

# **Circuit Theory and Electronics Fundamentals**

Department of Electrical and Computer Engineering, Técnico, University of Lisbon

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## **Laboratory Assignment - T2**

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## **Contents**

<b>1</b>	<b>Introduction</b>	<b>2</b>
<b>2</b>	<b>Theoretical Analysis</b>	<b>3</b>
2.1	Task 1)	4
2.2	Task 2)	6
2.3	Task 3)	7
2.4	Task 4)	8
2.5	Task 5)	9
2.6	Task 6)	9
<b>3</b>	<b>Simulation Analysis</b>	<b>12</b>
3.1	Task 1)	12
3.2	Task 2)	13
3.3	Task 3)	15
3.4	Task 4)	16
3.5	Task 5)	18
<b>4</b>	<b>Conclusion</b>	<b>19</b>

# 1 Introduction

The objective of this laboratory assignment is to study a circuit containing:

- seven resistors ( $R_1$ - $R_7$ )
- one voltage source ( $V_s$ )
- one capacitor ( $C$ )
- one voltage-controlled current source ( $I_b$ )
- one current-controlled voltage source ( $V_d$ )

Circuit T2 is presented in Figure 1. All components, including nodes ( $N1$ - $N8$ ) are identified with their respective names (ground is marked with its symbol).

The voltage source  $v_s$  obeys the following equations:

$$v_s(t) = V_s u(-t) + \sin(2\pi f t) u(t) \quad (1)$$

$$u(t) = \begin{cases} 0 & t < 0 \\ 1 & t \geq 0 \end{cases}$$

In Section 2, a theoretical analysis of the circuit is presented. In Section 3, the circuit is analysed by simulation, and the results are compared to the theoretical results obtained in Section 2. The conclusions of this study are outlined in Section 4.

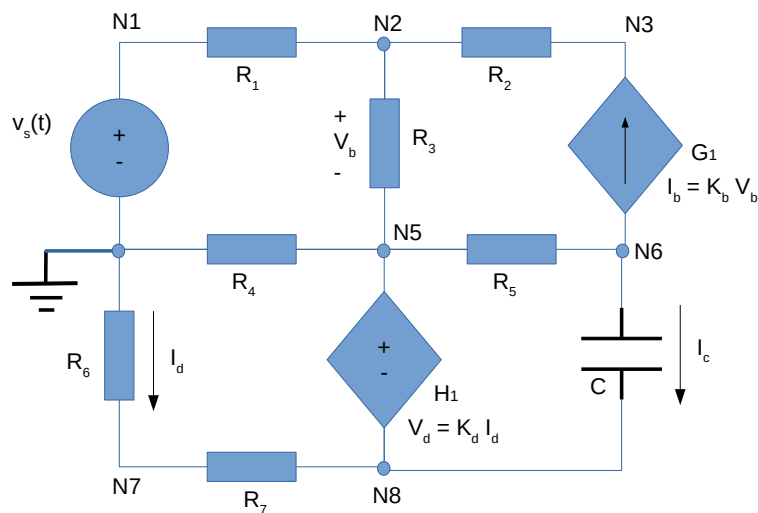


Figure 1: Circuit T2

For this laboratory assignment, the values considered for all the variables can be found on Table 1. They were obtained through a Python script that generates random values.

Name	Value
$R_1$	1.00359089673
$R_2$	2.04298963569
$R_3$	3.02503141993
$R_4$	4.05647775356
$R_5$	3.07781188185
$R_6$	2.01277040929
$R_7$	1.01993304256
$V_s$	5.11402517827
$C$	1.03896393154
$K_b$	7.23768458527
$K_d$	8.33526265782

Table 1: Values provided by the Python script. Units for the values: V, mA, kOhm, mS and uF

## 2 Theoretical Analysis

In this section, the Circuit T2 is analysed theoretically. In figure 2, apart from all the components being identified, the assumed currents are also shown. Only the node method was used in this section. Each subsection refers to each task.

The node method uses KCL in conjunction with Ohm's law to define equations that when solved give the voltage value of each node in relation to ground (Node 4,  $V_4 = 0$ ).

The algebraic sum of all the currents in any given node is zero:

$$\sum I_i = 0 \quad (2)$$

In order to have equations that solve for the node's voltage, a relation between current and voltage is made using Ohm's law (given a resistance between two nodes, the current that passes the resistance can be written as  $I = \frac{V_2 - V_1}{R_1}$ )

## 2.1 Task 1)

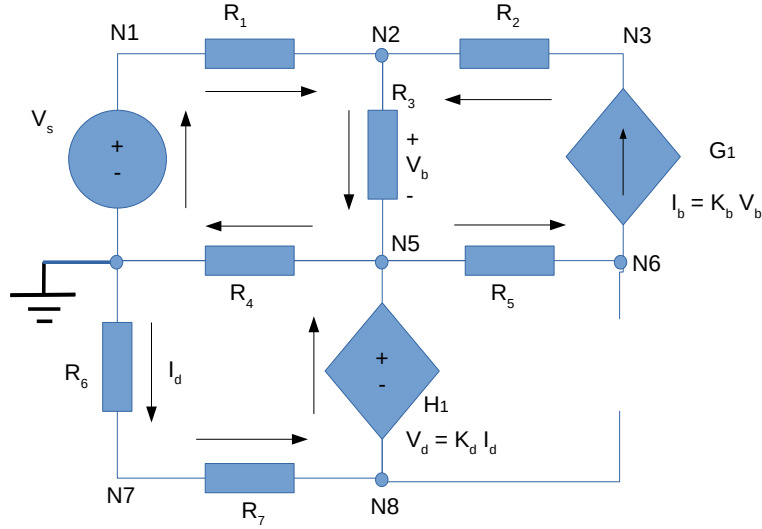


Figure 2: Circuit T2 when  $t < 0$

When  $t < 0$  the value of  $V_s$  is constant and so we can perform DC analysis on the circuit. We can assume that enough time has passed and so it is reasonable to assume that the circuit is in steady-state.

When performing a DC steady-state analysis on a circuit we can use the fact that the current flowing through the capacitor is null (the circuit behaves as if the capacitor was removed).

A node analysis was performed to find the voltage value of each node and the current in each branch.

To simplify the equations it is useful to use the conductance  $G_n$  which is the inverse of the resistance  $R_n$  ( $G_n = \frac{1}{R_n}$ ).

