SMART GRIDS: FROM TRADITIONAL TO MODERNIZED RESILIENT SYSTEMS

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SMART GRIDS

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1. INTRODUCTION

2. PHASE 1

A system such as the one displayed in Figure 1 is analyzed. The network operates at the transmission level and feds dispersed demand points that symbolyze distribution grids. The grid has an interconnection with a transmission grid, and at the same time, some power is provided by the nuclear power plant. Initially, there are no renewable power plants nor storage systems, which compromises the security of the grid.

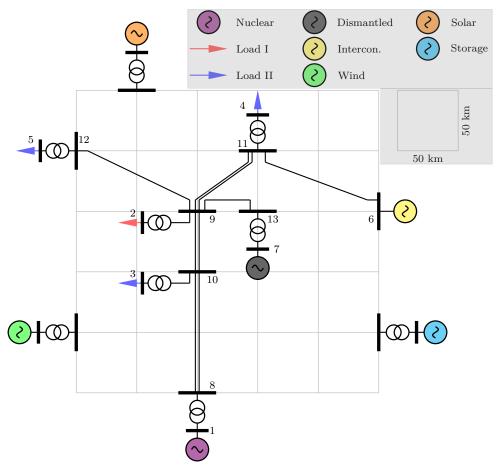


Figure 1. Overview of the network

The first step to analyze the system is to know the demand and the generation profile. In order to model them, the hourly demand and generation data of Spain have been collected [1]. To obtain a typical working day, a statistical analysis has been performed taking into account only the days from the 1st of January to the 31st of March, from Tuesday to Thursday and removing the national holidays. The result then has been normalized. analyze the system is This way, the consumption profile is obtained by from the product of the normalized demand and the peak power consumption of 375 MW for load type I and 140 MW for type II. For the generation profile, for simplicity, it has been assumed that the nuclear power plant follows the demand curve, i.e., it is not acting as a constant generator.

| Bus Hour | 1 | 2 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 11 | 12 |
|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 1.050 | 0.963 | 0.989 | 0.972 | 0.937 | 1.000 | 1.031 | 0.986 | 1.000 | 0.984 | 0.950 |
| 1 | 1.050 | 0.974 | 0.998 | 0.982 | 0.952 | 1.000 | 1.035 | 0.995 | 1.008 | 0.993 | 0.963 |
| 2 | 1.050 | 0.981 | 1.003 | 0.988 | 0.961 | 1.000 | 1.037 | 1.001 | 1.013 | 0.998 | 0.972 |
| 3 | 1.050 | 0.984 | 1.005 | 0.990 | 0.965 | 1.000 | 1.038 | 1.003 | 1.015 | 1.000 | 0.975 |
| 4 | 1.050 | 0.985 | 1.006 | 0.991 | 0.966 | 1.000 | 1.038 | 1.004 | 1.015 | 1.001 | 0.976 |
| 5 | 1.050 | 0.981 | 1.003 | 0.988 | 0.961 | 1.000 | 1.037 | 1.001 | 1.013 | 0.998 | 0.972 |
| 6 | 1.050 | 0.967 | 0.992 | 0.975 | 0.942 | 1.000 | 1.032 | 0.989 | 1.003 | 0.987 | 0.955 |
| 7 | 1.050 | 0.938 | 0.969 | 0.950 | 0.905 | 1.000 | 1.022 | 0.965 | 0.983 | 0.964 | 0.920 |
| 8 | 1.050 | 0.915 | 0.952 | 0.931 | 0.876 | 1.000 | 1.014 | 0.947 | 0.967 | 0.946 | 0.893 |
| 9 | 1.050 | 0.904 | 0.944 | 0.921 | 0.862 | 1.000 | 1.010 | 0.938 | 0.960 | 0.938 | 0.880 |
| 10 | 1.050 | 0.900 | 0.941 | 0.918 | 0.856 | 1.000 | 1.009 | 0.935 | 0.957 | 0.935 | 0.875 |
| 11 | 1.050 | 0.901 | 0.941 | 0.919 | 0.857 | 1.000 | 1.009 | 0.936 | 0.958 | 0.935 | 0.876 |
| 12 | 1.050 | 0.904 | 0.944 | 0.921 | 0.861 | 1.000 | 1.010 | 0.938 | 0.960 | 0.938 | 0.879 |
| 13 | 1.050 | 0.906 | 0.945 | 0.923 | 0.864 | 1.000 | 1.011 | 0.939 | 0.961 | 0.939 | 0.882 |
| 14 | 1.050 | 0.916 | 0.953 | 0.931 | 0.877 | 1.000 | 1.014 | 0.948 | 0.968 | 0.947 | 0.894 |
| 15 | 1.050 | 0.922 | 0.957 | 0.936 | 0.884 | 1.000 | 1.016 | 0.953 | 0.972 | 0.952 | 0.901 |
| 16 | 1.050 | 0.925 | 0.960 | 0.939 | 0.889 | 1.000 | 1.018 | 0.955 | 0.974 | 0.954 | 0.905 |
| 17 | 1.050 | 0.926 | 0.961 | 0.940 | 0.890 | 1.000 | 1.018 | 0.956 | 0.975 | 0.955 | 0.906 |
| 18 | 1.050 | 0.921 | 0.957 | 0.936 | 0.884 | 1.000 | 1.016 | 0.952 | 0.972 | 0.951 | 0.900 |
| 19 | 1.050 | 0.903 | 0.943 | 0.920 | 0.860 | 1.000 | 1.010 | 0.937 | 0.959 | 0.937 | 0.878 |
| 20 | 1.050 | 0.891 | 0.933 | 0.910 | 0.844 | 1.000 | 1.005 | 0.927 | 0.950 | 0.927 | 0.863 |
| 21 | 1.050 | 0.897 | 0.939 | 0.915 | 0.853 | 1.000 | 1.008 | 0.933 | 0.955 | 0.932 | 0.871 |
| 22 | 1.050 | 0.921 | 0.957 | 0.936 | 0.884 | 1.000 | 1.016 | 0.952 | 0.972 | 0.951 | 0.900 |
| 23 | 1.050 | 0.946 | 0.975 | 0.957 | 0.915 | 1.000 | 1.025 | 0.972 | 0.988 | 0.970 | 0.929 |

