Lecture 5

Linear stability of parallel shear flows II

AE209 Hydrodynamic stability
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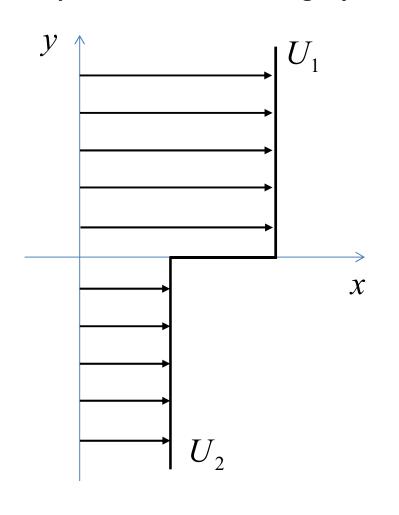
- 1. Linear stability analysis of inviscid mixing layer
- 2. Linearised equation for viscous parallel flows
- 3. Normal mode solution
- 4. Squire's transformation

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Example 1: Piecewise mixing layer



Base flow profile

$$U(y) = \begin{cases} U_1 & \text{for } y > 0 \\ U_2 & \text{for } y < 0 \end{cases}$$

Velocity ratio

$$R = \frac{U_1 - U_2}{U_1 + U_2} = \frac{\Delta U}{2\overline{U}}$$

Jump condition 1: Continuity of displacement

$$\frac{\widetilde{v}}{U-c} \qquad \text{at} \quad y=0$$

Jump condition 2: Continuity of pressure (force)

$$\widetilde{p} = \frac{i}{\alpha} [DU\widetilde{v} - (U - c)D\widetilde{v}]$$
 at $y = 0$

Summary:

Rayleigh equation

$$(U-c)(D^2-\alpha^2)\widetilde{v}-D^2U\widetilde{v}=0$$

with boundary conditions

$$\widetilde{v}(y=\infty) = \widetilde{v}(y=-\infty) = 0$$

and jump conditions

$$(U-c)D\widetilde{v} - DU\widetilde{v}$$
 and $\frac{\widetilde{v}}{U-c}$ are continuous at $y=0$

Solution

1) Rayleigh equation and the boundary condition gives

$$\widetilde{v}(y) = \begin{cases} Ae^{-\alpha y} \text{ for } y > 0 \\ Be^{\alpha y} \text{ for } y < 0 \end{cases} \text{ with } \alpha > 0$$

2) Apply the jump conditions

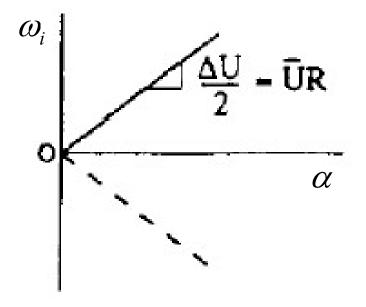
i)
$$-\alpha(U_1-c)A = \alpha(U_2-c)B$$

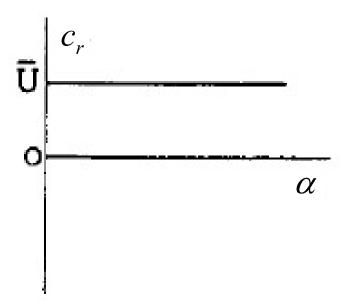
ii)
$$\frac{A}{\left(U_1 - c\right)} = \frac{B}{\left(U_2 - c\right)}$$

3) Solve the eigenvalue problem and obtain dispersion relation

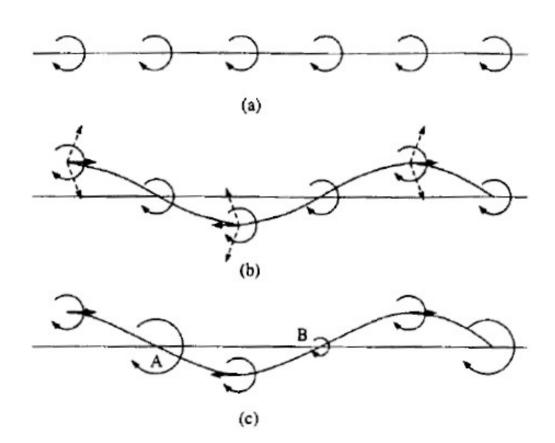
$$c = \overline{U} \pm \frac{i\Delta U}{2}$$

or
$$\omega = \alpha \overline{U} \pm i \alpha R \overline{U}$$





Physical mechanism



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Navier-Stokes equation

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \frac{1}{\text{Re}} \nabla^2 \mathbf{u}$$
$$\nabla \cdot \mathbf{u} = 0$$

Consider
$$\mathbf{u}(x, y, z, t) = (U(y), 0, 0) + \varepsilon \mathbf{u}'(x, y, z, t),$$

