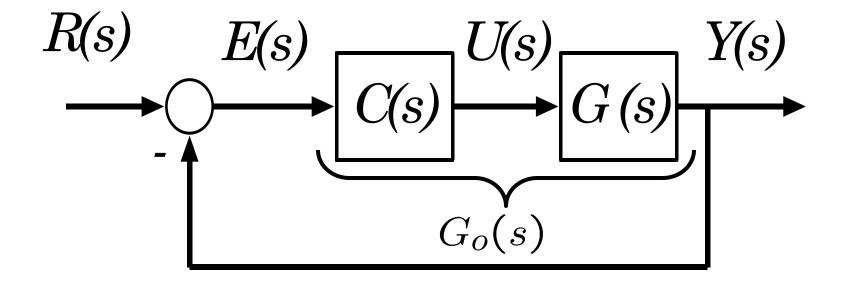
## [MEN573] Advanced Control Systems I

Lecture 20 - Properties of Optimal Linear Quadratic Regulators (LQR)

> Associate Professor Joonbum Bae Department of Mechanical Engineering UNIST

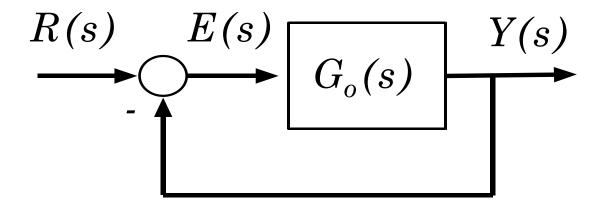
### **Outline**

- Brief review of SISO control systems
  - gain and phase margins
  - root locus
- LQR problem
- Return difference equality for LQR
  - SISO systems
- Guaranteed gain and phase margins of LQR
- Symmetric root locus for a SISO LQR



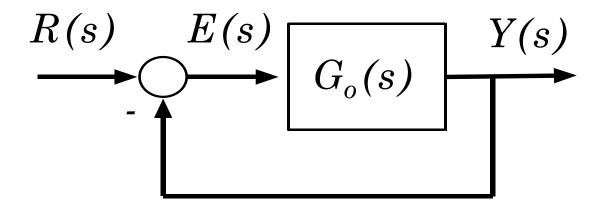
Open loop Transfer Function:

$$G_o(s) = C(s) G(s) = \frac{B(s)}{A(s)}$$



Open loop Transfer Function:

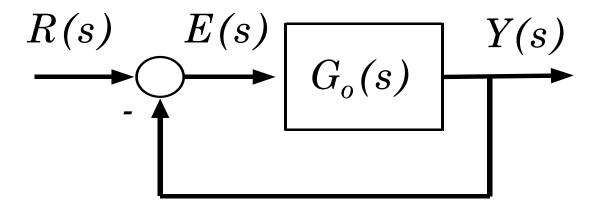
$$G_o(s) = \frac{B(s)}{A(s)} = \frac{b_m s^m + \dots + b_o}{s^n + \dots + a_o}$$



Open loop Transfer Function:

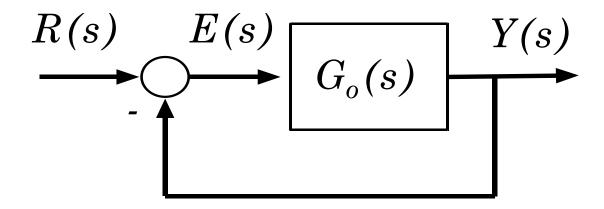
$$G_{o}(s) = \frac{B(s)}{A(s)} = \frac{b_{m}(s - z_{o1}) \cdots (s - z_{om})}{(s - p_{o1}) \cdots (s - p_{on})}$$

$$open loop poles$$



#### **Closed Transfer Functions:**

$$\frac{Y(s)}{R(s)} = G_o(s)$$
Return difference:
$$\frac{E(s)}{R(s)} = \frac{1}{1 + G_o(s)}$$
Return difference:

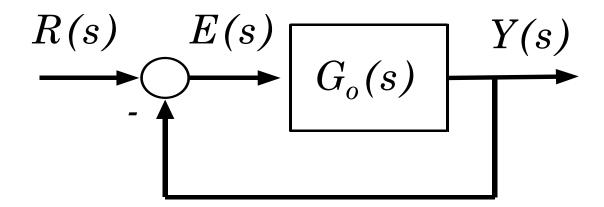


Closed Loop poles: roots of the return difference

$$D(s) = 1 + G_0(s) = 0$$

$$A_c(s) = 0$$

$$D(s) = 1 + \frac{B(s)}{A(s)} = \frac{A(s) + B(s)}{A(s)} = 0$$



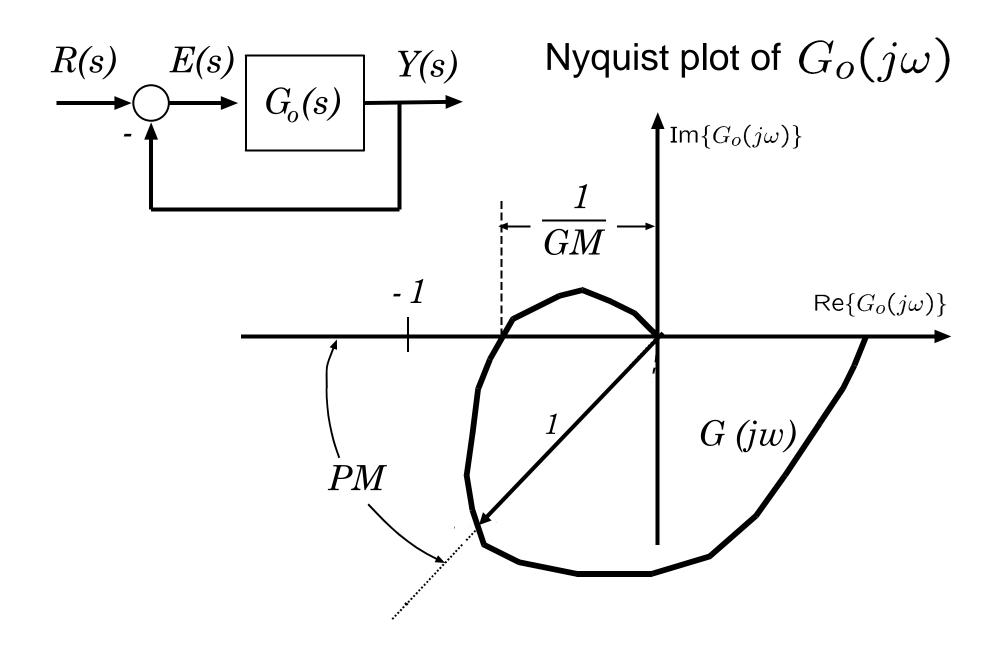
Return difference:

$$D(s) = 1 + G_o(s)$$

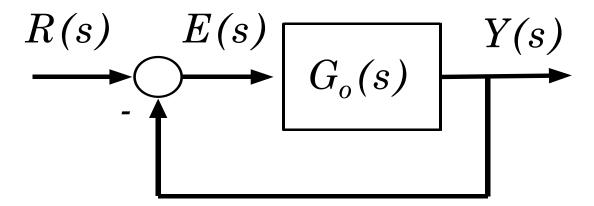
$$D(s) = \frac{A_c(s)}{A(s)} = \frac{(s - p_{c1}) \cdots (s - p_{cn})}{(s - p_{o1}) \cdots (s - p_{on})}$$

$$open loop poles$$

### Basic Review: Gain and Phase Margins



### **Basic Review: Root Locus**

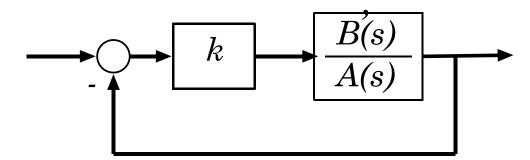


Closed Loop poles: roots of the return difference

$$D(s) = \frac{A_c(s)}{A(s)} = 1 + \frac{B(s)}{A(s)} = 1 + \frac{b_m s^m + \dots + b_o}{s^n + \dots + a_o}$$

$$= 1 + k \frac{s^m + \dots + b'_o}{s^n + \dots + a_o} = 1 + k \frac{B'(s)}{A(s)}$$

