

**Positive and negative sequence currents to improve voltages  
during unbalanced faults**

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# 1 Variable resistance/inductance ratio

In this section we try to answer to the question of what happens when the  $R/X$  ratio varies. This way we experiment with cases where the resistive part is considerably larger than in the aforementioned analysis. The fault impedance  $\underline{Z}_f$  has been set at 0.1, which is probably more realistic than  $0.0 + 0.1j$ .

## 1.1 Balanced fault

Figure 1 depicts the optimal currents for the balanced fault.

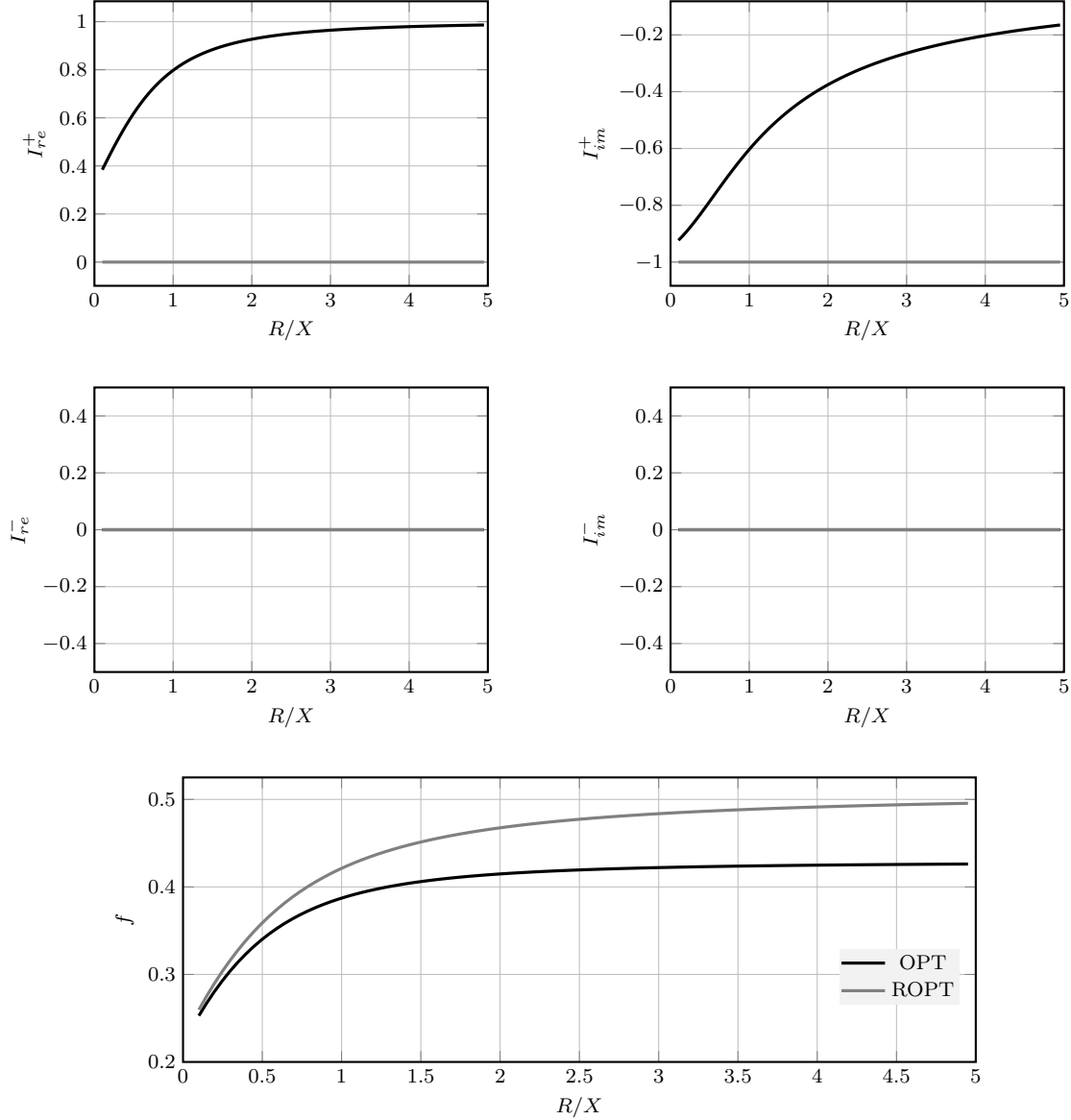


Figure 1: Influence of the currents on the objective function for the balanced fault with  $\underline{Z}_f = 0.05$  and a changing  $R/X$  ratio. OPT: solution to the optimization problem, ROPT: solution to the optimization problem restricted to only injecting reactive power.

It becomes clear that the optimal current is highly dependent on the  $R/X$  ratio. That is, when  $X > R$ , the imaginary positive sequence is dominant, and vice versa for  $R > X$ . This phenomena makes complete sense when considering that we want to amplify the voltage drop in the positive sequence. However, even when there are serious differences between  $R$  and  $X$  in magnitude, neither the real nor the imaginary part go to zero. Thus, the objective function for the OPT case becomes slightly lower when compared to the ROPT case. Besides, since the negative sequence equivalent circuit is decoupled from the positive sequence one, the negative sequence currents are null in all cases.

