## Galactic Astronomy: Problem Set 2

Jonas Powell, Wesleyan University February 20, 2019

Due: Thursday, Feb. 21 by midnight. Late papers are not accepted. If you cannot complete the assignment, hand in what you have completed before the deadline. Consider the deadline to be like the boarding time for an airplane, or the deadline for a grant submission to NASA or NSF. If you miss the deadline, you do not get on the airplane, no matter how good your excuse is. If you miss an NSF or NASA deadline, you do not get the grant, no matter how good your project is. The best advice is ... finish early. You can submit multiple times, right up to the deadline. Whatever your latest submission is, when the deadline occurs, is what will be graded.

**Problem 1.** There is a small error in the book in the first paragraph of Section 2.3. What is the correction required?

**Answer 1.** In that first paragraph, the author gives the wrong units for  $f_{\nu}$ , saying that it comes in units of W m<sup>-2</sup> s<sup>-1</sup> Hz<sup>-1</sup>. This is wrong; the units should be power per area per frequency, meaning that the inverse time term that they have is unnecessary. The correct units are W m<sup>-2</sup> Hz<sup>-1</sup>.

**Problem 2.** Estimate the effective temperature of a star with the following properties, by fitting a black body curve to its flux density distribution:

$$B = 9.31, V = 8.94, J = 8.11, H = 7.93, K = 7.84$$

Plot the data and the black body that you chose as your best fit to the data and attach the plot to your answer. You can make this fit simply by eye, or you can use a more sophisticated fitting process – it is up to you. Based on the color of the star, estimate its spectral type, neglecting interstellar reddening. Compare the effective temperature based on the black body fit to the one based on the spectral type of the star and comment on the difference. Assuming that the star has luminosity class V, what is its distance, again neglecting interstellar reddening?

**Answer 2.** To fit the data, we first convert them from magnitudes to flux densities by recalling:

$$f_{\nu} = \text{zpf } 10^{-0.4 M},$$

where ZPF is the spectral band's zero-point flux (given on the course Moodle page), and M is the star's magnitude in the spectral band. As a model, we will use a blackbody curve, given by Planck's Law:

$$B(\nu, T) = \frac{2h\nu^3}{c^2} \frac{1}{e^{\frac{h\nu}{k_BT}} - 1}$$

However, Planck's law returns brightness (or specific intensity), but we would like to have it in units of flux density, to match our data. This is something of a problem, since the relationship between the two is given by

$$f_{\nu} \approx \int_{\text{source}} B(\nu, T) d\Omega$$
  
  $\approx \Omega_0 B(\nu, T),$ 

where  $\Omega$  is the solid angle subtended by the source. Since astronomical sources are very far away, this solid angle is bound to be extremely small, meaning that the resulting scaling factor,  $\Omega_0$ , between  $B(\nu)$  and  $f_{\nu}$  will be an extremely small number. Further complicating this is the fact that, since we don't know the star's distance, we don't know the solid angle it subtends anyways. Therefore, we must now fit both for temperature, T, as well as for  $\Omega_0$ .

Since I find manually fitting two dimensions by hand to be a bit tedious, I decided to fit the two dimensions using a Markov Chain Monte Carlo (MCMC) routine. MCMC is a valuable tool for modeling in astronomy, and the field has benefited greatly from the Python package emcee (Foreman-Mackey et al. 2012), which makes this algorithm accessible fairly easily. MCMC works by sampling, in a pseudo-random walk, the probability distribution for a given parameter space, which means that not only is a best-fit value accessible (at the high-point of that distribution), but so too is an approximation of the distribution itself, which is an extremely informative feature to have.

To run my MCMC, I developed a probability function that sampled a blackbody curve of a given temperature at the frequencies of the given data, then calculated a  $\chi^2$  value between the data and model ( $\chi^2 = \sum_i (\text{data} - \text{model})^2$ ), which was then turned into a log-probability (ln prob =  $-0.5\chi^2$ ) value and fed back into the MCMC run, informing the run's next step. The log-probabilities are shown in Fig. in  $\Omega_0 - T$  parameter space.

As we see, there is some degree of degeneracy between the two parameters. This is somewhat reasonable, since increases in temperature and solid angle-subtended will both result in increased flux density for a source. However, the resulting fit (Fig ) looks pretty splendid, returning a best-fit temperature of 6745 K, which is characteristic of an F3 star. This is quite close to the F2 stellar type that is predicted by the star's 0.37 B-V color, indicating that the star is either truly an F3 that has been a bit reddened, or it is an F2 star that is slightly too cool.

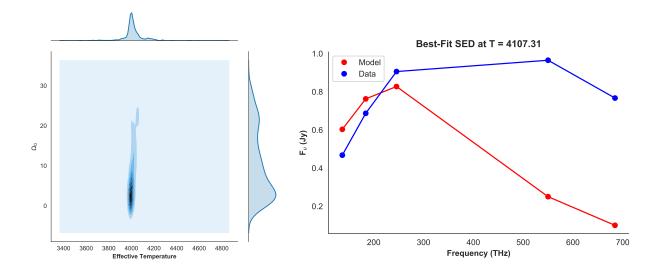


Figure 1: Results from an MCMC fitting run. The kernel-density estimate (KDE) on the left characterizes the probability distribution of points in  $\Omega_0 - T$  parameter space, where darker regions correspond to better fits. On the right, data and best-fit model are overlaid, demonstrating that a good solution was found.

**Problem 3.** Given the information on a fictitious star, as listed in the table below, determine its other properties. Present your results as a table and explain each calculation in comments below the table.

Table of data on a fictious star				
$\alpha, \delta$	13:42:25.6, -7:13:42.1 (J2000.00)			
$\mu$	$13.7 \text{ mas y}^{-1}$			
PA	122			
$\mathbf{v}_r$	$-13 \ {\rm km} \ {\rm s}^{-1}$			
V	10.86			
B-V	1.63			
$\operatorname{SpT}$	K2V			

**Properties for you to determine and tabulate:** (l,b),  $M_V$ , E(B-V),  $A_V$ , d, the magnitude of heliocentric space velocity ( $v_{space}$ ),  $M_{bol}$ ,  $L/L_{\odot}$ ,  $T_e$ ,  $R/R_{\odot}$ , and  $M/M_{\odot}$ . Explain how you obtained each of the requested quantities in comments below the table. In addition, comment on the likely age and chemical composition of this star and whether it is likely to have a planetary system. As always, justify your answers.

## Results

l, b	$(324.52^{\circ}, 53.49^{\circ})$
$\mathrm{M}_V$	6.19
E(B-V)	0.75
$\mathrm{A}_V$	2.25
d	$30.48~\mathrm{pc}$
$V_{space}$	$2628 \rm \ km \ s^{-1}$
$M_{bol}$	5.9
$\mathrm{T}_e$	5040
${ m L/L_{\odot}}$	0.27
${ m M}/{ m M}_{\odot}$	0.72
$\rm R/R_{\odot}$	0.68

Answer 3. How I found these values: Many of these questions required looking up values in a table. For any question where this was the case (i.e. where I say "I looked up this value"), the table I am referring to can be found here: http://www.pas.rochester.edu/~emamajek/EEM\_dwarf\_UBVIJHK\_colors\_Teff.txt

**l, b**: Using the calculator I made for the last problem set, I found that the (l, b) coordinates of this source are (324.52°, 53.49°).

E(B-V): Recalling the definition  $E(B-V) = (B-V) - (B-V)_0$ , where the first term is the observed color and the second term is the color we would expect from a star of this spectral type, we just have to look up this expected color and subtract it from the given B-V color. I looked up a value of  $(B-V)_0 = 0.884$  for a K2V star which yields a value of E(B-V) = 0.75.

 $\mathbf{A}_V$ : Recalling the definition  $A_V = 3.1$  E(B-V), we may just multiply our existing answer by 3.1. Doing so, we find  $A_V = 2.25$ .

 $\mathbf{M}_V$ : Looking up in our table, we find that for a K2V star,  $\mathbf{M}_V = 6.19$ .

 $\mathbf{M}_{bol}$ : We recall that  $\mathbf{M}_{bol} = M_V + BC_V$ , where  $BC_V$  is the Bolometric Correction in the V-band, and can be looked up to be -0.29. This yields a result of  $\mathbf{M}_{bol} = \mathbf{M}_V + \mathbf{BC}_V = 6.19$  - 0.29 = 5.9.

**d**: We may rearrange the magnitude equation for distance:

$$V - M_V = 5 \log d - 5 + A_V$$
  
 $\rightarrow \log d = \frac{V - M_V - A_V + 5}{5} = 1.48$   
 $\rightarrow d = 10^{1.48}$   
 $= 30.48 \text{ pc}$ 

 $\mathbf{v}_{space}$ : The space velocity is the triangulation of the proper motion,  $\mu$ , and the radial velocity, i.e.  $v_{space} = \sqrt{v_{rad}^2 + v_{trans}^2}$ . To solve this, we must turn proper motion into a velocity, using the familiar equation,  $v_{trans} = 4.74 \ \mu \ d = 4.74 \ (13.7)(30.48) = 2628 \ \mathrm{km \ s^{-1}}$ . Therefore,  $v_{space} = \sqrt{(13)^2 + (2628)^2} \approx 2628 \ \mathrm{km \ s^{-1}}$ . This feels way too high, but I don't really have any justification to back up that intuition and the math seems tight, so I guess that's what I'll submit.

 $\mathbf{T}_{eff}$ : Looking it up, we find that for a K2V star,  $\mathbf{T}_{eff} = 5040$ .

