

SMART GRIDS: FROM TRADITIONAL TO MODERNIZED RESILIENT SYSTEMS

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SMART GRIDS

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CONTENTS

1	Introduction	2
2	Phase 1	3
2.1	Operating costs	6
2.2	Problem identification	7
2.3	Solution suggestion	8
3	Phase 2	9
3.1	Addition of lines	9
3.1.1	Formulation	9
3.1.2	Results	11
3.2	Rising the voltage level	12
3.2.1	Description	12
3.2.2	Results	13
4	Phase 3	15
4.1	Overview	15
4.2	Renewable's integration	16
4.2.1	Solar PV	16
4.2.2	Wind	17
4.3	Base case analysis	18
4.4	Contingency analysis	19
5	Phase 4	20
5.1	Storage	20
5.2	Dismantled plant	22
5.3	Base case results	23
5.4	Contingency analysis	24
6	Code	26
	Bibliography	34

1. INTRODUCTION

2. PHASE 1

A system such as the one displayed in Figure 1 is analyzed. The network operates at the transmission level and feeds dispersed demand points that symbolize distribution grids. The grid has an interconnection with a transmission grid, and at the same time, some power is provided by the nuclear power plant. Initially, there are no renewable power plants nor storage systems, which compromises the security of the grid.

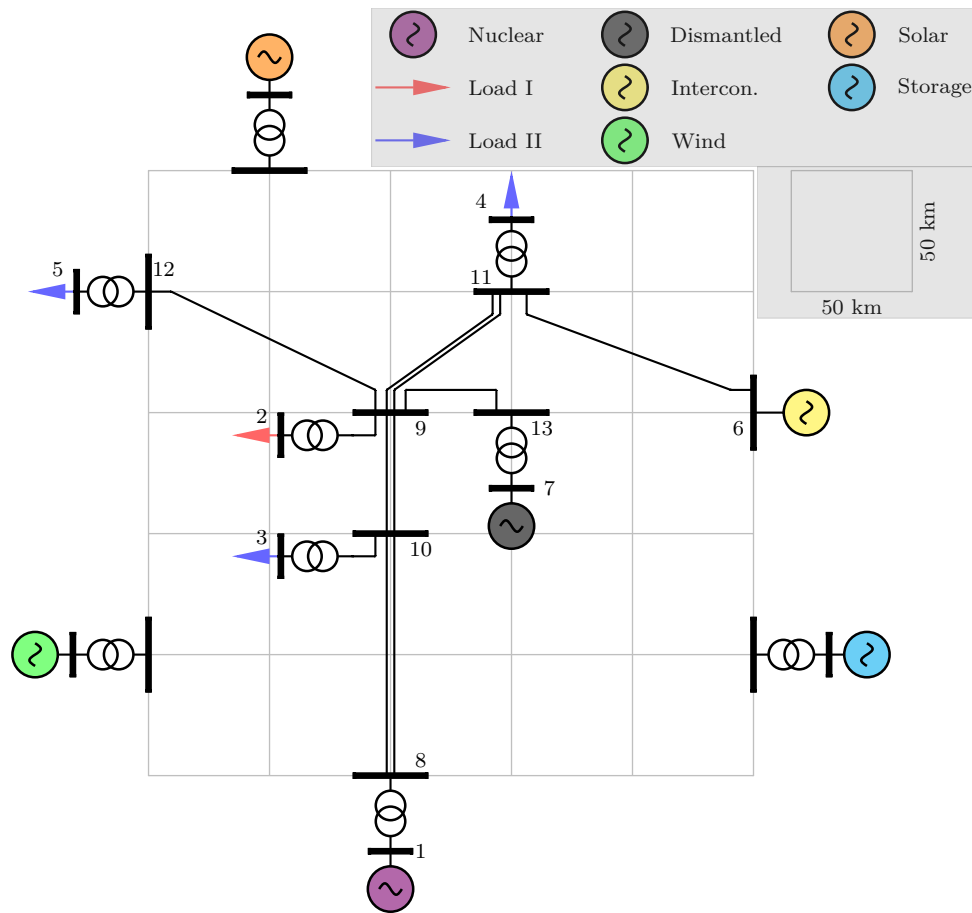


Figure 1. Overview of the network

The first step to analyze the system is to know the demand and the generation profile. In order to model them, the hourly demand and generation data of Spain have been collected [1]. To obtain a typical working day, a statistical analysis has been performed taking into account only the days from the 1st of January to the 31st of March, from Tuesday to Thursday and removing the national holidays. The result then has been normalized. analyze the system is This way, the consumption profile is obtained by from the product of the normalized demand and the peak power consumption of 375 MW for load type I and 140 MW for type II. For the generation profile, for simplicity, it has been assumed that the nuclear power plant follows the demand curve, i.e., it is not acting as a constant generator.

