



LM5109A High Voltage 1A Peak Half Bridge Gate Driver

1 Features

- Drives Both a High-Side and Low-Side N-Channel MOSFET
- 1A peak Output Current (1.0A Sink / 1.0A Source)
- Independent TTL Compatible Inputs
- Bootstrap Supply Voltage to 108V DC
- Fast Propagation Times (30 ns Typical)
- Drives 1000 pF Load with 15ns Rise and Fall Times
- Excellent Propagation Delay Matching (2 ns Typical)
- Supply Rail Under-Voltage Lockout
- Low Power Consumption
- Pin Compatible with ISL6700
- Industry Standard SOIC-8 and Thermally Enhanced WSON-8 Package

2 Applications

- Current Fed Push-Pull Converters
- Half and Full Bridge Power Converters
- Solid State Motor Drives
- Two Switch Forward Power Converters

3 Description

The LM5109A is a cost effective, high voltage gate driver designed to drive both the high-side and the low-side N-Channel MOSFETs in a synchronous buck or a half bridge configuration. The floating high-side driver is capable of working with rail voltages up to 90V. The outputs are independently controlled with TTL compatible input thresholds. The robust level shift technology operates at high speed while consuming low power and providing clean level transitions from the control input logic to the high-side gate driver. Under-voltage lockout is provided on both the low-side and the high-side power rails. The device is available in the SOIC and the thermally enhanced WSON packages.

Device Information⁽¹⁾

PART NUMBER	PACKAGE	BODY SIZE (NOM)
LM5109A	SOIC (8)	4.90 mm × 3.91 mm
	WSON (8)	4.00 mm × 4.00 mm

(1) For all available packages, see the orderable addendum at the end of the datasheet.

Simplified Application Diagram

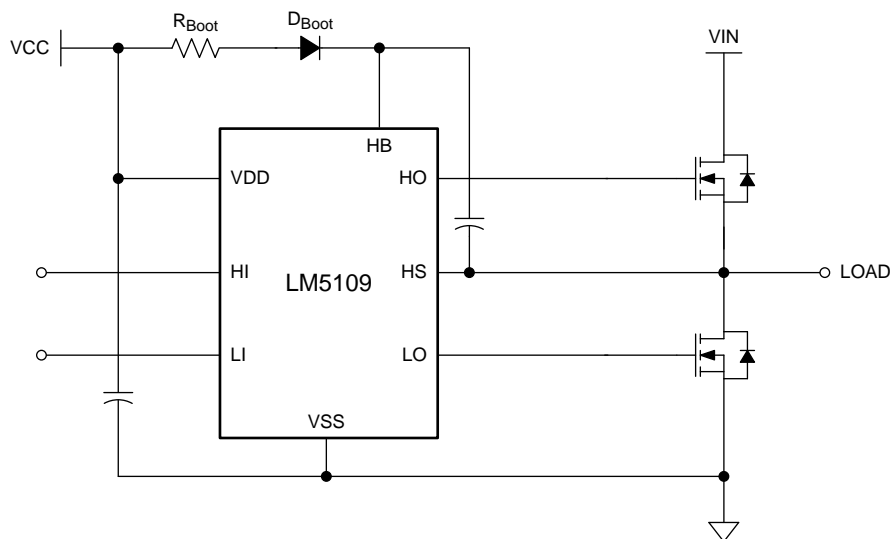


Table of Contents

1 Features	1	7.4 Device Functional Modes.....	9
2 Applications	1	8 Application and Implementation	10
3 Description	1	8.1 Application Information.....	10
4 Revision History	2	8.2 Typical Application	11
5 Pin Configuration and Functions	3	9 Power Supply Recommendations	15
6 Specifications	3	10 Layout	16
6.1 Absolute Maximum Ratings	3	10.1 Layout Guidelines	16
6.2 ESD Ratings.....	4	10.2 Layout Example	16
6.3 Recommended Operating Conditions.....	4	11 Device and Documentation Support	17
6.4 Thermal Information	4	11.1 Documentation Support	17
6.5 Electrical Characteristics.....	4	11.2 Receiving Notification of Documentation Updates	17
6.6 Switching Characteristics	5	11.3 Community Resource.....	17
6.7 Typical Performance Characteristics	6	11.4 Trademarks	17
7 Detailed Description	8	11.5 Electrostatic Discharge Caution.....	17
7.1 Overview	8	11.6 Glossary	17
7.2 Functional Block Diagram	8	12 Mechanical, Packaging, and Orderable	17
7.3 Feature Description.....	8	Information	17

4 Revision History

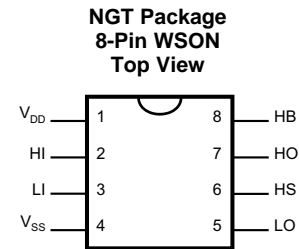
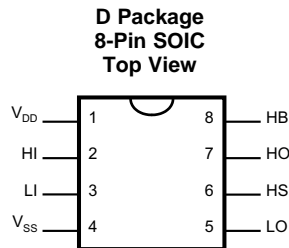
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision B (March 2016) to Revision C	Page
• Updated values in the <i>Thermal Information</i> table to align with JEDEC standards.....	4
• Added <i>Overview</i> section.	8
• Added <i>Feature Description</i> section.	8
• Added <i>Device Functional Modes</i> section.	9
• Added <i>Typical Application</i> section.	11
• Added <i>Power Supply Recommendations</i> section.	15

Changes from Revision A (March 2013) to Revision B	Page
• Added <i>Device Information</i> table, <i>ESD Ratings</i> , <i>Pin Configuration and Functions</i> section, <i>Detailed Description</i> section, <i>Application and Implementation</i> section, <i>Layout</i> section, <i>Device and Documentation Support</i> section, and <i>Mechanical, Packaging, and Orderable Information</i> section.	1

Changes from Original (March 2013) to Revision A	Page
• Changed layout of National Semiconductor Data Sheet to TI format	10

5 Pin Configuration and Functions



Pin Functions

Pin #		NAME	DESCRIPTION	APPLICATION INFORMATION
SOIC	WSON ⁽¹⁾			
1	1	V _{DD}	Positive gate drive supply	Locally decouple to V _{SS} using low ESR/ESL capacitor located as close to IC as possible.
2	2	HI	High side control input	The HI input is compatible with TTL input thresholds. Unused HI input should be tied to ground and not left open
3	3	LI	Low side control input	The LI input is compatible with TTL input thresholds. Unused LI input should be tied to ground and not left open.
4	4	V _{SS}	Ground reference	All signals are referenced to this ground.
5	5	LO	Low side gate driver output	Connect to the gate of the low-side N- MOS device.
6	6	HS	High side source connection	Connect to the negative terminal of the bootstrap capacitor and to the source of the high-side N-MOS device.
7	7	HO	High side gate driver output	Connect to the gate of the high-side N-MOS device.
8	8	HB	High side gate driver positive supply rail	Connect the positive terminal of the bootstrap capacitor to HB and the negative terminal of the bootstrap capacitor to HS. The bootstrap capacitor should be placed as close to IC as possible.