### **Basic Review: Root Locus**



Root Locus: How close loop poles change with k
 closed loop poles

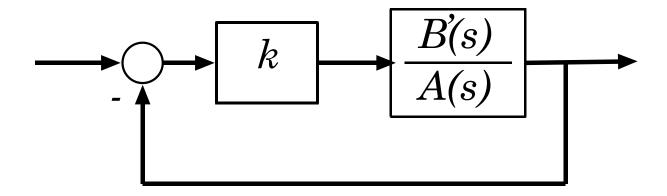
$$\frac{A_c(s)}{A(s)} = 1 + k \frac{B'(s)}{A(s)}$$
 open loop zeros

open loop poles

 All polynomials must be monic,

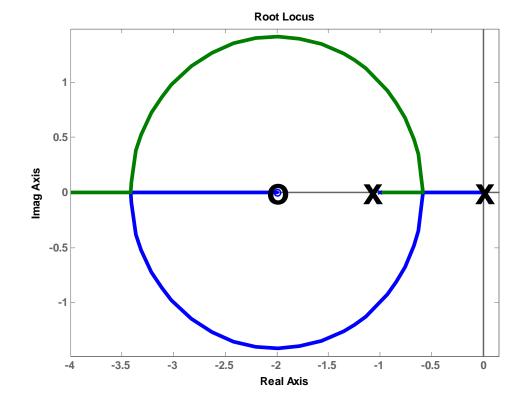
$$A(s) = s^n + \dots + a_0$$

### Basic Review: Root Locus



### • Example:

$$\frac{B'(s)}{A(s)} = \frac{s+2}{s(s+1)}$$



## Infinite Horizon LQ Regulator (LQR)

In the remainder we will analyze LQRs and show:

- LQR exhibit some nice robustness properties
  - guaranteed gain and phase margins
- Closed loop eigenvalues of LQR can be plotted as the function of the control input weight
  - Symmetric root locus techniques

## Infinite Horizon LQ Regulator (LQR)

Consider a controllable and observable nth order LTI system:

$$\dot{x}(t) = Ax(t) + Bu(t) \qquad x(0) = x_0$$

Under the optimal control:

$$u(t) = -Kx(t)$$

which minimizes the cost functional:

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T Q x + u^T R u \right\} dt$$
$$Q = Q^T \succ 0$$
$$R = R^T \succ 0$$

## Optimal LQR

The optimal control law is given by:

$$u(t) = -Kx(t)$$

where:

$$K = R^{-1}B^T P$$

and P satisfies the following  $Algebraic\ Riccati\ Equation$  (ARE):

$$0 = A^{T} P + P A + C^{T} C - P B R^{-1} B^{T} P$$

### Cost function

Notice that the cost functional

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T Q x + u^T R u \right\} dt$$
$$Q = C^T C$$

defining,

$$y = Cx$$

we have,

$$J = \frac{1}{2} \int_0^\infty \left\{ y^T y + u^T R u \right\} dt$$

### Cost function

$$J = \frac{1}{2} \int_0^\infty \left\{ y^T y + u^T R u \right\} dt$$

Where,

$$y = Cx Q = C^T C$$

define the transfer function:

$$G(s) = C(sI - A)^{-1}B = C\Phi(s)B$$
  
 $\phi(s) = (sI - A)^{-1} = \mathcal{L}\{\phi(t)\} = \mathcal{L}\{e^{At}\}$ 

### Optimal LQR

The closed loop system,

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$u(t) = -K x(t) + v(t)$$

$$v = 0$$

exogenous reference input

Output (for cost function)

$$y = Cx$$

$$J = \frac{1}{2} \int_0^\infty \left\{ y^T y + u^T R u \right\} dt$$

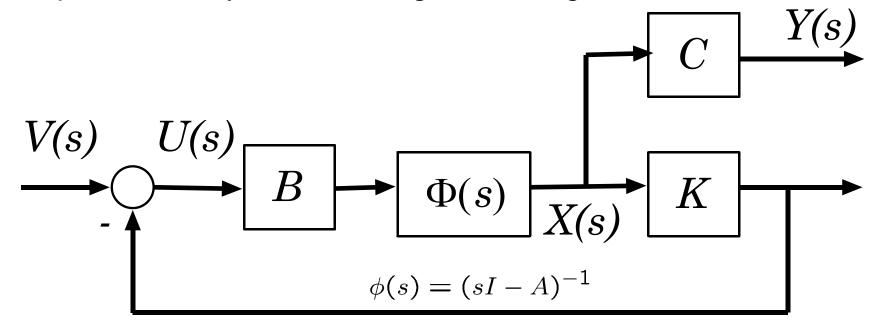
## Optimal LQR

The closed loop system,

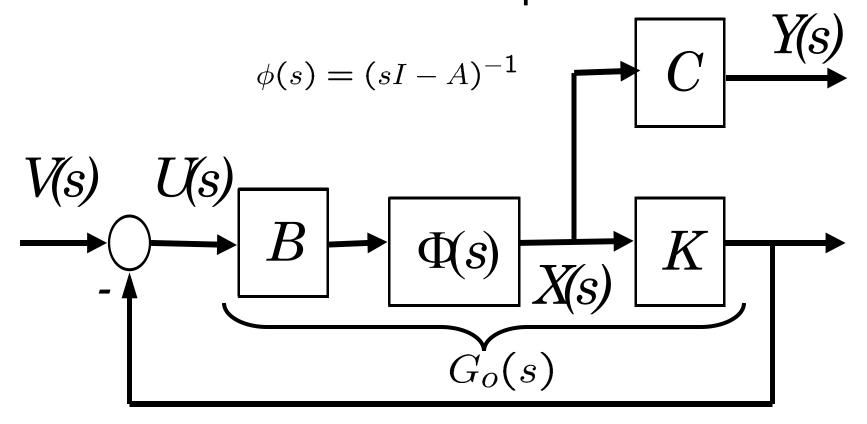
$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$u(t) = -Kx(t) + v(t) \qquad y = Cx$$

Is represented by the following block diagram:



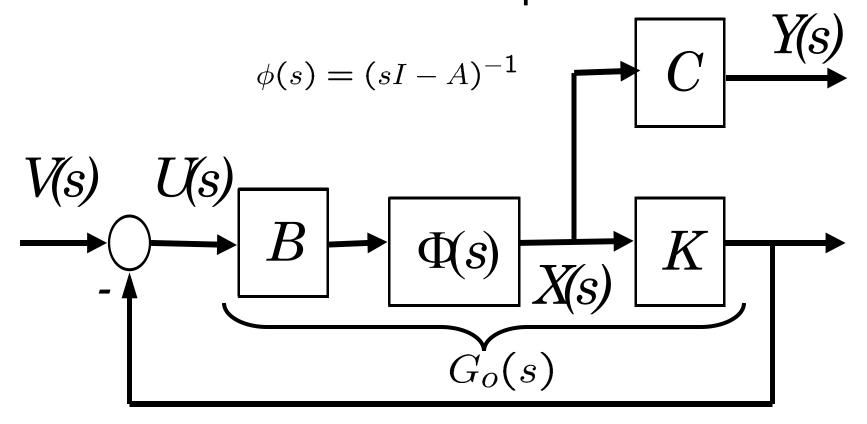
# Open Loop & Closed Loop Transfer Functions of the Optimal LQR