Bus Hour	1	2	3	4	5	6	8	9	10	11	12
0	1.050	0.963	0.989	0.972	0.937	1.000	1.031	0.986	1.000	0.984	0.950
1	1.050	0.974	0.998	0.982	0.952	1.000	1.035	0.995	1.008	0.993	0.963
2	1.050	0.981	1.003	0.988	0.961	1.000	1.037	1.001	1.013	0.998	0.972
3	1.050	0.984	1.005	0.990	0.965	1.000	1.038	1.003	1.015	1.000	0.975
4	1.050	0.985	1.006	0.991	0.966	1.000	1.038	1.004	1.015	1.001	0.976
5	1.050	0.981	1.003	0.988	0.961	1.000	1.037	1.001	1.013	0.998	0.972
6	1.050	0.967	0.992	0.975	0.942	1.000	1.032	0.989	1.003	0.987	0.955
7	1.050	0.938	0.969	0.950	0.905	1.000	1.022	0.965	0.983	0.964	0.920
8	1.050	0.915	0.952	0.931	0.876	1.000	1.014	0.947	0.967	0.946	0.893
9	1.050	0.904	0.944	0.921	0.862	1.000	1.010	0.938	0.960	0.938	0.880
10	1.050	0.900	0.941	0.918	0.856	1.000	1.009	0.935	0.957	0.935	0.875
11	1.050	0.901	0.941	0.919	0.857	1.000	1.009	0.936	0.958	0.935	0.876
12	1.050	0.904	0.944	0.921	0.861	1.000	1.010	0.938	0.960	0.938	0.879
13	1.050	0.906	0.945	0.923	0.864	1.000	1.011	0.939	0.961	0.939	0.882
14	1.050	0.916	0.953	0.931	0.877	1.000	1.014	0.948	0.968	0.947	0.894
15	1.050	0.922	0.957	0.936	0.884	1.000	1.016	0.953	0.972	0.952	0.901
16	1.050	0.925	0.960	0.939	0.889	1.000	1.018	0.955	0.974	0.954	0.905
17	1.050	0.926	0.961	0.940	0.890	1.000	1.018	0.956	0.975	0.955	0.906
18	1.050	0.921	0.957	0.936	0.884	1.000	1.016	0.952	0.972	0.951	0.900
19	1.050	0.903	0.943	0.920	0.860	1.000	1.010	0.937	0.959	0.937	0.878
20	1.050	0.891	0.933	0.910	0.844	1.000	1.005	0.927	0.950	0.927	0.863
21	1.050	0.897	0.939	0.915	0.853	1.000	1.008	0.933	0.955	0.932	0.871
22	1.050	0.921	0.957	0.936	0.884	1.000	1.016	0.952	0.972	0.951	0.900
23	1.050	0.946	0.975	0.957	0.915	1.000	1.025	0.972	0.988	0.970	0.929

Table 1. Voltage profile, in pu, for 24 hours

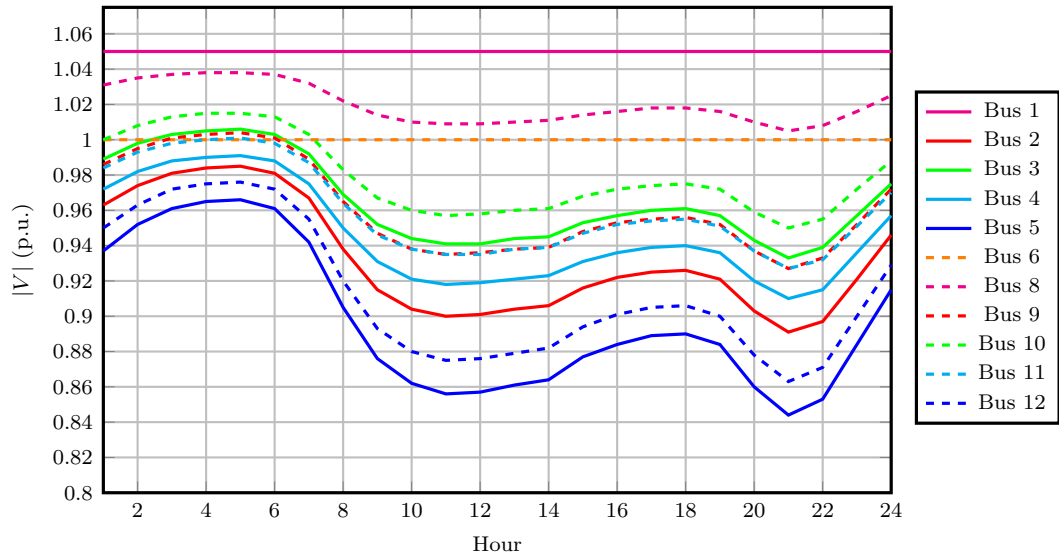


Figure 2. Voltage profile during 24 hours for the initial grid. The low-voltage buses are plotted in solid lines; the high-voltage ones are in dashed lines.

Load Hour	8-10	10-9	9-11	9-12	11-6
0	26.423	19.999	9.388	30.774	63.562
1	24.385	18.464	8.850	28.312	59.190
2	23.089	17.491	8.517	26.761	56.451
3	22.549	17.087	8.381	26.117	55.319
4	22.458	17.019	8.358	26.009	55.130
5	23.082	17.486	8.515	26.752	56.435
6	25.729	19.475	9.203	29.932	62.065
7	30.615	23.176	10.549	35.928	72.752
8	34.100	25.846	11.559	40.331	80.765
9	35.690	27.073	12.031	42.383	84.443
10	36.296	27.542	12.213	43.173	85.847
11	36.166	27.441	12.174	43.002	85.544
12	35.740	27.111	12.046	42.448	84.558
13	35.480	26.910	11.969	42.110	83.956
14	33.997	25.766	11.528	40.198	80.526
15	33.090	25.069	11.262	39.042	78.435
16	32.569	24.669	11.110	38.381	77.234
17	32.392	24.534	11.059	38.158	76.828
18	33.187	25.143	11.290	39.165	78.657
19	35.865	27.208	12.084	42.610	84.847
20	37.641	28.588	12.620	44.945	88.969
21	36.689	27.847	12.332	43.688	86.759
22	33.143	25.110	11.278	39.109	78.557
23	29.319	22.190	10.183	34.319	69.877