 $p(x, y, z, t) = P(x, y) + \varepsilon p'(x, y, z, t)$

and neglect the terms at $O(arepsilon^2)$. Then,

Linearised Navier-Stokes equation around parallel base flow

$$\frac{\partial u'}{\partial t} + U \frac{\partial u'}{\partial x} + v' \frac{dU}{dy} = -\frac{\partial p'}{\partial x} + \frac{1}{Re} \left(\frac{\partial^2 u'}{\partial x^2} + \frac{\partial^2 u'}{\partial y^2} + \frac{\partial^2 u'}{\partial z^2} \right)$$

$$\frac{\partial v'}{\partial t} + U \frac{\partial v'}{\partial x} = -\frac{\partial p'}{\partial y} + \frac{1}{Re} \left(\frac{\partial^2 v'}{\partial x^2} + \frac{\partial^2 v'}{\partial y^2} + \frac{\partial^2 v'}{\partial z^2} \right)$$

$$\frac{\partial w'}{\partial t} + U \frac{\partial w'}{\partial x} = -\frac{\partial p'}{\partial z} + \frac{1}{Re} \left(\frac{\partial^2 w'}{\partial x^2} + \frac{\partial^2 w'}{\partial y^2} + \frac{\partial^2 w'}{\partial z^2} \right)$$

$$\frac{\partial u'}{\partial x} + \frac{\partial v'}{\partial y} + \frac{\partial w'}{\partial z} = 0$$

Velocity and vorticity form of linearised Navier-Stokes equation

$$\left[\left(\frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) \nabla^2 - \frac{d^2 U}{dy^2} \frac{\partial}{\partial x} - \frac{1}{\text{Re}} \nabla^4 \right] v' = 0$$

$$\left(\frac{\partial}{\partial t} + U \frac{\partial}{\partial x} - \frac{1}{\text{Re}} \nabla^2\right) \eta' + \frac{dU}{dy} \frac{\partial v'}{\partial z} = 0$$

with the boundary condition,

$$v' = \frac{\partial v'}{\partial n} = \eta' = 0$$
 at solid boundary and/or the far field

and the initial condition,

$$v'(x, y, z, t = 0) = v'_0(x, y, z)$$

$$\eta'(x, y, z, t = 0) = \eta'_0(x, y, z)$$

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Consider full three-dimensional case such that

$$\left[\left(\frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) \nabla^2 - \frac{d^2 U}{dy^2} \frac{\partial}{\partial x} - \frac{1}{\text{Re}} \nabla^4 \right] v' = 0$$

$$\left(\frac{\partial}{\partial t} + U \frac{\partial}{\partial x} - \frac{1}{\text{Re}} \nabla^2 \right) \eta' + \frac{dU}{dy} \frac{\partial v'}{\partial z} = 0$$

Then, the normal mode solution takes the following form:

$$v'(x, y, z, t) = \widetilde{v}(y)e^{i(\alpha x + \beta z - \omega t)} + c.c$$
$$\eta'(x, y, z, t) = \widetilde{\eta}(y)e^{i(\alpha x + \beta z - \omega t)} + c.c$$

where $\alpha, \beta \in R$ and $\omega \in C$.

Orr-Sommerfeld equation (for wall-normal velocity):

$$\left[\left(-i\omega + i\alpha U \right) \left(D^2 - k^2 \right) - i\alpha D^2 U - \frac{1}{\text{Re}} \left(D^2 - k^2 \right)^2 \right] \widetilde{v} = 0$$

Squire equation (for wall-normal vorticity):

$$\left[\left(-i\omega + i\alpha U \right) - \frac{1}{\text{Re}} \left(D^2 - k^2 \right) \right] \widetilde{\eta} = -i\beta DU \widetilde{v}$$

where $k^2 = \alpha^2 + \beta^2$ with boundary conditions:

$$\widetilde{v}=D\widetilde{v}=\widetilde{\eta}=0$$
 at a solid wall and in the far field.

Remark

If $\alpha, \beta \in R$ are given, then $\omega \in C$ becomes unknown with \widetilde{v} and $\widetilde{\eta}$ Resulting in an **eigenvalue problem** as in Rayleigh equation.

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Squire transformation

Theorem: Damped Squire modes

The solutions to the Squire equation are always damped, i.e. $\omega_i < 0$ for all α, β and Re .

Remark

Instability comes from Orr-Sommerfeld equation.

Consider the Orr-Sommerfeld equation for $\beta = 0$ in the following form:

$$\[(U-c)(D^2 - \alpha_{2D}^2) - D^2 U - \frac{1}{i\alpha_{2D} \operatorname{Re}_{2D}} (D^2 - \alpha_{2D}^2)^2 \] \widetilde{v} = 0$$

Now, consider the Orr-Sommerfeld for $\beta \neq 0$ by setting $\operatorname{Re}_{3D} = \frac{\alpha}{k}\operatorname{Re}$

$$\[(U-c)(D^2-k^2)-D^2U-\frac{1}{ik\operatorname{Re}_{3D}}(D^2-k^2)^2 \] \widetilde{v}=0$$

It follows that the critical Reynolds numbers for the onset of an instability should be α

$$Re_{2D,c} = Re_{3D,c} = \frac{\alpha}{k} Re_c,$$

indicating that

$$Re_{2D,c} < Re_c$$

Theorem: Squire

Given Re_L as the critical Reynolds number for the onset of linear instability for a given α and β , the Reynolds number Re_c below which no exponential instabilities exist for any wave numbers satisfies

$$\operatorname{Re}_{c} \equiv \min_{\alpha,\beta} \operatorname{Re}_{L}(\alpha,\beta) = \min_{\alpha} \operatorname{Re}_{L}(\alpha,0)$$

Remark

The most unstable linear instability is always two dimensional.

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- 1. Linear stability analysis of inviscid mixing layer
- 2. Linearised equation for viscous parallel flows
- 3. Orr-Sommefed and Squire equation
- 4. Squire's transformation and theorem