

Además para el 2° orden entones es:  $T(s) = \frac{s^2 + \frac{\omega_z}{\omega_p} s + \omega_z^2}{s^2 + \frac{\omega_p}{\omega_p} s + \omega_p^2}$

Además para  $\theta_N(\omega) - \theta_D(\omega) = \theta(T_{gr})$

En el caso del prototipo  $(T_{gr}) = \frac{1}{s^2 + \frac{\omega_p}{\omega_p} s + \omega_p^2}$

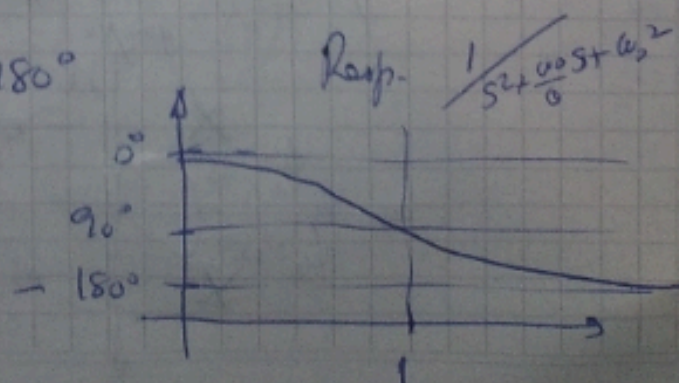
Reemplazando  $s = j\omega$   $|T(j\omega)| = \frac{1}{\sqrt{\underbrace{(1-\omega^2)^2}_{\text{parte real}} + \underbrace{\left(\frac{\omega}{Q}\right)^2}_{\text{parte im.}}}}$

$\theta_D(\omega) = -\tan^{-1}\left(\frac{\frac{\omega}{Q}}{1-\omega^2}\right)$

$\theta_D(\omega) \Big|_{\omega=j0} = 0^\circ$

$\theta_D(\omega) \Big|_{\omega=j1} = -\tan^{-1}(\infty) \approx -90^\circ$

$\theta_D(\omega) \Big|_{\omega=j\infty} \Rightarrow -180^\circ$





De esa deducción que si agregamos  $-180^\circ$  en el numerador  
podríamos obtener la misma respuesta.

Una deducción casi directa es usar la misma función en  
el numerador:

$$s^2 + \frac{\omega_z}{Q_z} s + \omega_z^2$$

Pero queremos que el signo sea opuesto. luego

$$\theta_N(j\omega) = -180^\circ$$

$$\theta_N(j1) = -90^\circ$$

$$\theta_N(j0) = 0^\circ$$

$$\theta_N = \left( \frac{\frac{\omega_z}{Q_z}}{1 - \omega_z^2} \right)$$

↓

Reestamos ~~con~~ invertir el signo del  
numerador  $\Rightarrow$

$$s^2 - \frac{\omega_z}{Q_z} s + \omega_z^2$$

luego  $T(s) = \frac{s^2 - \frac{\omega_z}{Q_z} s + \omega_z^2}{s^2 + \frac{\omega_p}{Q_p} s + \omega_p^2}$

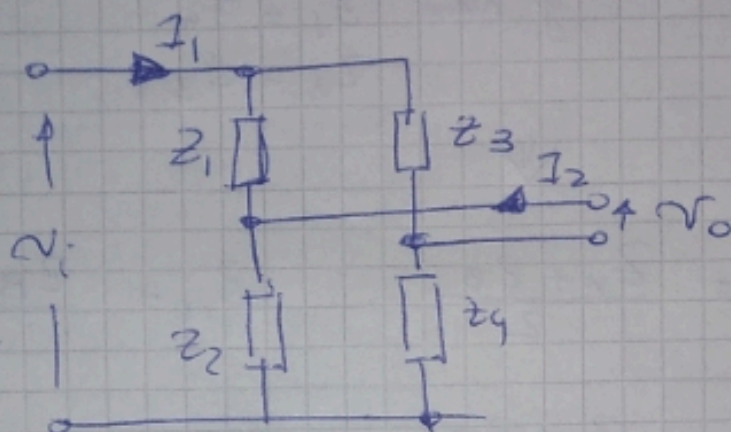
Esta función corresponde a un pasotodo.



