ESP4 - MCR - 2302 0 = tai (3) = 36.87° (1) · Analitando el nodo F · Analitando el nodo E: 900 16 ++ 2 Fy = 0; -900 - FAF DON 0 = 0 1200 16 FAF = 0; FRF + FAF COS 0 = 0 : FDE = 1200 16 .. FEF = - FAF COS 0 = 1200 16 | FAF = 0 FAF = 1 500 16 @ FDE = 1200 16 1 FFF = 1 200 16 1 · Analytimes et nodo D = } Por inspección en l's salemos que: · Analizando et nodo A = 1500 10 1250 16 + EFx = 0; 1500 cos 0 - 1250 cos 0 + FAB = 1 1200 16 / 600 16 F_{Ay} = $F_{AB} = -1500 (0.8) + 1250 (0.8)$ 95 = 0; -1200 - FAD COS 0 + FCD COS 0 = 0 F_{AD} F_{CO} - 0.8 F_{AD} + 0.8 F_{CD} = 1200 -.. (i) · Analitondo el nodo B \$ZFy=0; -600 - Fab sen0 - Fco sen0 = 0 +1 2 Fy = 0; FBD = 0 - 0.6 FaD - 0.6 Fco = 600 - .. (ii) $F_{BC} = 0$ $F_{BC} = 0$ Resolvendo para FAD y FeD - FAD = -1250 16 FCO = 250 16 :- FR =-200 11 :. Fap = 1250 16 @ | Fcp = 250 16 @ Por simetica de la carga y occametria de la consadure - Ag = 21 kN | Ax = 0 | Hy = 21 KN | \$\delta = 36.87° · Analitando ul nodo A: 0 = tarí (2.4) = 18.92° (· Analizando el nulo c $F_{CE} = \frac{10.5 \text{ kn}}{500 \text{ kn}} = 17.5 \text{ kn}$ $F_{AB} = \frac{5.3 - 21}{f_{AB}} = \frac{47.19}{f_{AB}} = 0$ ZIKN = 5 Fx = 0; FAB WSB + FAC = 0 * ZFx = 0; -44.64 + Fco cos \$ + Fce = 0 -- FAC = - FAB COS 0 = 44:69 KN FCF = 44.64 - FCO (OS \$\phi = 30.69 kN) FAB = 47.19 KN @ FAC = 44.64 KN D · Analizando il nodo E: HTTFy=0; FDE = 0 FEG = 30.64 KN C · Analizando el nodo B 30.69 KN FEG + EFX = 0; -30.64 + FEG = 0 ... FEG = 30.64 KM 105 FRO 15 Fx = 0; 47.19 (050 + FRO (050 = 0 617 Fgo = - 47.19 KN · Vor sinction de las cargas y grammerates de la anuclera, se trans 47.19 KN TBC +1 EFy = 0; - 10.5 - FBC + 47.19 gan + (+ FBD for 0 = 0 For = FRD = 47.19 KNO "> Fec = - 10.5 + 47.19 gan 0 + Feo 800 0 Fpg = Frn = 17.5 KN (1) FRC = - 10,5 KN Fra = Fra = 10.5 kN (c) FRD = 47.19 KN @ FRC = 10.5 KN @ FFH = FAB = 47.19 KN @ FGH = FAC = 44.64 KN (7)