 ${f L}/{f L}_{\odot}$ : Since luminosity and magnitudes are related as  $M-M_{\odot}=-2.5\log\frac{L}{L_{\odot}}$ , then we may look up values for M and  $M_{\odot}$  and find  $\frac{L}{L_{\odot}}=10^{-0.4~(M-M_{\odot})}=10^{-0.4~(6.19-4.79)}=0.27$ 

 $\mathbf{M}/\mathbf{M}_{\odot}$ : From the Mass/Luminosity relation, we know that  $\frac{M}{M_{\odot}} = \frac{L}{L_{\odot}}^{1/4} = 0.72$ 

 $\mathbf{R}/\mathbf{R}_{\odot}$ : We may find the radius by first recalling:

$$T_{eff}^4 = \frac{L}{4\pi R^2 \sigma}$$

Since we know  $T_{eff}$  for our fictional star and the Sun (another lookup reveals that a G2V's effective temperature is 5770), and we know the two's luminosity ratio, we may construct the following ratio by rearranging the above equation and solving for the radius relationship:

$$\frac{L}{L_{\odot}} = \frac{4\pi R^2 T_{eff}^4}{4\pi R_{\odot}^2 T_{eff,\odot}^4}$$

$$\rightarrow \frac{R}{R_{\odot}} = \sqrt{\frac{L}{L_{\odot}} \left(\frac{T_{eff,\odot}}{T_{eff}}\right)^4}$$

$$= \sqrt{0.27 \times \left(\frac{5770}{5040}\right)^4}$$

$$= 0.68$$

Thus,  $R/R_{\odot} \approx 0.55$ .

Given that this is a K-star, we expect it to have a high metallicity. Lower mass stars tend to live much longer, so it is more likely that this star is an older star than it's higher-mass companions.

To determine the star's planet forming potential, I decided to see what the real data say about planets around this type of star. To do so, I used the Python package kplr, an API wrapper of the Kepler database's data portal, to download information about ~2300 planets. Each planet's information contained a field with information about it's host star. This allowed me to develop my own little database with features like metallicity, effective temperature, colors, and so on for each confirmed planet's host.

Unfortunately, one feature that my database did not yet contain was spectral type. This is obviously critical, since the whole point of this little project was to determine the relative frequency of planets around stars by spectral type. I decided to use effective temperature as a spectral type proxy, since it goes linearly with spectral type and I had access to good data on the spectral class/ $T_{eff}$  relationship. To do this, I copied, processed, and tabulated the table that I used above for other reference values into a robust dataframe in Python. I was then able to iterate through each star in my database, cross-check its reported  $T_{eff}$  against the list of effective temperatures in the linked table, and label the star with the spectral type attached to the nearest  $T_{eff}$  value in the linked table. This is a somewhat sketchy way of

spectral-typing stars and, were this a more serious project, is definitely something I would give more thought to, but for the time being, it gave me a good, quick way to get approximate spectral types.

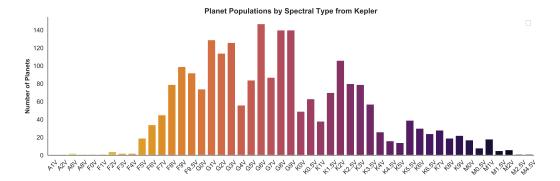


Figure 2: Planetary populations around stars of different spectral types, drawn from Kepler data. Unfortunately, it's hard to set photos in a two-column layout, so the inclusion of this plot forced me back into a one-column submission. Still, I'm really excited about how the plot turned out, so I think it's worth it.

Once I had these types, it was simply a matter of making an histogram of the results.

## Planet Counts by Spectral Class

A	F	G	K	Μ
5	378	1097	760	56

We can see from Table that K stars have the second most detections of planets orbiting them, trailing only our beloved G stars. This indicates that planet-forming potential is likely high. Zooming in on this particular star's subtype, a K2V star, we see from Fig 2 that this specific class actually has the highest planetary detection rate of all K-stars, and the seventh highest rate overall. Therefore, from this data, I would say its planet-forming potential is high.

NOTE: I have entirely ignored, of course, the very significant issue of detection bias in this dataset. For example, we know that planets are extremely common around M-dwarfs, but since they are faint and hard to detect, they are underrepresented in this distribution. Still, since this is nothing more than a first-order diagnostic and the fictious star in question happens to be of a spectral type that has lots of observed planets, I think it's a reasonable sacrifice to make. Also, while it might not be enormously informative of the "true" planet-forming potential, it certainly is a useful way to predict how likely it is that we'd actually be able to find a planet around it. Finally, my data is all from the Kepler mission; a more robust implementation would, at the very least, also draw on K2 data and hopefully would reach out to other telescopes as well.

**Problem 4.** Fun with magnitudes and colors! If a star with a parallax of 25 mas that initially appears to be single and is measured to have V=6.50, later turns out to be a spectroscopic binary with equal mass components, what is the apparent magnitude of each component? Neglecting reddening, what is the absolute magnitude of each component? If that same star has a measured B-V=1.25, what is the B-V of each component?

**Answer 4.** Since magnitude is given by

$$V = -2.5 \log \frac{f}{f_0},$$

then f, the flux of a star, is

$$f/f_0 = 10^{-0.4 \text{ V}}$$

Therefore, given that the V-magnitude of a binary is V=6.5, then we know that

$$(f_1 + f_2)/f_0 = 10^{-0.4 V}$$
  
= 0.0025

Given that the two sources have the same mass, we may draw on the Mass-Luminosity relationship (and recall that flux is just distance-scaled luminosity) to infer that they have the same fluxes. Therefore, the flux of one of the sources is

$$f_1/f_0 = \frac{0.0025}{2}$$

We can now plug this value back into our original equation for magnitude and find a single source's contribution.

$$V = -2.5 \log \frac{f_1}{f_0}$$
  
= -2.5 \log (1.25 \times 10^{-3})  
= 7.26

We find a final apparent V magnitude of 7.26 for each star. To find the B-V color of each component, we can play the same game as above, just in the B-band. Again,

$$B = -2.5 \log \frac{f}{f_0}$$
$$\to f/f_0 = 10^{-0.4 B}.$$

Since our apparent B-magnitude is B = 1.25 + (V = 6.5) = 7.75, then:

$$(f_1 + f_2)/f_0 = 10^{-0.4 B}$$
  
=  $7.94 \times 10^{-4}$ 

Again, we may recall that the two sources have the same mass and thus the same flux contributions, so

$$f_1/f_0 = \frac{0.000794}{2}$$

We can now plug this value back into our original equation for magnitude and find a single source's contribution.

$$B = -2.5 \log \frac{f_1}{f_0}$$
= -2.5 log (3.97 × 10<sup>-4</sup>)
= 8.51

We see that each source has an apparent B-magnitude of 8.51, resulting in B-V color of 8.51-7.26 = 1.25, the same as the binary's combined color. I guess this is fairly obvious; the combined color of two identical sources should be the same as the color of each source. Still, it's pretty neat to get to walk through the actual equations themselves and see that that relationship does, in fact, hold.

To find the star's absolute magnitude, we recall the relationship between apparent magnitude, absolute magnitude, and distance.

$$V - M = 5\log d - 5 + A_V$$

Here  $d = \frac{1}{25 \text{ mas}} = 400 \text{ pc}$  and  $A_V$ , the reddening, is taken to be zero. Therefore,

$$M = V - 5\log 400 + 5 + 0$$
  
= -0.75,

so each star has an absolute magnitude in the V-band of -0.75. This is quite bright, perhaps a bit brighter than what I'd expect, but I guess it is quite far away, so maybe that does make sense.

**Problem 5.** More fun with magnitudes and colors! Suppose a binary system is composed of an A star, with V = 7.80 and B-V = 0.00, and a K star, with V = 8.20 and B-V = +1.50. If the stars are so close together on the sky that that they cannot be resolved as individual objects (i.e. an unresolved binary), what will be the measured V magnitude and B-V color of the "star" (that is actually the combined light of both components)?

**Answer 5.** We may use the same logic as before again to find the star's fluxes in each band and then work backward to single-source magnitudes.

$$f_{A,V}/f_0 = 10^{-0.4} V_{A,V}$$

$$= 7.59 \times 10^{-4}$$

$$f_{A,B}/f_0 = 10^{-0.4} V_{A,B}$$

$$= 7.59 \times 10^{-4}$$

$$f_{B,V}/f_0 = 10^{-0.4} V_{B,V}$$

$$= 5.25 \times 10^{-4}$$

$$f_{B,B}/f_0 = 10^{-0.4} V_{B,B}$$

$$= 1.32 \times 10^{-4}$$

Combining sources A and B's V-band and B-band fluxes, we find:

$$V_{both} = -2.5 \log [(7.59 + 5.25) \times 10^{-4}]$$

$$= 7.23$$

$$B_{both} = -2.5 \log [(7.59 + 1.32) \times 10^{-4}]$$

$$= 7.96$$

Solving, we find that the binary would present as a star with V=7.23, B-V=0.73.

```
<sup>2</sup> Calculations for Problem Set 2
3 Galactic Astronomy
4 Due Feb. 14
5
7 import sys
8 import emcee
9 import cPickle
10 import numpy as np
11 import pandas as pd
12 import seaborn as sns
13 import astropy.units as u
14 import matplotlib.pyplot as plt
15 from astropy.coordinates import SkyCoord, Angle, get_constellation
from astropy.constants import c, h, k_B
  from collections import Counter
  from inspect import *
  sns.set_style('white')
20
  # Load the data for problem 2
mags = [9.31, 8.94, 8.11, 7.93, 7.84]
23
24
25
26
  # Problem 2
28
  def spectrum(t, coeff, show=False):
29
30
      temp = t * u.K
31
      mags = [9.31, 8.94, 8.11, 7.93, 7.84]
32
      wavelengths = [0.438 * u.um, 0.545 * u.um, 1.22 * u.um, 1.63 * u.um, 2.19]
33
      freqs = [(c/(lam).decompose()).to('Hz') for lam in wavelengths] # Hz
34
35
      unit_nu = (1e-20 * u.erg / (u.cm**2 * u.s * u.Hz)).to('Jy')
36
      zpfs_nu = [4.063 * unit_nu, 3.636 * unit_nu, 1.589 * unit_nu, 1.021 *
37
      unit_nu, 0.64 * unit_nu
      data_f_nu = [zpf * 10**(-0.4*mag) for mag, zpf in zip(mags, zpfs_nu)]
38
39
      fudge = (coeff * 1e18*u.Jy)**(-1)
40
      model_f_nu = [((2 * h * nu**3 * c**(-2)) / (-1 + np.exp(h * nu/(k_B * temp)))]
41
      )))).to('Jy') * fudge
                    for nu in freqs]
42
43
      freqs_thz = [nu.to('THz').value for nu in freqs]
44
      model = [f.value for f in model_f_nu]
45
      data = [f.value for f in data_f_nu]
46
47
48
       if show:
49
           plt.show()
50
```

```
else:
51
52
           pass
       return (freqs_thz, model, data)
54
55
56
57
  def lnprob(p, mags, priors, save=False):
58
      t, coeff = p
59
60
      # Check on priors:
61
       for param, prior in zip(p, priors):
62
           if not prior['min'] < param < prior['max']:</pre>
63
               return -np.inf
64
65
66
      temp = t * u.K
      wavelengths = [0.438 * u.um, 0.545 * u.um, 1.22 * u.um, 1.63 * u.um, 2.19]
67
       freqs = [(c/(lam).decompose()).to('Hz') for lam in wavelengths] # Hz
68
69
70
       unit_nu = (1e-20 * u.erg / (u.cm**2 * u.s * u.Hz)).to('Jy')
71
       zpfs_nu = [4.063 * unit_nu , 3.636 * unit_nu , 1.589 * unit_nu , 1.021 *
72
      unit_nu, 0.64 * unit_nu
       data_f = [zpf * 10**(-0.4*mag) for mag, zpf in zip(mags, zpfs_nu)]
74
       fudge = (coeff * 1e18*u.Jy)**(-1)
75
      model_f_nu = [((2 * h * nu**3 * c**(-2)) / (-1 + np.exp(h * nu/(k_B * temp)))]
76
      ))))).to('Jy') * fudge
                     for nu in freqs]
77
78
       freqs4plotting = [nu.to('THz').value for nu in freqs]
79
      model = np.array([f.value for f in model_f_nu])
80
       data = np.array([f.value for f in data_f_nu])
81
82
       chisq = np.sum((model - data)**2)
83
      lnp = -0.5 * chisq
84
       return lnp
85
86
87
88
  def run_mcmc(mags=mags, nsteps=1000):
89
90
      ndim, nwalkers = 2, 30
91
       priors_t = \{ 'min' : 0, 'max' : 20000 \}
92
       priors\_coeff = \{ 'min': 0, 'max': 30 \}
93
       priors = [priors_t, priors_coeff]
94
95
      p0 = np.random.normal(loc=(4000, 4), size=(nwalkers, ndim))
96
      sampler = emcee. EnsembleSampler (nwalkers, ndim, lnprob, args=[mags, priors
97
      pos, prob, state = sampler.run\_mcmc(p0, 10)
98
      prob
99
```

```
sampler.reset()
100
       print "Finished burn-in; starting full run now."
101
       # sampler.run_mcmc(pos, nsteps)
       run = sampler.sample(pos, iterations=nsteps, storechain=True)
104
       steps = []
       for i, result in enumerate(run):
106
           # Maybe do this logging out in the Inprob function itself?
107
           pos, lnprobs, blob = result
108
           new\_step = [np.append(pos[k], lnprobs[k])  for k in range(nwalkers)]
111
           steps += new_step
112
           sys.stdout.write("Completed step {} of {} \r".format(i, nsteps))
113
           sys.stdout.flush()
       df = pd.DataFrame(steps)
       df.columns = ['temp', 'coeff', 'lnprob']
118
       print "Finished MCMC."
119
       print ("Mean acceptance fraction: {0:.3f}".format(np.mean(sampler.
120
      acceptance_fraction)))
121
      # xlims, ylims = (priors_t ['min'], priors_t ['max']), (priors_coeff ['min'],
       priors_coeff['max'])
124
       return (sampler, df)
126
127
128
  def mcmc_full_driver(prev_run=None, nsteps=20, save=False):
129
130
       plt.close()
       # First, execute the MCMC run. If one is passed as an argument, don't.
       if not prev_run:
133
           sampler, df = run_mcmc(nsteps=nsteps)
135
       else:
           sampler, df = prev_run
136
      # Now make some plots.
138
       jp = sns.jointplot(x=sampler.flatchain[:,0], y=sampler.flatchain[:,1],
139
                           kind="kde")
140
       jp.set_axis_labels('Effective Temperature', r"$\Omega_0$", weight='bold')
       plt.tight_layout()
142
       if save:
143
           plt.savefig('prob2_kde.pdf')
144
           print "Saved plot to prob2_kde.pdf"
145
       else:
146
           plt.show()
147
148
149
      # Get the data for the SED.
150
```

```
t = df[df['lnprob'] = max(df['lnprob'])]['temp']. values[0]
151
       coeff = df[df['lnprob'] = max(df['lnprob'])]['coeff'].values[0]
       freqs, model, data = spectrum(t, coeff, show=False)
       print "Got spectrum."
154
       plt.plot(freqs, model, 'or', label='Model')
156
       {\tt plt.plot(freqs\;,\;data\;,\;'ob'\;,\;label='Data')}
       plt.plot(freqs, model, '-r')
158
       plt.plot(freqs, data, '-b')
       plt.xlabel('Frequency (THz)', weight='bold')
161
       plt.ylabel(r"F_{-}\{ \setminus nu \}  (Jy)", weight='bold')
163
       plt.title("Best-Fit SED at T = {}".format(round(t, 2)), weight='bold')
164
       plt.legend()
166
       plt.tight_layout()
       sns.despine()
167
168
       if save:
169
           plt.savefig('prob2_spectrum.pdf')
           print "Saved plot to prob2_spectrum.pdf"
       else:
           plt.show()
173
174
   mcmc_full_driver(save=True)
175
177
178
179
  # Problem 3
180
181
   test\_coords = ['04h37m48s', '-0d21m25s']
182
183
   pos_radec = ('13h42m25.6s', '-7d13m42.1s')
   def radec_to_galactic_astropy(pos_radec):
185
186
       Convert RA/dec coordinates to galactic (1, b) coordinates.
188
       Args: coords (tuple of strs): RA, dec values in a format understood
189
                                       by astropy.coordinates.Angle
190
       Returns: (1, b) tuple, in degrees.
       ra_hms, dec_hms = Angle(pos_radec[0]), Angle(pos_radec[1])
       radec_coords_deg = SkyCoord(ra=ra_hms, dec=dec_hms, frame='icrs')
       galactic_coords_str = radec_coords_deg.transform_to('galactic').to_string
195
       galactic_coords_degs = [float(coord) for coord in galactic_coords_str.
196
      split('')]
       return galactic_coords_degs
198
   def radec_to_galactic(coords):
199
200
       Convert RA/dec coordinates to galactic (1, b) coordinates by hand.
201
```

```
202
        Sources:
203
            NGP coords taken from:
204
            https://en.wikipedia.org/wiki/Galactic_coordinate_system
205
206
            Conversion formula adapted from:
207
            http://www.atnf.csiro.au/people/Tobias.Westmeier/tools_coords.php
208
        Args:
209
            coords (tuple of strs): RA, dec values in a format understood
210
                                               by astropy.coordinates.Angle
        Returns: (1, b) tuple, in degrees.
213
214
        def gross_coords_to_rads(coords):
215
            ra, dec = coords
            coords = SkyCoord(ra=ra, dec=dec, frame='icrs')
217
            ra_rad, dec_rad = [float(a) * np.pi/180]
218
                                  for a in coords.to_string().split()]
219
            return (ra_rad, dec_rad)
221
       ra, dec = gross_coords_to_rads(coords)
       ra_NGP, dec_NGP = gross_coords_to_rads(['12h51m26.00s', '+27d 7m 42.0s'])
       1_NCP = 122.93 * np.pi/180
224
225
       b = np. arcsin(np. sin(dec\_NGP) * np. sin(dec) \setminus
                       + \text{ np.} \cos(\text{dec\_NGP}) * \text{np.} \cos(\text{dec}) \setminus
                        * np.cos(ra - ra_NGP))
228
       x1 = np.cos(dec) * np.sin(ra - ra_NGP)
230
       x2 = np.cos(dec_NGP) * np.sin(dec)
231
             - \text{ np. sin} (\text{dec\_NGP}) * \text{np. cos} (\text{dec}) * \text{np. cos} (\text{ra} - \text{ra\_NGP})
232
       # Arctan2 is basically a smart version of \arctan(x1/x2)
234
       1 = 1-NCP - np.arctan2(x1, x2)
235
236
       # Convert to degrees and round out to 4 decs for prettiness.
237
       l, b = round(l * 180/np.pi, 4), round(b * 180/np.pi, 4)
        return [1, b]
239
240
241
242
243
244 # Kepler populations
   def plot_planet_pops_by_stellar_type(cmap='inferno_r', spectral_grouping=False
246
       , save=True):
247
       # cmaps: viridis, Spectral, ocean, inferno
248
        host_stars_df = pd.read_csv('plotting_data.csv')
250
251
        if spectral_grouping:
252
            fig, ax = plt.subplots(figsize = (10, 6))
253
```

```
254
           sns.countplot(x=host_stars_df['spectral_group'], palette=cmap, ax=ax)
255
           # sns.countplot(x=host_stars_df['spectral_group'], palette='ocean', ax
257
      =ax2
258
           ax.legend().remove
259
           ax.set_ylabel('Number of Planets', weight='bold')
260
           ax.set_xlabel('Spectral Type', weight='bold')
261
           ax.set_title('Planet Populations by Spectral Type from Kepler', weight
262
      ='bold')
263
           sns.despine()
264
           if save:
265
               plt.savefig('planet_dist_by_spectral_group.pdf')
266
267
           else:
                plt.show()
268
       else:
269
           labs = []
270
           for id in sorted(list(set(host_stars_df['spt_id']))):
271
               spt_name = host_stars_df[host_stars_df['spt_id'] == id]['spt'].
      values [0]
               labs.append(spt_name)
273
274
           fig, ax = plt.subplots(figsize = (14, 4))
           # fig, (ax1, ax2) = plt.subplots(1, 2, figsize = (15, 7))
276
           sns.countplot(x=host_stars_df['spt_id'], palette=cmap, ax=ax)
278
279
           ax.legend().remove
280
           ax.set_ylabel('Number of Planets', weight='bold')
281
           ax.set_xlabel('Spectral Type', weight='bold')
282
           ax.set_title('Planet Populations by Spectral Type from Kepler', weight
283
      ='bold')
           ax.set_xticklabels(labs, rotation=45)
284
           sns.despine()
287
           if save:
288
                plt.savefig('planet_dist_by_spt.pdf')
           else:
290
               plt.show()
294 # Counter(host_stars_df['spt'])
295 # host_stars_df
  # sorted (Counter (host_stars_df['spt']).values())
    host_stars_df['spt_id']/Counter(host_stars_df['spt_id']).values()
297
298
# stellar_info = pd.read_csv('spectraltype_data.csv')
  # stellar_info[stellar_info['SpT'] == 'G2V']['Mv']
```

```
303
304
305
306
307
308
309
310
311
312
312
313 # The End

1 """
2 Gather, clean, and organize data on stellar types. Drawn from:
3 http://www.pas.rochester.edu/~emamajek/EEM_dwarf_UBVIJHK_colors_Teff.txt
"""
```

```
6 import pandas as pd
7 import numpy as np
8 import cPickle
  import kplr
10
  import sys
11
12
  def export_spectral_type_info():
       headers_list = filter (None, headers.split(','))
14
15
       all_stars = o_stars + b_stars + a_stars + f_stars + g_stars + k_stars +
16
      m_stars
      df_{-}unbound = []
17
       spt_id = 0
18
       for stellar_type in all_stars:
20
           d = \{\}
           # Get a list of feature values
21
           spt_features = filter(None, stellar_type.split(''))
22
           for i in range(len(headers_list)):
23
               try:
                    feature = float (spt_features [i])
25
               except ValueError:
26
                    feature = spt_features[i]
                    feature = np.nan if '...' in feature else feature
28
29
30
               d[headers_list[i]] = feature
31
           d['spt_id'] = spt_id
32
           spt_id += 1
33
34
           df_unbound.append(d)
35
       df = pd. DataFrame (df_unbound)
36
37
       df.to_csv('spectraltype_data.csv', index=False)
38
       print "Saved spectral type info to spectraltype_data.csv"
39
40
```

```
41
  def export_planets_to_pkl():
42
      client = kplr.API()
43
      planets = client.planets(koi_prad=">1.5") + client.planets(koi_prad="<=1.5")
     ")
      with open('planets.pkl', 'rb') as input_f:
45
           pickled_planets = cPickle.load(input_f)
46
      print "Saved planet info to planets.pkl"
47
48
  def export_good_log(n_sources=-1):
50
      with open('planets.pkl', 'rb') as input_f:
51
           pickled_planets = cPickle.load(input_f)
52
      # Get SPT data:
54
      spt_info = pd.read_csv('spectraltype_data.csv')
56
      planets = pickled_planets if n_sources is -1 else pickled_planets [:
      n_sources]
      host_stars = []
58
      for i in range(len(planets)):
          p = planets[i]
60
           s = p.star
61
           j_min_k = s.kic_jmag - s.kic_hmag
62
           t_eff = s.kic_teff
           metallicity = s.kic_feh
64
65
               row = spt_info[abs(spt_info['Teff'] - s.kic_teff) = min(abs(
66
      spt_info['Teff'] - s.kic_teff))]
               spt = row['SpT'].values[0]
67
               spt_id = row['spt_id'].values[0]
68
               predicted_teff = row['Teff'].values[0]
69
70
               spectral\_group = spt[0]
           except TypeError:
71
               pass
72
           d = \{ 't_eff' : s.kic_teff, \}
74
                'metallicity': s.kic_feh,
75
                # 'j_min_k ': s.kic_jmag - s.kic_hmag,
                # 'predicted_teff': predicted_teff,
                'spt': spt,
78
                'spectral_group': spectral_group,
                'spt_id': spt_id}
80
           host_stars.append(d)
82
           pct\_complete = round(100 * i/float(len(planets)), 2)
83
          # sys.stdout.write("Gotten %i% stars \r" % (i) )
84
           sys.stdout.write("Gathered info for {}% of the stars
                                                                    pct_complete) )
           sys.stdout.flush()
86
      host_stars_df = pd.DataFrame(host_stars)
87
      host_stars_df.to_csv('plotting_data.csv')
88
      print "Saved plotting data to plotting_data.csv"
89
```

```
90
92 ### THE ACTUAL, RAW TABLE FROM THE LINKED WEBSITE.
93 # Real ugly, gets processed in the functions above.
94 headers = 'SpT Teff logT BCv Mv logL B-V Bt-Vt G-V U-B
                  V–Ks
M. I
      V–Rc V–Ic
                             J–H
                                    H–Ks Ks–W1 W1–W2 W1–W3 W1–W4 Msun
                             M_Ks Mbol i-z z-Y R_Rsun SpT'
      logAge b-v
                     M_{J}
95
96
   o_stars = |
                                        5.80 -0.32 \dots
       'O3V
               46000 \ 4.663 \ -4.05 \ -5.7
                                                                      -1.22
98
                                                               . . .
               .... .... .... ...
       . . . . .
                                                                . . .
                                                                      . . . .
                                                                               . . .
                                         ... 12.5
                                                      O3V',
                \dots \qquad \dots \qquad -9.75 \quad \dots
       'O4V
               43000 \ 4.633 \ -3.92 \ -5.5
                                         5.67 -0.32
                                                                      -1.20
99
                .....
                                         ... ...
       . . . . .
                                         ... 12.3
                                                      O4V',
               \dots \qquad \dots \qquad -9.42 \quad \dots
       . . . . .
               41500 4.618 -3.77 -5.4
       'O5V
                                         5.58 -0.32
                                                                      -1.19
100
                .....
       . . . . .
                                                                      . . . .
                                                                . . .
                                                      O5V',
                                         ... 11.9
      -0.133
                \dots \qquad \dots \qquad -9.20 \quad \dots
               40000 \ 4.602 \ -3.65 \ -5.2
       'O5.5V
                                         5.46 - 0.32
                                                                      -1.18
                                                                . . .
                                         ... 11.2
                .....
                                                                       . . . .
                \dots \qquad \dots \qquad -8.90 \quad \dots
      -0.133
                                                      O5.5V'
       'O6V
               39000 \ 4.591 \ -3.57 \ -5.1
                                         5.37 - 0.32
                                                                      -1.17
                                                       . . .
       . . . . .
                .....
                                         ...
                                         ... 10.6
                \dots \qquad \dots \qquad -8.67 \quad \dots
      -0.132
                                                      O6V',
       '06.5V
               37300 \ 4.573 \ -3.45 \ -4.9
                                         5.24 - 0.32
                                                                      -1.16
103
                                                                . . .
                .....
                                         ...
       . . . . .
                                                                . . .
                                                                       . . . . .
                                                                               . . .
                                         ... 10.0
                \dots \qquad -8.35 \dots
      -0.131
                                                      06.5,
               36500 \ 4.562 \ -3.38 \ -4.8
       'O7V
                                         5.17 -0.32
                                                                      -1.15
                .....
                                                                       28
        . . . . .
                                                      O7V',
                                         \dots 9.62
      -0.130
                \dots -8.18 \dots
               35000 \ 4.544 \ -3.27 \ -4.6
       '07.5V
                                         5.05 -0.32
                                                                      -1.14
                                                                . . .
                                         ...
                .....
                                                                       24
       . . . . .
                                                                . . .
                                         ... 9.11 O7.5V
                \dots -7.87 \dots
      -0.130
       'O8V
               34500 \ 4.538 \ -3.22 \ -4.5
                                         4.99 - 0.32
                                                                      -1.13
106
                                                      . . .
                                                                               . . .
                                                                . . .
                .....
                                                                       22.9
                                         ... 8.75
                                                      O8V',
                \dots \qquad \dots \qquad -7.72 \quad \dots
      -0.129
       '08.5V
               33000 \ 4.519 \ -3.13 \ -4.3
                                         4.87 - 0.32
                                                                      -1.12
                                         ... ...
       . . . . .
                .....
                                                                . . .
                                                                       20.5
                                                                               . . .
               \dots \quad \dots \quad -7.43 \quad \dots \\ 32500 \quad 4.512 \quad -3.09 \quad -4.2
                                         ... 8.33 O8.5V'
      -0.128
       ,O9A
                                         4.82 -0.318 \dots
                                                                      -1.114
108
                                                                . . .
               -1.000 \quad -0.164 \quad -0.071
                                         ... ... ...
       -0.369
                                                                       19.7
                                                                               6.6
                                                                . . .
               -3.44 \quad -3.20 \quad -7.29 \quad \dots
                                         ... 8.11 O9V',
      -0.127
               32000 \ 4.505 \ -3.06 \ -4.1
                                         4.76 -0.312 \dots
       '09.5V
                                                                      -1.087
109
                                         ... ...
       -0.361
               -0.977 \quad -0.161 \quad -0.069
                                                                . . .
                                                                       18.5
                                                                               6.7
      -0.125
              -3.35 \quad -3.12 \quad -7.15 \quad \dots
                                         ... 7.80 	 O9.5V'
110
111
  b_stars = [
112
       'B0V
               31500 \ 4.498 \ -3.02 \ -4.0 \ 4.70 \ -0.307 \ \dots 
                                                                      -1.067
       -0.355 -0.958 -0.159 -0.067 ... 7.53 BoV',
                                                                               6.8
                                                                       17.5
      -0.122
'B0.5V 29000 4.462 -2.87 -3.6 4.47 -0.295 ... ...
                                                                      -1.026
```

```
... ... ... 15
         -0.338 \quad -0.913 \quad -0.153 \quad -0.063
                                                 ... 6.81 B0.5V,
        -0.120 -2.90 -2.69 -6.43 ...
                   26000 \ 4.415 \ -2.61 \ -3.1
                                                   4.13 -0.278 \dots
         'B1V
                                                                                      -0.995
                                                                                                -0.115
115
         -0.325 \quad -0.874 \quad -0.148 \quad -0.059
                                                   ... ...
                                                                                       11
                                                                                                 7.0
                                                                               . . .