Table 2. Percentual loading of the lines for a full day operation

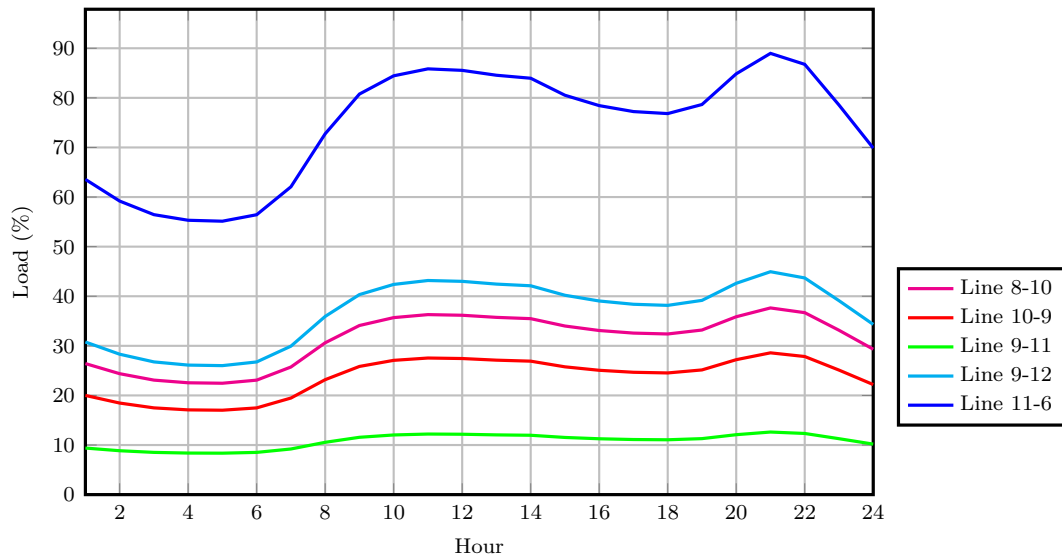


Figure 3. Representation of the percentual loading of the lines during 24 hours

2.1. Operating costs

Regarding the operating costs, some estimations are made in order to assess the influence of importing energy and the impact of faults on lines and transformers.

First, the cost of importing energy depends on the time zone: valley, flat or peak. The analysis that follows considers a working day, which is precisely the date for which the voltages and loading profiles have been shown in Figures 2 and 3 respectively. The cost of importing the energy is mathematically expressed as:

$$C_{imp} = \sum_{k=1}^{n=24} P_{s,k} c(k), \quad (1)$$

where C_{imp} stands for the cost of importing energy for a full day, k denotes the index of a given hour, n the total number of hours in a day, $P_{s,k}$ the energy provided by the slack bus (interconnection point) in MWh at hour k , and $c(k)$ the cost at a certain hour in €/MWh. This last term is equal to 45 €/MWh from 0 to 8 hours, 65 €/MWh from 8 to 10, 14 to 18 and 22 to 24 hours, and 90 €/MWh from 10 to 14 and 18 to 22 hours.

Equation 1 can be treated as a weighting sum. With the generation data obtained from the timeseries power flow, the total importing cost of importing energy becomes 418753.03 €/day, or about 152.84 M€ in a full year. It is important to note that the study related to the cost of importing energy is decoupled from the fault analysis. This is not a hundred percent realistic, because it could be that a switch trips and hence a line or a transformer are disconnected. Then, it could happen that the interconnection has to provide more power. However, since the probabilities are extremely low, they are discarded when computing this cost.

On the other hand, there are the costs due to faults in transformers or lines. About 0.05 failures per km and year are expected in lines, while transformers are meant to fail 0.15 times a year. The penalty for not providing energy is 180 €/MWh. Given that the length of the lines has an impact on its probability of failure, Table 3 shows the length and the subsequent failures per year.

Line	Length (km)	Failures/year
8-10	100.00	5.00
10-9	50.00	2.50
9-11	70.71	3.54
9-12	111.80	5.59
11-6	111.80	5.59

Table 3. Length and failures per year of all active lines

Figure 3 shows that the line connected to the interconnection point operates at a high load. It is critical to note that if line 8-10 fails, the slack should provide all power, but this would result in exceeding the thermal capacity of the line. Thus, if line 8-10 fails, no power can reach the loads.

In the case of line failures, there is a total disconnection time of 2.5 hours; instead, for transformers it is 8 hours. The expected time that an element will be disconnected in a year is found by multiplying the aforementioned disconnection time by the number of failures that take place during a year. Table 4 displays the yearly disconnection time and explains the consequences spotted by

running the power flow. This will allow to estimate the penalties due disconnection.

Element	Disconnection time (h)	Consequences
Line 8-10	12.50	No load served - divergence
Line 9-10	6.25	No load served - divergence
Line 9-11	8.85	Loads at buses 2, 3 and 5 unserved
Line 9-12	13.98	Load at bus 5 unserved
Line 11-6	13.98	No load served
Trafo 1-8	1.20	No load served - divergence
Trafo 2-9	1.20	Load at bus 2 unserved
Trafo 3-10	1.20	Load at bus 3 unserved
Trafo 4-11	1.20	Load at bus 4 unserved
Trafo 5-12	1.20	Load at bus 5 unserved

Table 4. Disconnection time and consequences of losing each element

Once the unserved loads and the associated disconnection times are known, the next step has to do with applying the penalty as follows:

$$C_{discon} \approx \sum_{i=1}^{10} \bar{P}_{uns,i} t_{discon,i} C_p, \quad (2)$$

where C_{discon} is the total disconnection cost, i represents the index of the line or transformer with a total of 10 elements prone to be disconnected (see Table 4), $\bar{P}_{uns,i}$ is the mean unserved power, $t_{discon,i}$ the disconnection time, and C_p the penalty cost to apply. Equation 2 is an approximation in the sense that the unserved power varies according to the time of the day. To not overcomplicate the problem, it has been decided to pick a representative value such as the average.