The equations used to solve the circuit were organized in matrix form and were solved using Octave.

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ G1 & -(G1 + G2 + G3) & G2 & G3 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -G2 & G2 & 0 & 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & G3 & 0 & -(G3 + G4 + G5) & G5 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -G5 & G5 & 0 & 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 0 & 0 & G7 & -G7 & -1 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & -(G6 + G7) & G7 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 1 & 0 & G6 * K_d & -1 & 0 & 0 & 0 \\ 0 & K_b & 0 & -K_b & 0 & 0 & 0 & 0 & -1 & 0 \end{bmatrix} \begin{bmatrix} V1 \\ V2 \\ V3 \\ V5 \\ V6 \\ V7 \\ V8 \\ IH1 \\ Ib \\ Ic \end{bmatrix} = \begin{bmatrix} V_s \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Figure 1. In addition, assume  $V_{Ni}$  to be the voltage in node  $Ni$  (every node position can also be found in Figure 1).

Name	Value [A or V]
$V_{N1}$	5.114025e+00
$V_{N2}$	4.830792e+00
$V_{N3}$	4.226624e+00
$V_{N5}$	4.871651e+00
$V_{N6}$	5.781844e+00
$V_{N7}$	-1.849204e+00
$V_{N8}$	-2.786253e+00
@ $I_b$	-2.957272e-04
@ $I_c$	0.000000e+00
@ $I_{R1}$	2.822201e-04
@ $I_{R2}$	-2.957272e-04
@ $I_{R3}$	-1.350709e-05
@ $I_{R4}$	1.200956e-03
@ $I_{R5}$	-2.957272e-04
@ $I_d$	-9.187358e-04
@ $I_{R6}$	9.187358e-04

Table 2: Values computed by Octave. Variables identified with a '@' have a corresponding value in Ampere (A). The others are expressed in Volts (V).

## 2.2 Task 2)

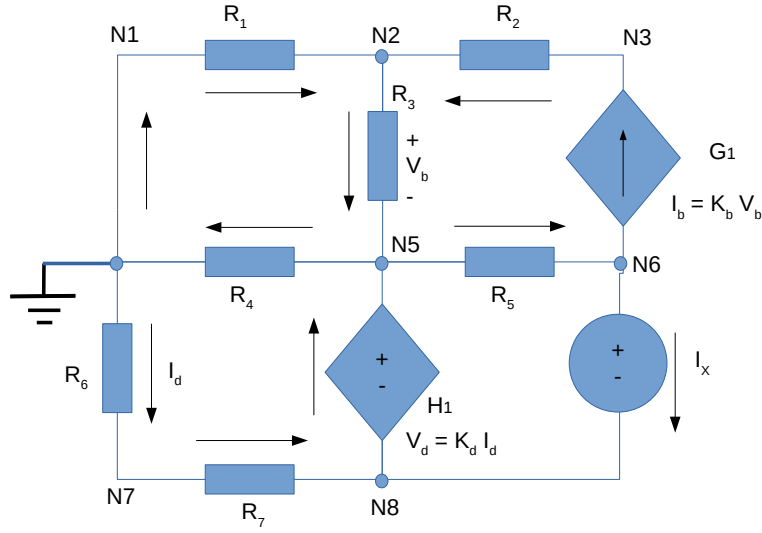


Figure 3: Circuit T2 at  $t = 0$

In this section the capacitor is replaced with a voltage source  $V_x$  with value  $V_x = V_6 - V_8$  as shown in figure 3. The same type of analysis was made to this circuit but with a slightly modification on some of the rows to represent the modified circuit.

$$\begin{bmatrix}
 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 G1 & -(G1 + G2 + G3) & G2 & G3 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & -G2 & G2 & 0 & 0 & 0 & 0 & 0 & -1 & 0 \\
 0 & G3 & 0 & -(G3 + G4 + G5) & G5 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & -G5 & G5 & 0 & 0 & 0 & 1 & 1 \\
 0 & 0 & 0 & 0 & 0 & G7 & -G7 & -1 & 0 & 1 \\
 0 & 0 & 0 & 0 & 0 & -(G6 + G7) & G7 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 \\
 0 & 0 & 0 & 1 & 0 & G6 * K_d & -1 & 0 & 0 & 0 \\
 0 & K_b & 0 & -K_b & 0 & 0 & 0 & 0 & -1 & 0
 \end{bmatrix}
 \begin{bmatrix}
 V1 \\
 V2 \\
 V3 \\
 V5 \\
 V6 \\
 V7 \\
 V8 \\
 IH1_2 \\
 Ib_2 \\
 Ic_2
 \end{bmatrix}
 =
 \begin{bmatrix}
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0
 \end{bmatrix}$$

By performing this analysis we can compute the current  $I_x$  that flows through  $V_x$ . Using Ohm's law we can calculate the equivalent resistance  $R_{eq}$ :

$$R_{eq} = \frac{V_x}{I_x}$$

This procedure is important to compute the circuit's time constant  $\tau$  by using the equation  $\tau = CR_{eq}$ . The time constant in conjunction with the boundary conditions of the circuit are required to compute the natural solution of the circuit.

Name	Value [A or V]
$V_{N1}$	0.000000e+00
$V_{N2}$	-7.143971e-16
$V_{N3}$	-2.238283e-15
$V_{N5}$	-6.113379e-16
$V_{N6}$	8.568097e+00
$V_{N7}$	1.476238e-16
$V_{N8}$	-0.000000e+00
@ $I_b$	-7.459097e-19
@ $I_d$	7.334357e-20
@ $I_{H1}$	-2.783827e-03
@ $V_x$	8.568097e+00
@ $I_x$	-2.783827e-03
$R_{eq}$	3.077812e+03
$\tau$	3.197736e-03

Table 3: Values computed by Octave. Variables identified with a '@' have a corresponding value in Ampere (A). The others are expressed in Volts (V), Ohm and time (s).