The open loop transfer function:

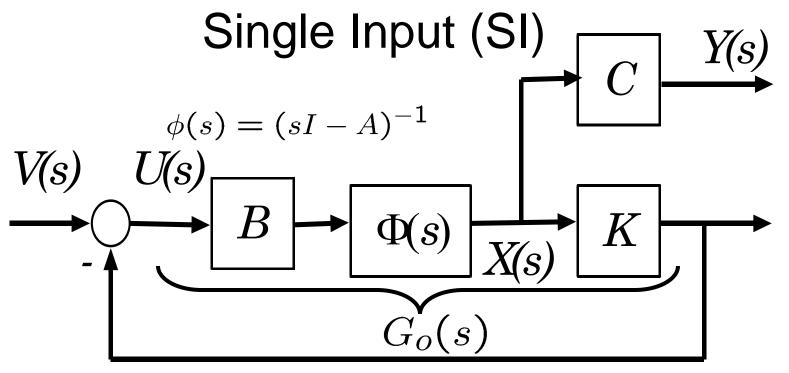
$$G_o(s) = K\Phi(s)B$$

## Open Loop & Closed Loop Transfer Functions of the Optimal LQR



The closed loop transfer function from V(s) to U(s):

$$U(s) = (I + K\Phi(s)B)^{-1}V(s)$$



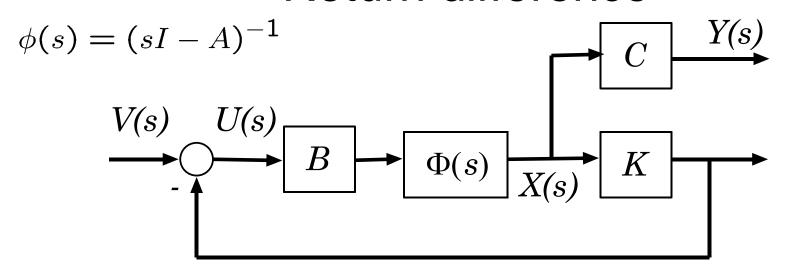
The open loop transfer function:

$$G_o(s) = K\Phi(s)B$$

The closed loop transfer function from V(s) to U(s):

$$\frac{U(s)}{V(s)} = \frac{1}{(1 + G_o(s))} = \frac{1}{(1 + K\Phi(s)B)}$$

### Return difference



### **Return difference:**

$$D(s) = (I + G_o(s))$$

$$G_o(s) = K\Phi(s)B$$
  $G(s) = C\Phi(s)B$ 

## Optimal LQR

The cost functional can be rewritten as:

$$J = \frac{1}{2} \int_0^\infty \left\{ y^T y + u^T R u \right\} dt$$

Where, 
$$y = Cx$$
  
 $u = -Kx$   $\phi(s) = (sI - A)^{-1}$ 

Return difference:

$$D(s) = (I + K\Phi(s)B)$$

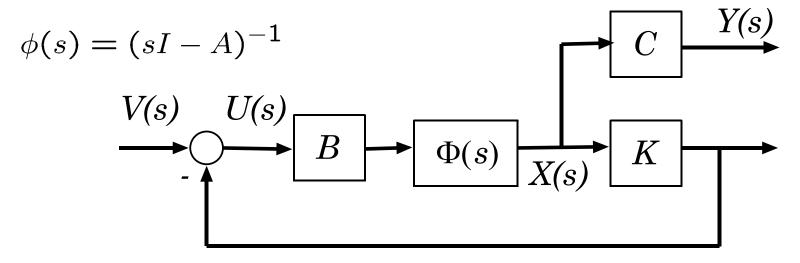
TF from U(s) to Y(s):

$$G(s) = C\Phi(s)B$$

Open loop transfer function:

$$G_o(s) = K\Phi(s)B$$

### Return difference equality



#### Return difference equality:

$$(I + G_o^T(-s)) R (I + G_o(s)) = R + G^T(-s) G(s)$$

$$G_o(s) = K\Phi(s)B$$
  $G(s) = C\Phi(s)B$ 

## Return difference equality (SISO)

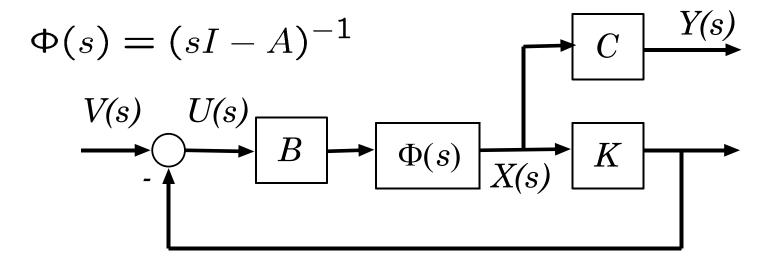
$$(1 + G_o(s)) R (1 + G_o(s)) = R + G(-s) G(s)$$

Multiply both sides by  $\frac{1}{R}$ 

$$(1+G_o(-s))(1+G_o(s))=1+\frac{1}{R}G(-s)G(s)$$

$$G_o(s) = K\Phi(s)B$$
  $G(s) = C\Phi(s)B$ 

## Return difference equality (SISO)

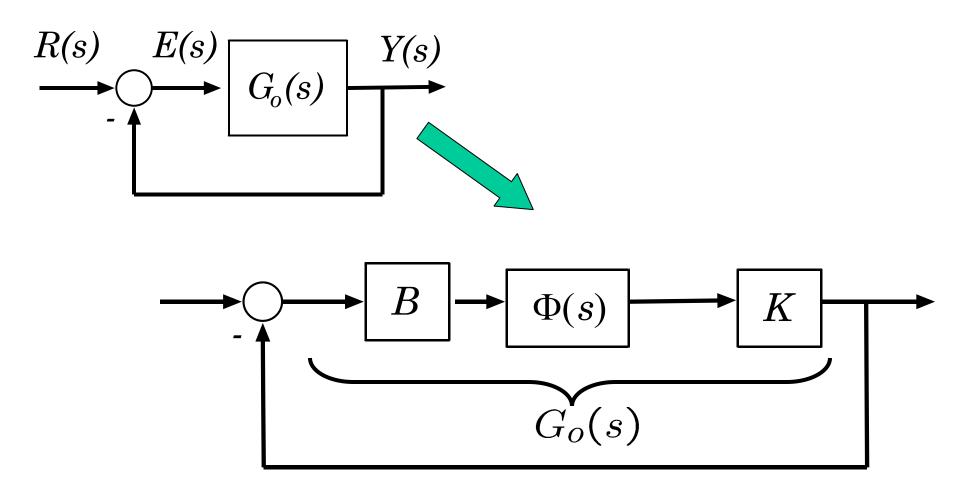


Return difference equality:

$$(1+G_o(-s))(1+G_o(s))=1+\frac{1}{R}G(-s)G(s)$$

$$G_o(s) = K\Phi(s)B$$
  $G(s) = C\Phi(s)B$ 

## Gain and Phase Margins for LQR



$$(1+G_o(-s))(1+G_o(s)) = 1 + \frac{1}{R}G(-s)G(s)$$

## Stability Margins of SISO LQR

$$(1+G_o(-s))(1+G_o(s)) = 1 + \frac{1}{R}G(-s)G(s)$$

Set s = j w:

$$(1 + G_o(-j\omega)) (1 + G_o(j\omega)) = 1 + \frac{1}{R} G(-j\omega) G(j\omega)$$

$$D^*(j\omega) \qquad D(j\omega)$$

$$|D(j\omega)|^2 \qquad 1 + \frac{1}{R} |G(j\omega)|^2$$

$$|1 + G_o(j\omega)|^2$$

## Stability Margins of SISO LQR

$$(1 + G_o(-s))(1 + G_o(s)) = 1 + \frac{1}{R}G(-s)G(s)$$

Set s = j w:

$$(1 + G_o(-j\omega)) (1 + G_o(j\omega)) = 1 + \frac{1}{R} G(-j\omega) G(j\omega)$$

$$D^*(j\omega) \qquad D(j\omega) \qquad G^*(j\omega) G(j\omega)$$

$$|(1 + G_o(j\omega))|^2 = 1 + \frac{1}{R}|G(j\omega)|^2$$

## Stability Margins of SISO LQR

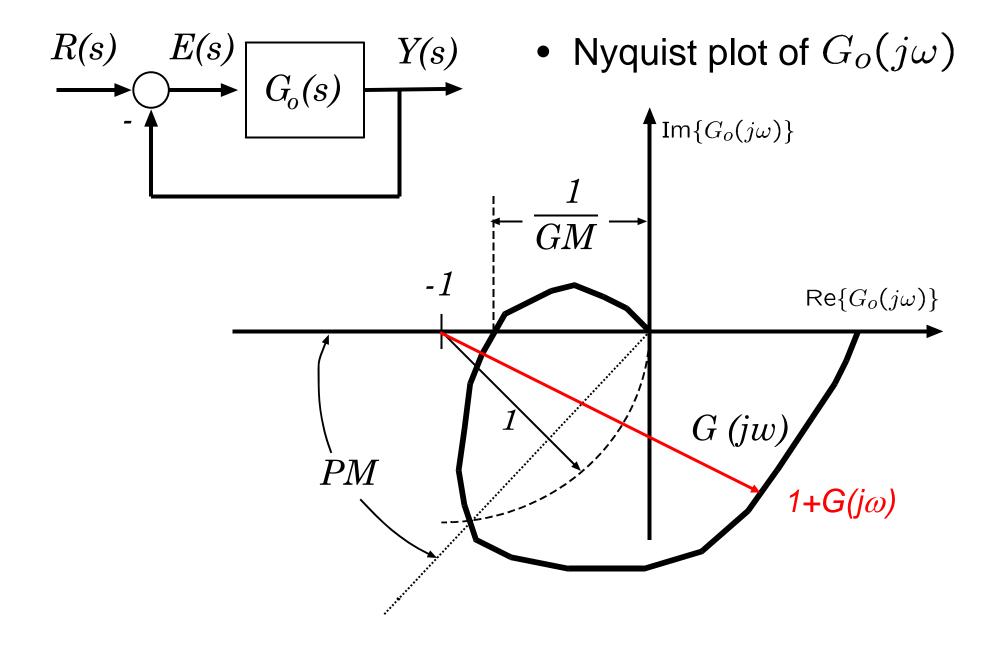
$$|(1 + G_o(j\omega))|^2 = 1 + \frac{1}{R} |G(j\omega)|^2$$