- (1) For WSON package it is recommended that the exposed pad on the bottom of the package be soldered to ground plane on the PCB and the ground plane should extend out from underneath the package to improve heat dissipation.

6 Specifications

6.1 Absolute Maximum Ratings

See ⁽¹⁾⁽²⁾

	MIN	MAX	UNIT
V _{DD} to V _{SS}	–0.3	18	V
HB to HS	–0.3	18	V
LI or HI to V _{SS}	–0.3	V _{DD} + 0.3	V
LO to V _{SS}	–0.3	V _{DD} + 0.3	V
HO to V _{SS}	V _{HS} – 0.3	V _{HB} + 0.3	V
HS to V _{SS} ⁽³⁾	–5	90	V
HB to V _{SS}		108	V
Junction Temperature	–40	150	°C
Storage Temperature Range	–55	150	°C

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Operating Ratings are conditions under which operation of the device is specified. Operating Ratings do not imply performance limits. For performance limits and associated test conditions, see the [Electrical Characteristics](#).
- (2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/Distributors for availability and specifications.
- (3) In the application the HS node is clamped by the body diode of the external lower N-MOSFET, therefore the HS voltage will generally not exceed –1V. However in some applications, board resistance and inductance may result in the HS node exceeding this stated voltage transiently. If negative transients occur on HS, the HS voltage must never be more negative than V_{DD} – 15V. For example, if V_{DD} = 10V, the negative transients at HS must not exceed –5V.

LM5109A

SNVS412C – APRIL 2006 – REVISED SEPTEMBER 2016

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6.2 ESD Ratings

		VALUE	UNIT
V_{ESD}	Electrostatic discharge Human-body model (HBM) ⁽¹⁾	±1500	V

(1) The human body model is a 100 pF capacitor discharged through a 1.5kΩ resistor into each pin.

6.3 Recommended Operating Conditions

	MIN	NOM	MAX	UNIT
V_{DD}	8		14	V
HS ⁽¹⁾	–1		90	V
HB	$V_{\text{HS}} + 8$		$V_{\text{HS}} + 14$	V
HS Slew Rate			< 50	V/ns
Junction Temperature	–40		125	°C

(1) In the application the HS node is clamped by the body diode of the external lower N-MOSFET, therefore the HS voltage will generally not exceed –1V. However in some applications, board resistance and inductance may result in the HS node exceeding this stated voltage transiently. If negative transients occur on HS, the HS voltage must never be more negative than $V_{\text{DD}} - 15\text{V}$. For example, if $V_{\text{DD}} = 10\text{V}$, the negative transients at HS must not exceed –5V.

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾		LM5109A		UNIT
		D (SOIC)	NGT (WSON)	
		8 PINS	8 PINS	
$R_{\theta\text{JA}}$	Junction-to-ambient thermal resistance	117.6	42.3	°C/W
$R_{\theta\text{JC(top)}}$	Junction-to-case (top) thermal resistance	64.9	34	°C/W
$R_{\theta\text{JB}}$	Junction-to-board thermal resistance	58.1	19.3	°C/W
Ψ_{JT}	Junction-to-top characterization parameter	17.4	0.4	°C/W
Ψ_{JB}	Junction-to-board characterization parameter	57.6	19.5	°C/W
$R_{\theta\text{JC(bot)}}$	Junction-to-case (bottom) thermal resistance	–	8.1	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

6.5 Electrical Characteristics

Unless otherwise specified, $V_{\text{DD}} = V_{\text{HB}} = 12\text{V}$, $V_{\text{SS}} = V_{\text{HS}} = 0\text{V}$, No Load on LO or HO ⁽¹⁾. Typical limits are for $T_{\text{J}} = 25^\circ\text{C}$, and minimum and maximum limits apply over the operating junction temperature range (–40°C to 125°C).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY CURRENTS						
I_{DD}	V_{DD} quiescent current	LI = HI = 0V		0.3	0.6	mA
I_{DDO}	V_{DD} operating current	f = 500 kHz		1.8	2.9	mA
I_{HB}	Total HB quiescent current	LI = HI = 0V		0.06	0.2	mA
I_{HBO}	Total HB operating current	f = 500 kHz		1.4	2.8	mA
I_{HBS}	HB to V_{SS} current, quiescent	$V_{\text{HS}} = V_{\text{HB}} = 90\text{V}$		0.1	10	μA
I_{HBSO}	HB to V_{SS} current, operating	f = 500 kHz		0.5		mA
INPUT PINS LI and HI						
V_{IL}	Low-level input voltage threshold		0.8	1.8		V
V_{IH}	High-level input voltage threshold			1.8	2.2	V
R_{I}	Input pulldown resistance		100	200	500	kΩ
UNDER-VOLTAGE PROTECTION						
V_{DDR}	V_{DD} rising threshold	$V_{\text{DDR}} = V_{\text{DD}} - V_{\text{SS}}$	6.0	6.7	7.4	V
V_{DDH}	V_{DD} threshold hysteresis			0.5		V
V_{HBR}	HB rising threshold	$V_{\text{HBR}} = V_{\text{HB}} - V_{\text{HS}}$	5.7	6.6	7.1	V

(1) Minimum and maximum limits are 100% production tested at 25°C. Limits over the operating temperature range are specified through correlation using Statistical Quality Control (SQC) methods. Limits are used to calculate Average Outgoing Quality Level (AOQL).

Electrical Characteristics (continued)

Unless otherwise specified, $V_{DD} = V_{HB} = 12V$, $V_{SS} = V_{HS} = 0V$, No Load on LO or HO⁽¹⁾. Typical limits are for $T_J = 25^\circ C$, and minimum and maximum limits apply over the operating junction temperature range ($-40^\circ C$ to $125^\circ C$).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
V_{HBH}	HB threshold hysteresis			0.4		V
LO GATE DRIVER						
V_{OLL}	Low-level output voltage	$I_{LO} = 100\text{ mA}$, $V_{OHL} = V_{LO} - V_{SS}$		0.38	0.65	V
V_{OHL}	High-level output voltage	$I_{LO} = -100\text{ mA}$, $V_{OHL} = V_{DD} - V_{LO}$		0.72	1.20	V
I_{OHL}	Peak pullup current	$V_{LO} = 0V$		1.0		A
I_{OLL}	Peak pulldown current	$V_{LO} = 12V$		1.0		A
HO GATE DRIVER						
V_{OLH}	Low-level output voltage	$I_{HO} = 100\text{ mA}$, $V_{OLH} = V_{HO} - V_{HS}$		0.38	0.65	V
V_{OHH}	High-level output voltage	$I_{HO} = -100\text{ mA}$, $V_{OHH} = V_{HB} - V_{HO}$		0.72	1.20	V
I_{OHH}	Peak pullup current	$V_{HO} = 0V$		1.0		A
I_{OLH}	Peak pulldown current	$V_{HO} = 12V$		1.0		A