### 2.3 Task 3)

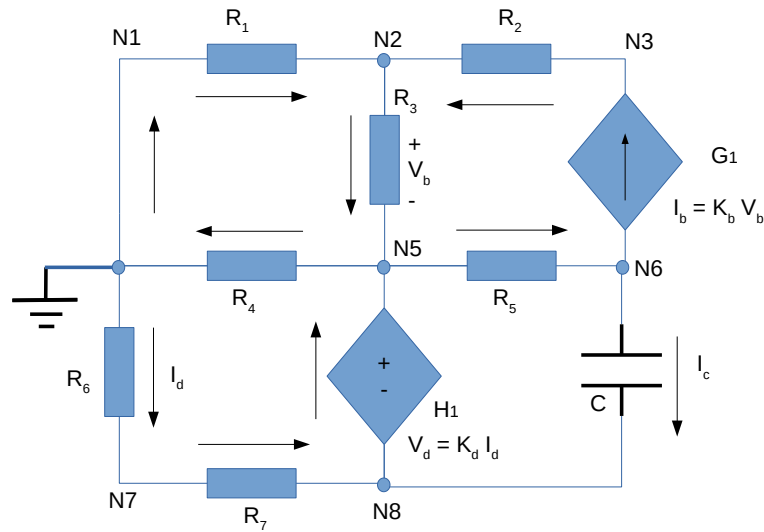


Figure 4: Circuit T2, natural response

In this task we computed the natural response of the circuit. For that reason we assume that the voltage source  $V_s$  is shorted as shown in figure 4.

With the circuit's time constant  $\tau$  and boundary conditions calculated in the previous task we can use following equation to get the natural solution of the circuit:

$$V_{6n}(t) = V_6(\infty) + [V_6(0) - V_6(\infty)]e^{\frac{-t}{\tau}}$$

Since  $V_s$  is considered to be null on this circuit, the value of node 6 is 0 at infinity  $V_6(\infty) = 0$

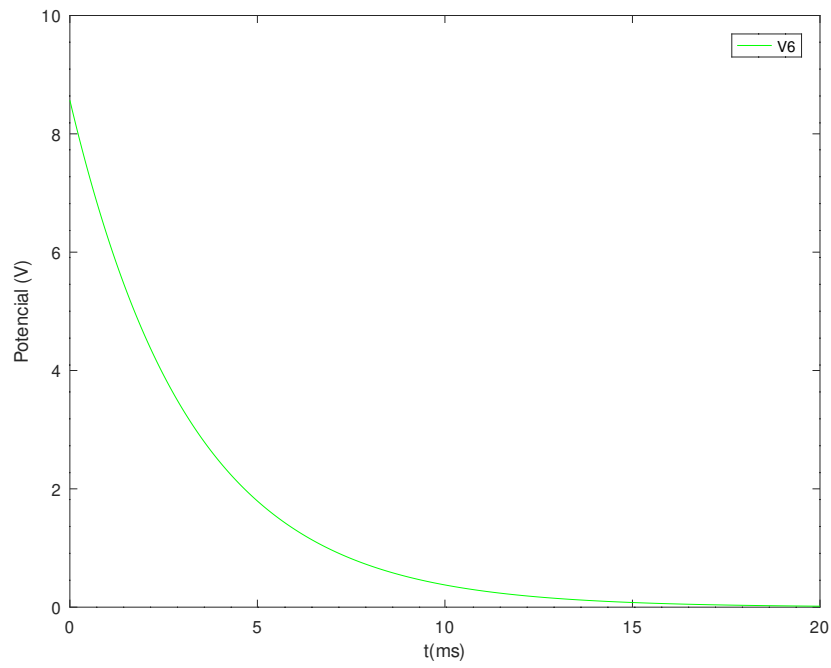


Figure 5: Natural response

## 2.4 Task 4)

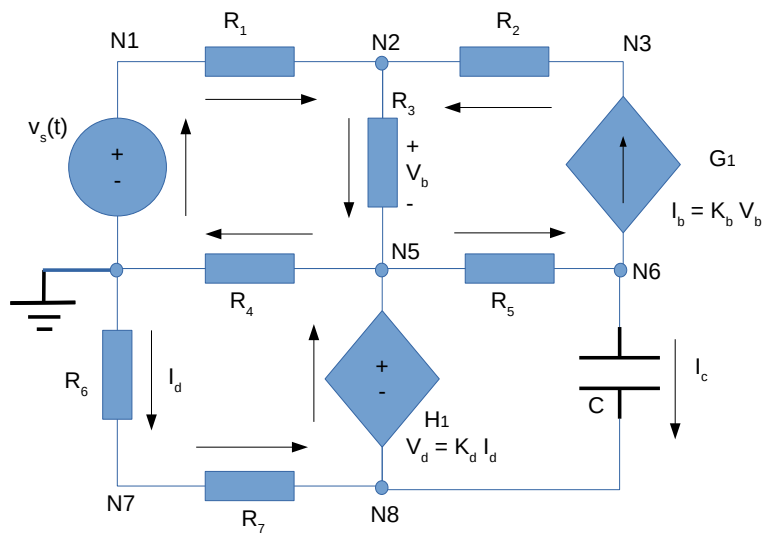


Figure 6: Circuit T2



In this task the forced solution of the circuit is computed. To accomplish this objective, we do an analysis using a phasor voltage source  $V_s = 1$  and replacing C with its impedance:

$$Z_c = j \frac{1}{C\omega}$$

Doing an analysis similar to the previous ones, with a slightly modified matrix we can determine the phasor voltages in all nodes.

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ G1 & -(G1 + G2 + G3) & G2 & G3 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -G2 & G2 & 0 & 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & G3 & 0 & -(G3 + G4 + G5) & G5 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -G5 & G5 & 0 & 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 0 & 0 & G7 & -G7 & -1 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & -(G6 + G7) & G7 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1/Z_c & 0 & 1/Z_c & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & G6 * K_d & -1 & 0 & 0 & 0 \\ 0 & K_b & 0 & -K_b & 0 & 0 & 0 & 0 & -1 & 0 \end{bmatrix} \begin{bmatrix} V1 \\ V2 \\ V3 \\ V5 \\ V6 \\ V7 \\ V8 \\ IH1 \\ Ib \\ Ic \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

The following table shows the phasor magnitudes in each node.

Name	Value [V]
$V_{N1}$	1.000000e+00
$V_{N2}$	9.446163e-01
$V_{N3}$	8.264770e-01
$V_{N5}$	9.526060e-01
$V_{N6}$	5.470469e-01
$V_{N7}$	3.615947e-01
$V_{N8}$	5.448259e-01

Table 4: Values computed by Octave.

## 2.5 Task 5)

In this task we compute the final total solution  $v_6(t)$  with a frequency of 1000Hz. To achieve the final result the phasors are converted to real time functions and then superimposed with the natural solution found before.