The fault impedance has a noticeable effect on the results. When it is extremely small, the objective function almost does not vary. Opting for a too large fault impedance may cause the presence of multiple solutions. Hence, the real and imaginary currents may take unexpected values so it is hard to build intuition around the problem. We have checked that  $\underline{Z}_f = 0.05$  for the balanced fault was a convenient value.

In addition, Figure 2 shows the absolute value of the voltages depending on the  $R/X$  ratio and together with the objective function.

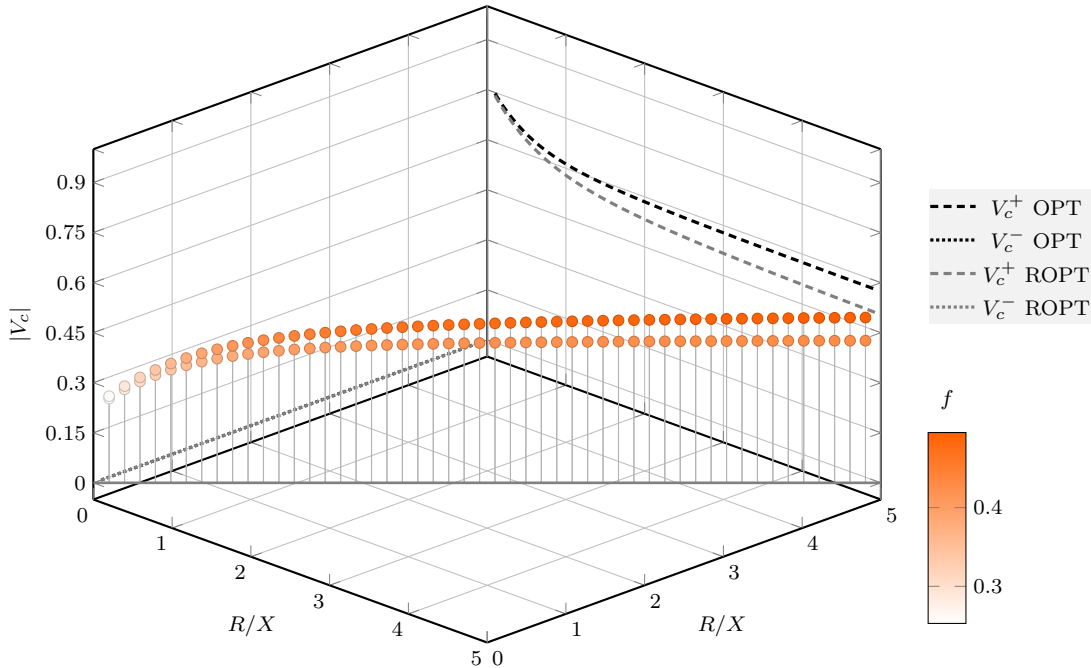


Figure 2: Sequence voltages together with the objective function for the balanced fault with  $\underline{Z}_f = 0.05$  and a varying  $R/X$  ratio

As already noted in Figure 1, the objective function for the OPT case is inferior than the one for the ROPT case, and hence, closer to the ideal situation. Nevertheless, independently on having constraints on the active current, the negative sequence voltages remain at exactly zero for all the  $R/X$  range. They end up being superposed. The positive sequence voltages, instead, experience some variations depending on the  $R/X$  value. In some sense the positive sequence voltage trend is the contrary of the objective function pattern.