Table 1. Voltage profile, in pu, for 24 hours

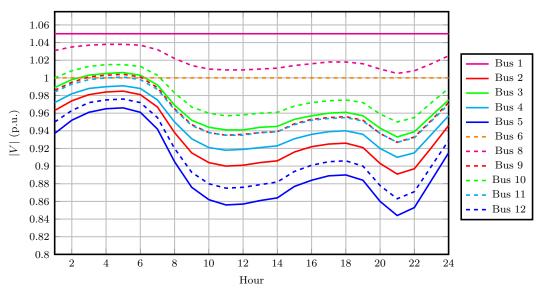


Figure 2. Voltage profile during 24 hours for the initial grid. The low-voltage buses are plotted in solid lines; the high-voltage ones are in dashed lines.

| Load Hour | 8-10 | 10-9 | 9-11 | 9-12 | 11-6 |
|--------------|--------|--------|--------|--------|--------|
| 0 | 26.423 | 19.999 | 9.388 | 30.774 | 63.562 |
| 1 | 24.385 | 18.464 | 8.850 | 28.312 | 59.190 |
| 2 | 23.089 | 17.491 | 8.517 | 26.761 | 56.451 |
| 3 | 22.549 | 17.087 | 8.381 | 26.117 | 55.319 |
| 4 | 22.458 | 17.019 | 8.358 | 26.009 | 55.130 |
| 5 | 23.082 | 17.486 | 8.515 | 26.752 | 56.435 |
| 6 | 25.729 | 19.475 | 9.203 | 29.932 | 62.065 |
| 7 | 30.615 | 23.176 | 10.549 | 35.928 | 72.752 |
| 8 | 34.100 | 25.846 | 11.559 | 40.331 | 80.765 |
| 9 | 35.690 | 27.073 | 12.031 | 42.383 | 84.443 |
| 10 | 36.296 | 27.542 | 12.213 | 43.173 | 85.847 |
| 11 | 36.166 | 27.441 | 12.174 | 43.002 | 85.544 |
| 12 | 35.740 | 27.111 | 12.046 | 42.448 | 84.558 |
| 13 | 35.480 | 26.910 | 11.969 | 42.110 | 83.956 |
| 14 | 33.997 | 25.766 | 11.528 | 40.198 | 80.526 |
| 15 | 33.090 | 25.069 | 11.262 | 39.042 | 78.435 |
| 16 | 32.569 | 24.669 | 11.110 | 38.381 | 77.234 |
| 17 | 32.392 | 24.534 | 11.059 | 38.158 | 76.828 |
| 18 | 33.187 | 25.143 | 11.290 | 39.165 | 78.657 |
| 19 | 35.865 | 27.208 | 12.084 | 42.610 | 84.847 |
| 20 | 37.641 | 28.588 | 12.620 | 44.945 | 88.969 |
| 21 | 36.689 | 27.847 | 12.332 | 43.688 | 86.759 |
| 22 | 33.143 | 25.110 | 11.278 | 39.109 | 78.557 |
| 23 | 29.319 | 22.190 | 10.183 | 34.319 | 69.877 |

Table 2. Percentual loading of the lines for a full day operation



Figure 3. Representation of the percentual loading of the lines during 24 hours

2.1. Operating costs

Regarding the operating costs, some estimations are made in order to asses the influence of importing energy and the impact of faults on lines and transformers.

First, the cost of importing energy depends on the time zone: valley, flat or peak. The analysis that follows considers a working day, which is precisely the date for which the voltages and loading profiles have been shown in Figures 2 and 3 respectively. The cost of importing the energy is mathematically expressed as:

$$C_{imp} = \sum_{k=1}^{n=24} P_{s,k} c(k), \tag{1}$$

where C_{imp} stands for the cost of importing energy for a full day, k denotes the index of a given hour, n the total number of hours in a day, $P_{s,k}$ the energy provided by the slack bus (interconnection point) in MWh at hour k, and c(k) the cost at a certain hour in ϵ /MWh. This last term is equal to 45ϵ /MWh from 0 to 8 hours, 65ϵ /MWh from 8 to 10, 14 to 18 and 22 to 24 hours, and 90ϵ /MWh from 10 to 14 and 18 to 22 hours.

Equation 1 can be treated as a weighting sum. With the generation data obtained from the timeseries power flow, the total importing cost of importing energy becomes 418753.03 €/day, or about 152.84 M€ in a full year. It is important to note that the study related to the cost of importing energy is decoupled from the fault analysis. This is not a hundred percent realistic, because it could be that a switch trips and hence a line or a transformer are disconnected. Then, it could happen that the interconnection has to provide more power. However, since the probabilities are extremely low, they are discarded when computing this cost.

On the other hand, there are the costs due to faults in transformers or lines. About 0.05 failures per km and year are expected in lines, while transformers are meant to fail 0.15 times a year. The penalty for not providing energy is $180 \in /MWh$. Given that the length of the lines has an impact on its probability of failure, Table 3 shows the length and the subsequent failures per year.

| Line | Length (km) | Failures/year |
|------|-------------|---------------|
| 8-10 | 100.00 | 5.00 |
| 10-9 | 50.00 | 2.50 |
| 9-11 | 70.71 | 3.54 |
| 9-12 | 111.80 | 5.59 |
| 11-6 | 111.80 | 5.59 |

Table 3. Length and failures per year of all active lines

Figure 3 shows that the line connected to the interconnection point operates at a high load. It is critical to note that if line 8-10 fails, the slack should provide all power, but this would result in exceeding the thermal capacity of the line. Thus, if line 8-10 fails, no power can reach the loads.

In the case of line failures, there is a total disconnection time of 2.5 hours; instead, for transformers it is 8 hours. The expected time that an element will be disconnected in a year is found by multiplying the aforementioned disconnection time by the number of failures that take place during a year. Table 4 displays the yearly disconnection time and explains the consequences spotted by

| Element | Disconnection time (h) | Consequences |
|-------------|------------------------|------------------------------------|
| Line 8-10 | 12.50 | No load served - divergence |
| | | _ |
| Line $9-10$ | 6.25 | No load served - divergence |
| Line 9-11 | 8.85 | Loads at buses 2, 3 and 5 unserved |
| Line 9-12 | 13.98 | Load at bus 5 unserved |
| Line 11-6 | 13.98 | No load served |
| Trafo 1-8 | 1.20 | No load served - divergence |
| Trafo 2-9 | 1.20 | Load at bus 2 unserved |
| Trafo 3-10 | 1.20 | Load at bus 3 unserved |
| Trafo 4-11 | 1.20 | Load at bus 4 unserved |
| Trafo 5-12 | 1.20 | Load at bus 5 unserved |

running the power flow. This will allow to estimate the penalties due disconnection.