The force solution will have the form:

$$V_{6f}(t) = V * \sin(\omega t + \phi)$$

The constant  $\omega$  is the angular frequency of the voltage source,  $V$  is the amplitude of the node phasor and  $\phi$  is the phase shift of the node phasor.

The final solution will have the form:

$$V_6(t) = V_{6n} + V_{6f}$$

The following graph plots the results computed by octave in interval [-5, 20]ms.

## 2.6 Task 6)

In this task, the frequency response of  $v_c(f) = v_6(f) - v_8(f)$ ,  $v_6(f)$  and  $v_s$  is determined for a frequency range of 0.1Hz to 1 MHz. For the calculation of the frequency response a similar analysis to the one in task 4) was made for a multitude of frequencies in the set frequency range. The following graph shows the achieved results:

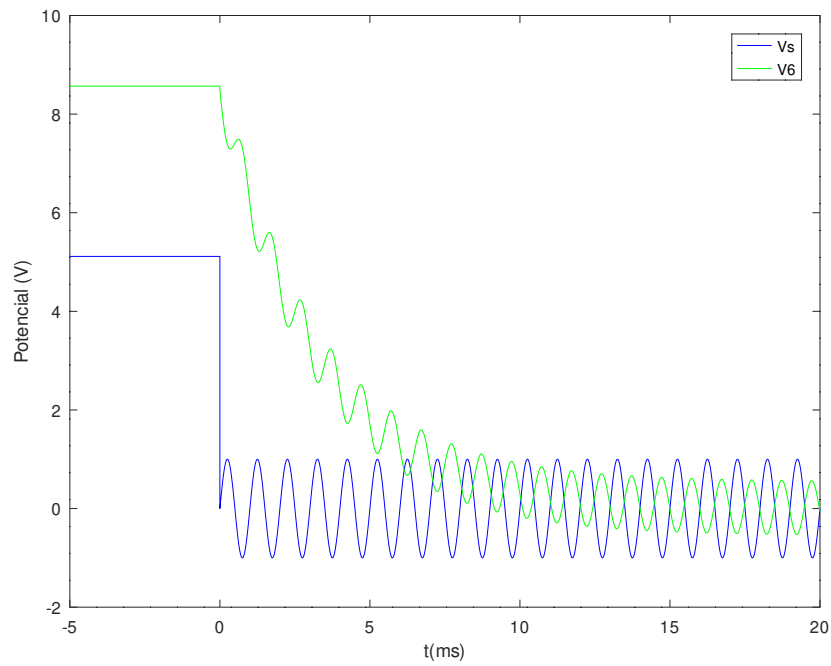


Figure 7: Final total response at 1kHz

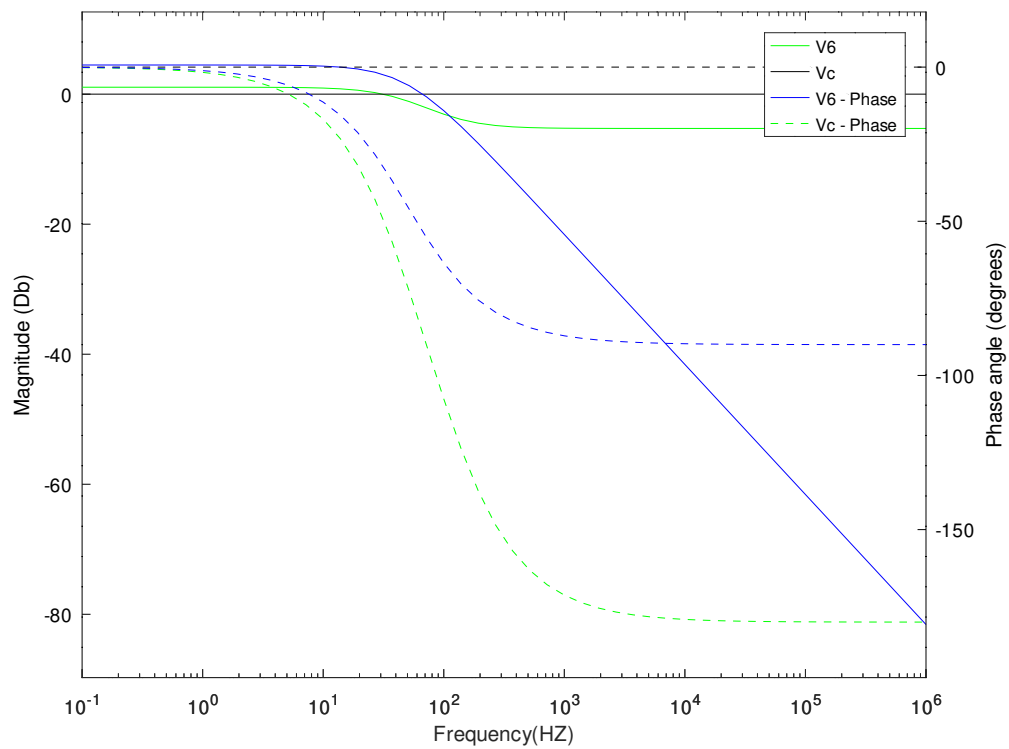


Figure 8: Frequency response analysis

Since the frequency response is made by changing  $V_s$  itself, the values of magnitude and phase of  $V_s$  aren't dependent on frequency. For this reason the plot lines of these values are constant.

By contrast the magnitude and phase of  $V_6$  change with frequency. At low frequencies  $V_6$  is in phase with  $V_s$  but as the frequency increases, the phase shift also increases until it reaches a phase difference of  $180^\circ$ , meaning it's totally out of phase with the source. The magnitude starts at a value of around 1.065dB than  $V_s$  and with increasing value it decreases until it hits a plateau at around -5.275dB.

These values are in accordance with the node voltage values one would get if the capacitor was removed or shorted, respectively. This is due to the fact that the impedance value of a capacitor follows the equation  $\frac{1}{j\omega C}$ . At low frequencies the impedance is very large and so it's almost like the connection between  $N6$  and  $N8$  didn't exist. In contrast, at high frequencies the impedance is almost null so the circuit behaves almost as  $N6$  and  $N8$  were shorted.