The best possible situation is having the reactive part larger than the real part of the impedance. This is when the positive sequence voltage tends to 0.75. Since the resistive characteristics of the impedance are so minimized, the ROPT case yields the same results as the OPT. When the resistance increases, the differences are exaggerated due to the fact that no active current can be injected in the ROPT situation.

## 1.2 Line to ground fault

Figure 3 depicts the optimal currents for the line to ground fault.

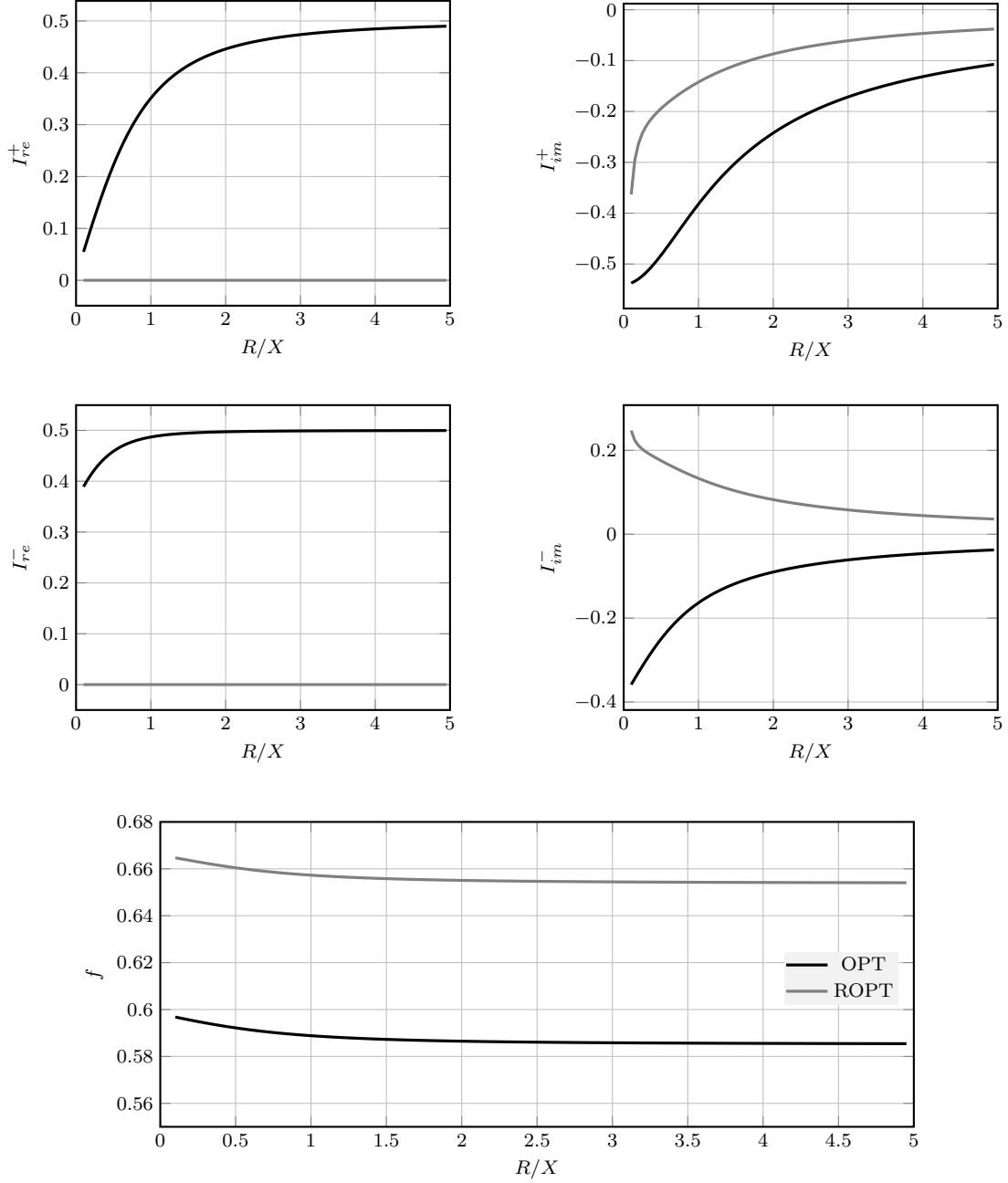


Figure 3: Influence of the currents on the objective function for the line to ground fault and a changing  $R/X$  ratio and  $\underline{Z}_f = 0.001$ . OPT: solution to the optimization problem, ROPT: solution to the optimization problem restricted to only injecting reactive power.

The line to ground fault has been analyzed for a fault impedance of 0.001 because otherwise the fault may not be severe enough. This is deduced from the presence of multiple optimal points for a

same  $R/X$  ratio while the objective function improves substantially due to the injection of currents. Instead, in this case the objective function does not vary much for all the  $R/X$  range. Notice also that it is not far apart from the objective function in the balanced fault case. Consequently, we are able to conclude that the severity of the fault is similar thanks to the convenient adjustment of the fault impedance.

On the other hand, the differences between the OPT and the ROPT are relevant. Despite that, there is not much room for improvement in the sense that real currents, for both the positive and negative sequences, take ideally values close to 0.5 for big enough  $R/X$  ratios. Imposing the constraint of not injecting any real current causes that all influence on the voltages is achieved by means of the imaginary currents, which are not enough to improve the voltages. For instance, for  $R/X \approx 5$ , the maximum absolute value of the  $abc$  currents is one order of magnitude lower than the maximum allowed current  $I_{max}$ . Therefore, this suggests that no combination of currents is able to reduce more the objective function.

Even though we can expect that the positive sequence voltage is far from the unit value and the negative sequence is also distant from zero, the evaluation of voltages becomes worth of a particular study. Figure 4 shows the objective function along with the positive and negative sequence for the OPT and the ROPT cases.