The application of Equation 2 yields a total yearly penalty cost of 4.99 M€. For the most part, it is due to the disconnection of lines. Meshing more the system would decrease this cost, but on the other side, it would increase the investment cost. Hence, there is a trade-off between cost and reliability.

All the calculations related to costs have not set an inferior limit to the voltages. However, some of them are likely to be unacceptable in reality. The project will proceed to discuss solutions to this issue in the following phases.

2.2. Problem identification

The network modeled presents some serious issues. First, in case of fault, the demand cannot be covered. The network is a ramified line but does not have any interconnection within the system. If a fault occurs, the two branches are not connected and have to support the demand of the remaining part on its own. In the case of the nuclear power plant, it cannot produce enough energy to fulfill all the demand and in the case of the interconnection, if it was to cover all, it would be overloaded.

This leads to the second problem the network faces, there is a risk of overloading. This may happen in case of fault or if the the nuclear power plant shuts down because there is no other source of generation. This could lead to burning hence security and material damage issue. A third drawback is the high impact of the interruptions. As many line are single lines and there are

no multiple connections, only ramifications, a fault has a high chance to directly disconnect the network. Finally, the voltage cannot be kept constant enough. It is usually accepted to fluctuate 10% around the nominal 1 p.u. while in the current transmission network, the voltage reaches almost 0.8 p.u..

2.3. Solution suggestion

As some of the lines present some overloading and demand coverage problems, we suggest improving lines to better ones which are able to transport more power. In order to do so, the critical lines could be changed from single to double lines and/or even change the conductors to thicker cables which allow a larger amount of power flow. Another approach would be to add more lines to the grid to overcome the demand coverage but we must also be aware that when adding new lines to the system we are also increasing the possibility of line failures which may affect interruptibility and cause economic losses to the system.

On the other hand, adding generation points to the system would also help overcome the stated problems in the previous point. If power is more accessible in different locations, the demand can be fulfilled from various points without saturating the most critical lines while evenly distributing the generation. Finally, another solution could be to change the 220 kV existing lines to 400 kV ones in order to allow these to transport higher amounts of power. With this change, only the amount of power transported would be around three times higher than the current one. However, it has to be taken into account that there would have to be an additional transformer to adapt the 220 kV from the interconnection to 400 kV, and the rest of the transformers would have to be replaced to match nominal voltages.

3. PHASE 2

This chapter considers upgrading the system by means of installing additional lines. In the previous analysis, it was visible that the disconnection of specific lines resulted in an unsolvable problem. Often, no solution was obtained as a result of an exceedingly high demand compared to the available generation. The criteria $N - 1$ was therefore not met, yet it is usually treated as a requirement by control center operators [2], [3].

The central aim of this chapter is reaching a robust grid, where a single failure does not compromise the full system. Several solutions were proposed, such as meshing the network, rising the voltage level, etc. This chapter is devoted to exploring the implications of such proposals. First, a more theoretical explanation describing the formulation is presented, and then, the analysis of results takes place. These results include electrical magnitudes as well as economic data. An optimal configuration is finally provided.

3.1. Addition of lines

Recall that the original system depicted in Figure 1 was for the most part a radial system, in the sense that there was no redundancy in the connection of lines. The operating costs are non-negligible since a significant amount of energy cannot be delivered during faults. To combat this issue, the installation of various new lines (in red) is contemplated, as shown in Figure 4.

By installing new lines, an additional installation cost has to be considered, but a reduction on the operating costs is expected. It is worth mentioning that not all contemplated new lines ought to be installed. Rather, by adding one or two of them, the system could already be operating under the desired conditions. There is a cost-benefit tradeoff, so only a few specific new lines will be selected.

3.1.1. Formulation

The formulation of the topology deserves special attention. Mathematically, it is defined as:

$$\{\mathcal{N} \in \mathcal{P}([n]) \mid |\mathcal{N}| = k\}, \quad (3)$$

where \mathcal{N} denotes a subset, that is, possible topology out of the full set of configurations $\mathcal{P}([n])$, $[n] = \{\mathbf{1}_{\sigma_1}, \mathbf{1}_{\sigma_2}, \dots, \mathbf{1}_{\sigma_n}\}$ represents the set of elements that cause variations on the topology, and k symbolizes the total amount of possibilities. In the contingency analysis, the set $[n]$ is a function of the state of the elements (mainly, lines). These can be in service or out of service, so can be regarded as boolean variables. The employed notation, of the form $\mathbf{1}_{\sigma_i}$, is 1 if the indicator variable σ_i holds true; otherwise, it is 0. The indicator variable, in the case under study, is simply the state of each particular line.

Note that the whole set \mathcal{P} can be further divided into the set composed of the original lines \mathcal{A} , and the set of new lines \mathcal{B} . Let j indicate the number of lines in the original set \mathcal{A} , and $n - j$ the amount of lines in the new set \mathcal{B} . In the particularized case shown in Figure 4, $j = 6$ and $n - j = 8$.