                                                  ... 5.72 B1V',
        -0.113 \quad -2.43 \quad -2.23 \quad -5.68 \quad \dots
        'B1.5V 24500 4.389 -2.43 -2.8
                                                   3.89 -0.252 -0.274
                                                                                      -0.910
                                                                                                -0.114
116
         -0.281 \quad -0.752 \quad -0.132 \quad -0.047
                                                   0.035 ... ...
                                                                                       10
                                                                               . . .
        -0.103 -2.23 -2.05 -5.24 ...
                                                   ... 4.89 B1.5V',
        'B2V
                  20600 \ 4.314 \ -2.06 \ -1.7
                                                   3.38 -0.210 -0.219
                                                                                      -0.790
                                                                                                -0.094
117
                                                                              . . .
                                                  0.036 ... ... ...
... 3.85 B2V',
         -0.230 \quad -0.602 \quad -0.113 \quad -0.032
                                                                                                 7.2
                                                                                       7.3
                                                                               . . .
        -0.094 -1.24 -1.10 -3.71 ...
                                                   3.10 -0.198 -0.206
        'B2.5V 18500 4.267 -1.79 -1.4
                                                                                      -0.732
                                                                                                -0.087
118
                                                                              . . .
                                                   0.036 ... ...
         -0.210 \quad -0.544 \quad -0.105 \quad -0.026
                                                                               . . .
                                                                                       6.1
                                                                                                7.3
        -0.087 -0.99 -0.86 -3.15 ...
                                                   ... 3.45 B2.5V,
                  17000 \ 4.230 \ -1.58 \ -1.1
                                                   2.96 -0.178 -0.184
                                                                                                -0.080
                                                                                      -0.673
119
         -0.192 \quad -0.492 \quad -0.098 \quad -0.021
                                                   0.036 ... ...
                                                                              . . .
                                                                                       5.4
                 -0.73 \quad -0.61 \quad -2.64 \quad \dots
                                                   ... 3.48 B3V',
        -0.083
        'B4V
                   16700 \ 4.223 \ -1.53 \ -1.0
                                                   2.91 -0.165 -0.170
120
                                                                                      -0.619
                                                                                                -0.074
                                                   0.036 ... ...
         -0.176 \quad -0.447 \quad -0.092 \quad -0.016
                                                                                       5.0
                                                                                                 7.5
                                                  ... 3.41 B4V',
                 -0.66 \quad -0.55 \quad -2.52 \quad \dots
        -0.078
                                                   2.80 \quad -0.156 \quad -0.160 \quad \dots \quad -0.581
        'B5V
                  15700 \ 4.196 \ -1.35 \ -0.9
                                                                                                -0.070
121
                                                   0.036 \quad -0.045 \quad -0.117 \quad -0.070 \quad 4.6
         -0.165 \quad -0.417 \quad -0.089 \quad -0.013
                                                                                                 7.7
        -0.072 \quad -0.59 \quad -0.48 \quad -2.25 \quad \dots
                                                   \dots 3.40 B5V',
                                                   2.54 \quad -0.140 \quad -0.142 \quad \dots \quad -0.504
                 14500 \ 4.161 \ -1.16 \ -0.5
                                                                                                -0.062
122
                                                   0.035 \quad -0.045 \quad -0.117 \quad -0.070 \quad 4.0
         -0.145 \quad -0.358 \quad -0.081 \quad -0.007
                                                                                                 7.8
                                                  ... 2.95 B6V',
        -0.066
                 -0.23 \quad -0.14 \quad -1.66 \quad \dots
                  14000 \ 4.146 \ -1.07 \ -0.4
                                                   2.49 -0.128 -0.129 \dots -0.459
                                                                                                -0.058
123
         -0.133 \quad -0.325 \quad -0.077 \quad -0.004
                                                   0.035 \quad -0.045 \quad -0.117 \quad -0.070 \quad 3.9
                                                                                                7.9
                  -0.16 -0.08 -1.47 ...
                                                   ... 2.99 B7V',
        -0.062
                                                   2.27 -0.109 -0.107 \dots -0.364
        'B8V
                  12500 \ 4.097 \ -0.81 \ -0.2
                                                                                                -0.048
124
         -0.108
                  -0.254 \quad -0.067 \quad 0.003
                                                   0.034 \quad -0.046 \quad -0.116 \quad -0.067 \quad 3.4
                                                                                                 8.1
                  -0.01 0.05 -0.91 ...
                                                   \dots 2.91 B8V',
        -0.045
                   10700 \ 4.029 \ -0.42 \ 0.7
                                                   1.79 -0.070 -0.063 \dots -0.200
        'B9V
                                                                                                -0.028
125
                   -0.121 \quad -0.050 \quad 0.016
                                                   0.032 \quad -0.063 \quad -0.104 \quad -0.054 \quad 2.8
         -0.061
                                                                                                 8.3
        -0.029
                   0.79 \quad 0.82 \quad 0.28 \dots
                                                  ... 2.28 B9V',
                                                  1.73 \quad -0.050 \quad -0.040 \quad \dots \quad -0.130
        ^{\prime}\mathrm{B9.5V}
                   10400 \ 4.017 \ -0.38 \ 0.8
                                                                                                -0.017
126
                   -0.048 \quad -0.044 \quad 0.021
                                                   0.031 \quad -0.044 \quad -0.091 \quad -0.043 \quad 2.5
         -0.035
                                                                                                 8.4
        -0.021
                   0.83 \quad 0.85 \quad 0.44 \quad \dots \quad 2.26 \quad B9.5V'
127
   a_stars = [
128
                   9700 \quad 3.987 \quad -0.24 \qquad 1.11 \quad 1.54 \quad 0.000 \quad 0.013 \quad -0.023 \quad -0.005
         'A0V
                                                                                                 0.001
129
                   0.041 \quad -0.032 \quad 0.028 \quad 0.030 \quad -0.041 \quad -0.074 \quad -0.022 \quad 2.3
          0.004
                                                                                                 8.5
                   1.07 \quad 1.07 \quad 0.87 \quad \dots \quad 2.09 \quad AoV',
                   9200 \quad 3.965 \quad -0.15 \qquad 1.34 \quad 1.41 \quad 0.043 \quad 0.056 \quad -0.024 \quad 0.033
         'A1V
                                                                                                 0.019
130
                   0.101 \quad -0.024 \quad 0.031 \quad 0.030 \quad -0.036 \quad -0.068 \quad -0.023 \quad 2.15
         0.044
         0.017
                   1.25 \quad 1.24 \quad 1.19 \quad \dots \quad 2.00 \quad AIV',
         'A2V
                   8840 \quad 3.946 \quad -0.10 \quad 1.48 \quad 1.33 \quad 0.074 \quad 0.091 \quad -0.025 \quad 0.063
                                                                                                 0.042
131
                   0.188 \quad -0.010 \quad 0.034 \quad 0.029 \quad -0.034 \quad -0.067 \quad -0.029 \quad 2.05
         0.091
                                                                                                 8.7
                   1.32 1.29 1.38 ... 1.97 A2V',
         0.038
                   8550 3.932 -0.06 1.55 1.29 0.090 0.109 -0.026 0.077
                                                                                                 0.050
132
         0.108
                   0.228 \quad -0.002 \quad 0.034 \quad 0.029 \quad -0.033 \quad -0.066 \quad -0.029 \quad 2.00
                                                                                                 8.7
                   1.35 \quad 1.32 \quad 1.49 \quad \dots \quad 2.01 \quad A3V',
         0.055
                   8270 \quad 3.917 \quad -0.04 \quad 1.76 \quad 1.20 \quad 0.140 \quad 0.166 \quad -0.029 \quad 0.097
         'A4V
                                                                                               0.078
133
```

```
0.164 \quad 0.353 \quad 0.022 \quad 0.037 \quad 0.029 \quad -0.031 \quad -0.059 \quad -0.021 \quad 1.90 \quad 8.8
                    1.47 \quad 1.41 \quad 1.72 \quad \dots \quad 1.94 \quad A4V',
          0.071
                    8080 \quad 3.907 \quad -0.03 \quad 1.84 \quad 1.16 \quad 0.160 \quad 0.185 \quad -0.031 \quad 0.100
          'A5V
                                                                                                        0.089
134
                     0.403 \quad 0.031 \quad 0.038 \quad 0.029 \quad -0.030 \quad -0.058 \quad -0.021 \quad 1.85
          0.186
                    1.51 \quad 1.44 \quad 1.81 \quad \dots \quad 1.94 \quad A5V',
          'A6V
                    8000 \quad 3.903 \quad -0.02 \quad 1.89 \quad 1.14 \quad 0.170 \quad 0.194 \quad -0.032 \quad 0.098
                                                                                                        0.094
135
                     0.428 \quad 0.036 \quad 0.038 \quad 0.029 \quad -0.030 \quad -0.057 \quad -0.018 \quad 1.83
          0.197
                    1.54 1.46 1.87 ... 1.93 A6V',
          0.099
          'A7V
                    7800 \quad 3.892 \quad 0.00 \quad 2.07 \quad 1.06 \quad 0.210 \quad 0.233 \quad -0.037 \quad 0.091
                                                                                                         0.117
136
                     0.528 0.055 0.040 0.029 -0.030 -0.056 -0.017 1.76
          0.242