Table 4. Disconnection time and consequences of losing each element

Once the unserved loads and the associated disconnection times are known, the next step has to do with applying the penalty as follows:

$$C_{discon} \approx \sum_{i=1}^{10} \overline{P}_{uns,i} t_{discon,i} C_p, \tag{2}$$

where C_{discon} is the total disconnection cost, i represents the index of the line or transformer with a total of 10 elements prone to be disconnected (see Table 4), $\overline{P}_{uns,i}$ is the mean unserved power, $t_{discon,i}$ the disconnection time, and C_p the penalty cost to apply. Equation 2 is an approximation in the sense that the unserved power varies according to the time of the day. To not overcomplicate the problem, it has been decided to pick a representative value such as the average.

The application of Equation 2 yields a total yearly penalty cost of $4.99 \text{ M} \in$. For the most part, it is due to the disconnection of lines. Meshing more the system would decrease this cost, but on the other side, it would increase the investment cost. Hence, there is a trade-off between cost and reliability.

All the calculations related to costs have not set an inferior limit to the voltages. However, some of them are likely to be unacceptable in reality. The project will proceed to discuss solutions to this issue in the following phases.

2.2. Problem identification

The network modeled presents some serious issues. First, in case of fault, the demand cannot be covered. The network is a ramified line but does not have any interconnection within the system. If a fault occurs, the two branches are not connected and have to support the demand of the remaining part on its own. In the case of the nuclear power plant, it cannot produce enough energy to fulfill all the demand and in the case of the interconnection, if it was to cover all, it would be overloaded.

This leads to the second problem the network faces, there is a risk of overloading. This may happen in case or fault or if the the nuclear power plant shuts down because there is no other source of generation. This could lead to burning hence security and material damage issue. A third drawback is the high impact of the interruptions. As many line are single lines and there are

no multiple connections, only ramifications, a fault has a high chance to directly disconnect the network. Finally, the voltage cannot be kept constant enough. It is usually accepted to fluctuate 10% around the nominal 1 p.u. while in the current transmission network, the voltage reaches almost 0.8 p.u..

2.3. Solution suggestion

As some of the lines present some overloading and demand coverage problems, we suggest improving lines to better ones which are able to transport more power. In order to do so, the critical lines could be changed from single to double lines and/or even change the conductors to thicker cables which allow a larger amount of power flow. Another approach would be to add more lines to the grid to overcome the demand coverage but we must also be aware that when adding new lines to the system we are also increasing the possibility of line failures which may affect interruptibility and cause economic losses to the system.

On the other hand, adding generation points to the system would also help overcome the stated problems in the previous point. If power is more accessible in different locations, the demand can be fulfilled from various points without saturating the most critical lines while evenly distributing the generation. Finally, another solution could be to change the 220 kV existing lines to 400 kV ones in order to allow these to transport higher amounts of power. With this change, only the amount of power transported would be around three times higher than the current one. However, it has to be taken into account that there would have to be an additional transformer to adapt the 220 kV from the interconnection to 400 kV, and the rest of the transformers would have to be replaced to match nominal voltages.

3. PHASE 2

This chapter considers upgrading the system by means of installing additional lines. In the previous analysis, it was visible that the disconnection of specific lines resulted in an unsolvable problem. Often, no solution was obtained as a result of an exceedingly high demand compared to the available generation. The criteria N-1 was therefore not met, yet it is usually treated as a requirement by control center operators [2], [3].

The central aim of this chapter is reaching a robust grid, where a single failure does not compromise the full system. Several solutions were proposed, such as meshing the network, rising the voltage level, etc. This chapter is devoted to exploring the implications of such proposals. First, a more theoretical explanation describing the formulation is presented, and then, the analysis of results takes place. These results include electrical magnitudes as well as economic data. An optimal configuration is finally provided.

3.1. Addition of lines

Recall that the original system depicted in Figure 1 was for the most part a radial system, in the sense that there was no redundancy in the connection of lines. The operating costs are non-negligible since a significant amount of energy cannot be delivered during faults. To combat this issue, the installation of various new lines (in red) is contemplated, as shown in Figure 4.

By installing new lines, an additional installation cost has to be considered, but a reduction on the operating costs is expected. It is worth worth mentioning that not all contemplated new lines ought to be installed. Rather, by adding one or two of them, the system could already be operating under the desired conditions. There is a cost-benefit tradeoff, so only a few specific new lines will be selected.

3.1.1. Formulation

The formulation of the topology deserves special attention. Mathematically, it is defined as:

$$\{\mathcal{N} \in \mathcal{P}([n]) \mid |\mathcal{N}| = k\},\tag{3}$$

where \mathcal{N} denotes a subset, that is, possible topology out of the full set of configurations $\mathcal{P}([n])$, $[n] = \{\mathbf{1}_{\sigma_1}, \mathbf{1}_{\sigma_2}, ..., \mathbf{1}_{\sigma_n}\}$ represents the set of elements that cause variations on the topology, and k symbolizes the total amount of possibilities. In the contingency analysis, the set [n] is a function of the state of the elements (mainly, lines). These can be in service or out of service, so can be regarded as boolean variables. The employed notation, of the form $\mathbf{1}_{\sigma_i}$, is 1 if the indicator variable σ_i holds true; otherwise, it is 0. The indicator variable, in the case under study, is simply the state of each particular line.

Note that the whole set \mathcal{P} can be further divided into the set composed of the original lines \mathcal{A} , and the set of new lines \mathcal{B} . Let j indicate the number of lines in the original set \mathcal{A} , and n-j the amount of lines in the new set \mathcal{B} . In the particularized case shown in Figure 4, j=6 and n-j=8.