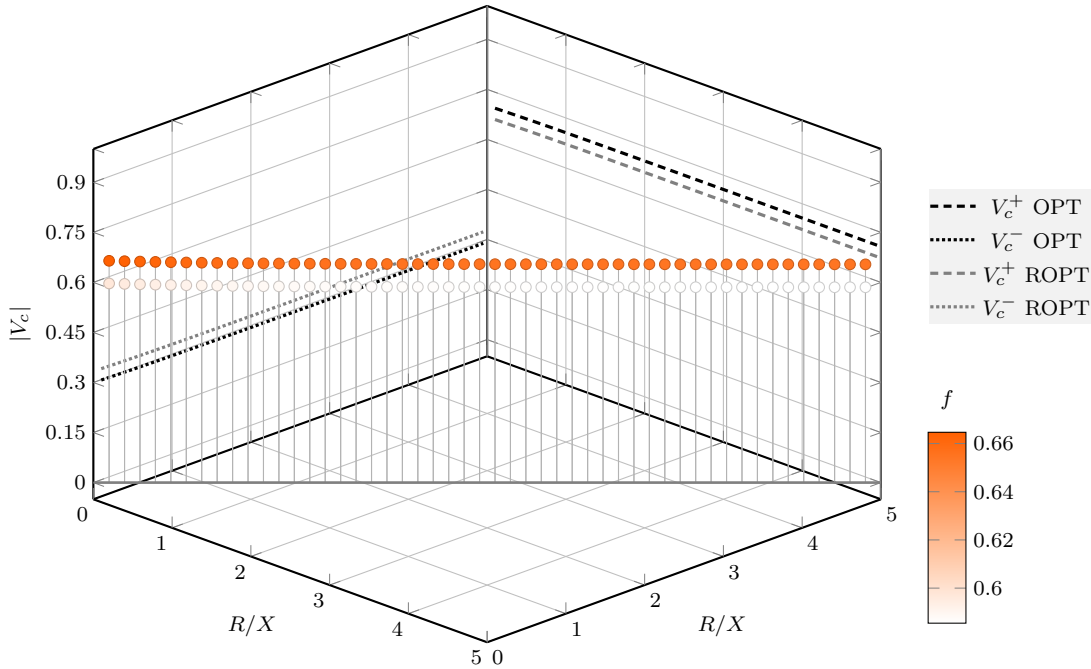


Figure 4: Sequence voltages together with the objective function for the line to ground fault with  $\underline{Z}_f = 0.001$  and a varying  $R/X$  ratio

When looking at the bigger picture the objective function remains almost always the same, yet there exists a permanent difference between the OPT and the ROPT cases. The positive sequence voltages in the OPT situation are always above the ROPT ones for about 0.04 pu. For the negative sequence voltage the pattern is reversed. It is relevant to take into account that even if the voltages turn out to be practically constant, the currents experience large variations, as shown in Figure 3. Extracting conclusions regarding the fault by only observing the voltages may be misleading, as they can be maintained at the expense of injecting the specific optimal currents. Besides, just like it happened with the balanced fault, the shape of the objective function resembles the shape of the voltages. This is logical when considering the proportionality between the objective function and the voltages.

### 1.3 Line to line fault

Figure 5 depicts the optimal currents for the line to line fault.