                                                                                                        8.9
          0.107
                    1.64 \quad 1.54 \quad 2.07 \quad \dots \quad 1.86 \quad A7V',
          'A8V
                    7500 \quad 3.874 \quad 0.00 \quad 2.29 \quad 0.97 \quad 0.250 \quad 0.274 \quad -0.042 \quad 0.082
                                                                                                        0.140
137
                     0.626 0.075 0.042 0.028 -0.028 -0.055 -0.009 1.67
          0.288
                                                                                                        9.0
                     1.78 \quad 1.66 \quad 2.29 \quad \dots \quad 1.81 \quad A8V',
          0.132
                    7440 \quad 3.872 \quad 0.00 \quad 2.30 \quad 0.97 \quad 0.255 \quad 0.279 \ -0.043 \quad 0.080
         'A9V
                                                                                                        0.143
138
                    0.638 0.078 0.043 0.028 -0.028 -0.055 -0.007 1.67
          0.294
                                                                                                        9.0
                            1.66 2.30 ... 1.84 A9V']
          0.145
                    1.78
139
f_s t a r s = 
                    7220 \quad 3.857 \quad -0.01 \quad 2.51 \quad 0.89 \quad 0.294 \quad 0.317 \quad -0.049 \quad 0.053
         'F0V
                                                                                                         0.166
141
                     0.732 0.098 0.045 0.028 -0.026 -0.050 0.003 1.59
          0.339
                                                                                                        9.1
                    1.90 \quad 1.76 \quad 2.50 \dots \quad 1.79 \quad \text{FoV}',
          0.158
         'F1V
                    7030 \quad 3.847 \quad -0.01 \qquad 2.79 \quad 0.77 \quad 0.334 \quad 0.350 \quad -0.057 \quad 0.021
                                                                                                        0.190
142
          0.385
                     0.828 0.119 0.047 0.028 -0.026 -0.047 0.009 1.50
          0.204
                    2.13
                            1.96 	 2.78 	 \dots 	 1.64 	 \text{F1V}',
                    6810 \quad 3.833 \quad -0.02 \qquad 2.99 \quad 0.70 \quad 0.374 \quad 0.390 \quad -0.066 \quad -0.008
         F2V
                                                                                                         0.213
143
                    0.925 0.140 0.050 0.028 -0.027 -0.046 0.011 1.44
          0.432
          0.250
                            2.07 	 2.97 	 \dots 	 1.61 	 F2V',
                    6720 \quad 3.827 \quad -0.03 \quad 3.08 \quad 0.67 \quad 0.389 \quad 0.405 \quad -0.069 \quad -0.016
         'F3V
                                                                                                        0.222
                     0.961 \qquad 0.147 \qquad 0.051 \qquad 0.028 \quad -0.028 \quad -0.046 \quad 0.008 \quad 1.43
          0.449
          0.263
                    2.32 2.12 3.05 ... 1.60 F3V',
                    6640 \quad 3.822 \quad -0.04 \quad \quad 3.23 \quad \quad 0.61 \quad \quad 0.412 \quad \quad 0.428 \quad -0.075 \quad -0.026
145
                    1.017 \quad 0.159 \quad 0.052 \quad 0.028 \quad -0.029 \quad -0.046 \quad 0.000 \quad 1.39
          0.476
                                                                                                        9.2
                            2.21 \quad 3.19 \quad \dots \quad 1.53 \quad \text{F4V}',
          0.277
                    2.42
         'F5V
                    6510 \quad 3.814 \quad -0.04 \quad 3.40 \quad 0.54 \quad 0.438 \quad 0.455 \quad -0.081 \quad -0.029
                                                                                                        0.252
146
          0.506
                     1.079 \quad 0.173 \quad 0.054 \quad 0.028 \quad -0.030 \quad -0.045 \quad -0.004 \quad 1.33
                                                                                                        9.3
                     2.55 2.32 3.36 ... 1.46 F5V',
          0.290
         'F6V
                    6340 \quad 3.802 \quad -0.05 \quad 3.70 \quad 0.43 \quad 0.484 \quad 0.504 \quad -0.093 \quad -0.021
                                                                                                        0.276
147
                    1.185 \quad 0.199 \quad 0.057 \quad 0.028 \quad -0.033 \quad -0.045 \quad -0.012 \quad 1.25
          0.553
                    0.317
         'F7V
                                                                                                         0.290
148
                    1.244 \quad 0.213 \quad 0.060 \quad 0.027 \quad -0.036 \quad -0.045 \quad -0.013 \quad 1.21
          0.579
          0.332
                            2.63 \quad 3.81 \quad \dots \quad 1.30 \quad \text{F7V}',
         'F8V
                    6170 \quad 3.790 \quad -0.07 \quad \  \  4.01 \quad \  0.31 \quad \  0.530 \quad \  0.558 \quad -0.105 \quad 0.001
                                                                                                        0.300
149
                     1.290 \quad 0.225 \quad 0.061 \quad 0.027 \quad -0.039 \quad -0.044 \quad -0.016 \quad 1.18
          0.599
          0.350
                    3.01 \quad 2.72 \quad 3.96 \quad \dots \quad 1.25 \quad \text{F8V}',
                    6060 \quad 3.782 \quad -0.08 \quad 4.15 \quad 0.26 \quad 0.552 \quad 0.587 \quad -0.111 \quad 0.014
                                                                                                        0.312
                     1.340 \quad 0.237 \quad 0.063 \quad 0.027 \quad -0.041 \quad -0.044 \quad -0.014 \quad 1.14
          0.620
                                                                                                        9.7
                    3.11 \quad 2.81 \quad 4.07 \quad \dots \quad 1.23 \quad \text{F9V}',
          0.378
                    6000 \quad 3.778 \quad -0.08 \quad 4.29 \quad 0.21 \quad 0.572 \quad 0.615 \quad -0.117 \quad 0.033
         'F9.5V
                                                                                                        0.323
          0.640
                    1.385 \quad 0.249 \quad 0.065 \quad 0.027 \quad -0.042 \quad -0.043 \quad -0.012 \quad 1.11
                                                                                                        9.7
                     3.22 \quad 2.91 \quad 4.22 \quad \dots \quad 1.18 \quad \text{F9.5V'}
          , . .
152
```

```
g_stars = [
          'G0V
                      5920 \quad 3.772 \quad -0.09 \quad \  \  4.45 \quad \  0.14 \quad \  0.596 \quad \  0.650 \quad -0.124 \quad \  0.058
                                                                                                                  0.336
154
                      1.440 \quad 0.262 \quad 0.067 \quad 0.027 \quad -0.043 \quad -0.043 \quad -0.010 \quad 1.08
           0.664
                                                                                                                 9.7
                      3.34 \quad 3.01 \quad 4.40 \quad \dots \quad 1.12 \quad \text{GoV}',
          'G1V
                      5880 \quad 3.769 \quad -0.10 \quad 4.50 \quad 0.13 \quad 0.604 \quad 0.661 \quad -0.133 \quad 0.067
           0.672
                       1.458 \quad 0.267 \quad 0.068 \quad 0.027 \quad -0.044 \quad -0.042 \quad -0.010 \quad 1.07
                                                                                                                 9.8
                      3.38 \quad 3.04 \quad 4.40 \quad \dots \quad 1.12 \quad \text{GIV}',
           . . .
                      5770 \quad 3.761 \quad -0.11 \qquad 4.79 \quad 0.01 \quad 0.650 \quad 0.724 \quad -0.141 \quad 0.133
          'G2V
                                                                                                                  0.363
156
           0.713
                       1.564 0.293 0.073 0.028 -0.050 -0.040 -0.016 1.02
                      3.57
                              3.20 	 4.68 	 \dots 	 1.01 	 G2V',
           . . .
                      5720 \quad 3.757 \quad -0.12 \quad 4.86 \quad -0.01 \quad 0.661 \quad 0.739 \quad -0.144 \quad 0.152
           'G3V
                                                                                                                  0.368
                      1.590 \quad 0.299 \quad 0.074 \quad 0.028 \quad -0.050 \quad -0.040 \quad -0.014 \quad 1.00
           0.722
                              3.27 	 4.74 	 \dots 	 1.01 	 G3V',
           . . .
                      5680 \quad 3.754 \quad -0.13 \quad 4.94 \quad -0.04 \quad 0.674 \quad 0.757 \quad -0.148 \quad 0.175
           'G4V
                                                                                                                  0.374
158
                       1.621 \quad 0.307 \quad 0.075 \quad 0.028 \quad -0.052 \quad -0.041 \quad -0.014 \quad 0.99
           0.733
                      3.70 \quad 3.32 \quad 4.80 \quad \dots \quad 0.986 \quad \text{G4V}',
           . . .
                      5660 \quad 3.753 \quad -0.13 \quad 4.98 \quad -0.05 \quad 0.680 \quad 0.764 \quad -0.150 \quad 0.185
          'G5V
                                                                                                                  0.377
159
                       1.635 \quad 0.310 \quad 0.076 \quad 0.028 \quad -0.052 \quad -0.041 \quad -0.014 \quad 0.98
           0.738
           . . .
                      3.74
                              3.35 \quad 4.84 \quad \dots \quad 0.982 \quad \text{G5V}',
          'G6V
                      5590 \quad 3.747 \quad -0.15 \quad 5.13 \quad -0.11 \quad 0.704 \quad 0.796 \quad -0.158 \quad 0.227
                                                                                                                  0.388
160
                       1.691 \quad 0.324 \quad 0.079 \quad 0.028 \quad -0.053 \quad -0.040 \quad -0.012 \quad 0.97
           0.758
                      3.84 3.44 4.98 ... 0.939 G6V',
           . . .
          'G7V
                      5530 \quad 3.743 \quad -0.16 \quad 5.18 \quad -0.12 \quad 0.713 \quad 0.809 \quad -0.161 \quad 0.243
                                                                                                                  0.393
161
           0.766
                      1.712 \quad 0.329 \quad 0.080 \quad 0.028 \quad -0.054 \quad -0.040 \quad -0.013 \quad 0.96
                      3.88
                              3.47 \quad 5.02 \quad \dots \quad 0.949 \quad \text{G7V}',
                      5490 \quad 3.734 \quad -0.17 \qquad 5.32 \quad -0.17 \quad 0.737 \quad 0.842 \quad -0.169 \quad 0.284
           'G8V
                                                                                                                  0.404
                       1.768 \quad 0.342 \quad 0.082 \quad 0.028 \quad -0.057 \quad -0.039 \quad -0.018 \quad 0.94
           0.786
                      3.97 \quad 3.55 \quad 5.15 \quad \dots \quad 0.909 \quad \text{G8V}',
           . . .
                      5340 \quad 3.728 \quad -0.21 \quad 5.55 \quad -0.25 \quad 0.777 \quad 0.894 \quad -0.182 \quad 0.358
           'G9V
                                                                                                                  0.423
           0.820
                       1.861 \quad 0.365 \quad 0.087 \quad 0.029 \quad -0.060 \quad -0.038 \quad -0.018 \quad 0.90
                      4.14 \quad 3.69 \quad 5.34 \quad \dots \quad 0.876 \quad \text{G9V'}
           . . .
164
165
    k_s tars = [
166
          'K0V
                      5280 \quad 3.723 \quad -0.22 \quad 5.76 \quad -0.33 \quad 0.816 \quad 0.944 \quad -0.23 \quad 0.436