6.6 Switching Characteristics

Unless otherwise specified, $V_{DD} = V_{HB} = 12V$, $V_{SS} = V_{HS} = 0V$, No Load on LO or HO. Typical limits are for $T_J = 25^\circ C$, and minimum and maximum limits apply over the operating junction temperature range ($-40^\circ C$ to $125^\circ C$).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{LPHL}	Lower turn-off propagation delay (LI falling to LO falling)			30	56	ns
t_{HPLH}	Upper turn-off propagation delay (HI falling to HO falling)			30	56	ns
t_{LPLH}	Lower turn-on propagation delay (LI rising to LO rising)			32	56	ns
t_{HPLH}	Upper turn-on propagation delay (HI rising to HO rising)			32	56	ns
t_{MON}	Delay matching: lower turn-on and upper turn-off			2	15	ns
t_{MOFF}	Delay matching: lower turn-off and upper turn-on			2	15	ns
t_{RC}, t_{FC}	Either output rise or fall time	$C_L = 1000\text{ pF}$		15	-	ns
t_{PW}	Minimum input pulse width that changes the output			50		ns

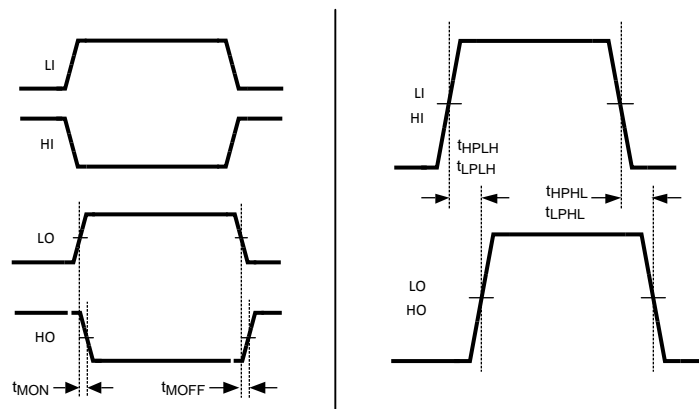
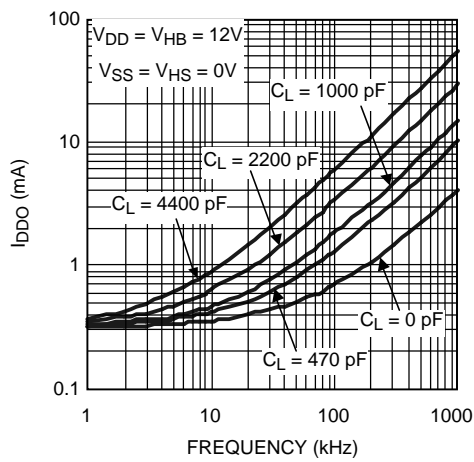
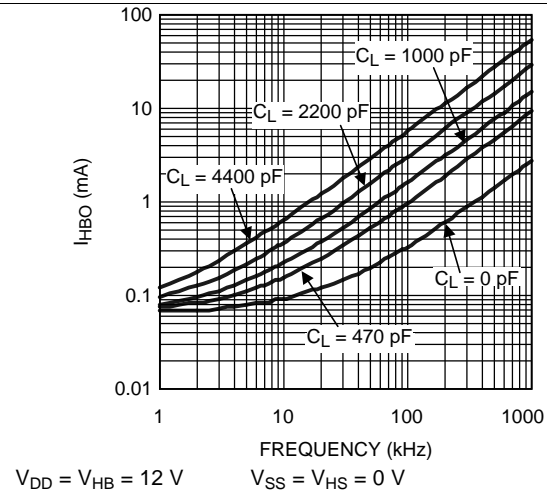
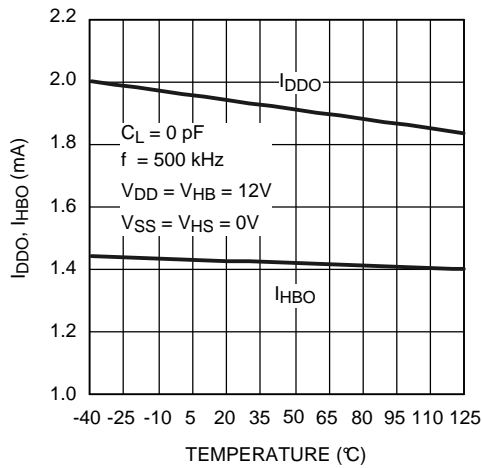
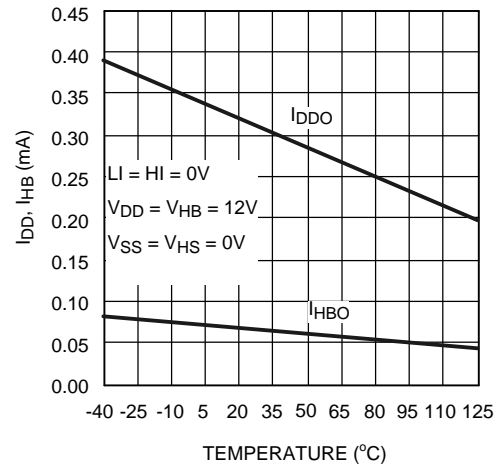
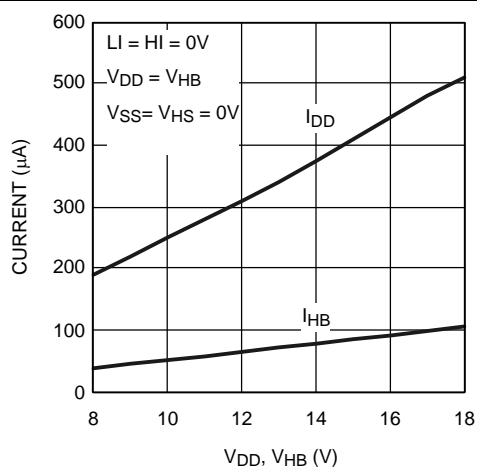
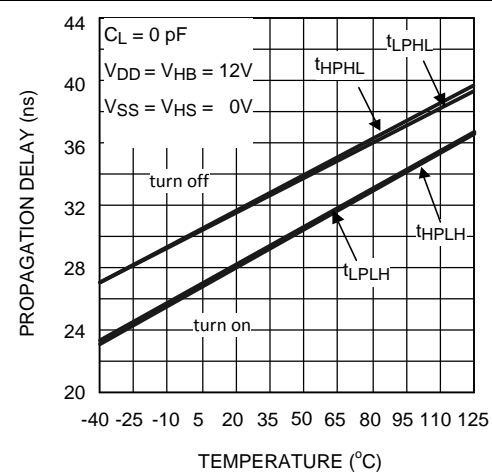


Figure 1. Timing Diagram

6.7 Typical Performance Characteristics


Figure 2. V_{DD} Operating Current vs Frequency

Figure 3. HB Operating Current vs Frequency

Figure 4. Operating Current vs Temperature

Figure 5. Quiescent Current vs Temperature

Figure 6. Quiescent Current vs Voltage

Figure 7. Propagation Delay vs Temperature

Typical Performance Characteristics (continued)