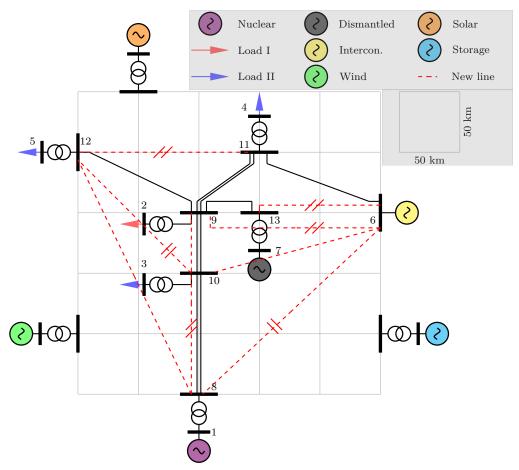


Figure 4. Overview of the network with the addition of lines. Double line if double circuit.

Thus, these subsets are expanded and explicitly become:

$$\begin{cases} \mathcal{A} = \{\mathbf{1}_{\sigma_1}, \mathbf{1}_{\sigma_2}, ..., \mathbf{1}_{\sigma_j}\}, \\ \mathcal{B} = \{\mathbf{1}_{\sigma_{j+1}}, \mathbf{1}_{\sigma_{j+2}}, ..., \mathbf{1}_{\sigma_n}\}. \end{cases}$$
(4)

To perform the contingency analysis, we consider that one of the original lines if faulted. For instance, if line i ends up disconnected, $\sigma_i \leftarrow \texttt{false}$ while the rest of original lines $\sigma_r \leftarrow \texttt{true}$ for $r = \{1, 2, ..., i-1, i+1, ..., j\}$.

On the other hand, in the subset \mathcal{B} it is not straightforward to estimate which lines should be connected or disconnected. Perhaps installing a single additional line is enough to meet the N-1 criteria, or maybe more lines are required. Hence, it has been decided that all permutations have to be analyzed. Since σ are boolean variables, the total number k of contingencies to simulate are:

$$k = j2^{(n-j)},\tag{5}$$

so if j = 6 and n - j = 8, this results in k = 1536 different topologies. Thus, a total of 1536 timeseries power flows are computed.

Security analysis in power systems has been traditionally based on the usage of the DC power flow [4], [5]. It offers the advantage of being non-iterative (and consequently, fast), and allows to determine the influence of faults with the usage of transmission factors. However, its solution is

just an approximation. Since the amount of situations remains reasonable, it has been decided to solve them with the typical Newton-Raphson up to the default precision of $1 \cdot 10^{-8}$ MVA [6].

The general procedure to perform the contingency analysis is shown in Algorithm 1.

```
Algorithm 1: Pseudocode to solve the contingencies
```

```
Input: net initialized class, j, n
      Output: stored results
 1 Generate permutations \forall \boldsymbol{\sigma}_g where g = [1, 2, ..., 2^{(n-j)}]
 2 for i = [1, 2, ..., j] do
            \sigma_i \leftarrow \mathtt{false}
            \sigma_r \leftarrow \mathsf{true}, where r \neq i and r \leq j
            \mathcal{A} \leftarrow \{\mathbf{1}_{\sigma_1}, \mathbf{1}_{\sigma_2}, ..., \mathbf{1}_{\sigma_j}\}
            for g = [1, 2, ..., 2^{(n-j)}] do
 6
                    [\sigma_{j+1}, \sigma_{j+2}, ..., \sigma_n] \leftarrow \boldsymbol{\sigma}_g
 7
                   \mathcal{B} \leftarrow \{\mathbf{1}_{\sigma_{j+1}}, \mathbf{1}_{\sigma_{j+2}}, ..., \mathbf{1}_{\sigma_n}\}
 8
                   \mathcal{N} \leftarrow \mathcal{A} \cup \mathcal{B}
 9
                   pandapower.timeseries.run_timeseries(\mathcal{N},net)
10
                   Store results
```

Out of all results extracted, an analysis procedure is required in order to determine which configuration meets the N-1 criteria. The requirements are listed below:

- The losses in the lines have to stay below 2%.
- The voltages have to be between a range of $\pm 10\%$.
- All lines have to remain below 80% its maximum capacity.

Apart from these requirements, an additional criteria has to do with the costs. These will be critical when choosing the best configuration out of all possible ones. Table 5 displays the costs for the lines, depending on their representative voltage level and the number of circuits.

| Type | Mean (€) | Min-max range (€) | Median (€) |
|--------------------------|----------|-------------------|------------|
| 380-400 kV, 2 circuits | 1060919 | 579771 - 1401585 | 1023703 |
| 380-400 kV, 1 circuits | 598231 | 302664 - 766802 | 597841 |
| 220-225 kV, 2 circuits | 407521 | 354696 - 461664 | 437263 |
| 220-225 kV, 1 circuits | 288289 | 157926 - 298247 | 218738 |

Table 5. Network infraestructure costs for the lines. Data from [7].

It has been decided to calculate the costs with mean value.

3.1.2. Results

Out of all results extracted, an analysis procedure is required in order to determine which configuration meets the N-1 criteria. The prechosen configurations are the ones that ensure that in spite of the disconnection of a given element, the power flow remains feasible and the design criterias are met. A total of 39 have satisfied all requirements. Table 6 shows the top 10 cheapest topologies, according to the costs in Table 5.

| Identifier | New lines | Infraestructure cost (M€) |
|------------|---------------------------------|---------------------------|
| 19 | [6-13, 6-10, 8-9, 10-12] | 359.50 |
| 214 | [6-13, 6-10, 11-12, 8-9] | 362.99 |
| 77 | [6-13, 8-9, 10-12, 9-6] | 375.04 |
| 49 | [6-13, 11-12, 8-9, 9-6] | 378.54 |
| 80 | [6-13, 6-10, 11-12, 8-9, 10-12] | 420.63 |
| 189 | [6-13, 6-10, 8-9, 10-12, 9-6] | 420.63 |
| 45 | [6-13, 6-10, 8-9, 10-12, 8-12] | 423.96 |
| 70 | [6-13, 8-9, 10-12, 9-6] | 424.12 |
| 157 | [6-13, 6-10, 11-12, 8-9, 8-12] | 427.46 |
| 250 | [6-13, 11-12, 8-9, 10-12, 9-6] | 436.17 |

Table 6. Best configurations with the additional lines

The results indicate that the differences in the infraestructure costs are rather minimal. However, installing only four additional lines tends to be the best option. Line 6-13 has been found necessary to ensure a proper operating state of the system under all near-optimal configurations. This makes sense considering that the interconnection usually provides most of the power. Hence, a strong connection to the network is convenient. In fact, the best topology includes two lines connecting the slack bus to the rest of the system are present.