                                                                                                                  0.443
167
                       1.953 \quad 0.387 \quad 0.091 \quad 0.030 \quad -0.063 \quad -0.037 \quad -0.015 \quad 0.87
           0.853
                      4.29 \quad 3.81 \quad 5.54 \quad \dots \quad 0.817 \quad \text{KoV}',
           . . .
                      5240 \quad 3.719 \quad -0.23 \quad 5.80 \quad -0.33 \quad 0.828 \quad 0.955 \quad -0.24 \quad 0.456
          'K0.5V
                                                                                                                  0.448
168
           0.862
                       1.977 \quad 0.393 \quad 0.092 \quad 0.030 \quad -0.064 \quad -0.038 \quad -0.018 \quad 0.86
                                                                                                                  . . .
           . . .
                      4.31 \quad 3.82 \quad 5.57 \quad \dots \quad 0.828 \quad \text{K0.5V'},
                      5170 \quad 3.713 \quad -0.26 \quad 5.89 \quad -0.36 \quad 0.847 \quad 0.976 \quad -0.26
           'K1V
                                                                                                                  0.457
169
                       2.021 0.402 0.094 0.030 -0.064 -0.038 -0.013 0.85
           0.879
                      4.37 3.87 5.65 ... 0.814 KIV',
                      5140 \quad 3.711 \quad -0.27 \quad 5.97 \quad -0.39 \quad 0.859 \quad 0.999 \quad -0.28
           'K1.5V
                                                                                                   0.528
                                                                                                                  0.467
170
                       2.066 \quad 0.412 \quad 0.096 \quad 0.030 \quad -0.063 \quad -0.037 \quad -0.016 \quad 0.82
           0.895
                      4.41 \quad 3.90 \quad 5.70 \quad \dots \quad 0.809 \quad K1.5V',
           . . .
                      5040 \quad 3.702 \quad -0.29 \quad 6.19 \quad -0.47 \quad 0.884 \quad 1.035 \quad -0.30
          'K2V
                                                                                                                  0.482
171
                       2.132 \quad 0.427 \quad 0.098 \quad 0.031 \quad -0.068 \quad -0.037 \quad -0.009 \quad 0.78
           0.920
                      4.57 \quad 4.04 \quad 5.88 \quad \dots \quad 0.763 \quad \text{K2V}',
                      4990 \quad 3.698 \quad -0.32 \quad 6.34 \quad -0.51 \quad 0.938 \quad 1.101 \quad -0.30
          'K2.5V
                                                                                                   0.691
                                                                                                                  0.513
172
                       2.274 \quad 0.459 \quad 0.104 \quad 0.032 \quad -0.071 \quad -0.032 \quad -0.006 \quad 0.76
           0.974
                      4.63 	 4.07 	 6.02 	 \dots 	 0.742 	 K2.5V',
           . . .
          'K3V
                      4830 \quad 3.684 \quad -0.41 \qquad 6.57 \quad -0.58 \quad 0.980 \quad 1.150 \quad -0.31 \qquad 0.776
                                                                                                                 0.537
```

```
1.013 2.380 0.483 0.109 0.033 -0.071 -0.031 -0.008 0.75 ...
                   4.76 4.16 6.16 ... 0.729 K3V',
                   4700 \quad 3.672 \quad -0.45 \quad 6.79 \quad -0.64 \quad 1.050 \quad 1.239 \quad -0.37 \quad 0.917
                                                                                                     0.592
174
          1.108
                    2.582 \quad 0.520 \quad 0.118 \quad 0.036 \quad -0.074 \quad -0.031 \quad -0.005 \quad 0.73
                    4.85 4.21 6.34 ... 0.720 K3.5V',
         . . .
                   4600 \quad 3.663 \quad -0.56 \quad 6.98 \quad -0.67 \quad 1.100 \quad 1.306 \quad -0.43 \quad 1.004
         'K4V
                                                                                                     0.640
                    2.733 \qquad 0.544 \qquad 0.125 \qquad 0.039 \quad -0.073 \ -0.031 \quad 0.009 \quad 0.72
          1.190
                    4.92 4.25 6.42 ... 0.726 K4V',
                   4540 \quad 3.657 \quad -0.60 \quad 7.04 \quad -0.68 \quad 1.116 \quad 1.328 \quad -0.42 \quad 1.028
         'K4.5V
                                                                                                     0.654
176
                    2.781 \quad 0.552 \quad 0.127 \quad 0.040 \quad -0.073 \quad -0.030 \quad 0.017 \quad 0.71
         1.216
                    4.94 4.26 6.44 ... 0.737 K4.5V',
         . . .
                   4410 \quad 3.644 \quad -0.68 \quad 7.36 \quad -0.78 \quad 1.150 \quad 1.373 \quad -0.41 \quad 1.081
                                                                                                     0.685
         'K5V
177
                    2.883 \quad 0.568 \quad 0.132 \quad 0.042 \quad -0.073 \quad -0.029 \quad 0.019 \quad 0.68
         1.272
                    5.18 4.48 6.68 ... 0.698 K5V',
          . . .
                   4330 \quad 3.636 \quad -0.75 \qquad 7.60 \quad -0.84 \quad 1.200 \quad 1.414 \quad -0.44
         'K5.5V
                                                                                         1.144
                                                                                                    0.728
178
         1.357
                    3.034 \quad 0.591 \quad 0.139 \quad 0.045 \quad \dots \quad \dots
                                                                                          0.66
                                                                                                    . . .
                    5.30 \quad 4.57 \quad 6.85 \quad \dots \quad 0.672 \quad K5.5V',
         . . .
                   4230 \quad 3.626 \quad -0.81 \quad 7.80 \quad -0.90 \quad 1.240 \quad 1.439 \quad -0.48
         'K6V
179
                                                                                          1.184
                                                                                                     0.759
                    3.143 \quad 0.601 \quad 0.148 \quad 0.049 \quad \dots \quad \dots
          1.420
                                                                                          0.65
                    5.41 4.66 6.99 ... 0.661 K6V',
         . . .
                   4190 \quad 3.622 \quad -0.92 \quad 8.01 \quad -0.96 \quad 1.310 \quad 1.491 \quad -0.52
         'K6.5V
                                                                                          1.213
                                                                                                     0.796
180
                    3.288 \quad 0.613 \quad 0.159 \quad 0.055 \quad \dots \quad \dots
          1.505
                                                                                          0.64
         ...
                    5.56 	 4.78 	 7.09 	 \dots 	 0.656 	 K6.5V',
                   4070 \quad 3.610 \quad -0.95 \quad 8.15 \quad -0.98 \quad 1.330 \quad 1.506 \quad -0.57
         'K7V
                                                                                          1.221
                                                                                                    0.806
181
          1.529
                    3.330 \quad 0.617 \quad 0.162 \quad 0.057 \quad \dots \quad \dots
                                                                                          0.63
                    5.60 4.82 7.18 ... 0.654 K7V',
         . . .
                   4000 \quad 3.602 \quad -1.03 \quad 8.47 \quad -1.10 \quad 1.356 \quad 1.562 \quad -0.63
         'K8V
                                                                                          1.216
                                                                                                     0.843
                    3.487 \quad 0.623 \quad 0.176 \quad 0.081 \quad \dots \quad \dots
         1.632
                                                                                          0.59
                                                                                                    . . .
                    5.78 4.98 7.44 ... 0.587 K8V',
          . . .
                   3940 \quad 3.595 \quad -1.10 \quad 8.69 \quad -1.18 \quad 1.382 \quad 1.593 \quad -0.69
         'K9V
                                                                                         1.210
                                                                                                    0.866
183
                   3.584 \quad 0.625 \quad 0.184 \quad 0.101 \quad \dots \quad \dots
         1.699
                                                                                          0.56
         . . .
                    5.92 5.11 7.59 ... 0.552 K9V']
   m_stars = [
185
         'MOV
                   3870 \quad 3.588 \quad -1.16 \quad 8.91 \quad -1.20 \quad 1.408 \quad 1.623 \quad -0.65
                                                                                         1.204
                                                                                                    0.889
         1.766
                    3.680 \quad 0.626 \quad 0.193 \quad 0.122 \quad \dots \quad \dots
                                                                                          0.55
                    6.04 \quad 5.22 \quad 7.75 \quad 0.33 \quad \dots \quad 0.559 \quad MoV',
         . . .
                   3800 \quad 3.580 \quad -1.38 \quad 9.20 \quad -1.27 \quad 1.441 \quad \dots
         'M0.5V
                                                                               -0.74
                                                                                          1.184
                                                                                                    0.924
187
                    3.84 \quad 0.620 \quad 0.208 \quad 0.130 \quad \dots \quad \dots
                                                                                           0.54
          . . .
                    6.19 5.36 7.90 0.37 ... 0.535 M0.5V'
                   3700 \quad 3.568 \quad -1.44 \quad 9.69 \quad -1.40 \quad 1.475 \quad \dots
         'M1V
                                                                               -0.82
                                                                                          1.172
                                                                                                     0.959
188
          2.019
                    4.02 \qquad 0.613 \qquad 0.225 \qquad 0.137 \qquad \dots
                                                                                           0.49
                    6.51 5.67 8.25 0.41 ... 0.496 MIV',
                   'M1.5V
                                                                                          1.170
                                                                                                     0.978
                                                                               -0.85
          2.089
                                                                                           0.47
                    6.69 \quad 5.85 \quad 8.40 \ 0.47 \ \dots \ 0.460 \quad M1.5V',
         . . .
                   3550 \quad 3.550 \quad -1.65 \quad 10.30 \quad -1.57 \quad 1.500 \quad \dots
         'M2V
                                                                                -0.92
                                                                                          1.170
                                                                                                    1.001