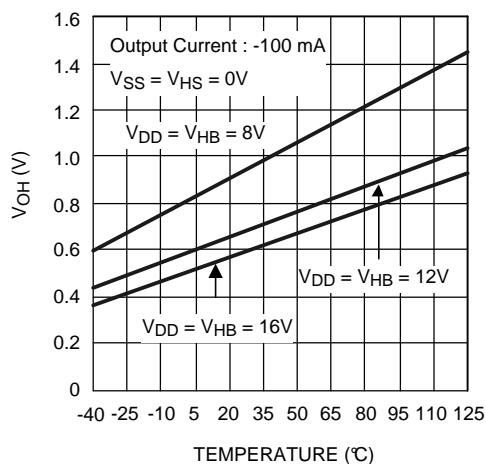


Figure 8. LO and HO High Level Output Voltage vs Temperature

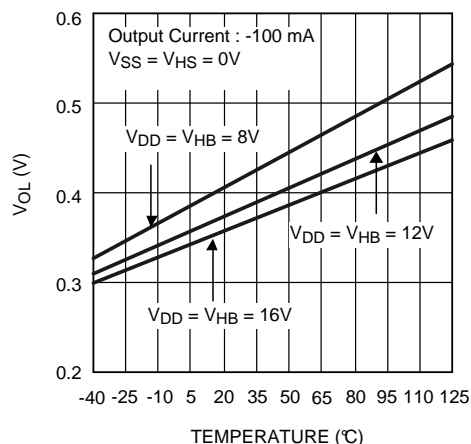


Figure 9. LO and HO Low Level Output Voltage vs Temperature

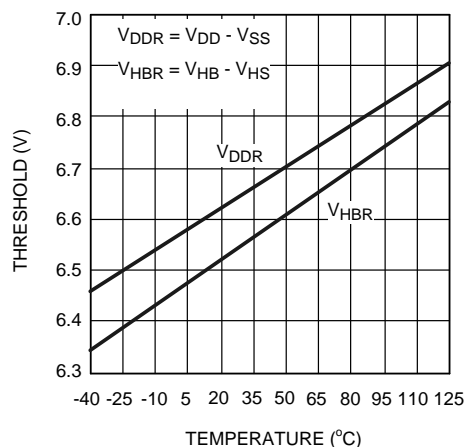


Figure 10. Undervoltage Rising Thresholds vs Temperature

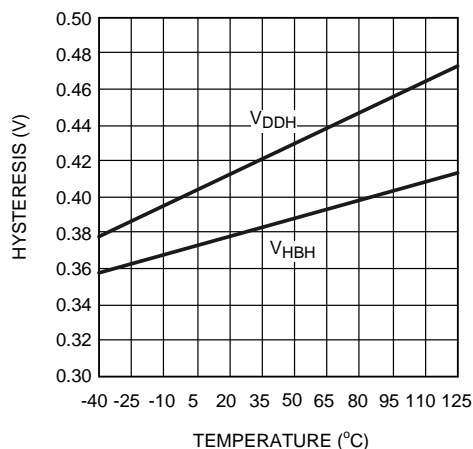


Figure 11. Undervoltage Hysteresis vs Temperature

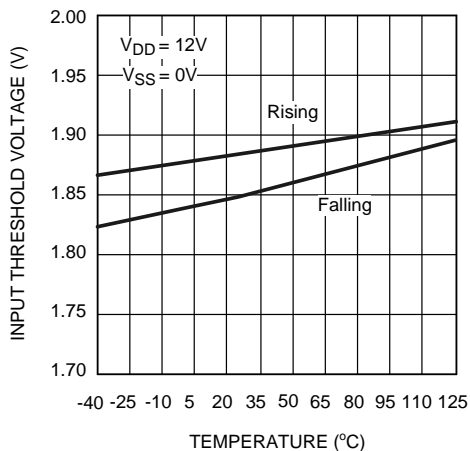


Figure 12. Input Thresholds vs Temperature

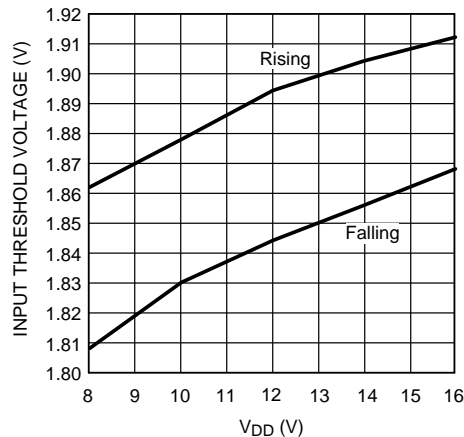


Figure 13. Input Thresholds vs Supply Voltage

Feature Description (continued)

7.3.3 Output Stages

The output stages are the interface to the power MOSFETs in the power train. High slew rate, low resistance, and high-peak current capability of both outputs allow for efficient switching of the power MOSFETs. The low-side output stage is referenced to VSS and the high-side is referenced to HS.

7.4 Device Functional Modes

The device operates in normal mode and UVLO mode. See [Start-Up and UVLO](#) for more information on UVLO operation mode. In normal mode when the V_{DD} and V_{HB-HS} are above UVLO threshold, the output stage is dependent on the states of the HI and LI pins. The output HO and LO will be low if input state is floating.

Table 1. INPUT and OUTPUT Logic Table

HI	LI	HO ⁽¹⁾	LO ⁽²⁾
L	L	L	L
L	H	L	H
H	L	H	L
H	H	H	H
Floating	Floating	L	L

(1) HO is measured with respect to the HS.

(2) LO is measured with respect to the VSS.

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

To operate power MOSFETs at high switching frequencies and to reduce associated switching losses, a powerful gate driver is employed between the PWM output of controller and the gates of the power semiconductor devices. Also, gate drivers are indispensable when it is impossible for the PWM controller to directly drive the gates of the switching devices. With the advent of digital power, this situation is often encountered because the PWM signal from the digital controller is often a 3.3-V logic signal which cannot effectively turn on a power switch. Level shift circuit is needed to boost the 3.3-V signal to the gate-drive voltage (such as 12 V) to fully turn on the power device and minimize conduction losses. Traditional buffer drive circuits based on NPN and PNP bipolar transistors in totem-pole arrangement prove inadequate with digital power because they lack level-shifting capability. Gate drivers effectively combine both the level-shifting and buffer-drive functions. Gate drivers also find other needs such as minimizing the effect of high-frequency switching noise (by placing the high-current driver IC physically close to the power switch), driving gate-drive transformers and controlling floating power-device gates, reducing power dissipation and thermal stress in controllers by moving gate charge power losses from the controller into the driver.

The LM5109A is the high-voltage gate drivers designed to drive both the high-side and low-side N-channel MOSFETs in a half-bridge configuration, full-bridge configuration, or in a synchronous buck circuit. The floating high-side driver is capable of operating with supply voltages up to 90 V. This allows for N-channel MOSFETs control in half-bridge, full-bridge, push-pull, two-switch forward and active clamp topologies. The outputs are independently controlled. Each channel is controlled by its respective input pins (HI and LI), allowing full and independent flexibility to control ON and OFF-time of the output.