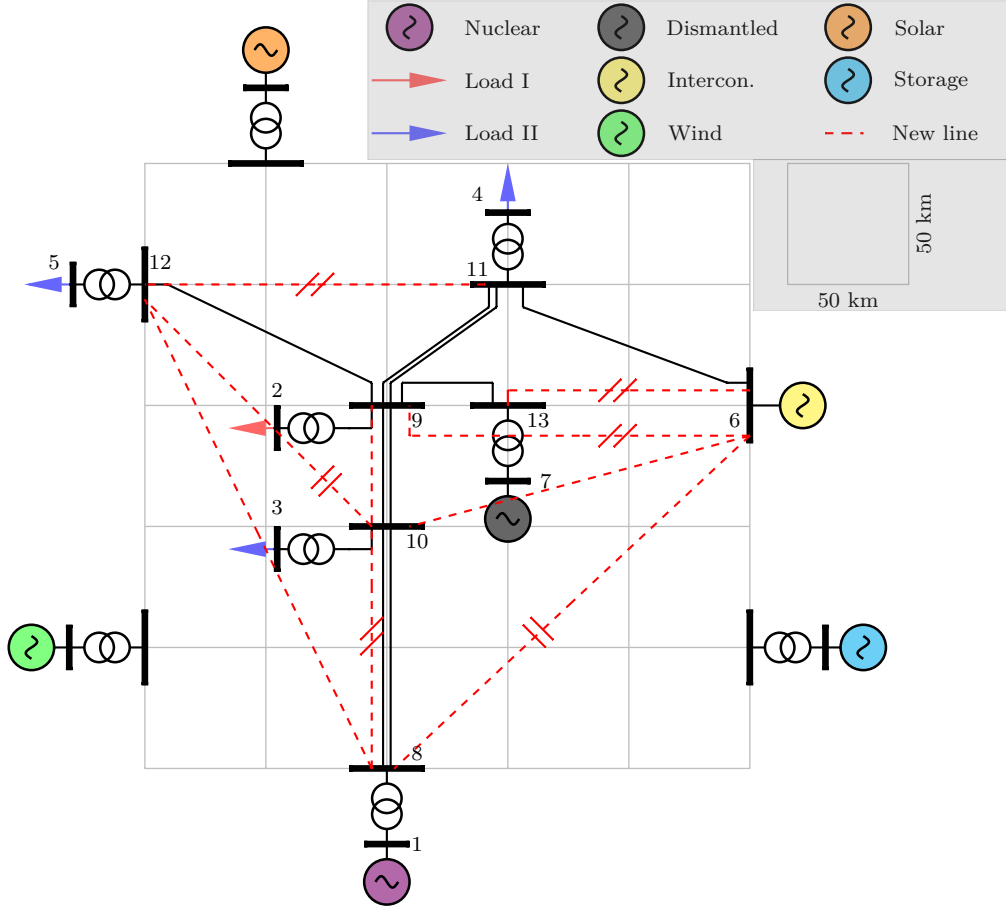


Figure 4. Overview of the network with the addition of lines. Double line if double circuit.

Thus, these subsets are expanded and explicitly become:

$$\begin{cases} \mathcal{A} = \{\mathbf{1}_{\sigma_1}, \mathbf{1}_{\sigma_2}, \dots, \mathbf{1}_{\sigma_j}\}, \\ \mathcal{B} = \{\mathbf{1}_{\sigma_{j+1}}, \mathbf{1}_{\sigma_{j+2}}, \dots, \mathbf{1}_{\sigma_n}\}. \end{cases} \quad (4)$$

To perform the contingency analysis, we consider that one of the original lines is faulted. For instance, if line i ends up disconnected, $\sigma_i \leftarrow \text{false}$ while the rest of original lines $\sigma_r \leftarrow \text{true}$ for $r = \{1, 2, \dots, i-1, i+1, \dots, j\}$.

On the other hand, in the subset \mathcal{B} it is not straightforward to estimate which lines should be connected or disconnected. Perhaps installing a single additional line is enough to meet the $N-1$ criteria, or maybe more lines are required. Hence, it has been decided that all permutations have to be analyzed. Since σ are boolean variables, the total number k of contingencies to simulate are:

$$k = j2^{(n-j)}, \quad (5)$$

so if $j = 6$ and $n - j = 8$, this results in $k = 1536$ different topologies. Thus, a total of 1536 timeseries power flows are computed.

Security analysis in power systems has been traditionally based on the usage of the DC power flow [4], [5]. It offers the advantage of being non-iterative (and consequently, fast), and allows to determine the influence of faults with the usage of transmission factors. However, its solution is

just an approximation. Since the amount of situations remains reasonable, it has been decided to solve them with the typical Newton-Raphson up to the default precision of $1 \cdot 10^{-8}$ MVA [6].

The general procedure to perform the contingency analysis is shown in Algorithm 1.

Algorithm 1: Pseudocode to solve the contingencies

Input: net initialized class, j , n

Output: stored results

```

1 Generate permutations  $\forall \sigma_g$  where  $g = [1, 2, \dots, 2^{(n-j)}]$ 
2 for  $i = [1, 2, \dots, j]$  do
3    $\sigma_i \leftarrow \text{false}$ 
4    $\sigma_r \leftarrow \text{true}$ , where  $r \neq i$  and  $r \leq j$ 
5    $\mathcal{A} \leftarrow \{\mathbf{1}_{\sigma_1}, \mathbf{1}_{\sigma_2}, \dots, \mathbf{1}_{\sigma_j}\}$ 
6   for  $g = [1, 2, \dots, 2^{(n-j)}]$  do
7      $[\sigma_{j+1}, \sigma_{j+2}, \dots, \sigma_n] \leftarrow \sigma_g$ 
8      $\mathcal{B} \leftarrow \{\mathbf{1}_{\sigma_{j+1}}, \mathbf{1}_{\sigma_{j+2}}, \dots, \mathbf{1}_{\sigma_n}\}$ 
9      $\mathcal{N} \leftarrow \mathcal{A} \cup \mathcal{B}$ 
10    pandapower.timeseries.run_timeseries( $\mathcal{N}$ , net)
11    Store results

```

Out of all results extracted, an analysis procedure is required in order to determine which configuration meets the $N - 1$ criteria. The requirements are listed below:

- The losses in the lines have to stay below 2%.
- The voltages have to be between a range of $\pm 10\%$.
- All lines have to remain below 80% its maximum capacity.