By ensuring that the N-1 criteria is met, we guarantee that all power will be provided independently of which element fails. In reality, this matter may be a bit more complex as two lines could fail simultaneously. Nevertheless, the associated cross-probability is extremely low, and hence, neglected. This implies that no operating costs have to be calculated; it is known beforehand that they will be null as all power is provided for the optimal configuration.

3.2. Rising the voltage level

3.2.1. Description

While installing more lines is a technically feasible strategy, it may not be the most optimal in terms of costs since the voltage level of the grid could be increased. The price to pay for such a change is the replacement of the initial transformers of 25/220 kV and 36/220 kV, for transformers that raise the voltage up to 400 kV (thus, 25/380 kV and 36/380 kV).

In practical terms, raising the voltage may not be as simple as replacing four transformers. For instance, the insulators and the switchgear would have to be changed as well. In the worst scenario, the lines in the towers would have to be more separated, which could cause a replacement of the whole set of supports. To keep the problem arguably simple, it is taken into account that the cost of the transformer station is proportional to the voltage — as can be deduced in [7].

The benefits of increasing the votlage become obvious when observing that the power in a threephase system such as this one is given by:

$$S = \sqrt{3}V_{ll}I,\tag{6}$$

where V_{ll} identifies the line voltage. With this simple relationship, if it is assumed that S remains constant, and V_{ll} increases by a factor of $380/220 \approx \sqrt{3}$, the current would decrease by approx-

imately a factor of $\sqrt{3}$. This means that the active power losses, which are proportional to the square of the current, are roughly reduced by a factor of 3.

Regarding the costs, representative values in ϵ /km are gathered in Table 7. While there is a certain dependence on the type, a generic substation could be taken as reference. Thus, a cost of 42627 ϵ /kV is chosen as an indicator. It is considered that all elements in the substation would have to be replaced to adapt the new voltage level of 380 kV. If there are four substations to be replaced, the total cost for doing so becomes 64.79 M ϵ .

| Type | Mean (€/kV) | Min-max range (€/kV) | Median (€/kV) |
|---------------------|-------------|----------------------|---------------|
| All substations | 42627 | 24994 - 55508 | 36755 |
| All GIS substations | 46237 | 29837 - 56017 | 37449 |
| AIS with 9+ bays | 44008 | 28838 - 56157 | 41080 |
| AIS with 5-8 bays | 35593 | 19936 - 37251 | 29021 |
| AIS with 1-4 bays | 33192 | 20276 - 48319 | 26628 |

Table 7. Network infraestructure costs for the substation. Data from [7].

3.2.2. Results

The same amount of contingencies as before are computed. Out of the 1536, this time more permutations have become feasible (52 in total). Of course, raising the voltage has a positive effect in this regard, as previously hypothesized. In any case there is a trade-off situation: while the kilometers of new lines may decrease, there is an additional cost due to the new substations. It has to be assessed if the saving due to raising the voltage outweights the cost of installing new substations. Table 8 shows such results for the 10 cheapest options, where the cost of the substations are independent on the topology.

| Identifier | New lines | Lines (M€) | Transformers (M€) | Total (M€) |
|------------|--------------------------|------------|-------------------|------------|
| 163 | [6-13, 8-9, 10-12] | 313.92 | 64.79 | 378.71 |
| 133 | [6-13, 11-12, 8-9] | 317.41 | 64.79 | 382.20 |
| 235 | [6-13, 8-9, 8-12] | 320.75 | 64.79 | 385.54 |
| 30 | [6-13, 8-12, 6-8] | 346.07 | 64.79 | 410.86 |
| 19 | [6-13, 6-10, 8-9, 10-12] | 359.50 | 64.79 | 424.29 |
| 214 | [6-13, 6-10, 11-12, 8-9] | 362.99 | 64.79 | 427.78 |
| 58 | [6-13, 6-10, 8-9, 8-12] | 366.33 | 64.79 | 431.12 |
| 77 | [6-13, 8-9, 10-12, 9-6] | 375.04 | 64.79 | 439.83 |
| 169 | [6-13, 8-9, 10-12, 8-12] | 378.38 | 64.79 | 443.17 |
| 49 | [6-13, 11-12, 8-9, 9-6] | 378.54 | 64.79 | 443.33 |

Table 8. Economic results of replacing the substations

A similar conclusion as before is reached. A new line that connects the interconnection with the dismantled plant is required to meet the planning requirements and achieve an optimal topology. Notice that thanks to the increase in the voltage level, only three new lines should be installed in the optimal configurations. This allows to reduce the cost of these new lines up to 313.92 M \in in the best scenario. However, the extra cost due to the replacement of the transformers implies that the total cost of 378.71 M \in surpasses the minimum cost indicated in Table 6, which is equal to 359.50 M \in .

Therefore, even if both options do not differ much in costs, it would still be better to operate around the nominal voltage of 220 kV. This does not mean, however, that installing more lines is the only feasible solution to confront the technical issues. This may have been true some decades ago, but nowadays, power systems can benefit from the penetration of renewables. Renewable sources of generation can be connected near the loads, which allows to reduce the losses and improve the efficiency of the system. A scenario with renewables is covered in the following chapter.