8.1.1 HS Transient Voltages Below Ground

The HS node will always be clamped by the body diode of the lower external FET. In some situations, board resistances and inductances can cause the HS node to transiently swing several volts below ground. The HS node can swing below ground provided:

1. HS must always be at a lower potential than HO. Pulling HO more than -0.3V below HS can activate parasitic transistors resulting in excessive current flow from the HB supply, possibly resulting in damage to the IC. The same relationship is true with LO and VSS. If necessary, a Schottky diode can be placed externally between HO and HS or LO and GND to protect the IC from this type of transient. The diode must be placed as close to the IC pins as possible in order to be effective.
2. HB to HS operating voltage should be 15V or less. Hence, if the HS pin transient voltage is -5V , VDD should be ideally limited to 10V to keep HB to HS below 15V.
3. Low ESR bypass capacitors from HB to HS and from VDD to VSS are essential for proper operation. The capacitor should be located at the leads of the IC to minimize series inductance. The peak currents from LO and HO can be quite large. Any series inductances with the bypass capacitor will cause voltage ringing at the leads of the IC which must be avoided for reliable operation.

8.2 Typical Application

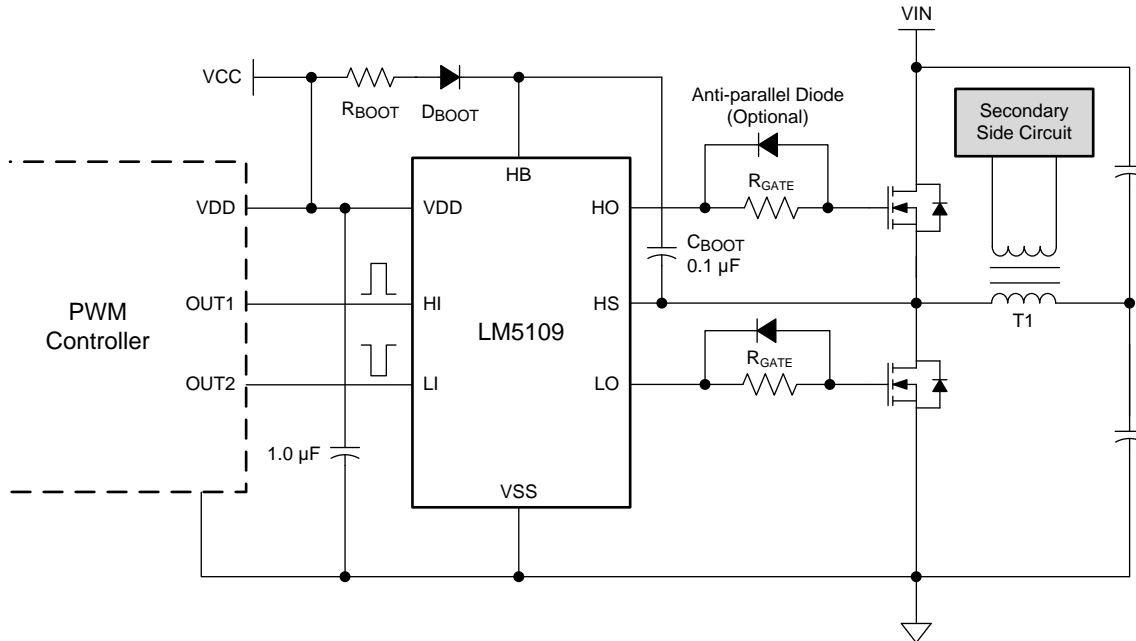


Figure 14. LM5109A Driving MOSFETs in a Half-Bridge Converter

8.2.1 Design Requirements

Table 2 lists the design parameters of the LM5109A.

Table 2. Design Example

PARAMETER	VALUE
Gate Driver	LM5109A
MOSFET	CSD19534KCS
V_{DD}	10 V
Q_G	17 nC
f_{SW}	500 kHz

8.2.2 Detailed Design Procedure

8.2.2.1 Select Bootstrap and VDD Capacitor

The bootstrap capacitor must maintain the V_{HB-HS} voltage above the UVLO threshold for normal operation. Calculate the maximum allowable drop across the bootstrap capacitor with Equation 1.

$$\Delta V_{HB} = V_{DD} - V_{DH} - V_{HBL} = 10 \text{ V} - 1 \text{ V} - 6.7 \text{ V} = 2.3 \text{ V}$$

where

- V_{DD} = Supply voltage of the gate drive IC
- V_{DH} = Bootstrap diode forward voltage drop
- $V_{HBL} = V_{HBRmax} - V_{HBH}$, HB falling threshold

(1)

Then, the total charge needed per switching cycle is estimated by Equation 2.

$$Q_{Total} = Q_G + I_{HBS} \times \frac{D_{Max}}{f_{SW}} + \frac{I_{HB}}{f_{SW}} = 17 \text{ nC} + 10 \mu\text{A} \times \frac{0.95}{500 \text{ kHz}} + \frac{0.2 \text{ mA}}{500 \text{ kHz}} = 17.5 \text{ nC}$$

where

- Q_G = Total MOSFET gate charge

- I_{HBS} = HB to VSS Leakage current
- D_{Max} = Converter maximum duty cycle
- I_{HB} = HB Quiescent current

Therefore, the minimum C_{Boot} must be:

$$C_{Boot} = \frac{Q_{Total}}{\Delta V_{HB}} = \frac{17.5 \text{ nC}}{2.3 \text{ V}} = 7.6 \text{ nF} \quad (3)$$

In practice, the value of the C_{Boot} capacitor must be greater than calculated to allow for situations where the power stage may skip pulse due to load transients. TI recommends having enough margins and place the bootstrap capacitor as close to the HB and HS pins as possible.

$$C_{Boot} = 100 \text{ nF} \quad (4)$$

As a general rule the local V_{DD} bypass capacitor must be 10 times greater than the value of C_{Boot} , as shown in [Equation 5](#).

$$C_{VDD} = 1 \text{ } \mu\text{F} \quad (5)$$

The bootstrap and bias capacitors must be ceramic types with X7R dielectric. The voltage rating must be twice that of the maximum V_{DD} considering capacitance tolerances once the devices have a DC bias voltage across them and to ensure long-term reliability.

8.2.2.2 Select External Bootstrap Diode and Its Series Resistor

The bootstrap capacitor is charged by the V_{DD} through the external bootstrap diode every cycle when low-side MOSFET turns on. The charging of the capacitor involves high peak currents, and therefore transient power dissipation in the bootstrap diode may be significant and the conduction loss also depends on its forward voltage drop. Both the diode conduction losses and reverse recovery losses contribute to the total losses in the gate driver circuit.