$$T(s) = \frac{s^2 - \sqrt{2}s + 1}{s^2 + \sqrt{2}s + 1}$$



Una posible implementación pasiva es mediante estructura Tipo Loffle



Podemos analizar este circuito mediante matriz de impedancias

$$\begin{cases} V_i = z_{11} I_1 + z_{12} I_2 \\ V_o = z_{21} I_1 + z_{22} I_2 \end{cases}$$

$$z_{11} = \left. \frac{V_i}{I_1} \right|_{I_2=0} = (z_1 + z_2) \parallel (z_3 + z_4)$$

$$z_{12} = \left. \frac{V_i}{I_2} \right|_{I_1=0} = (z_1 + z_3) \parallel (z_2 + z_4)$$

$$z_{21} = \left. \frac{V_o}{I_1} \right|_{I_2=0} = (z_1 + z_3) \parallel (z_2 + z_4)$$

$$z_{22} = \left. \frac{V_o}{I_2} \right|_{I_1=0} = (z_1 + z_2) \parallel (z_3 + z_4)$$



Lo hacemos simétrico de tal manera que:

$$z_{12} = z_{21}$$

y hacemos  $z_1 = z_4$   
 $z_2 = z_3$



$$z_{11} = \frac{z_A + z_B}{2}$$

$$z_{12} = \frac{z_B - z_A}{2} = z_{21}$$

$$z_{22} = \frac{z_A + z_B}{2}$$

Lo metemos en transferencia & solo por definición:

$$\begin{cases} V_i = AV_o - I_o B \\ I_i = CV_o - I_o D \end{cases} \Rightarrow \begin{aligned} A &= \left. \frac{V_i}{V_o} \right|_{I_o=0} & B &= \left. \frac{V_o}{I_o} \right|_{V_i=0} \\ C &= \left. \frac{I_i}{V_o} \right|_{I_o=0} & D &= \left. \frac{I_i}{-I_o} \right|_{V_i=0} \end{aligned}$$

Despejando:

$$A = \frac{V_i}{V_o} = \frac{z_{11} z_o}{z_{21} I_i} \Rightarrow A = \frac{z_{11}}{z_{21}} \Rightarrow \frac{1}{A} = \frac{V_o}{V_i} = T(s)$$

luego ya sabemos que  $\boxed{T(s) = \frac{z_{12}}{z_{11}}}$

$$B = \frac{z_{11} z_{22} - z_{12} z_{21}}{z_{21}}$$

$$C = \frac{1}{z_{21}}$$

$$D = \frac{z_{22}}{z_{21}}$$



Otro igualar  $T(s)$  a nuestro  $\Phi$  modelo.

$$T(s) = \frac{s^2 - \sqrt{2}s + 1}{s^2 + \sqrt{2}s + 1} = \frac{z_B - z_A}{z_A + z_B} = \frac{z_B - z_A}{z_B + z_A}$$

$$N(s) = z_B - z_A = s^2 - \sqrt{2}s + 1$$

$$D(s) = z_B + z_A = s^2 + \sqrt{2}s + 1$$

$D(s)$  es fácil poderla sacar en  $z_B = LC$  y  $z_A = R$ :

$$\frac{1}{s} + sL + R = \frac{1 + s^2LC + sRC}{sC}$$

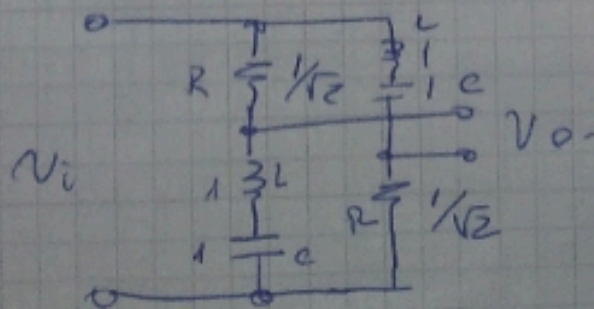
$$\text{y } N(s): \frac{1}{sC} + sL - R \Rightarrow \frac{1 + s^2LC - sRC}{sC}$$

$$\frac{N(s)}{D(s)} = \frac{1 + s^2LC - sRC}{1 + s^2LC + sRC} \Rightarrow T(s) = \frac{s^2 - \frac{1}{RC}s + 1}{s^2 + \frac{1}{LC}s + 1}$$

$$\text{Con lo cual } \frac{1}{RC} = \sqrt{2} \quad \frac{1}{LC} = 1$$

$$\text{Si } C = 1 \Rightarrow \left[ R = \frac{1}{\sqrt{2}} \right] \Rightarrow \left[ L = 1 \right]$$

El circuito antetizado sera:





Cálculo de la Matriz  $Z$  y  $T_{ABCD}$ .