We can see that the value of  $v_c(f)$  in dB decreases with increasing frequency. This behaviour is due to the impedance of the capacitor decreasing with larger frequencies and so the phasor voltage difference tends to zero (since the magnitude is plotted in dB, when a voltage approaches 0 the dB values goes to negative values).

### 3 Simulation Analysis

In this section, Circuit T2 is reproduced with the help of Ngspice (each section corresponds to each task). Ngspice is a simulator for electronic circuits that can output a variety of results. This emulator computes the voltages in every node, as well as the potential difference between two given nodes. Apart from that, the group made use of the command `.options savecurrents` which also enables the output of the currents that pass through all branches.

With the limitation that Ngspice only provides the current in the components and not through the nodes, an additional voltage source ( $V_{aux}$ ) was added so that the current in  $R_6$  ( $I_d$ ) is known. This source (not displayed in Figure 16) has a voltage of 0V and it was implemented between  $R_6$  and  $R_7$ . Therefore an additional node had to be added (node  $N7$ ).

As previously stated,  $I_b$  is referred to as  $G_1$ . This is because, in Ngspice, a voltage-controlled current source is identified with capital 'g' ( $G$ ). In the case of  $V_c$ , all current-controlled voltage source are identified with  $H$ .

#### 3.1 Task 1)

In this subsection, the circuit is simulated when  $t < 0$ . There is no need for a transient analysis because  $v_s(t) = V_s$  (according to the data given), therefore all values are constant in time.

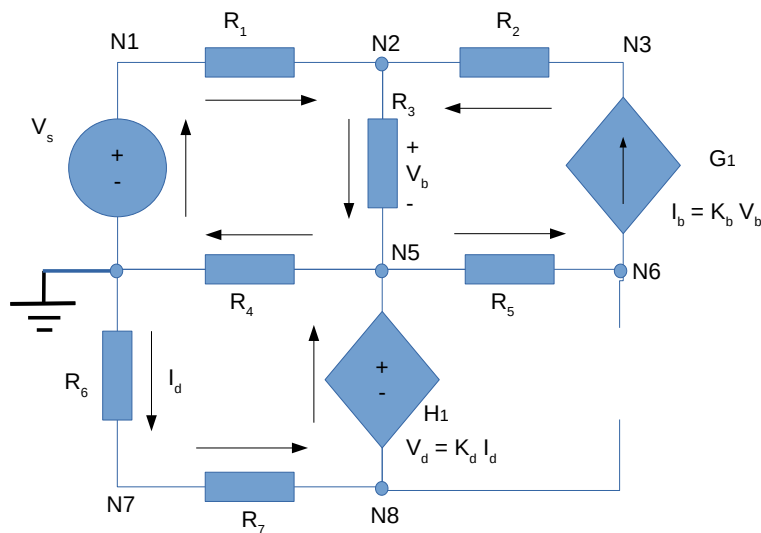


Figure 9: Circuit T2 when  $t < 0$

Table 10 shows the simulated operating point results for Circuit T2.

Name	Value [A or V]
i(vaux)	9.187354e-04
i(h1)	-9.18735e-04
@c[i]	0.000000e+00
@g1[i]	-2.95726e-04
@r1[i]	-2.82220e-04
@r2[i]	-2.95726e-04
@r3[i]	1.350647e-05
@r4[i]	-1.20096e-03
@r5[i]	-2.95726e-04
@r6[i]	9.187354e-04
@r7[i]	-9.18735e-04
n1	5.114025e+00
n2	4.830792e+00
n3	4.226625e+00
n5	4.871649e+00
n6	5.781840e+00
n7	-1.84920e+00
n7.	-1.84920e+00
n8	-2.78625e+00
v(n5,n2)	4.085748e-02
v(n5,n8)	7.657901e+00
v(n6,n8)	8.568092e+00

Table 5: Values from Ngspice. Variables identified with a '@' or are of the type  $i(...)$  have a corresponding value in Ampere (A). The others are expressed in Volts (V).

The three last entries in Table 10 provides the potential difference between important branches:  $V_b = v(n5, n2)$  and  $V_d = v(n5, n8)$ .

### 3.2 Task 2)

In this subsection, the circuit is simulated when  $t = 0$ . Since we can assume that enough time has passed for the circuit to reach steady-state, the capacitor is charge and so, at the instant  $t = 0$  it can be replaced with a voltage source, with its value being equal to the difference between the voltages in nodes  $n6$  and  $n8$  (or  $V_x = V(n6) - V(n8)$ ) obtained in subsection 3.1.  $V_s$  is also set to 0.

This step is necessary to find the boundary conditions of the circuit at  $t = 0$ , which will be used in the next section to calculate the natural response of the T2 circuit.

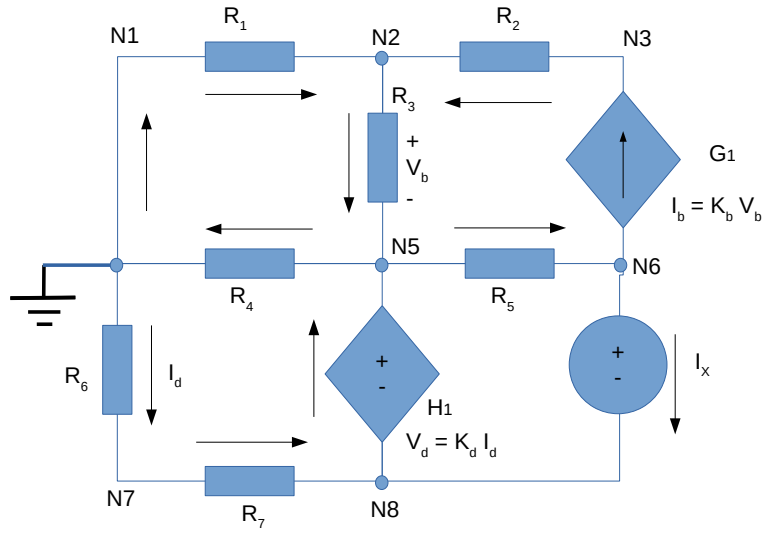


Figure 10: Circuit T2 at  $t = 0$

Table 6 shows the simulated operating point results for Circuit T2.