Apart from these requirements, an additional criteria has to do with the costs. These will be critical when choosing the best configuration out of all possible ones. Table 5 displays the costs for the lines, depending on their representative voltage level and the number of circuits.

Type	Mean (€)	Min-max range (€)	Median (€)
380-400 kV, 2 circuits	1060919	579771 - 1401585	1023703
380-400 kV, 1 circuits	598231	302664 - 766802	597841
220-225 kV, 2 circuits	407521	354696 - 461664	437263
220-225 kV, 1 circuits	288289	157926 - 298247	218738

Table 5. Network infrastructure costs for the lines. Data from [7].

It has been decided to calculate the costs with mean value.

3.1.2. Results

Out of all results extracted, an analysis procedure is required in order to determine which configuration meets the $N - 1$ criteria. The prechosen configurations are the ones that ensure that in spite of the disconnection of a given element, the power flow remains feasible and the design criterias are met. A total of 39 have satisfied all requirements. Table 6 shows the top 10 cheapest topologies, according to the costs in Table 5.

Identifier	New lines	Infraestructure cost (M€)
19	[6-13, 6-10, 8-9, 10-12]	359.50
214	[6-13, 6-10, 11-12, 8-9]	362.99
77	[6-13, 8-9, 10-12, 9-6]	375.04
49	[6-13, 11-12, 8-9, 9-6]	378.54
80	[6-13, 6-10, 11-12, 8-9, 10-12]	420.63
189	[6-13, 6-10, 8-9, 10-12, 9-6]	420.63
45	[6-13, 6-10, 8-9, 10-12, 8-12]	423.96
70	[6-13, 8-9, 10-12, 9-6]	424.12
157	[6-13, 6-10, 11-12, 8-9, 8-12]	427.46
250	[6-13, 11-12, 8-9, 10-12, 9-6]	436.17

Table 6. Best configurations with the additional lines

The results indicate that the differences in the infraestructure costs are rather minimal. However, installing only four additional lines tends to be the best option. Line 6-13 has been found necessary to ensure a proper operating state of the system under all near-optimal configurations. This makes sense considering that the interconnection usually provides most of the power. Hence, a strong connection to the network is convenient. In fact, the best topology includes two lines connecting the slack bus to the rest of the system are present.

By ensuring that the $N - 1$ criteria is met, we guarantee that all power will be provided independently of which element fails. In reality, this matter may be a bit more complex as two lines could fail simultaneously. Nevertheless, the associated cross-probability is extremely low, and hence, neglected. This implies that no operating costs have to be calculated; it is known beforehand that they will be null as all power is provided for the optimal configuration.

3.2. Rising the voltage level

3.2.1. Description

While installing more lines is a technically feasible strategy, it may not be the most optimal in terms of costs since the voltage level of the grid could be increased. The price to pay for such a change is the replacement of the initial transformers of 25/220 kV and 36/220 kV, for transformers that raise the voltage up to 400 kV (thus, 25/380 kV and 36/380 kV).

In practical terms, raising the voltage may not be as simple as replacing four transformers. For instance, the insulators and the switchgear would have to be changed as well. In the worst scenario, the lines in the towers would have to be more separated, which could cause a replacement of the whole set of supports. To keep the problem arguably simple, it is taken into account that the cost of the transformer station is proportional to the voltage — as can be deduced in [7].

The benefits of increasing the voltage become obvious when observing that the power in a three-phase system such as this one is given by:

$$S = \sqrt{3}V_l I, \quad (6)$$

where V_l identifies the line voltage. With this simple relationship, if it is assumed that S remains constant, and V_l increases by a factor of $380/220 \approx \sqrt{3}$, the current would decrease by approx-

imately a factor of $\sqrt{3}$. This means that the active power losses, which are proportional to the square of the current, are roughly reduced by a factor of 3.

Regarding the costs, representative values in €/km are gathered in Table 7. While there is a certain dependence on the type, a generic substation could be taken as reference. Thus, a cost of 42627 €/kV is chosen as an indicator. It is considered that all elements in the substation would have to be replaced to adapt the new voltage level of 380 kV. If there are four substations to be replaced, the total cost for doing so becomes 64.79 M€.

Type	Mean (€/kV)	Min-max range (€/kV)	Median (€/kV)
All substations	42627	24994 - 55508	36755
All GIS substations	46237	29837 - 56017	37449
AIS with 9+ bays	44008	28838 - 56157	41080
AIS with 5-8 bays	35593	19936 - 37251	29021
AIS with 1-4 bays	33192	20276 - 48319	26628

Table 7. Network infrastructure costs for the substation. Data from [7].

3.2.2. Results

The same amount of contingencies as before are computed. Out of the 1536, this time more permutations have become feasible (52 in total). Of course, raising the voltage has a positive effect in this regard, as previously hypothesized. In any case there is a trade-off situation: while the kilometers of new lines may decrease, there is an additional cost due to the new substations. It has to be assessed if the saving due to raising the voltage outweighs the cost of installing new substations. Table 8 shows such results for the 10 cheapest options, where the cost of the substations are independent on the topology.