4. CODE

```
1 import pandapower as pp
2 import pandas as pd
3 import numpy as np
 4 \quad {\tt import \ pandapower.control \ as \ control}
5\, import pandapower.networks as nw
 6\, import pandapower.timeseries as timeseries
7 \quad {\tt from \ pandapower.timeseries.data\_sources.frame\_data \ import \ DFData}
8 from pandapower.plotting import simple_plot
10 from line_param_calc import calc_line
11
12
13
14 pd.set_option('display.max_rows', 500)
15 \  \, {\tt pd.set\_option('display.max\_columns', 500)}
16 pd.set_option('display.width', 1000)
18 \ \mathsf{def} \ \mathsf{initialize\_net(path\_bus,\ path\_geodata,\ path\_line,\ path\_demand,\ path\_busload,\ path\_generation}
        , path_busgen, path_trafo):
19
20
       initialize the grid from the .csv files
21
22
       :param path_bus: path to the bus .csv file
23
       :param geodata: path to the geodata .csv file
       :param path_line: path to the line .csv file
24
25
       :param path_demand: path to the normalized demand .csv file
26
       :param busload: path to the bus-load look up table .csv file
27
       :param path_generation: path to the normalized generation .csv file
28
       :param busgen: path to the bus-generator look up table .csv file
29
       :param trafo: path to the trafo .csv file
30
       :return: the net class
31
32
33
       def create_bus(path_bus, path_geodata):
34
35
            adapts the data from the bus file (if needed)
36
37
           :param path_bus:
           :param path_geodata:
39
            :return: the net with the buses added
40
41
42
           df_bus = pd.read_csv(path_bus)
43
           df_geodata = pd.read_csv(path_geodata)
44
45
           net.bus = df_bus
46
47
            # adapt geodata
48
           for 11 in range(len(df_geodata)):
49
                indx_bus = pp.get_element_index(net, "bus", df_geodata['name'][11])
50
                df_geodata['name'][11] = indx_bus
51
52
           net.bus_geodata = df_geodata
53
54
            return net
55
56
57
       def create_line(path_line):
58
59
            adapts the data from the line file
61
           :param path_line:
62
            :return: the net with the lines added
63
64
         df_line = pd.read_csv(path_line)
```

```
66
             for _, line in df_line.iterrows():
 67
                 from_bus = pp.get_element_index(net, "bus", line.from_bus)
 68
                to_bus = pp.get_element_index(net, "bus", line.to_bus)
 69
 70
                rr. xx. cc. imax = calc line(line.a.
 71
                                              line.b,
 72
                                              line.c.
 73
                                               line.d,
 74
                                              line.e.
 75
                                              line.max_i,
 76
                                              int(line.parallel))
 77
 78
                 pp.create_line_from_parameters(net,
 79
                                                 from bus,
 80
                                                 to_bus,
 81
                                                 length km=line.length.
 82
                                                 r_ohm_per_km=rr,
 83
                                                 x_ohm_per_km=xx,
 84
                                                 c_nf_per_km=cc,
 85
                                                 max i ka=imax.
 86
                                                 name=line.name_1,
 87
                                                 parallel=line.parallel)
 89
             return net
 90
 91
 92
        def create_load(path_demand, path_busload, path_bus):
 93
 94
            adapts the load files
 95
 96
            :param path_demand:
 97
            :param path_busload:
 98
            :param path_bus:
 99
             :return: the net with the loads added
100
101
102
            df_demand = pd.read_csv(path_demand)
103
            df_busload = pd.read_csv(path_busload)
104
            df_bus = pd.read_csv(path_bus)
105
106
            # create basic load dataframe
107
            \mbox{\tt\#} find the bus index of each load
108
            load_indx = []
109
             for _, load in df_busload.iterrows():
110
                 bus_load = pp.get_element_index(net, "bus", load.bus)
111
                load_indx.append(bus_load)
112
113
             load_indx = pd.DataFrame(load_indx)
114
            load_indx = load_indx.rename(columns={0: "bus"})
115
116
             # load name and peak power
117
            load_name = df_busload['bus']
118
             load_pmw = df_busload['p_mw']
119
            load_gmvar = df_busload['q_mvar']
120
121
            # merge in a full dataframe
122
             headers = ["name", "bus", "p_mw", "q_mvar"]
            df_load = pd.concat([load_name, load_indx, load_pmw, load_qmvar], axis=1)
123
124
            df_load.columns.values[0] = "name"
125
126
             # create time series from the basic load df
127
            Nt = len(df_demand)
            N1 = len(df_load)
128
129
             pmw_ts = np.zeros((Nt, N1), dtype=float)
130
             qmvar_ts = np.zeros((Nt, N1), dtype=float)
131
            for i in range(Nt): # number of time periods
132
               pmw_ts[i,:] = df_load['p_mw'][:] * df_demand['norm'][i]
```

```
133
                qmvar_ts[i,:] = df_load['q_mvar'][:] * df_demand['norm'][i]
134
135
            # form loads as a static picture (initial time)
136
            for ll in range(len(df_busload)):
137
                pp.create_load(net, bus=load_indx['bus'][11], p_mw=pmw_ts[0, 11], q_mvar=qmvar_ts[0,
          11], name=load_name[11], index=int(11))
138
139
140
            df_pload_ts = pd.DataFrame(pmw_ts, index=list(range(Nt)), columns=net.load.index)
141
            df_qload_ts = pd.DataFrame(qmvar_ts, index=list(range(Nt)), columns=net.load.index)
142
            ds_pload_ts = DFData(df_pload_ts)
143
            ds_qload_ts = DFData(df_qload_ts)
            const_load = control.ConstControl(net, element='load', element_index=net.load.index,
144
         variable='p_mw', data_source=ds_pload_ts, profile_name=net.load.index)
145