Name	Value [A or V]
i(vaux)	-8.67362e-19
i(h1)	2.783826e-03
@g1[i]	-6.50208e-18
@r1[i]	-6.20511e-18
@r2[i]	-6.50208e-18
@r3[i]	2.969639e-19
@r4[i]	1.313719e-18
@r5[i]	-2.78383e-03
@r6[i]	-8.67362e-19
@r7[i]	2.995961e-20
n1	0.000000e+00
n2	-6.22740e-15
n3	-1.95111e-14
n5	-5.32907e-15
n6	8.568092e+00
n7	1.745800e-15
n7.	1.745800e-15
n8	1.776357e-15
v(n5,n2)	8.983252e-16
v(n5,n8)	-7.10543e-15

Table 6: Values from Ngspice. Variables identified with a '@' or are of the type  $i(...)$  have a corresponding value in Ampere (A). The others are expressed in Volts (V).

### 3.3 Task 3)

In this subsection, the natural response of the circuit was simulated using the boundary conditions  $V(n6)$  and  $V(n8)$  calculated in subsection 3.2. Thus,  $V_{n6}(t)$  was plotted in the interval  $[0;20]ms$  (Figure 12).

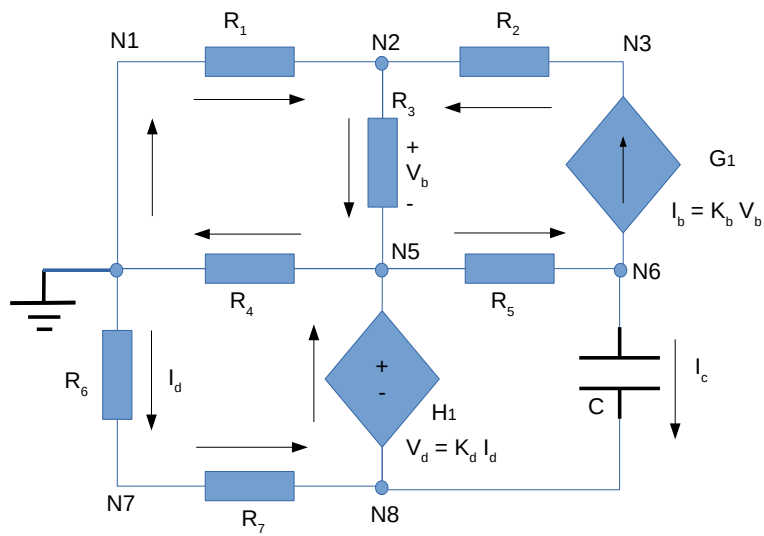


Figure 11: Circuit T2, natural response

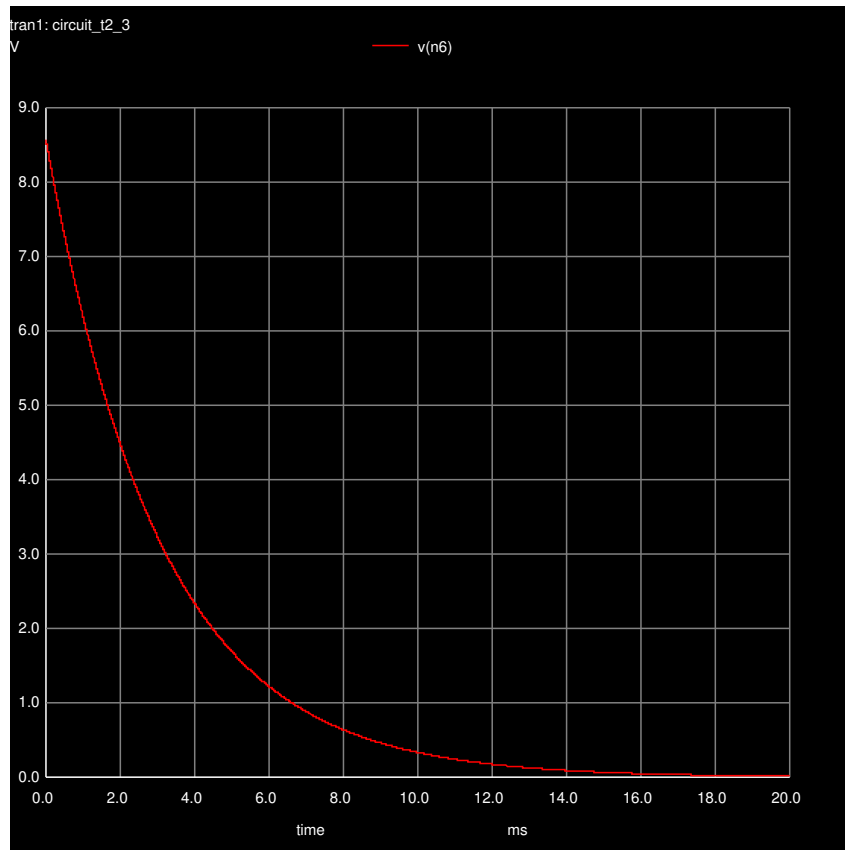


Figure 12: Transient analysis - Natural response on node  $n6$

### 3.4 Task 4)

In this subsection, the total (natural and forced) response on node  $n6$  is simulated. The boundary conditions used are the same as subsection 3.3 and a frequency of 1kHz ( $f=1\text{kHz}$ ) is considered for  $v_s(t)$ . Figure 14 shows the plot. It is worth noting that node  $n1$  has the same value as the stimulus ( $v_s(t)$ ), so  $V(n1)$  is used instead.