Identifier	New lines	Lines (M€)	Transformers (M€)	Total (M€)
163	[6-13, 8-9, 10-12]	313.92	64.79	378.71
133	[6-13, 11-12, 8-9]	317.41	64.79	382.20
235	[6-13, 8-9, 8-12]	320.75	64.79	385.54
30	[6-13, 8-12, 6-8]	346.07	64.79	410.86
19	[6-13, 6-10, 8-9, 10-12]	359.50	64.79	424.29
214	[6-13, 6-10, 11-12, 8-9]	362.99	64.79	427.78
58	[6-13, 6-10, 8-9, 8-12]	366.33	64.79	431.12
77	[6-13, 8-9, 10-12, 9-6]	375.04	64.79	439.83
169	[6-13, 8-9, 10-12, 8-12]	378.38	64.79	443.17
49	[6-13, 11-12, 8-9, 9-6]	378.54	64.79	443.33

Table 8. Economic results of replacing the substations

A similar conclusion as before is reached. A new line that connects the interconnection with the dismantled plant is required to meet the planning requirements and achieve an optimal topology. Notice that thanks to the increase in the voltage level, only three new lines should be installed in the optimal configurations. This allows to reduce the cost of these new lines up to 313.92 M€ in the best scenario. However, the extra cost due to the replacement of the transformers implies that the total cost of 378.71 M€ surpasses the minimum cost indicated in Table 6, which is equal to 359.50 M€.

Therefore, even if both options do not differ much in costs, it would still be better to operate around the nominal voltage of 220 kV. This does not mean, however, that installing more lines is the only feasible solution to confront the technical issues. This may have been true some decades ago, but nowadays, power systems can benefit from the penetration of renewables. Renewable sources of generation can be connected near the loads, which allows to reduce the losses and improve the efficiency of the system. A scenario with renewables is covered in the following chapter.

4. PHASE 3

This chapter covers the inclusion of renewables into the initial grid. It has been verified that the system, as it is configured in a beginning, lacks resiliency. One of its major issues is the presence of only two generation units placed far from the loads. This causes some lines to exceed their loading capacity, while voltages' absolute value may be well below 0.9 p.u.. Adding new lines is a possibility, or rather, a must in order to meet the $N - 1$ criteria. However, it is hypothesized that the performance of the system can still improve with the installation of a wind farm and a PV power plant.

To verify the above-presented hypothesis, the chapter first presents a general overview of the system, along with the sizing of the renewable power plants. Then, the optimal configuration found in the previous chapter is analyzed with the inclusion of renewables to verify the improvement. Finally, a contingency analysis takes place to assess the $N - 1$ criteria.

4.1. Overview

Figure 5 presents the general scheme of the system with the solar and wind plants connected through two parallel lines to nearby buses. Again, new lines that could become suitable for ensuring the robustness of the system are drawn.

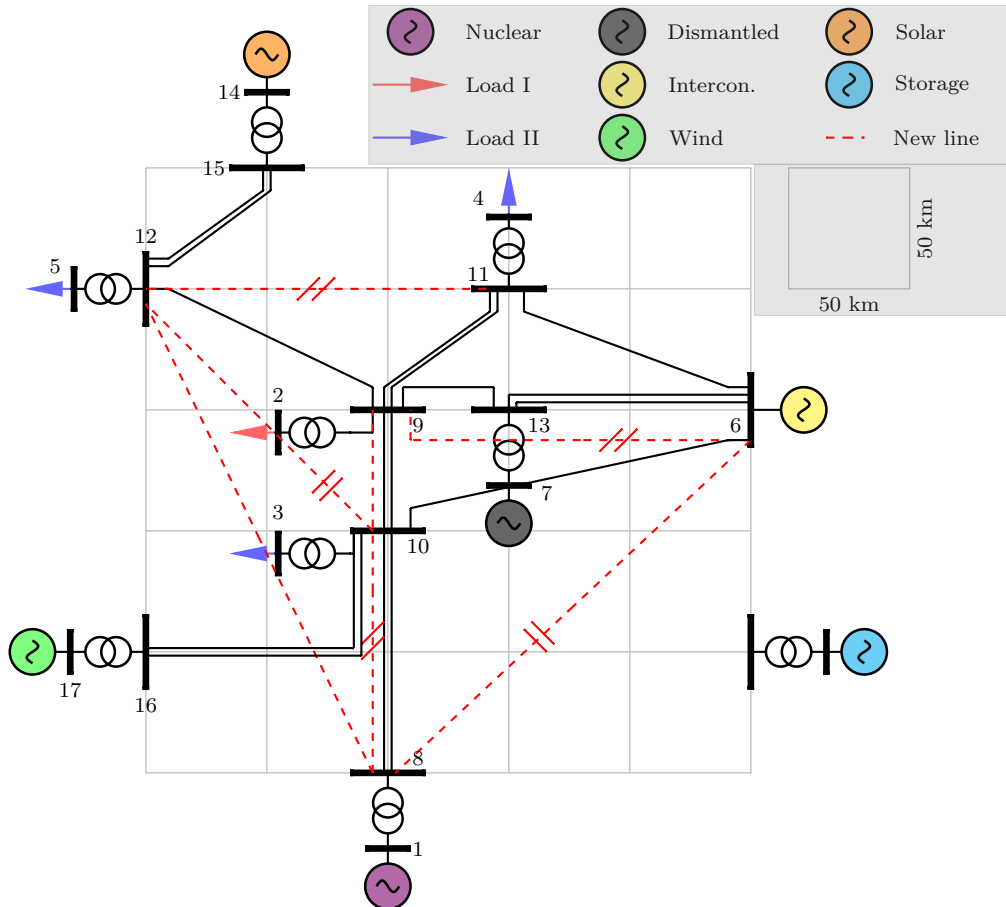


Figure 5. Overview of the network with renewables and the potential addition of lines

The optimal configuration with no renewables, as shown in Table 6, requires the installation of four additional lines: 6-13, 6-10, 8-9, 10-12. The first two are pretty much found in every other topology, as they represent a link with the interconnection. Since the interconnection can theoretically provide any power, it is a good idea to increase the number of associated lines to it. Consequently, lines 6-13 and 6-10 are not considered as potentially attractive new lines, but as already connected lines.