$$\ge 0$$

$$|(1+G_o(j\omega))|^2 \ge 1$$

$$G_o(s) = K\Phi(s)B$$
  $G(s) = C\Phi(s)B$ 

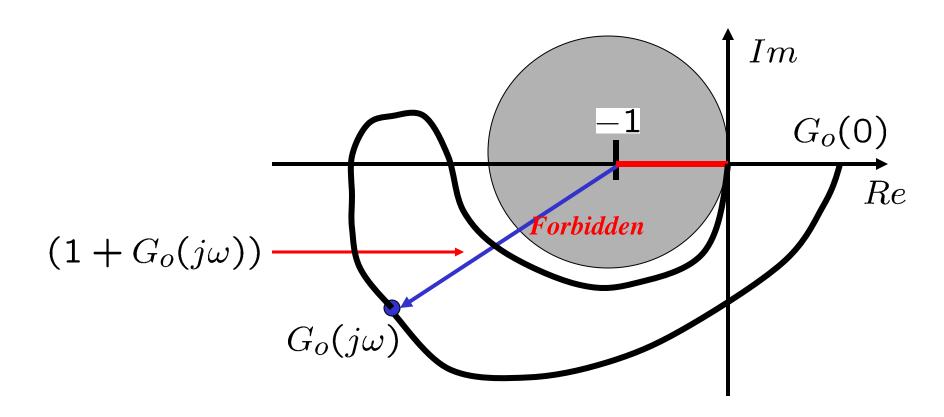
## Gain and Phase Margins



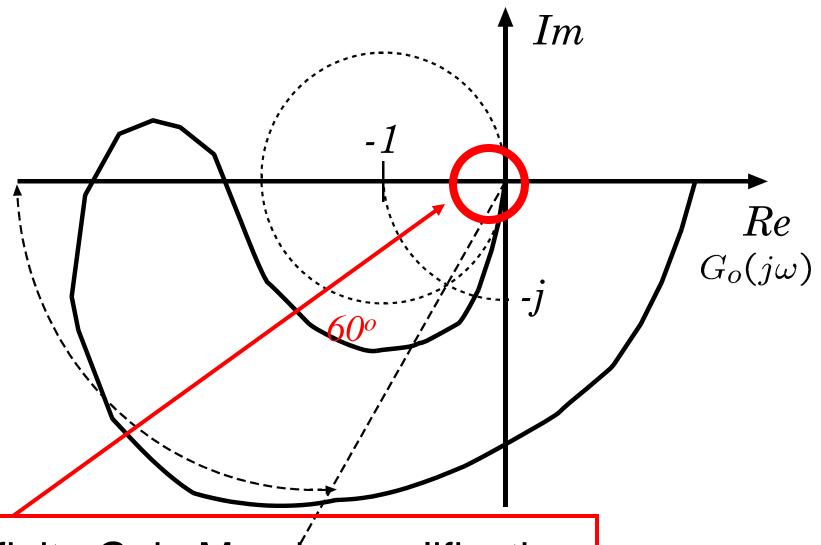
## Gain and Phase Margins for SI LQR

$$|(1+G_o(j\omega))|^2 \ge 1$$

Nyquist plot of  $G_o(j\omega)$ 

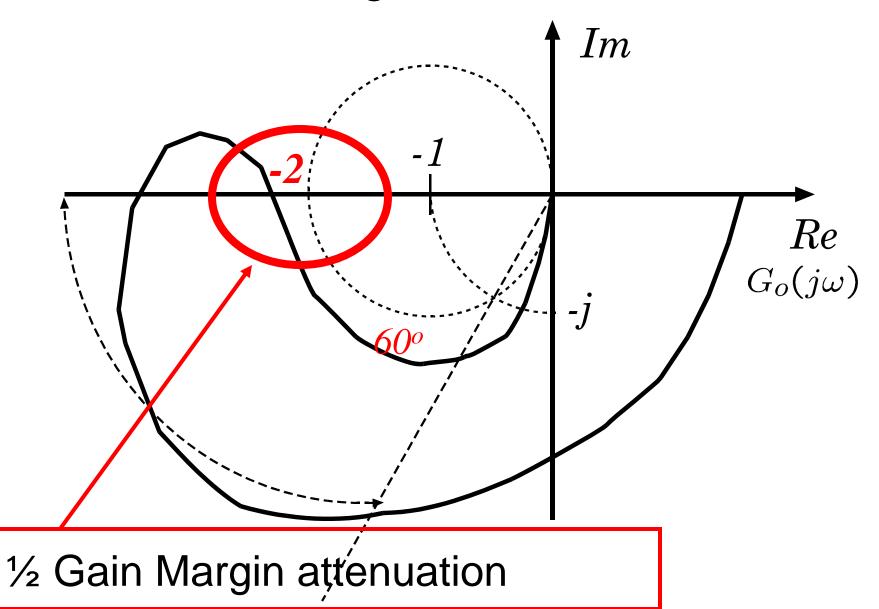


## Gain margin amplification

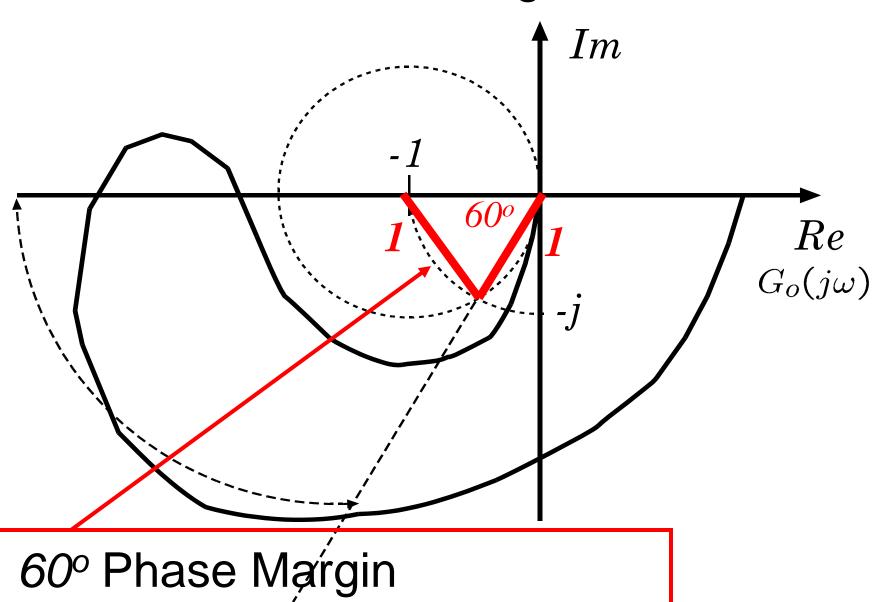


Infinite Gain Margin amplification

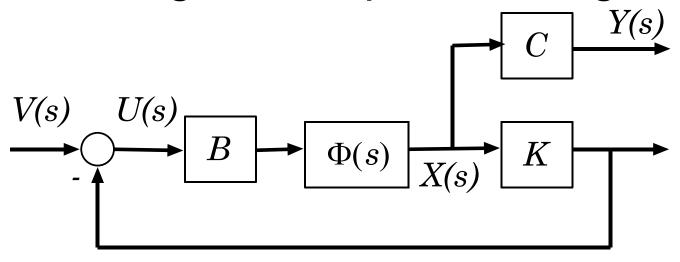
## Gain margin attenuation



## Phase margin



# LQR gain and phase margins



- Gain margins:
  - infinite gain margin amplification
  - ½ gain margin attenuation
- 60° phase margin

# Closed Loop Eigenvalues (SISO)

$$\dot{x} = Ax + Bu$$

$$u = -Kx + v$$

$$V(s) U(s)$$

$$W(s) V(s) V(s)$$

$$V(s) V(s) V(s)$$

$$V(s) V(s)$$

Open loop characteristic polynomial:

$$A(s) = \det(sI - A)$$

Closed loop characteristic polynomial:

$$A_c(s) = \det(sI - A + BK)$$

# Closed Loop Eigenvalues (SISO)

$$\Phi(s) = (sI - A)^{-1}$$

$$G_O(s) = K\Phi(s)B$$

$$V(s) \qquad U(s) \qquad B$$

$$\Phi(s) \qquad K$$

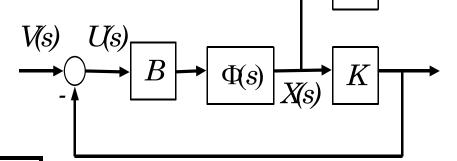
Notice that:

$$D(s) = 1 + G_o(s) = \frac{A_c(s)}{A(s)} = \frac{\det(sI - A + BK)}{\det(sI - A)}$$

$$= \frac{(s - p_{c1}) \cdots (s - p_{cn})}{(s - p_{o1}) \cdots (s - p_{on})}$$
open loop poles



$$1 + G_o(s) = \frac{A_c(s)}{A(s)} \qquad \frac{V(s)}{A(s)} U(s)$$



$$G(s) = C\Phi(s)B = \frac{B(s)}{A(s)}$$

Return difference equality:

$$(1 + G_o(-s))(1 + G_o(s)) = 1 + \frac{1}{R}G(-s)G(s)$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \frac{B(-s)}{A(-s)} \frac{B(s)}{A(s)}$$

Determine how closed loop eigenvalues change when the control weight, R, is varied from infinity to zero.

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \frac{B(-s)}{A(-s)} \frac{B(s)}{A(s)}$$

$$A_c(-s) A_c(s) = A(s) A(-s) + \frac{1}{R} B(-s) B(s)$$

$$A_c(-s) A_c(s) = A(s) A(-s) + \frac{1}{R} B(-s) B(s)$$

#### Open loop poles and zeros

$$A(s) = \prod_{i=1}^{n} (s - p_{oi}) = (s - p_{o1}) \cdots (s - p_{on})$$

$$B(s) = b_m \prod_{i=1}^{m} (s - z_{oi}) = b_m (s - z_{o1}) \cdots (s - z_{om})$$

#### Closed loop poles:

$$A_c(s) = \prod_{i=1}^n (s - p_{ci}) = (s - p_{c1}) \cdots (s - p_{cn})$$

$$A_c(-s) A_c(s) = A(s) A(-s) + \frac{1}{R} B(-s) B(s)$$

e.g.

What about?

$$A(s) = \prod_{i=1}^{n} (s - p_{oi}) \longrightarrow A(-s) = \prod_{i=1}^{n} (-s - p_{oi})$$

$$A(-s) = \prod_{i=1}^{n} -1(s+p_{oi}) = (-1)(s+p_{o1})\cdots(-1)(s+p_{on})$$

$$A(-s) = (-1)^n \prod_{i=1}^n (s + p_{oi})$$

$$A_c(-s) A_c(s) = A(s) A(-s) + \frac{1}{R} B(-s) B(s)$$

$$A(-s) = (-1)^n \prod_{i=1}^n (s + p_{oi})$$

$$B(-s) = b_m (-1)^m \prod_{i=1}^m (s + z_{oi})$$

$$A_c(-s) = (-1)^n \prod_{i=1}^n (s + p_{ci})$$

Thus, from

$$A_{c}(-s) \underline{A_{c}(s)} = A(-s) \underline{A(s)} + \frac{1}{R} B(-s) \underline{B(s)}$$

$$(-1)^{n} \prod_{i=1}^{n} (s + p_{ci}) \prod_{\underline{i=1}}^{n} (s - p_{ci}) = (-1)^{n} \prod_{i=1}^{n} (s + p_{oi}) \prod_{\underline{i=1}}^{n} (s - p_{0i})$$

$$+ \frac{1}{R} (-1)^{m} b_{m} \prod_{\underline{i=1}}^{m} (s + z_{oi}) b_{m} \prod_{\underline{i=1}}^{m} (s - z_{oi})$$

Thus, from

$$\frac{A_c(-s) A_c(s) = A(-s) A(s) + \frac{1}{R} B(-s) B(s)}{(-1)^n \prod_{i=1}^n (s + p_{ci}) \prod_{i=1}^n (s - p_{ci})} = (-1)^n \prod_{i=1}^n (s + p_{oi}) \prod_{i=1}^n (s - p_{0i}) + \frac{1}{R} (-1)^m b_m \prod_{i=1}^m (s + z_{oi}) b_m \prod_{i=1}^m (s - z_{oi})$$

$$(-1)^n \prod_{i=1}^n (s+p_{ci}) \prod_{i=1}^n (s-p_{ci}) = (-1)^n \prod_{i=1}^n (s+p_{oi}) \prod_{i=1}^n (s-p_{0i})$$

$$+ \frac{1}{R} (-1)^m b_m \prod_{i=1}^m (s+z_{oi}) b_m \prod_{i=1}^m (s-z_{oi})$$