For the selection of external bootstrap diodes, see [AN-1317 Selection of External Bootstrap Diode for LM510X Devices](#) (SNVSA083). Bootstrap resistor R_{BOOT} is selected to reduce the inrush current in D_{BOOT} and limit the ramp up slew rate of voltage of V_{HB-HS} during each switching cycle, especially when HS pin have excessive negative transient voltage. R_{BOOT} recommended value is between $2 \text{ } \Omega$ and $10 \text{ } \Omega$ depending on diode selection. A current limiting resistor of $2.2 \text{ } \Omega$ is selected to limit inrush current of bootstrap diode, and the estimated peak current on the D_{Boot} is shown in [Equation 6](#).

$$I_{DBoot(pk)} = \frac{V_{DD} - V_{DH}}{R_{Boot}} = \frac{10 \text{ V} - 1 \text{ V}}{2.2 \text{ } \Omega} \approx 4 \text{ A}$$

where

- V_{DH} is the bootstrap diode forward voltage drop

8.2.2.3 Selecting External Gate Driver Resistor

The external gate driver resistor, R_{GATE} , is sized to reduce ringing caused by parasitic inductances and capacitances and also to limit the current coming out of the gate driver.

Peak HO pullup current are calculated in [Equation 7](#).

$$I_{OHH} = \frac{V_{DD} - V_{DH}}{R_{HOH} + R_{Gate} + R_{GFET_Int}} = \frac{10 \text{ V} - 1 \text{ V}}{1.2 \text{ V} / 100 \text{ mA} + 4.7 \text{ } \Omega + 2.2 \text{ } \Omega} = 0.48 \text{ A}$$

where

- I_{OHH} = Peak pullup current
- V_{DH} = Bootstrap diode forward voltage drop
- R_{HOH} = Gate driver internal HO pullup resistance, provide by driver data sheet directly or estimated from the testing conditions, that is $R_{HOH} = V_{OHH} / I_{HO}$
- R_{Gate} = External gate drive resistance
- R_{GFET_Int} = MOSFET internal gate resistance, provided by transistor data sheet

Similarly, Peak HO pulldown current is shown in [Equation 8](#).

$$I_{OLH} = \frac{V_{DD} - V_{DH}}{R_{HOL} + R_{Gate} + R_{GFET_Int}}$$

where

- R_{HOL} is the HO pulldown resistance (8)

Peak LO pullup current is shown in Equation 9.

$$I_{OHL} = \frac{V_{DD}}{R_{LOH} + R_{Gate} + R_{GFET_Int}}$$

where

- R_{LOH} is the LO pullup resistance (9)

Peak LO pulldown current is shown in Equation 10.

$$I_{OLL} = \frac{V_{DD}}{R_{LOL} + R_{Gate} + R_{GFET_Int}}$$

where

- R_{LOL} is the LO pulldown resistance (10)

For some scenarios, if the applications require fast turnoff, an anti-parallel diode on R_{Gate} could be used to bypass the external gate drive resistor and speed up turnoff transition.

8.2.2.4 Estimate the Driver Power Loss

The total driver IC power dissipation can be estimated through the following components.

1. Static power losses, P_{QC} , due to quiescent current – I_{DD} and I_{HB}

$$P_{QC} = V_{DD} \times I_{DD} + (V_{DD} - V_{DH}) \times I_{HB} \quad (11)$$

2. Level-shifter losses, P_{IHBS} , due high-side leakage current – I_{HBS}

$$P_{IHBS} = V_{HB} \times I_{HBS} \times D$$

where

- D is the high-side switch duty cycle (12)

3. Dynamic losses, $P_{QG1\&2}$, due to the FETs gate charge – Q_G

$$P_{QG1\&2} = 2 \times V_{DD} \times Q_G \times f_{SW} \times \frac{R_{GD_R}}{R_{GD_R} + R_{Gate} + R_{GFET_Int}}$$

where

- Q_G = Total FETs gate charge
- f_{SW} = Switching frequency
- R_{GD_R} = Average value of pullup and pulldown resistor
- R_{Gate} = External gate drive resistor
- R_{GFET_Int} = Internal FETs gate resistor (13)

4. Level-shifter dynamic losses, P_{LS} , during high-side switching due to required level-shifter charge on each switching cycle – Q_P

$$P_{LS} = V_{HB} \times Q_P \times f_{SW} \quad (14)$$

In this example, the estimated gate driver loss in LM5109A is shown in Equation 15.

$$P_{LM5109A} = 10\text{ V} \times 0.6\text{ mA} + 9\text{ V} \times 0.2\text{ mA} + 72\text{ V} \times 10\text{ }\mu\text{A} \times 0.95 + 2 \times 10 \times 17\text{ nC} \times 500\text{ kHz} \times \frac{12\text{ }\Omega}{12\text{ }\Omega + 4.7\text{ }\Omega + 2.2\text{ }\Omega} + 72\text{ V} \times 0.5\text{ nC} \times 500\text{ kHz} = 0.134\text{ W} \quad (15)$$

For a given ambient temperature, the maximum allowable power loss of the IC can be defined as shown in Equation 16.

$$P_{LM5109A} = \frac{T_J - T_A}{R_{\theta JA}}$$

where

- $P_{LM5109B}$ = The total power dissipation of the driver
 - T_J = Junction temperature
 - T_A = Ambient temperature
 - $R_{\theta JA}$ = Junction-to-ambient thermal resistance
- (16)

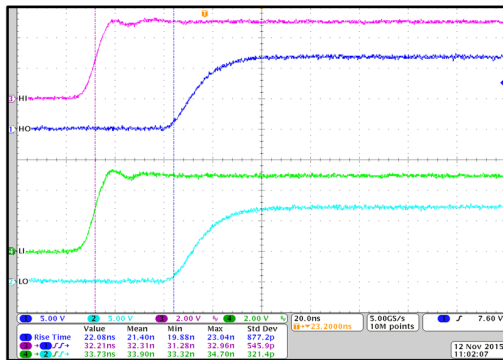
The thermal metrics for the driver package is summarized in the [Thermal Information](#) table of the data sheet. For detailed information regarding the thermal information table, please refer to the [Semiconductor and IC Package Thermal Metrics](#) (SPRA953).

8.2.3 Application Curves

[Figure 15](#) and [Figure 16](#) shows the rising and falling time as well as turnon and turnoff propagation delay testing waveform in room temperature, and waveform measurement data (see the bottom part of the waveform). Each channel (HI, LI, HO, and LO) is labeled and displayed on the left hand of the waveforms.

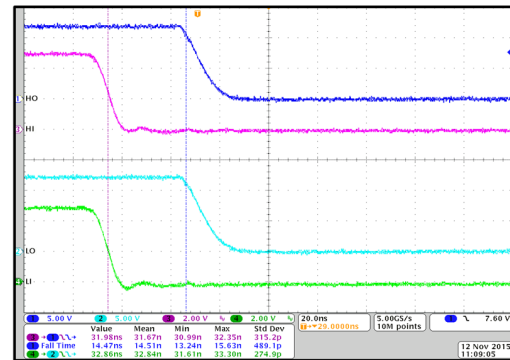
The testing condition: load capacitance is 1 nF, $V_{DD} = 12\text{ V}$, $f_{SW} = 500\text{ kHz}$.

HI and LI share one same input from function generator, therefore, besides the propagation delay and rising and falling time, the difference of the propagation delay between HO and LO gives the propagation delay matching data.