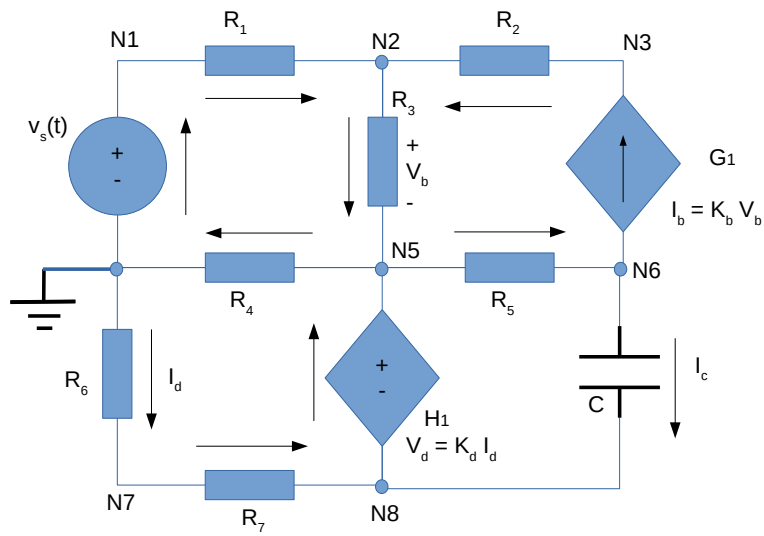


Figure 13: Circuit T2

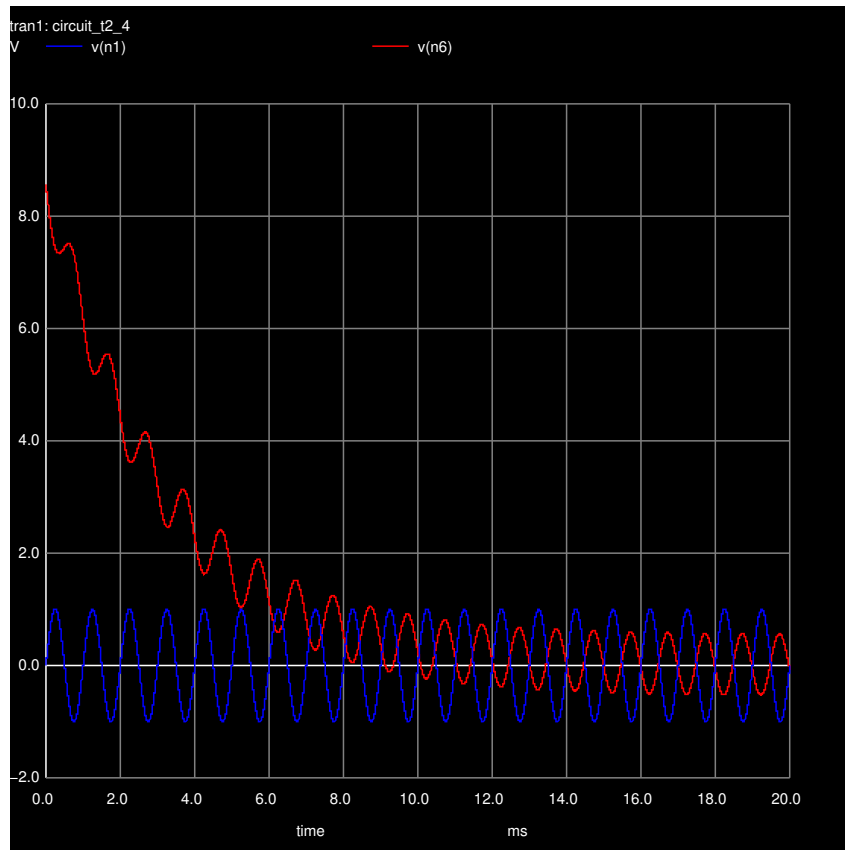


Figure 14: Transient analysis: final total response on node  $n6$

### 3.5 Task 5)

In this subsection, the frequency response on  $V_s$  and on node  $n6$  is computed (using the circuit diagram 13 and shown in the following plots).

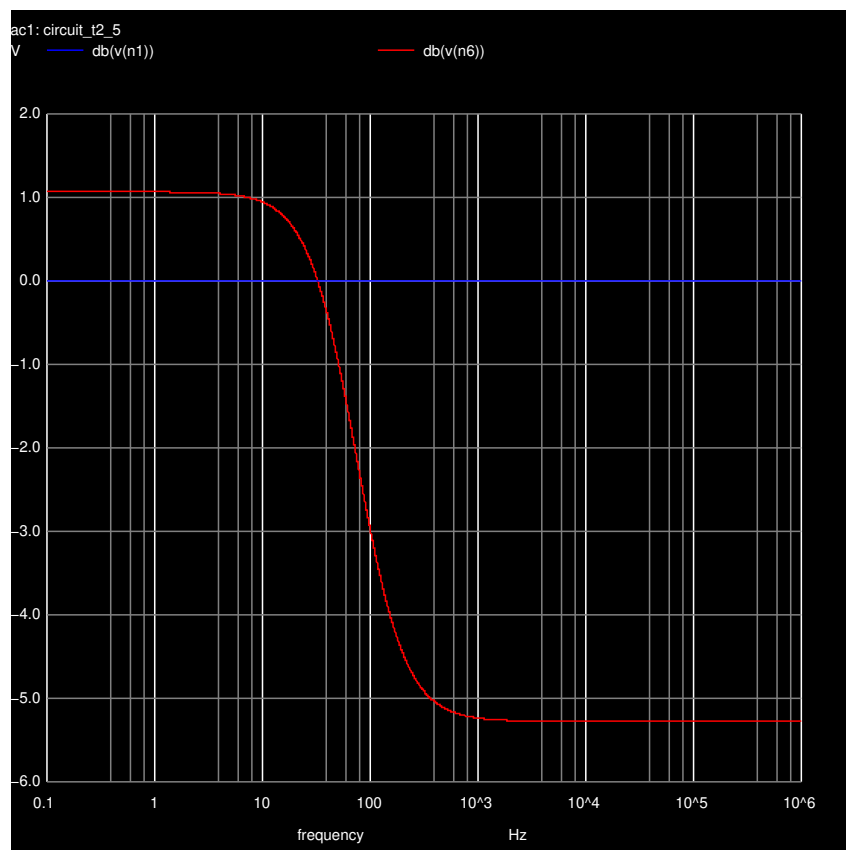


Figure 15: Frequency response - Magnitude (dB)