190
                    4.24 \qquad 0.600 \qquad 0.234 \qquad 0.110 \qquad \dots \qquad \dots
          2.173
                                                                                          0.44
                                                                                 . . . .
                    6.89 \quad 6.06 \quad 8.65 \quad 0.53 \quad \dots \quad 0.434 \quad M2V',
                   3500 \quad 3.544 \quad -1.76 \quad 10.70 \quad -1.68 \quad 1.522 \quad \dots
                                                                               -1.02
         M2.5V
                                                                                          1.175
                                                                                                    1.041
191
                   4.43 \qquad 0.589 \qquad 0.244 \qquad 0.117 \qquad \dots \qquad \dots
          2.306
                                                                                          0.40
                    7.01 \qquad 6.27 \qquad 8.94 \ 0.57 \ \dots \quad 0.393 \quad M2.5V'\,,
         . . .
                   3410 \quad 3.533 \quad -1.97 \quad 11.14 \quad -1.78 \quad 1.544 \quad \dots \quad -1.09 \quad 1.181
         'M3V
                                                                                                  1.079
```

```
4.60 \quad 0.579 \quad 0.252 \quad 0.122 \quad \dots \quad \dots
                                                                                  0.36
                                                                                         . . .
                          6.54 \quad 9.17 \quad 0.61 \quad \dots \quad 0.369 \quad M3V',
                  7.40
        'M3.5V
                 3250
                        3.512 - 2.27 \quad 12.19 \quad -2.07 \quad 1.602 \quad \dots
                                                                       -1.29
                                                                                1.200
                                                                                         1.178
193
                                     0.269
         2.680
                   5.00
                           0.558
                                               0.132
                                                                                  0.26
                                                                                         . . .
        . . .
                  8.02
                          7.19 \quad 9.92 \quad 0.66 \quad \dots \quad 0.291 \quad M3.5V',
        'M4V
                 3200
                        3.505 - 2.59 \quad 12.80 \quad -2.20 \quad 1.661 \quad \dots
                                                                       -1.41
                                                                                1.222
                                                                                         1.241
194
         2.831
                                    0.282
                                             0.139
                                                                                  0.22
                  5.25
                           0.557
                                                       . . .
                                                                                         . . .
                  8.39
                          7.55 \quad 10.21 \quad 0.71 \quad \dots \quad 0.258
                                                             M4V',
                        3.491 - 3.05 \quad 13.57 - 2.31 \quad 1.72
                                                                                1.23
                                                                                         1.345
        'M4.5V
                 3100
                                                                       -1.55
195
                                             ... ...
         3.073
                  5.64
                            0.564 \qquad 0.301
                                                                                  0.18
                          7.93 \quad 10.52 \quad 0.81 \quad \dots \quad 0.243 \quad M4.5V'
        . . .
                  8.79
                                                                                1.24
        'M5V
                 3030
                        3.481 \quad -3.28 \quad 14.30 \quad -2.52 \quad 1.874 \quad \dots
                                                                       -1.74
                                                                                         1.446
196
                                                       0.17 ...
         3.277
                   5.94
                            0.580
                                    0.311
                                              . . .
                                                                                 0.16
                                                                                         . . .
                          8.36 11.02 0.91 0.47 0.199 M5V',
        . . .
                  9.25
        'M5.5V
                 3000
                        3.477 - 3.80 \quad 15.51 \quad -2.79 \quad 1.91 \quad \dots
                                                                       -2.01
                                                                                1.3
                                                                                         1.656
         3.664
                                             0.19
                   6.50
                           0.588
                                    0.329
                                                                         . . .
                                                                                  0.12
                                                                                         . . .
        . . .
                  9.93
                          9.01 11.71 1.13 0.52 0.149 M5.5V'
        'M6V
                                                                       -2.14
198
                 2850
                        3.455 \quad -4.36 \quad 16.62 \quad -3.02 \quad 2.00 \quad \dots
                                                                                1.3
                                                                                          1.950
         4.13
                   7.30
                            0.605 \qquad 0.352 \qquad \dots
                                                       0.21
                                                                                  0.10
                          9.32 12.26 1.45 0.60 0.127 M6V',
        . . .
                 2710 \quad 3.433 \quad -4.60 \quad 17.07 \quad -3.09 \quad 2.06 \quad \dots
        'M6.5V
                                                                       -2.75
                                                                                         2.003
199
                                              0.22
         4.31
                           0.609
                                    0.364
                                                                                  0.097
                   7.60
                                                                                        . . .
                         9.47 12.47 1.58 0.64 0.129 M6.5V'
                10.47
        . . .
        'M7V
                        3.423 -5.06 17.81 -3.21 2.06 \dots
                                                                       -2.98
                                                                                . . .
                                                                                         2.180
200
                                     0.386
                                              ... 0.24 ...
                                                                                  0.090 ...
         4.45
                   8.05
                            0.613
                          9.76 12.75 1.77 0.70 0.118 M7V',
        . . .
                10.76
                 2600
                       3.415 -5.46 18.42 -3.29 2.17 \dots
                                                                       -3.09
        'M7.5V
                                                                                         2.160
201
                                                                                 0.089 ...
                                                       0.25 ...
         4.56
                   8.45
                           0.650
                                    0.422
                                              . . .
                                                                         . . .
                          9.97 12.97 1.85 0.74 0.112 M7.5V'
        . . .
                10.68
        'M8V
                 2500
                        3.398 -5.70 18.84 -3.36 2.20 \dots
                                                                       -3.11
                                                                                          2.150
202
                                                                                 0.082
        4.64
                           0.670 \quad 0.450 \quad \dots \quad 0.26 \quad \dots
                 8.73
                                                                        . . .
                                                                                         . . .
        • • •
                        10.11 13.14 1.93 0.77 0.111 M8V',
                11.23
                        3.387 -5.80 19.14 -3.44 \dots
                                                                       -3.09
                                                                                . . .
203
        'M8.5V
                 2440
                                                                                         1.967
                                              0.265 ...
                   8.92
                                     0.470
         4.71
                            0.685
                                                                                 0.081
        . . .
                11.45
                        10.22 13.34 1.96 0.80 0.107 M8.5V',
        'M9V
                        3.380 -5.90 19.36 -3.57 \dots
                                                                       -3.07
                 2400
                                                                                         1.890
204
                                             0.27
                                                                                  0.079 ...
         4.75
                  9.00
                            0.749
                                    0.480
                                                                         . . .
                        10.30 13.67 1.99 0.82 0.095 M9V',
                11.53
                        3.365 -6.13 	 19.75 -3.55 	 \dots 	 \dots
        'M9.5V
                 2320
                                                                       -3.10
                                                                                . . .
205
                 9.30 \quad 0.826 \quad 0.505 \quad \dots \quad 0.27 \quad \dots
         4.79
                                                                        . . .
                                                                                 0.078 ...
                       10.45 13.62 2.00 0.84 0.104 M9.5V']
206
207
   export_planets_to_pkl()
   export_spectral_type_info()
   export_good_log()
211
212
213
214 # The End
```