$C_L = 1\text{ nF}$ $V_{DD} = 12\text{ V}$ $f_{SW} = 500\text{ kHz}$

Figure 15. Rising Time and Turnon Propagation Delay



$C_L = 1\text{ nF}$ $V_{DD} = 12\text{ V}$ $f_{SW} = 500\text{ kHz}$

Figure 16. Falling Time and Turnoff Propagation Delay

9 Power Supply Recommendations

The recommended bias supply voltage range for LM5109A is from 8 V to 14 V. The lower end of this range is governed by the internal undervoltage lockout (UVLO) protection feature of the V_{DD} supply circuit blocks. The upper end of this range is driven by the 18-V absolute maximum voltage rating of the V_{DD} . TI recommends keeping a 4-V margin to allow for transient voltage spikes.

The UVLO protection feature also involves a hysteresis function. This means that once the device is operating in normal mode, if the V_{DD} voltage drops, the device continues to operate in normal mode as long as the voltage drop does not exceed the hysteresis specification, V_{DDH} . If the voltage drop is more than hysteresis specification, the device shuts down. Therefore, while operating at or near the 8-V range, the voltage ripple on the auxiliary power supply output must be smaller than the hysteresis specification of LM5109A to avoid triggering device-shutdown.

A local bypass capacitor must be placed between the VDD and GND pins. And this capacitor must be located as close to the device as possible. A low-ESR, ceramic surface mount capacitor is recommended. TI recommends using 2 capacitors across VDD and GND: a 100-nF, ceramic surface-mount capacitor for high-frequency filtering placed very close to VDD and GND pin, and another surface-mount capacitor, 220-nF to 10- μ F, for IC bias requirements. In a similar manner, the current pulses delivered by the HO pin are sourced from the HB pin. Therefore a 22-nF to 220-nF local decoupling capacitor is recommended between the HB and HS pins.

10 Layout

10.1 Layout Guidelines

Optimum performance of high and low-side gate drivers cannot be achieved without taking due considerations during circuit board layout. The following points are emphasized:

1. Low ESR / ESL capacitors must be connected close to the IC between VDD and VSS pins and between HB and HS pins to support high peak currents being drawn from VDD and HB during the turn-on of the external MOSFETs.
2. To prevent large voltage transients at the drain of the top MOSFET, a low ESR electrolytic capacitor and a good quality ceramic capacitor must be connected between the MOSFET drain and ground (VSS).
3. In order to avoid large negative transients on the switch node (HS) pin, the parasitic inductances between the top MOSFET source and the of the bottom MOSFET drain (synchronous rectifier) must be minimized.
4. Grounding considerations:
 - The first priority in designing grounding connections is to confine the high peak currents that charge and discharge the MOSFET gates to a minimal physical area. This will decrease the loop inductance and minimize noise issues on the gate terminals of the MOSFETs. The gate driver should be placed as close as possible to the MOSFETs.
 - The second consideration is the high current path that includes the bootstrap capacitor, the bootstrap diode, the local ground referenced bypass capacitor, and the low-side MOSFET body diode. The bootstrap capacitor is recharged on a cycle-by-cycle basis through the bootstrap diode from the ground referenced VDD bypass capacitor. The recharging occurs in a short time interval and involves high peak current. Minimizing this loop length and area on the circuit board is important to ensure reliable operation.

10.2 Layout Example

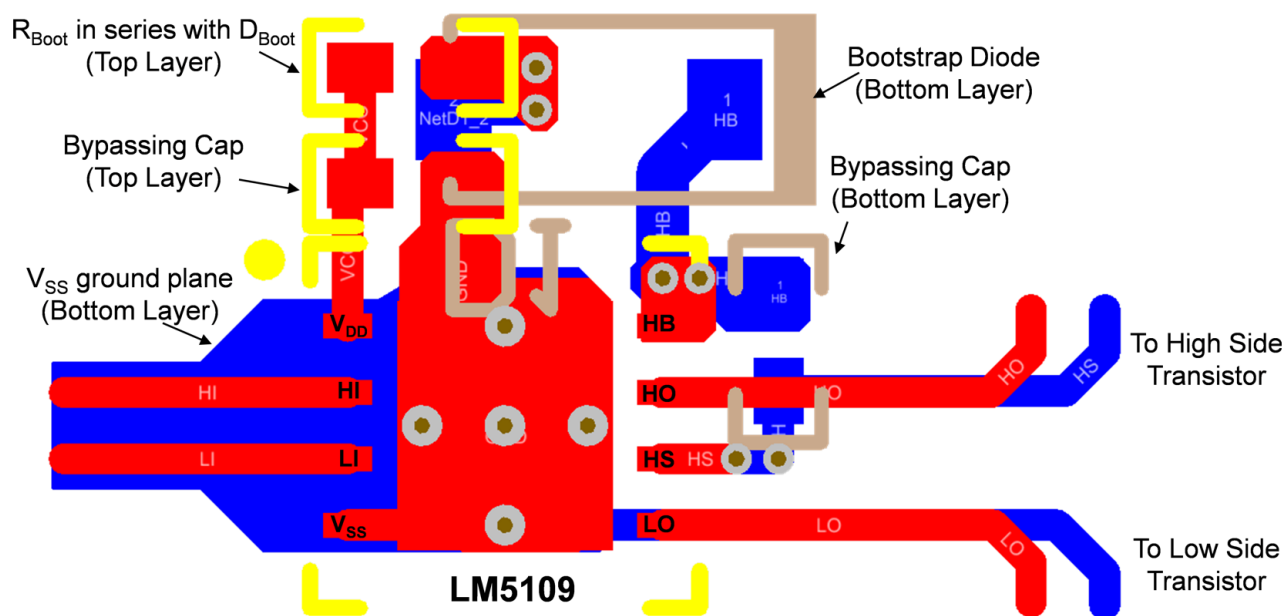


Figure 17. Layout Example

11 Device and Documentation Support

11.1 Documentation Support

11.1.1 Related Documentation

For additional information, see the following:

[AN-1317 Selection of External Bootstrap Diode for LM510x Devices](#) (SNVA083)

11.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

11.3 Community Resource

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

TI E2E™ Online Community *TI's Engineer-to-Engineer (E2E) Community*. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

Design Support *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

11.4 Trademarks

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11.5 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.6 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
LM5109AMA/NOPB	ACTIVE	SOIC	D	8	95	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	L5109 AMA	Samples
LM5109AMAX/NOPB	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	L5109 AMA	Samples
LM5109ASD/NOPB	ACTIVE	WSO	NGT	8	1000	Green (RoHS & no Sb/Br)	CU NIPDAU CU SN	Level-1-260C-UNLIM	-40 to 125	5109ASD	Samples
LM5109ASDX/NOPB	ACTIVE	WSO	NGT	8	4500	Green (RoHS & no Sb/Br)	CU NIPDAU CU SN	Level-1-260C-UNLIM	-40 to 125	5109ASD	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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TAPE AND REEL INFORMATION


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM5109AMAX/NOPB	SOIC	D	8	2500	330.0	12.4	6.5	5.4	2.0	8.0	12.0	Q1