            const_load = control.ConstControl(net, element='load', element_index=net.load.index,
         variable='q_mvar', data_source=ds_qload_ts, profile_name=net.load.index) # add the
         reactive like this?
146
147
            return net
148
149
150
        def create_generator(path_generation, path_busgen, path_bus):
151
152
            adapts the generation files
153
154
            :param path_generation:
155
            :param path_busgenerator:
156
            :param path_bus:
157
            :return: the net with the generators added
158
159
160
            df_generation = pd.read_csv(path_generation)
161
            df_busgen = pd.read_csv(path_busgen)
162
            df_bus = pd.read_csv(path_bus)
163
164
            # create basic generator dataframe
165
            # find the bus index of each gen
166
            gen_indx = []
167
            for _, gen in df_busgen.iterrows():
168
                bus_gen = pp.get_element_index(net, "bus", gen.bus)
169
                gen_indx.append(bus_gen)
170
171
            gen_indx = pd.DataFrame(gen_indx)
172
            gen_indx = gen_indx.rename(columns={0: "bus"})
173
174
            # load name and peak power
175
            gen_name = df_busgen['bus']
176
            gen_pmw = df_busgen['p_mw']
            gen_vpu = df_busgen['vm_pu']
177
178
179
            # merge in a full dataframe
180
            headers = ["name", "bus", "p_mw", "vm_pu"]
181
            df_gen = pd.concat([gen_name, gen_indx, gen_pmw, gen_vpu], axis=1)
182
            df_gen.columns.values[0] = "name"
183
184
            # create time series from the basic load df
185
            Nt = len(df_generation)
186
            Ng = len(df_gen)
187
            pmw_ts = np.zeros((Nt, Ng), dtype=float)
188
            for i in range(Nt): # number of time periods \[
                pmw_ts[i,:] = df_gen['p_mw'][:] * df_generation['norm'][i]
189
190
191
            # gen structure for 1 t
102
            for ll in range(len(df_busgen)):
193
                pp.create_gen(net, bus=gen_indx['bus'][11], p_mw=pmw_ts[0, 11], vm_pu=gen_vpu[11],
         name=gen_name[11], index=int(11))
194
```

```
195
196
             # timeseries
197
            df_gen_ts = pd.DataFrame(pmw_ts, index=list(range(Nt)), columns=net.gen.index)
ds_gen_ts = DFData(df_gen_ts)
198
            const_gen = control.ConstControl(net, element='gen', element_index=net.gen.index,
199
         variable='p_mw', data_source=ds_gen_ts, profile_name=net.gen.index)
200
201
             return net
202
203
204
        def create_intercon(path_bus):
205
206
             defines the interconnection (slack bus)
207
208
            :param path_bus:
209
             :return: the net with the interconnection added
210
211
212
            df_bus = pd.read_csv(path_bus)
213
214
             # find the slack index
215
             slack_indx = 0
216
            for ll in range(len(df_bus)):
217
                 # slack_indx = pp.get_element_index(net, "bus", bb.name)
                 if df_bus['name'][11] == 'intercon':
218
219
                     slack_indx = pp.get_element_index(net, "bus", df_bus['name'][11])
220
221
            pp.create_ext_grid(net, slack_indx, vm_pu=1.0, va_degree=0)
222
223
224
225
226
        def create_trafo(path_trafo):
227
228
             defines the transformers
229
230
            :param path_trafo:
231
             :return: the net with the transformers {\tt added}
232
233
234
            df_trafo = pd.read_csv(path_trafo)
235
236
             # for trafo in df_trafo:
237
             for _, trafo in df_trafo.iterrows():
238
                 hv_bus = pp.get_element_index(net, "bus", trafo.hv_bus)
239
                lv_bus = pp.get_element_index(net, "bus", trafo.lv_bus)
240
241
                 pp.create_transformer_from_parameters(net,
242
243
                                                         lv_bus,
244
                                                         trafo.sn_mva,
245
                                                         trafo.vn_hv_kv,
246
                                                         trafo.vn_lv_kv,
247
                                                         trafo.vkr_percent,
248
                                                         trafo.vk_percent,
249
                                                         trafo.pfe_kw,
250
                                                         trafo.i0_percent)
251
252
            return net
253
254
255
256
257
258
259
        # create empty network
260
        net = pp.create_empty_network()
```

```
261
262
        # buses
263
        net = create_bus(path_bus, path_geodata)
264
265
        # lines
266
        net = create_line(path_line)
267
268
269
        net = create_load(path_demand, path_busload, path_bus)
270
271
        # gens
272
        net = create_generator(path_generation, path_busgen, path_bus)
273
274
        # interconnection
275
        net = create_intercon(path_bus)
276
277
278
        net = create_trafo(path_trafo)
279
280
281
282
        return net
283
284
285 if __name__ == "__main__":
286
        # load paths
287
        path_bus = 'Datafiles/bus1.csv'
288
        path_geodata = 'Datafiles/geodata1.csv'
289
        path_line = 'Datafiles/line1.csv'
290
        path_demand = 'Datafiles/demand1.csv'
291
        path_busload = 'Datafiles/bus_load1.csv'
292
        path_generation = 'Datafiles/generation1.csv'
293
        path_busgen = 'Datafiles/bus_gen1.csv'
294
        path_trafo = 'Datafiles/trafo1.csv'
295
296
        # define net
297
        net = initialize_net(path_bus, path_geodata, path_line, path_demand, path_busload,
        path_generation, path_busgen, path_trafo)
298
299
        # run timeseries
300
        ow = timeseries.OutputWriter(net, output_path="./Results/", output_file_type=".xlsx")
301
        ow.log_variable('res_bus', 'vm_pu')
302
        ow.log_variable('res_line', 'loading_percent')
303
        timeseries.run_timeseries(net)
304
305
        # run diagnostic
306
        # pp.diagnostic(net)
307
        print(net.bus)
308
309
        # plot
310
        # pp.plotting.simple_plot(net)
311
        # simple_plot(net)
```