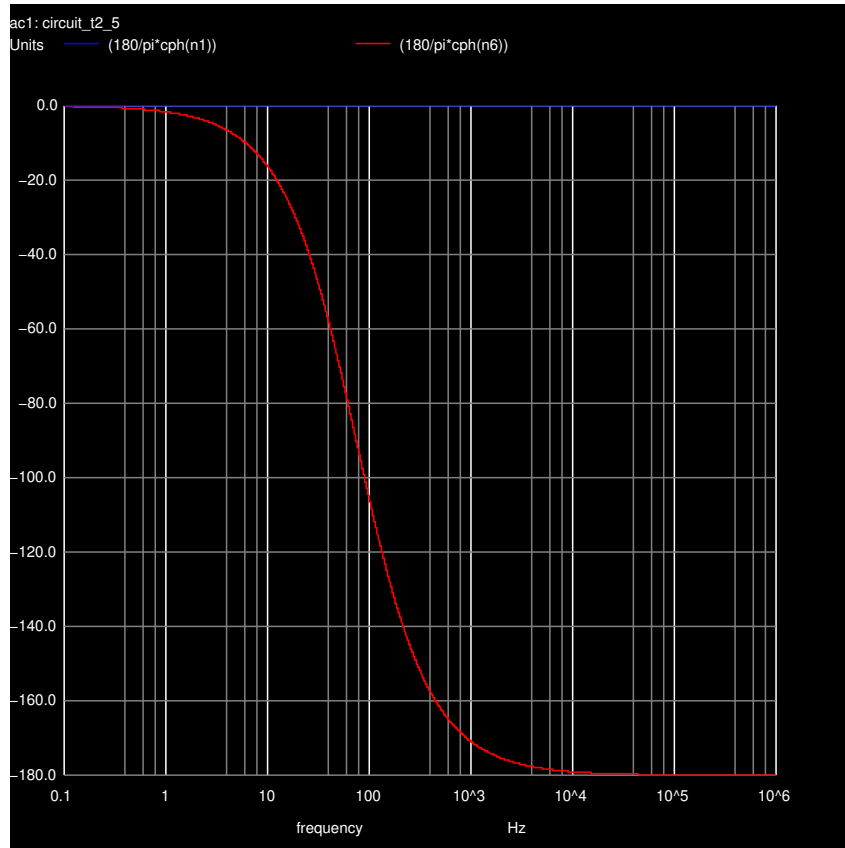


Figure 16: Frequency response - Phase shift (degrees)

Since the frequency response is made by changing  $V_s$  itself, the values of magnitude and phase of  $V_s$  aren't dependent on frequency. For this reason the plot lines of these values are constant.

By contrast the magnitude and phase of  $V_6$  change with frequency. At low frequencies  $V_6$  is in phase with  $V_s$  but as the frequency increases, the phase shift also increases until it reaches a phase difference of  $180^\circ$ , meaning it's totally out of phase with the source. The magnitude starts at a value of around 1.065dB than  $V_s$  and with increasing value it decreases until it hits a plateau at around -5.275dB.

These values are in accordance with the node voltage values one would get if the capacitor was removed or shorted, respectively. This is due to the fact that the impedance value of a capacitor follows the equation  $\frac{1}{j\omega C}$ . At low frequencies the impedance is very large and so it's almost like the connection between  $N6$  and  $N8$  didn't exist. In contrast, at high frequencies the impedance is almost null so the circuit behaves almost as  $N6$  and  $N8$  were shorted.

## 4 Conclusion

For this laboratory assignment, we were given a circuit composed by resistors, one dependent current source, one independent and one dependent voltage source and had the objective of analyzing and simulating it and then compare the results obtained.

Static, transient and frequency response analyses were performed theoretically, through the node analysis and by circuit simulation, using the Octave math tool and Ngspice tool, respectively.

It is safe to say that our objective was achieved successfully. We can compare the results of both analyses by looking at the graphs side by side.

Task 1):

Name	Value [A or V]
$V_{N1}$	5.114025e+00
$V_{N2}$	4.830792e+00
$V_{N3}$	4.226624e+00
$V_{N5}$	4.871651e+00
$V_{N6}$	5.781844e+00
$V_{N7}$	-1.849204e+00
$V_{N8}$	-2.786253e+00
@ $I_b$	-2.957272e-04
@ $I_c$	0.000000e+00
@ $I_{R1}$	2.822201e-04
@ $I_{R2}$	-2.957272e-04
@ $I_{R3}$	-1.350709e-05
@ $I_{R4}$	1.200956e-03
@ $I_{R5}$	-2.957272e-04
@ $I_d$	-9.187358e-04
@ $I_{R6}$	9.187358e-04

Table 7: Values computed by Octave - Theoretical Task 1)

Name	Value [A or V]
i(vaux)	9.187354e-04
i(h1)	-9.18735e-04
@c[i]	0.000000e+00
@g1[i]	-2.95726e-04
@r1[i]	-2.82220e-04
@r2[i]	-2.95726e-04
@r3[i]	1.350647e-05
@r4[i]	-1.20096e-03
@r5[i]	-2.95726e-04
@r6[i]	9.187354e-04
@r7[i]	-9.18735e-04
n1	5.114025e+00
n2	4.830792e+00
n3	4.226625e+00
n5	4.871649e+00
n6	5.781840e+00
n7	-1.84920e+00
n7.	-1.84920e+00
n8	-2.78625e+00
v(n5,n2)	4.085748e-02
v(n5,n8)	7.657901e+00
v(n6,n8)	8.568092e+00

Table 8: Values from Ngspice- Simulation Task 1)

Task 2):

Name	Value [A or V]
$V_{N1}$	0.000000e+00
$V_{N2}$	-7.143971e-16
$V_{N3}$	-2.238283e-15
$V_{N5}$	-6.113379e-16
$V_{N6}$	8.568097e+00
$V_{N7}$	1.476238e-16
$V_{N8}$	-0.000000e+00
@ $I_b$	-7.459097e-19
@ $I_d$	7.334357e-20
@ $I_{H1}$	-2.783827e-03
@ $V_x$	8.568097e+00
@ $I_x$	-2.783827e-03
$R_{eq}$	3.077812e+03
$\tau$	3.197736e-03

Table 9: Values computed by Octave - Theoretical Task 2)

Name	Value [A or V]
i(vaux)	-8.67362e-19
i(h1)	2.783826e-03
@g1[i]	-6.50208e-18
@r1[i]	-6.20511e-18
@r2[i]	-6.50208e-18
@r3[i]	2.969639e-19
@r4[i]	1.313719e-18
@r5[i]	-2.78383e-03
@r6[i]	-8.67362e-19
@r7[i]	2.995961e-20
n1	0.000000e+00
n2	-6.22740e-15
n3	-1.95111e-14
n5	-5.32907e-15
n6	8.568092e+00
n7	1.745800e-15
n7.	1.745800e-15
n8	1.776357e-15
v(n5,n2)	8.983252e-16
v(n5,n8)	-7.10543e-15

Table 10: Values from Ngspice- Simulation Task 2)

We can conclude that the theoretical values match the simulation ones, with relative high precision. The only differences were generated by the limitations of Octave and Ngspice, concerning rounding and truncating values.