# Crack Detection using Inductive Methods

Måns Bermell (mabe0395@student.umu.se) Joar Svartholm (josv0150@student.umu.se)

December 6, 2017

Abstract

## 1 Introduction

# 2 Theory

Light propagates through a medium at a lower velocity than in vaccum. This is described by the index of refraction of the medium

$$n = \frac{c_0}{v},\tag{1}$$

where  $c_0$  is the speed of light in vaccum and v is the velocity in the medium[1]. By this one can define the optical path length (OPL) as the length the light experiences, that is if the light propagates through a medium of length L and refractive index n, then the OPD will be

$$OPD = nL.$$

The refractive index is thus a measure of how dense a material is and must therefore be proportional to the pressure. Namely by increasing the pressure P from vaccum, then

$$n - 1 = \alpha \frac{\Delta P}{P_{atm}},\tag{2}$$

where  $P_{atm}$  is the atmospheric pressure and  $\alpha$  is the proportionality constant. Note that since P is measured from vaccum then  $\alpha = n - 1$  at atmospheric pressure.

#### 2.1 The Michelson Interferometer

A Michelson interferometer consists of a laser beam being splitted into a reference leg  $L_1$  and a signal leg  $L_2$ . The beams are then reflected back and reassembled at a sensor. A schematic sketch of this is found in Fig. 1. If the beams are aligned correctly they will interfere with each ocher and constructive interference will occur if

$$OPD = N\lambda, (3)$$

where OPD is the optical path difference between the legs, N is an integer and  $\lambda$  is the wavelength of the light.

#### 2.2 Method

If a gas chamber of length d is put on the sensor leg as is shown in Fig. 1 the the OPD can be found as

$$OPD = 2OPL_{L_2} - 2OPL_{L_1} = 2nd + const.$$
(4)

Using the interference condition Eq. (3) this can be reduced to

$$N\lambda = 2nd + \text{const.}.$$

Instead of counting the absolute number of interference maxima, called fringes, one can count the number of fringes that appear when changing the refractive index of the sample. This can then be rewritten as

$$\Delta N\lambda = 2d\Delta n. \tag{5}$$

If one measures this from vaccum one can make us of Eq. (2) in Eq. (5) and obtain

$$\Delta N = \frac{2d\alpha}{\lambda P_{atm}} \Delta P. \tag{6}$$

Thus, by increasing the pressure of a gas from vaccum and counting how many fringes that has passed a sensor one can find the refractive index from the slope of Eq. (6) and  $n = \alpha - 1$ .

# 3 Experimental setup

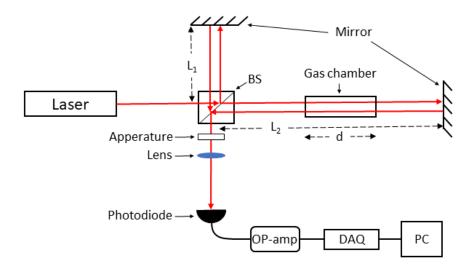


Figure 1 - Experimental setup.

## 4 Results and discussion

The number of fringes was plotted against the pressure change for the different gases and is found in Fig. 2. As one can see in the figures all gases showed a linear relation which was expected. When comparing Fig. 2b with the others the number of fringes is a lot lower than for the others. This means that the index of refraction must be a lot lower for this and the relative error will probably be larger. It also means that the relative error in the result will be quite larger in this result in comparison to the others.

The linear fit parameters are found in Tab. 1. As expected, the slope a for helium is a lot lower than the other slopes. From these slopes, the refractive indexes was estimated using Eq. (6) and tabulated in Tab. 2.

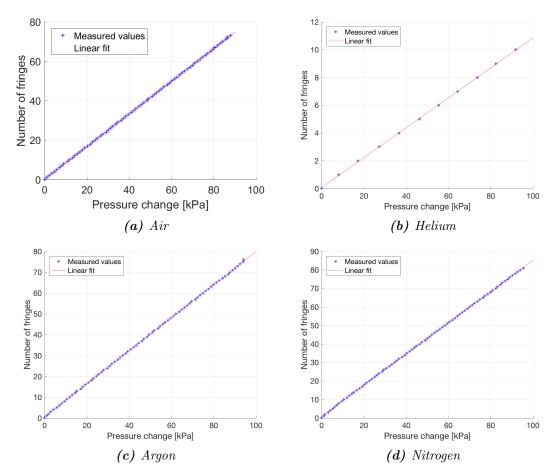


Figure 2 – Number of fringes and pressure change for the different gases with linear fits. Fitting parameters are found in Tab. 1

**Table 1** – Fitting parameters for the measured values in Fig. 2. Linear fit on the form  $y = \alpha x + \beta$ .

	$\alpha$	$\beta$
Air	$0.828(1) \text{ kPa}^{-1}$	0.16(6)
Helium	$0.108(1) \text{ kPa}^{-1}$	0.06(5)
Argon	$0.793(1) \text{ kPa}^{-1}$	0.61(5)
Nitrogen	$0.843(1) \text{ kPa}^{-1}$	0.86(5)

## References

[1] Nordling, C., 2006. Physics Handbook for Science and Engineering.

Table 2 – Estimated refractive indexes for the gases including tabulated values

	measured	tabulated	error
Air	1.00026410	1.00027116	7.05654305e-06
Helium	1.00003440	1.00003233	2.07707264e-06
Argon	1.00025283	1.00026106	8.23800429e-06
Nitrogen	1.00026891	1.00027646	7.55338923e-06