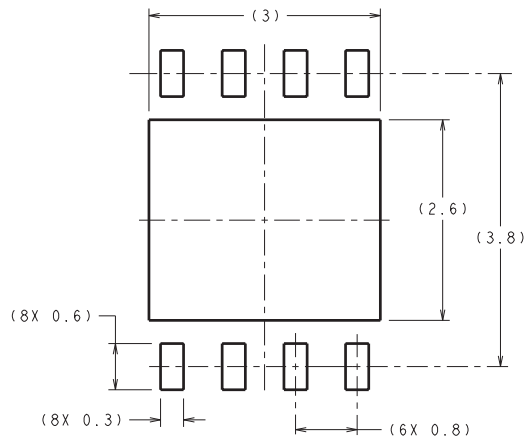
TAPE AND REEL BOX DIMENSIONS



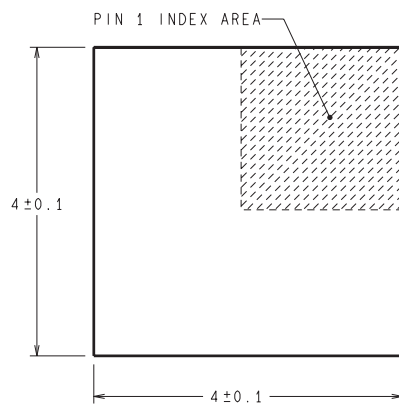
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM5109AMAX/NOPB	SOIC	D	8	2500	367.0	367.0	35.0

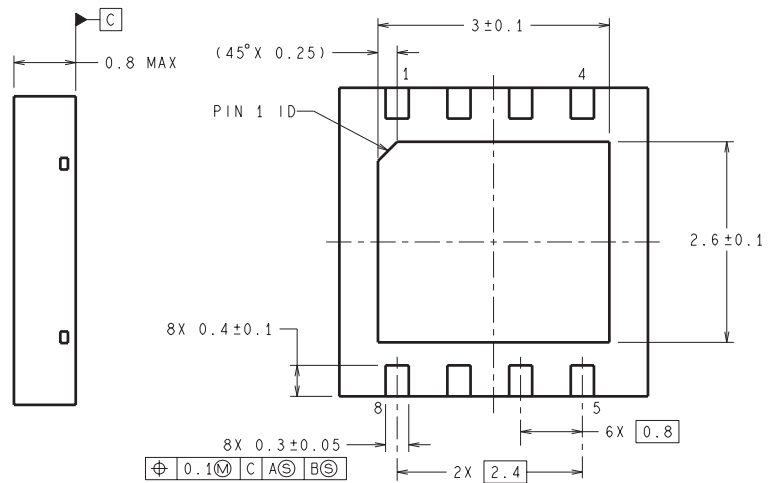
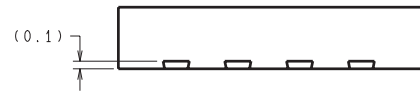
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RECOMMENDED LAND PATTERN



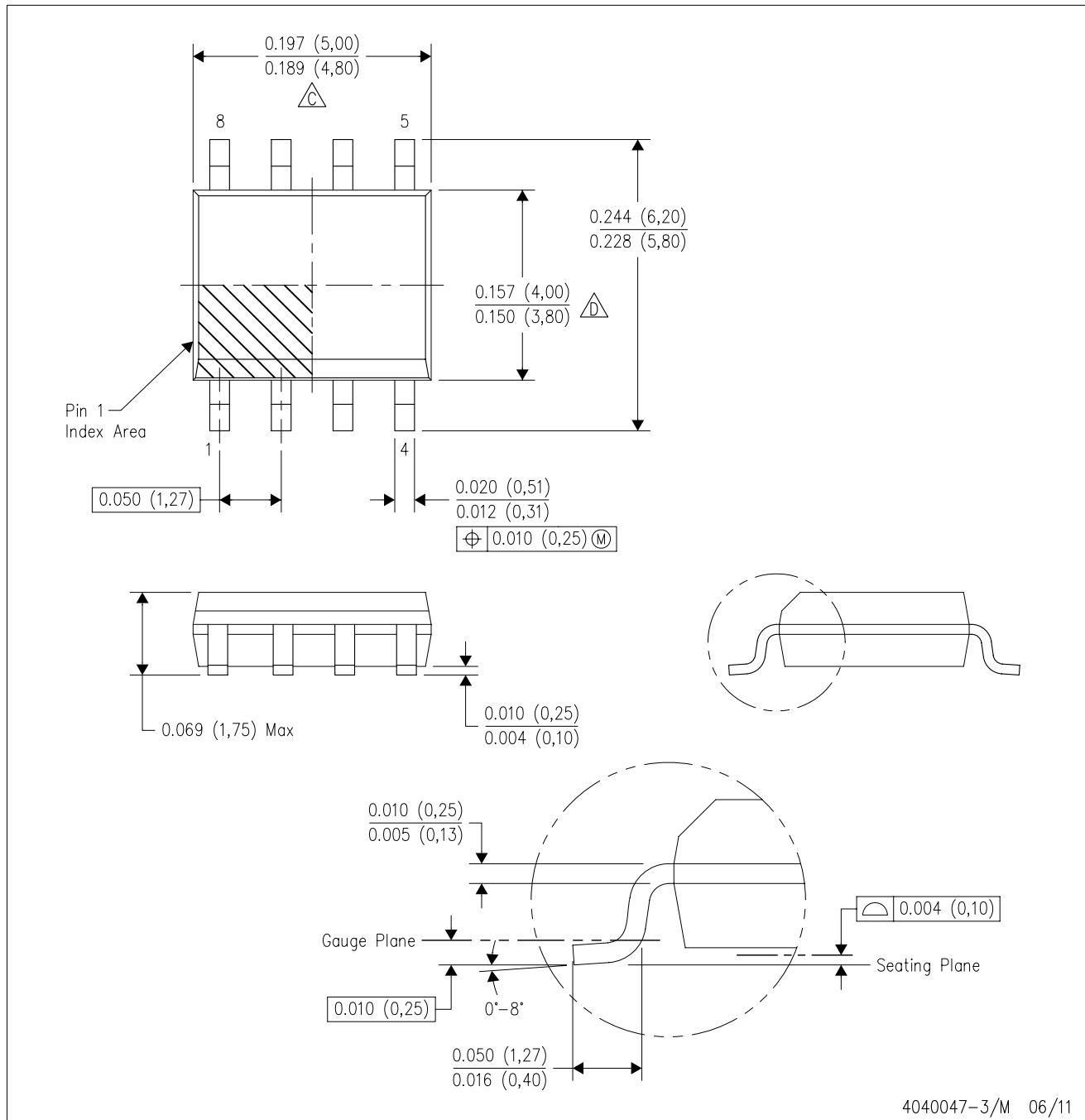
DIMENSIONS ARE IN MILLIMETERS
DIMENSIONS IN () FOR REFERENCE ONLY



SDC08A (Rev A)

D (R-PDSO-G8)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in inches (millimeters).
 - B. This drawing is subject to change without notice.
 - $\triangle C$ Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
 - $\triangle D$ Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
 - E. Reference JEDEC MS-012 variation AA.

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