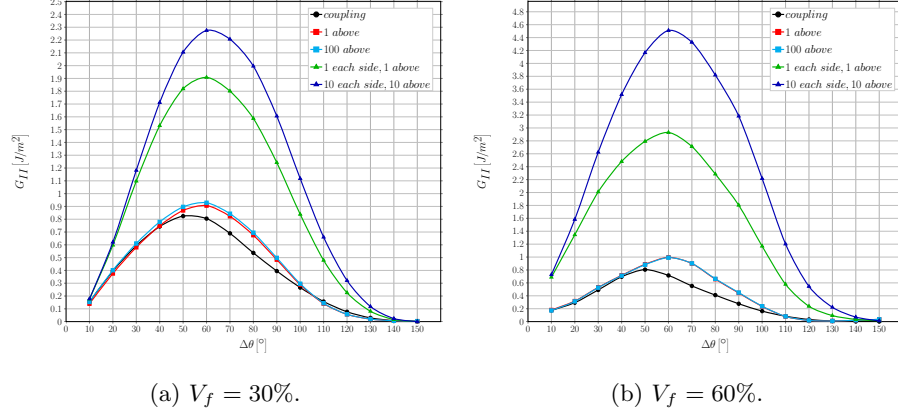


Figure 17: Comparison of Mode II ERR between the single fiber model with coupling conditions along the upper boundary and the multiple fibers model with fibers above and both above and on the side at different levels of fiber volume fraction V_f .

4. Conclusions & Outlook

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References

- [1] Simulia, Providence, RI, USA, ABAQUS/Standard User's Manual, Version 6.12 (2012).
- 340 [2] R. Krueger, Virtual crack closure technique: History, approach, and applications, Applied Mechanics Reviews 57 (2) (2004) 109. doi:10.1115/1.1595677.
 URL <https://doi.org/10.1115/1.1595677>

- [3] J. R. Rice, A path independent integral and the approximate analysis of
345 strain concentration by notches and cracks, *Journal of Applied Mechanics*
35 (2) (1968) 379. doi:10.1115/1.3601206.
URL <https://doi.org/10.1115/1.3601206>
- [4] C. Sandino, E. Correa, F. París, Numerical analysis of the influence of a
nearby fibre on the interface crack growth in composites under transverse
350 tensile load, *Engineering Fracture Mechanics* 168 (2016) 58–75. doi:10.
1016/j.engfracmech.2016.01.022.
URL <https://doi.org/10.1016/j.engfracmech.2016.01.022>