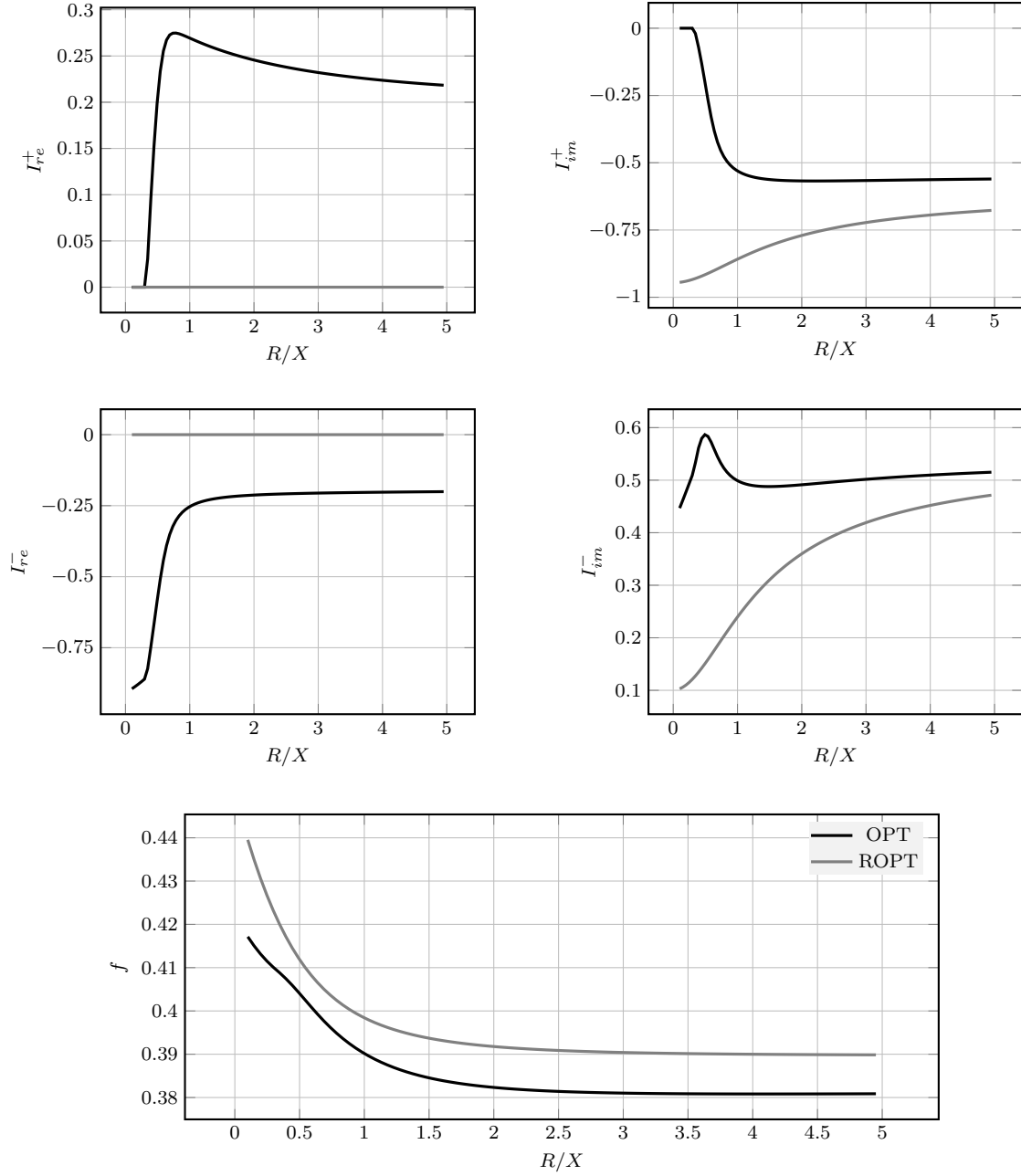


Figure 5: Influence of the currents on the objective function for the line to line fault and a changing  $R/X$  ratio. OPT: solution to the optimization problem, ROPT: solution to the optimization problem restricted to only injecting reactive power.

## 1.4 Double line to ground fault

Figure 6 depicts the optimal currents for the balanced fault.