#### Multiplying by $(-1)^n$ and grouping $b_m$ terms:

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{0i})$$

$$+\frac{b_m^2}{R}(-1)^{(n-m)}\prod_{i=1}^m(s+z_{oi})\prod_{i=1}^m(s-z_{oi})$$

non negative number, function of  $R \in (0, \infty)$ 

## Return difference equality - Left

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

$$+(-1)^{n-m}\frac{b_m^2}{R}\prod_{i=1}^m(s+z_{oi})\prod_{i=1}^m(s-z_{oi})$$

closed loop eigenvalues
(always asymptotically stable)

$$R \in (0, \infty)$$

negative of closed loop eigenvalues (always unstable)

# Return difference equality - Right

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

negatives of open loop poles

open loop poles

$$+(-1)^{n-m}\frac{b_m^2}{R}\prod_{i=1}^m(s+z_{oi})\prod_{i=1}^m(s-z_{oi})$$

negatives of open loop zeros

open loop zeros

## Return difference equality - Right

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

$$+(-1)^{n-m}\frac{b_m^2}{R}\prod_{i=1}^m(s+z_{oi})\prod_{i=1}^m(s-z_{oi})$$

n-m even  $\Rightarrow$  negative feedback

n-m odd  $\Rightarrow$  positive feedback

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

$$+(-1)^{n-m} \frac{b_m^2}{R} \prod_{i=1}^m (s+z_{oi}) \prod_{i=1}^m (s-z_{oi})$$

$$R o \infty \ \Rightarrow \ p_{ci} o ext{Stable} \left\{ egin{array}{l} p_{oi} \ ext{or} \ -p_{oi} \end{array} 
ight.$$
  $R o \infty \ \Rightarrow \ -p_{ci} o ext{Unstable} \left\{ egin{array}{l} p_{oi} \ ext{or} \ -p_{oi} \end{array} 
ight.$ 

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

$$+(-1)^{n-m} \frac{b_m^2}{R} \prod_{i=1}^m (s+z_{oi}) \prod_{i=1}^m (s-z_{oi})$$

$$R o 0 \ \Rightarrow \ p_{ci} o ext{Stable} \left\{egin{array}{l} z_{oi} \ -z_{oi} \ R o 0 \ \Rightarrow \ -p_{ci} o ext{Unstable} \left\{egin{array}{l} z_{oi} \ ext{or} \ -z_{oi} \ \end{array}
ight. \end{array}
ight. i = 1, \cdots, m 
ight.$$

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

$$i=n-m,\,\cdots,\,n$$

$$+(-1)^{n-m} \prod_{i=1}^{b_m^2} (s+z_{oi}) \prod_{i=1}^m (s-z_{oi})$$

$$R \to 0 \Rightarrow |p_{ci}|, |-p_{ci}| \to \infty$$

n-m: ODD

Angle of asymptotes

$$\frac{l \pi}{n-m}$$

$$l = 0, 1, \dots, 2(n-m)-1$$

$$\prod_{i=1}^{n} (s + p_{ci}) \prod_{i=1}^{n} (s - p_{ci}) = \prod_{i=1}^{n} (s + p_{oi}) \prod_{i=1}^{n} (s - p_{oi})$$

$$i=n-m, \cdots, n$$

$$i = n - m, \dots, n$$
  $+ (-1)^{n-m} \frac{b_m^2}{R} \prod_{i=1}^m (s + z_{oi}) \prod_{i=1}^m (s - z_{oi})$ 

$$R \to 0 \Rightarrow |p_{ci}|, |-p_{ci}| \to \infty$$

n-m: EVEN

Angle of 
$$\frac{(l+\frac{1}{2})\pi}{n-m}$$

$$l = 0, 1, \cdots, 2(n-m)-1$$

### LQ optimal control example

Double integrator

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$U(s)$$
 $1$ 
 $s$ 
 $x_2(s)$ 
 $x_1(s)$ 
 $x_1(s)$ 
 $x_2(s)$ 
 $x_3(s)$ 
 $x_4(s)$ 
 $x_4(s)$ 
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 $x_5(s)$ 
 $x_6(s)$ 
 $x_6(s)$ 
 $x_6(s)$ 
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 $x_1($ 

Double integrator

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \, C^T \, C \, x + R \, u^2 \right\} \, dt$$

with

Double integrator

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} x$$

$$G(s) = C(sI - A)^{-1}B = \frac{1}{s^2}$$

2 open loop poles at the origin

no open loop zeros

### Return Difference Equality

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \frac{B(-s)}{A(-s)} \frac{B(s)}{A(s)}$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \left(\frac{1}{-s}\right)^2 \left(\frac{1}{s}\right)^2$$

$$\frac{A_c(-s)}{(-s)^2} \frac{A_c(s)}{s^2} = 1 + \frac{1}{R} \left(\frac{1}{-s}\right)^2 \left(\frac{1}{s}\right)^2$$

$$A_c(-s) A_c(s) = (s)^2 (-s)^2 + \frac{1}{R}$$

Thus, from

$$A_c(-s) A_c(s) = (s)^2 (-s)^2 + \frac{1}{R}$$

We obtain

$$\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci}) = (s)^{4} + (-1)^{2} \frac{1}{R}$$

$$n-m=2$$
 EVEN

Symmetric Root Locus:

$$\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci}) = (s)^{4} + \frac{1}{R}$$

or

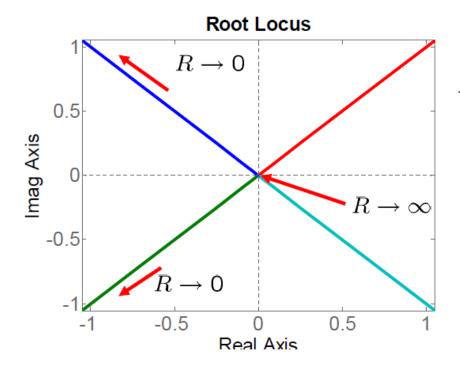
$$\frac{\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci})}{s^{4}} = 1 + \frac{1}{R} \frac{1}{s^{4}}$$

#### Double integrator

$$1 + \frac{1}{R} \frac{1}{s^4} = 0$$

$$R \to 0 \Rightarrow |p_{ci}|, |-p_{ci}| \to \infty$$

#### Asymptotes:



$$\frac{(l+\frac{1}{2})\pi}{2} \quad l = 0, 1, 2, 3$$

$$+45^{o}$$
 $+135^{o}$ 
 $-45^{o}$ 

 $-135^{o}$ 

Double integrator (change state weight matrix  $Q = C^T C$  )

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \, C^T \, C \, x + R \, u^2 \right\} \, dt$$

with

$$C = \begin{bmatrix} 1 & 1 \end{bmatrix}$$
  $R > 0$  position and velocity are penalized

Double integrator (change state weight matrix  $Q = C^T C$ )

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 1 \end{bmatrix} x$$

$$G(s) = C(sI - A)^{-1}B = \frac{s+1}{s^2}$$

2 open loop poles at the origin

1 open loop zero at -1

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \frac{B(-s)}{A(-s)} \frac{B(s)}{A(s)}$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \left( \frac{-s+1}{-s^2} \right) \left( \frac{s+1}{s^2} \right)$$

$$\frac{A_c(-s)}{(-s)^2} \frac{A_c(s)}{s^2} = 1 + \frac{1}{R} \left( \frac{-s+1}{-s^2} \right) \left( \frac{s+1}{s^2} \right)$$

$$A_c(-s) A_c(s) = (s)^2 (-s)^2 + \frac{1}{R} (-s+1)(s+1)$$

Thus, from

$$A_c(-s) A_c(s) = (s)^2 (-s)^2 + \frac{1}{R} (-s+1)(s+1)$$

We obtain

$$\prod_{i=1}^{2} (s+p_{ci}) \prod_{i=1}^{2} (s-p_{ci}) = (s)^{4} + \frac{1}{R} (-1)^{1} (s+1)(s-1)$$

$$n-m=2-1=1 \qquad \text{EVEN}$$

Symmetric Root Locus:

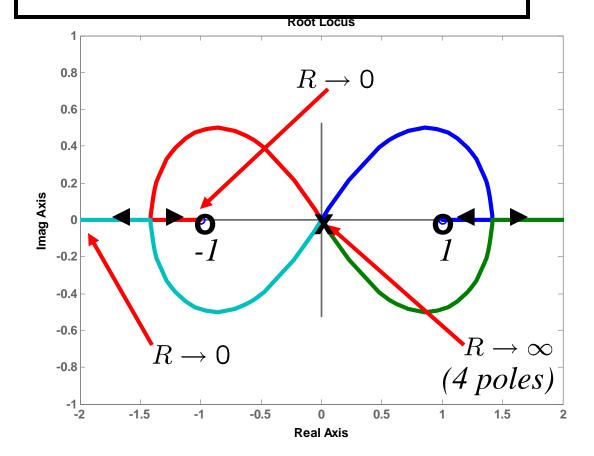
$$\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci}) = (s)^{4} - \frac{1}{R} (s + 1)(s - 1)$$

or

$$\frac{\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci})}{s^{4}} = 1 - \frac{1}{R} \frac{(s+1)(s-1)}{s^{4}}$$

Double integrator (change state weight matrix  $Q = C^T C$  )

$$1 - \frac{1}{R} \frac{(s+1)(s-1)}{s^4} = 0$$



$$R \longrightarrow 0$$
 $p_{c1} \rightarrow -1$ 
 $p_{c2} \rightarrow -\infty$ 
 $-p_{c1} \rightarrow 1$ 
 $-p_{c2} \rightarrow \infty$ 

Asymptotes:

$$l = 0, 1$$

$$+0^{o}$$

$$+180^{o}$$

Open-loop unstable system:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \, C^T \, C \, x + R \, u^2 \right\} \, dt$$

with

$$C = \begin{bmatrix} 1 & 0 \end{bmatrix}$$
  $R > 0$ 
Only  $x_1$  is penalized

Open-loop unstable system:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} x$$

$$G(s) = C(sI - A)^{-1}B = \frac{1}{(s+1)(s-2)}$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \frac{B(-s)}{A(-s)} \frac{B(s)}{A(s)}$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \left( \frac{1}{(s+1)(s-2)} \right) \left( \frac{1}{(-s+1)(-s-2)} \right)$$

$$A_c(-s) A_c(s) = (s+1)(-s+1)(s-2)(-s-2) + \frac{1}{R}$$

Thus, from

$$A_c(-s) A_c(s) = (s+1)(-s+1) (s-2)(-s-2) + \frac{1}{R}$$

We obtain

$$\prod_{i=1}^{2} (s+p_{ci}) \prod_{i=1}^{2} (s-p_{ci}) = (s+1)(s-1)(s-2)(s+2) + (-1)^{2} \frac{1}{R}$$

$$n-m=2$$
 EVEN

#### Symmetric Root Locus:

$$\prod_{i=1}^{2} (s+p_{ci}) \prod_{i=1}^{2} (s-p_{ci}) = (s+1)(s-1)(s-2)(s+2) + \frac{1}{R}$$

or

$$\frac{\prod_{i=1}^{2}(s+p_{ci})\prod_{i=1}^{2}(s-p_{ci})}{(s+1)(s-1)(s-2)(s+2)} =$$

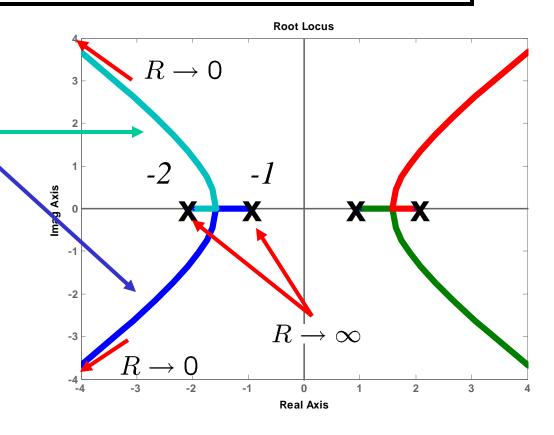
$$1 + \frac{1}{R} \frac{1}{(s+1)(s-1)(s-2)(s+2)}$$

Open-loop unstable system:

$$1 + \frac{1}{R} \frac{1}{(s+1)(s-1)(s-2)(s+2)} = 0$$

Close-loop poles (always asymptotically stable)  $R \in (0, \infty)$ 

Open-loop poles:



Open-loop unstable system(change state weight matrix  $Q = C^T C$ 

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \, C^T \, C \, x + R \, u^2 \right\} \, dt$$

with

$$C = \begin{bmatrix} 1 & 1 \end{bmatrix}$$
  $R > 0$   $x_1$  and  $x_2$  are penalized

Open-loop unstable system(change state weight matrix  $Q = C^T C$ 

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 1 \end{bmatrix} x$$

$$G(s) = C(sI - A)^{-1}B = \frac{(s+2)}{(s+1)(s-2)}$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \frac{B(-s)}{A(-s)} \frac{B(s)}{A(s)}$$

$$\frac{A_c(-s)}{A(-s)} \frac{A_c(s)}{A(s)} = 1 + \frac{1}{R} \left( \frac{s+2}{(s+1)(s-2)} \right) \left( \frac{-s+2}{(-s+1)(-s-2)} \right)$$

$$\prod_{i=1}^{2} (s+p_{ci}) \prod_{i=1}^{2} (s-p_{ci}) = (s+1)(s-1)(s-2)(s+2)$$
$$-\frac{1}{R}(s+2)(s-2)$$

#### Symmetric Root Locus:

$$\prod_{i=1}^{2} (s+p_{ci}) \prod_{i=1}^{2} (s-p_{ci}) = (s+1)(s-1)(s-2)(s+2)$$
$$-\frac{1}{R}(s+2)(s-2)$$

or

$$\frac{\prod_{i=1}^{2}(s+p_{ci})\prod_{i=1}^{2}(s-p_{ci})}{(s+1)(s-1)(s-2)(s+2)} =$$

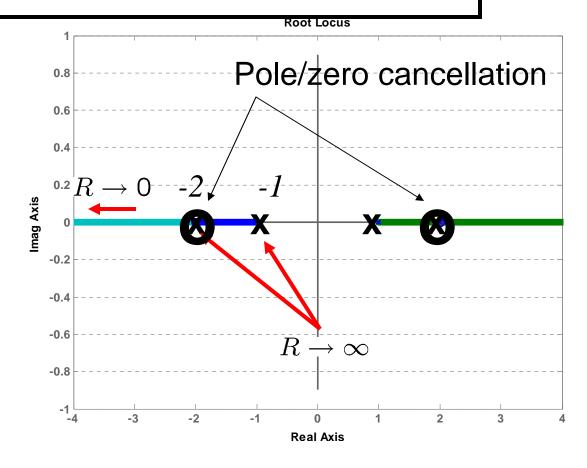
$$1 - \frac{1}{R} \frac{(s-2)(s+2)}{(s+1)(s-1)(s-2)(s+2)}$$

Open-loop unstable system(change state weight matrix  $Q = C^T C$ )