Listing 4.1. Main code in Python with the Pandapower library

```
1 import numpy as np
3 def calc_line(a, b, c, d, e, immax, npar, Rca, Dext, kgg):
4
5
       calculate r, x, c, and return also Imax
6
      :param a: horizontal distance between A1 and C2
7
8
      :param b: horizontal distance between B1 and B2
9
      :param c: horizontal distance between C1 and A2
10
       :param d: vertical distance between A1 and B1
11
       :param e: vertical distance between B1 and C1
12 :param immax: max current in A
```

```
13
       :param npar: number of parallel lines (1 or 2)
14
       :param Rca: ac resistance in ohm/km
15
       :param Dext: external diameter in mm
16
       :param kg: factor of roughly 0.8
17
       :return: r, x, c, imax
18
19
20
        def single_line(a, b, immax, Rca, Dext, kgg):
21
22
           calculate the R, X, C parameters, also return Imax
23
24
           :param a: horizontal distance between A and C
            :param b: vertical distance between A and B
25
26
           :param immax: max current in A
27
           :param Rca: ac resistance in ohm/km
28
           :param Dext: external diameter in mm
29
           :param kg: factor of roughly 0.8
30
31
            :return: R, X, C, Imax, in the units desired by pandapower
32
33
           # cardinal: https://www.elandcables.com/media/38193/acsr-astm-b-aluminium-conductor-
34
        steel-reinforced.pdf
35
           # 54 Al + 7 St, Imax = 888.98 A
36
37
           w = 2 * np.pi * 50 # rad / s
38
           Imax = immax * 1e-3 # kA
39
           \# Stot = 547.3 * 1e-6 \# m2, the total section
40
            \# R_ac_75 = 0.07316 * 1e-3 # ohm / m
41
           \# kg = 0.809 \# from the slides in a 54 + 7
42
           R_ac_75 = Rca * 1e-3 # ohm / m, should we correct by temperatures?
43
           Stot = np.pi * Dext ** 2 / 4 * 1e-6 # m2, the total section
44
45
           kg = kgg
46
47
           r = np.sqrt(Stot / np.pi) # considering the total section
48
49
           dab = np.sqrt((a / 2) ** 2 + b ** 2)
50
           dbc = np.sqrt((a / 2) ** 2 + b ** 2)
           dca = a
51
52
53
           GMD = (dab * dbc * dca) ** (1 / 3)
           GMR = kg * r
54
           RMG = r
55
56
57
           L = 4 * np.pi * 1e-7 / (2 * np.pi) * np.log(GMD / GMR) # H / m
58
59
           C = 2 * np.pi * 1e-9 / (36 * np.pi) / np.log(GMD / RMG) # F / m
60
61
            # in the units pandapower wants
62
           R_km = R_ac_75 * 1e3 # ohm / km
           X_{km} = L * w * 1e3 # ohm / km
63
            C_{km} = C * 1e9 * 1e3 # nF / km
64
66
           return R_km, X_km, C_km, Imax
67
68
69
       def double_line(a, b, c, d, e, immax, Rca, Dext, kgg):
70
71
            calculate the R, X, C parameters, also return Imax
72
73
            :param a: horizontal distance between A1 and C2
74
           :param b: horizontal distance between B1 and B2
75
           :param c: horizontal distance between C1 and A2
76
           :param d: vertical distance between A1 and B1
77
            :param e: vertical distance between B1 and C1
           :param immax: max current in A
78
```

```
79
            :param Rca: ac resistance in ohm/km
 80
            :param Dext: external diameter in mm
 81
            :param kgg: factor of roughly 0.8
 82
            :return: R, X, C, Imax, in the units desired by pandapower
 83
 84
            # cardinal: https://www.elandcables.com/media/38193/acsr-astm-b-aluminium-conductor-
 85
         steel-reinforced.pdf
            # 54 Al + 7 St, Imax = 888.98 A
 86
 87
 88
            w = 2 * np.pi * 50 # rad / s
 89
            Imax = immax * 1e-3 * 2 \# kA, for the full line, x2
            \# Stot = 547.3 * 1e-6 \# m2, the total section
 90
 91
            \# R_ac_75 = 0.07316 * 1e-3 # ohm / m
 92
            \# kg = 0.809 \# from the slides in a 54 + 7
 93
 94
            R_ac_75 = Rca * 1e-3 # ohm / m, should we correct by temperatures?
 95
            Stot = np.pi * Dext ** 2 / 4 * 1e-6 # m2, the total section
 96
            kg = kgg
 97
 98
99
100
            r = np.sqrt(Stot / np.pi) # considering the total section
101
102
            da1b1 = np.sqrt((b / 2 - a / 2) ** 2 + d ** 2)
            da1b2 = np.sqrt((a / 2 + b / 2) ** 2 + d ** 2)
103
            da2b1 = np.sqrt((c / 2 + b / 2) ** 2 + e ** 2)
104
105
            da2b2 = np.sqrt((b / 2 - c / 2) ** 2 + e ** 2)
106
            db1c1 = np.sqrt((b / 2 - c / 2) ** 2 + e ** 2)
107
            db1c2 = np.sqrt((b / 2 + a / 2) ** 2 + d ** 2)
108
109
            db2c1 = np.sqrt((b / 2 + c / 2) ** 2 + e ** 2)
110
            db2c2 = np.sqrt((b / 2 - a / 2) ** 2 + d ** 2)
111
112
            dc1a1 = np.sqrt((a / 2 - c / 2) ** 2 + (d + e) ** 2)
113
            dc1a2 = c
114
            dc2a1 = a
115
            dc2a2 = np.sqrt((a / 2 - c / 2) ** 2 + (d + e) ** 2)
116
117
            dab = (da1b1 * da1b2 * da2b1 * da2b2) ** (1 / 4)
118
            dbc = (db1c1 * db1c2 * db2c1 * db2c2) ** (1 / 4)
119
            dca = (dc1a1 * dc1a2 * dc2a1 * dc2a2) ** (1 / 4)
120
121
            rp = kg * r
122
123
            da1a2 = np.sqrt((a / 2 + c / 2) ** 2 + (d + e) ** 2)
124
            db1b2 = b
125
            dc1c2 = np.sqrt((c / 2 + a / 2) ** 2 + (d + e) ** 2)
126
127
            drap = np.sqrt(rp * da1a2)
128
            drbp = np.sqrt(rp * db1b2)
129
            drcp = np.sqrt(rp * dc1c2)
130
131
            dra = np.sqrt(r * da1a2)
132
            drb = np.sqrt(r * db1b2)
133
            drc = np.sqrt(r * dc1c2)
134
135
            GMD = (dab * dbc * dca) ** (1 / 3)
136
            GMR = (drap * drbp * drcp) ** (1 / 3)
137
            RMG = (dra * drb * drc) ** (1 / 3)
138
139
            L = 4 * np.pi * 1e-7 / (2 * np.pi) * np.log(GMD / GMR) # H / m
140
141
            C = 2 * np.pi * 1e-9 / (36 * np.pi) / np.log(GMD / RMG) # F / m
142
143
            # in the units pandapower wants
            R_km = R_ac_75 / 2 * 1e3 # ohm / km, like 2 resistances in parallel
144
```

```
145 X_km = L * w * 1e3 # ohm / km
146
           C_{km} = C * 1e9 * 1e3 # nF / km
147
148
           return R_km, X_km, C_km, Imax
149
150
       if npar == 1:
151
           rr, xx, cc, imm = single_line(a, b, immax, Rca, Dext, kgg)
152
        elif npar == 2:
153
          rr, xx, cc, imm = double_line(a, b, c, d, e, immax, Rca, Dext, kgg)
154
155
           print('Error: number of parallel lines is not 1 nor 2')
156
157
        return rr, xx, cc, imm
158
159 # rr, xx, cc, ii = double_line(11, 2, 4, 5, 6, 1000)
160 # print(rr, xx, cc, ii)
```

Listing 4.2. Code for the calculation of lines

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