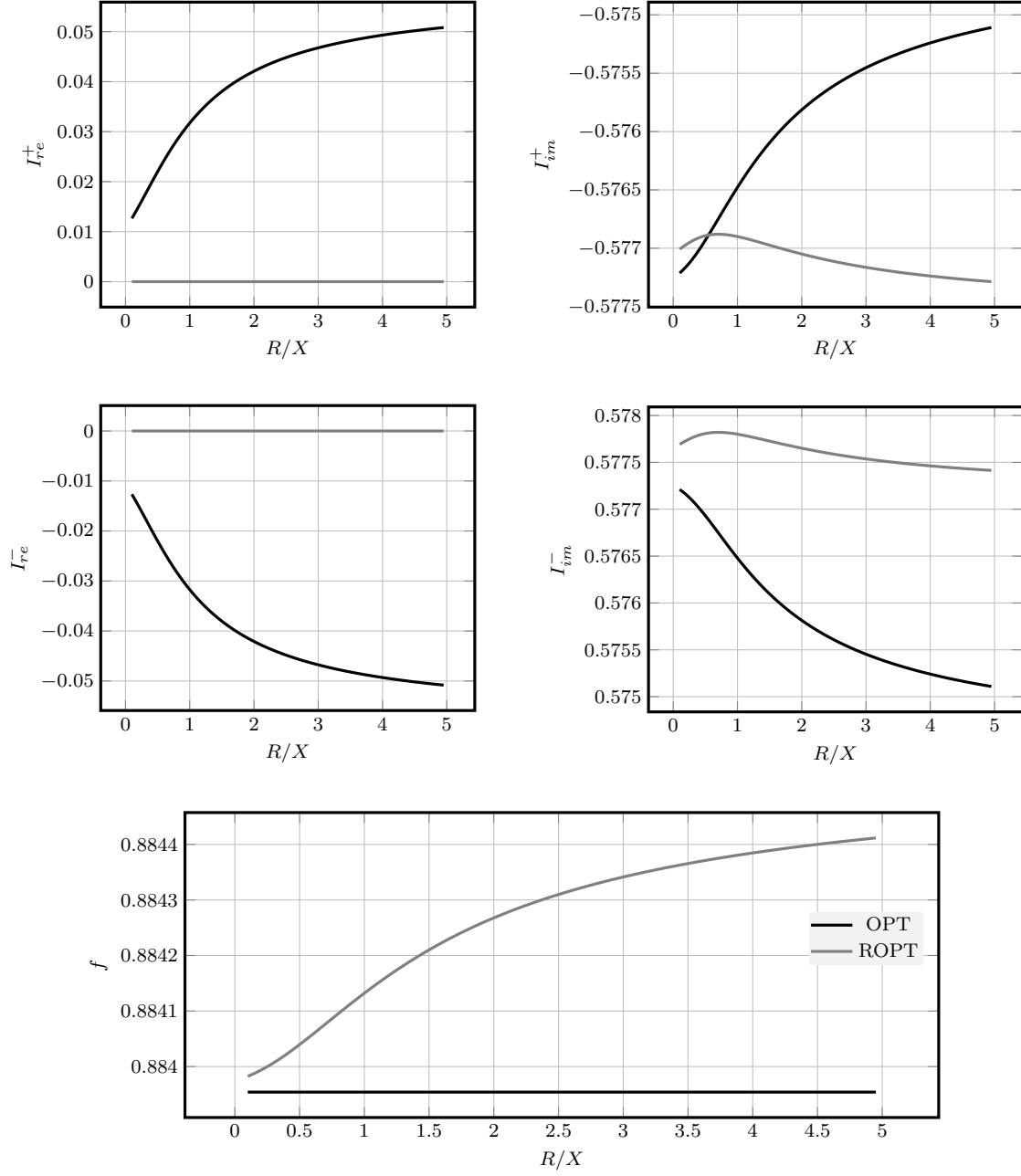


Figure 6: Influence of the currents on the objective function for the double line to ground fault and a changing  $R/X$  ratio. OPT: solution to the optimization problem, ROPT: solution to the optimization problem restricted to only injecting reactive power.

About the discussion of the plots, for the balanced fault it becomes clear that injecting a large imaginary positive sequence current (in absolute value) is the preferred option to minimize the objective

function. In the OPT case some of this current is traded for some real positive sequence current that allows the objective function to become slightly lower when compared to the ROPT case. Since the negative sequence equivalent circuit is decoupled from the positive sequence one, the negative sequence currents are null in all cases. Besides, the larger  $R$  becomes with respect to  $X$ , the larger the real positive current has to be as well. This phenomena makes complete sense when considering that we want to amplify the voltage drop in the positive sequence. However, even when  $R$  is about five times larger than  $X$ , the imaginary positive sequence current is dominant.

As explained in the initial discussion where no sweep was taking place, the line to ground case may have multiple minimums. The plots in Figure 3 indicate that this could also be the case here, as the evolution of currents does not follow a smooth trajectory. Rather, it is not continuously differentiable across all its path. This phenomena happens for all currents at the same  $R/X$  values but is not noticeable from the objective function plot. Such continuity on the objective function could be a great indicator of the presence of various equal minimums for a single  $R/X$  value.

The line to line fault ends up presenting a larger  $f$  value than in the two abovementioned cases. That is, it becomes a more severe fault. Note from the objective function that the OPT is superior to the ROPT case for all values of the  $R/X$  ratio. However, the distribution of currents hugely varies for small  $R/X$  ratios. When  $R$  tends to be way smaller than  $X$ , the negative sequence current is prioritized in the OPT case. When  $R$  becomes larger, this diminishes and then the imaginary positive and negative sequence currents are the major ones. Contrarily to the other faults, the bigger  $R$ , the better.

In the double line to ground fault the differences across all the sweep values is minimal. The objective functions remain at almost always the same values, and even though the OPT is again the winner, the difference with the ROPT situation does not become substantial. The imaginary positive and negative sequence currents tend to take the same values but with the opposite sign, whereas the real positive sequence currents is merely the reflection of the real negative sequence current. We can deduce that since the double line to ground fault involves a solid connection between phases, it makes this turns out to be the most severe situation.