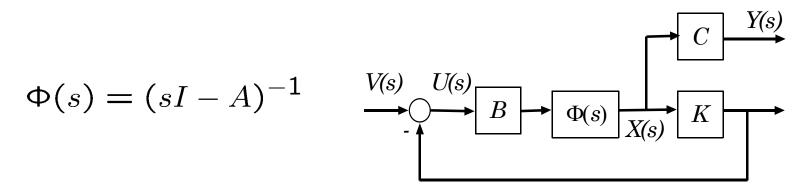
$$1 - \frac{1}{R} \frac{(s+2)(s-2)}{(s+1)(s-1)(s-2)(s+2)} = 0$$

Close-loop poles (always asymptotically stable)  $R \in (0, \infty)$ 

Open-loop poles: -1,+2



# Symmetric root locus for SIMO Systems



$$(1 + G_o(-s))(1 + G_o(s)) = 1 + \frac{1}{R}G(-s)^T G(s)$$

Let: 
$$y(t) \in \mathcal{R}^p$$
  $\Rightarrow$   $G_o(s) = K\Phi(s)B \in H(s)$   $\Rightarrow$   $u(t) \in \mathcal{R}$   $G(s) = C\Phi(s)B \in H^p(s)$ 

where H(s) is the class of rational functions of s

# Symmetric root locus for SIMO Systems

$$G(s) = \frac{1}{A(s)}B(s) = \frac{1}{A(s)}\begin{bmatrix} B_1(s) \\ \vdots \\ B_p(s) \end{bmatrix}$$

$$G^{T}(-s) G(s) = \frac{B^{T}(-s)B(s)}{A(-s)A(s)} = \frac{\sum_{i=1}^{p} B_{i}(-s)B_{i}(s)}{A(-s)A(s)}$$

We can always find a polynomial

$$\bar{B}(s) = \bar{b}_m s^m + \bar{b}_{m-1} s^{m-1} \cdots + \bar{b}_o$$

such that:

$$\bar{B}(-s)\bar{B}(s) = \sum_{i=1}^{p} B_i(-s) B_i(s)$$

# Symmetric root locus for SIMO Systems

$$(1 + G_o(-s))(1 + G_o(s)) = 1 + \frac{1}{R}G(-s)^T G(s)$$

for 
$$R \in (0, \infty)$$

$$(1 + G_o(s)) = \frac{A_c(s)}{A(s)}$$
  $G(-s)^T G(s) = \frac{\bar{B}(-s)\bar{B}(s)}{A(-s)A(s)}$ 

$$\frac{A_c(-s)A_c(s)}{A(-s)A(s)} = 1 + \frac{1}{R} \frac{\bar{B}(-s)\bar{B}(s)}{A(-s)A(s)}$$

Double integrator (change state weight matrix  $Q = C^T C$ )

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \, C^T \, C \, x + R \, u^2 \right\} \, dt$$

with

$$C = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \qquad R > 0$$

$$y_1 = \text{position and } y_2 = \text{velocity}$$

Double integrator (change state weight matrix  $Q = C^T C$ )

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} x$$

$$J = \frac{1}{2} \int_0^\infty \left\{ y^T y + R u^2 \right\} dt$$

$$G(s) = C(sI - A)^{-1}B = \frac{1}{s^2} \begin{bmatrix} 1 \\ s \end{bmatrix}$$

$$G^{T}(-s) G(s) = \frac{B^{T}(-s)B(s)}{A(-s)A(s)} = \frac{1 \times 1 + (-s)(s)}{((-s)^{2})(s^{2})} = \frac{(-s+1)(s+1)}{((-s)^{2})(s^{2})}$$

$$\frac{A_{c}(-s)}{A(-s)} \frac{A_{c}(s)}{A(s)} = 1 + \frac{1}{R} \left( \frac{-s+1}{(-s)^{2}} \right) \left( \frac{s+1}{s^{2}} \right)$$

$$A_{c}(-s) A_{c}(s) = A(-s) A(s) + \frac{1}{R} \bar{B}(-s) \bar{B}(s)$$

Open loop poles:

$$A(s) = s^2$$

Closed loop poles:

$$A_c(s) = \prod_{i=1}^{2} (s - p_{ci})$$

Open loop zero of G(s):

$$\bar{B}(s) = (s+1)$$

The symmetric root locus equation is the same as the one in Example 2.

Symmetric Root Locus:

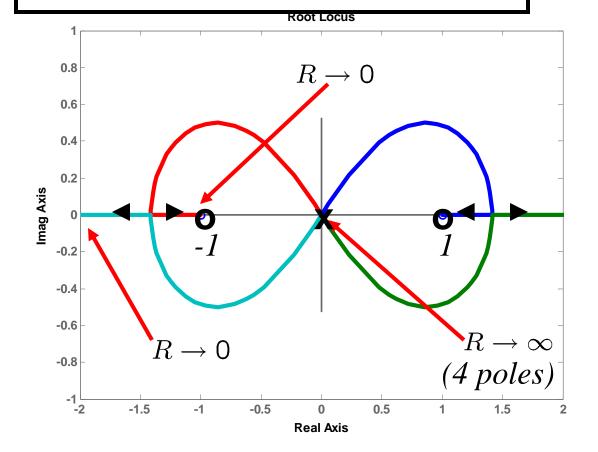
$$\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci}) = (s)^{4} - \frac{1}{R} (s+1)(s-1)$$

or

$$\frac{\prod_{i=1}^{2} (s + p_{ci}) \prod_{i=1}^{2} (s - p_{ci})}{s^{4}} = 1 - \frac{1}{R} \frac{(s+1)(s-1)}{s^{4}}$$

Double integrator (change state weight matrix  $Q = C^T C$ )

$$1 - \frac{1}{R} \frac{(s+1)(s-1)}{s^4} = 0$$



$$R \longrightarrow 0$$
 $p_{c1} \rightarrow -1$ 
 $p_{c2} \rightarrow -\infty$ 
 $-p_{c1} \rightarrow 1$ 
 $-p_{c2} \rightarrow \infty$ 

Asymptotes:

$$\frac{l}{\pi} \qquad l = 0, 1$$

$$+0^{\circ}$$

$$+180^{\circ}$$

### Cost Functions in Examples 2 & 5

• Example 2:

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} x + R u^2 \right\} dt$$

Example 5:

$$J = \frac{1}{2} \int_0^\infty \left\{ x^T \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} x + R u^2 \right\} dt$$

 The difference is in the off-diagonal elements of Q, but the two examples yielded the same symmetric root locus.

## Cost Functions in Examples 2 & 5

The off-diagonal element of Q gives:

$$J_{12} = \int_0^\infty \{x_1(t) \, x_2(t)\} \, dt$$

• Noting  $\frac{d}{dt}x_1(t) = x_2(t)$ 

$$J_{12} = \int_0^\infty \left\{ x_1(t) \frac{d}{dt} x_1(t) \right\} dt$$
$$= \frac{1}{2} \int_0^\infty \left\{ \frac{d}{dt} x_1^2(t) \right\} dt = -\frac{1}{2} x_1^2(0)$$

where the asymptotic stability has been assumed.

 The above equation means that J<sub>12</sub> does not depend on u(t).

#### Selection of Q and R in LQR

 Optimal control based on a wrong cost function (performance index) may performed poorly.

 In the quadratic cost function, the relative magnitudes between Q and R are important and not their absolute values.

#### Selection of Q and R in LQR

 In the absence of ideas about the structure of Q and R, start with diagonal Q and R.

 Diagonal elements of Q and R may be adjusted based on the expected (desired) magnitudes of state variables and inputs:

$$q_{ii} = 1/x_{i,max}^2$$
  $r_{ii} = 1/u_{i,max}^2$ 

#### Selection of Q and R in LQR

 Q and R can be made frequency dependent: Frequency Shaped Linear Quadratic (FSLQ) control.

 In some design approaches, the choice of Q and R is not based on physical considerations such as the one on the previous page: e.g. Loop Transfer Recovery (LTR) method.