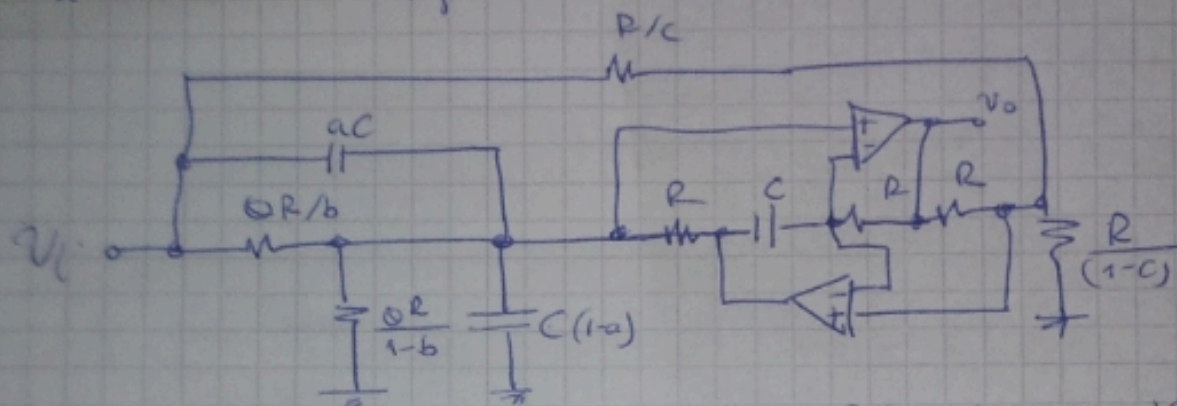
$$Z = \begin{pmatrix} \frac{1 + SRC + S^2 LC}{2SC} & \frac{1 - SRC + S^2 LC}{2SC} \\ \frac{1 - SRC + S^2 LC}{2SC} & \frac{1 + SRC + S^2 LC}{2SC} \end{pmatrix}$$

$$Z = \begin{pmatrix} \frac{1 + S\sqrt{2} + S^2}{2S} & \frac{1 - S\sqrt{2} + S^2}{2S} \\ \frac{1 - S\sqrt{2} + S^2}{2S} & \frac{1 + S\sqrt{2} + S^2}{2S} \end{pmatrix}$$

$$T_{ABCD} = \begin{pmatrix} \frac{S^2 + \sqrt{2}S + 1}{S^2 + \sqrt{2}S + 1} & \frac{(1 + \sqrt{2}S + S^2)^2 - (1 - \sqrt{2}S + S^2)^2}{2S(1 - S\sqrt{2} + S^2)} \\ \frac{2S}{1 - S\sqrt{2} + S^2} & \frac{1 + \sqrt{2}S + S^2}{1 - \sqrt{2}S + S^2} \end{pmatrix}$$



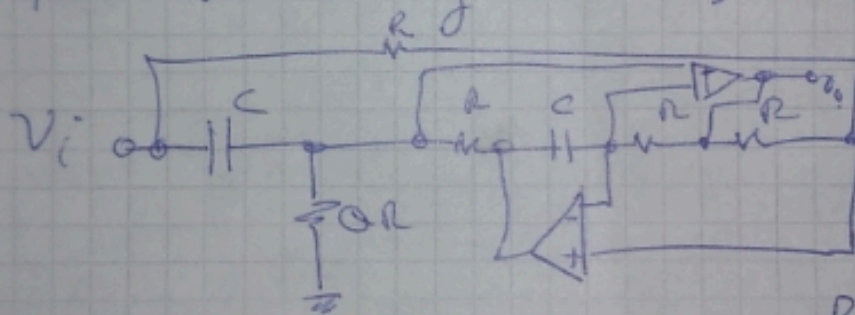
En la estructura biquadrática GIC..



Para un All-pass

$$T(s) = \frac{s^2(2a-c) + s\left(\frac{w_0}{c}\right)(2b-c) + cw_0^2}{s^2 + \frac{w_0}{c} + w_0^2}$$

entonces  $a=c=1$  y  $b=0 \Rightarrow$



$$R = \frac{1}{w_0 c}$$

luego si  $w_0=1 \Rightarrow R=C=1$  y

$$Q = \frac{1}{\sqrt{2}} \Rightarrow QR = \frac{1}{\sqrt{2}}$$