4.2. Renewable's integration

In this project, the integration of renewables takes place in the form of solar and wind. The characteristics of each one are particularly detailed. The goal is to characterize their hourly variation of power in relation to the availability of the natural resources. Despite the partial unpredictability that renewables suffer, a representative day in terms of solar irradiance and wind speed has been selected.

4.2.1. Solar PV

First, the PV panels cover an area of 60 ha. This, and some other relevant information is captured in Table 9.

Magnitude	Value	Units
Location	(40.8N; 0.48E)	-
Total area	60	ha
System efficiency	20.7	%
Cell type	Monocrystalline	-
Panel peak power	405	Wp
Panel area	1.95	m ²
Open circuit voltage	37.23	V
Short circuit current	13.87	A

Table 9. Technical characteristics of the PV plant with its panels 405W Deep Blue 3.0 JA Solar Mono [8]

The location has a certain importance to determine the incident irradiation, which is extracted from PVGIS' database [9]. In reality, the of the solar power plant would be located in Tortosa, Catalunya, Spain, according to the given coordinates. The chosen PV panels are of monocrystalline type. Monocrystalline cells generally offer larger efficiencies than polycrystalline cells [10], and although they become more expensive, no cost limitations have been set.

Let n_p denote the total number of panels, G the irradiance, η the efficiency and S_p the area of a single panel. Then, the total generated power follows:

$$P_{PV} = n_p G \eta S_p. \quad (7)$$

It has to be noted that the irradiance G is varying along the day, and it generally has a peak around noon. The data have been selected for the 15th of February. There are a total of $n_p = 63692$ panels as it has been assumed that the 60 ha surface is the useful one. Figure 6 shows the hourly irradiance and power of the PV plant. Clearly, they are proportional, just like it has been already shown in Equation 7.

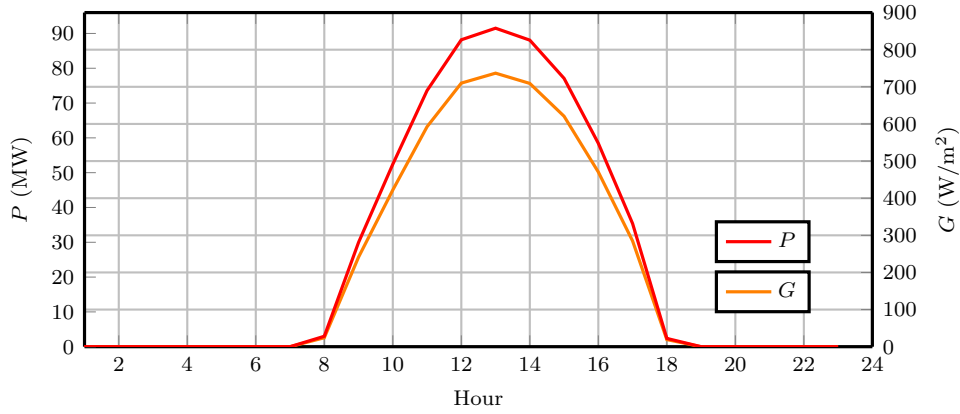


Figure 6. Irradiance and power from the PV plant along a representative day. Data from [9].

The peak in power takes place at hour 13, more or less as expected, and the curves follow a profile that resembles a Gaussian bell. The maximum power generated by the PV plant is 91.5 MW. Although this is a respectable amount, it is roughly one tenth of the load peak. As a consequence, results are not expected to change significantly. Most likely we will observe slight improvements.

4.2.2. Wind

On the other hand, wind power is proposed as the second renewable alternative. The chosen wind turbines are the Siemens-Gamesa G132-5.0MW. They are rather voluminous turbines, with a rotor diameter of 132 m. Table 10 shows their most notorious technical characteristics.

Magnitude	Value	Units
Location	(42.28N; 3.16E)	-
Total area	80	ha
Nominal power	5.0	MW
Cut-in wind speed	1.5	m/s
Rated wind speed	13.0	m/s
Cut-out wind speed	27.0	m/s
Swept area	13685	m ²

Table 10. Technical characteristics of the wind power plant with its turbines Gamesa G132-5.0MW [11]

The power provided by a wind turbine is given by:

$$P_{wt} = \frac{1}{2} \rho A C_p v^3, \quad (8)$$

where ρ is the air density of approximately 1.225 kg/m³, A stands for the swept area, C_p is the power coefficient limited to 16/27 (known as Betz's limit [12]), and v represents the wind speed. If the power P_{wt} exceeds the nominal power of the turbine, some power will be curtailed so as not to surpass the machine's ratings. In normal operation, the power coefficient is likely to take values around 0.4.

The available area to install the wind turbines is 80 ha. Nonetheless, wind turbines have to be generously separated one from the others. It has been decided that wind turbines should be separated by a minimum of 5 diameters. Similar separations are adopted in the literature [13]. Thus, a total of two wind turbines are installed. The nominal power of the wind farm becomes

10 MW, which is significantly lower than PV. Despite that, this should not come as a surprise since wind power has a relatively low power density [14].

With this, Figure 7 shows the evolution of the wind speed and the total generated power by the wind farm in an orientative day.

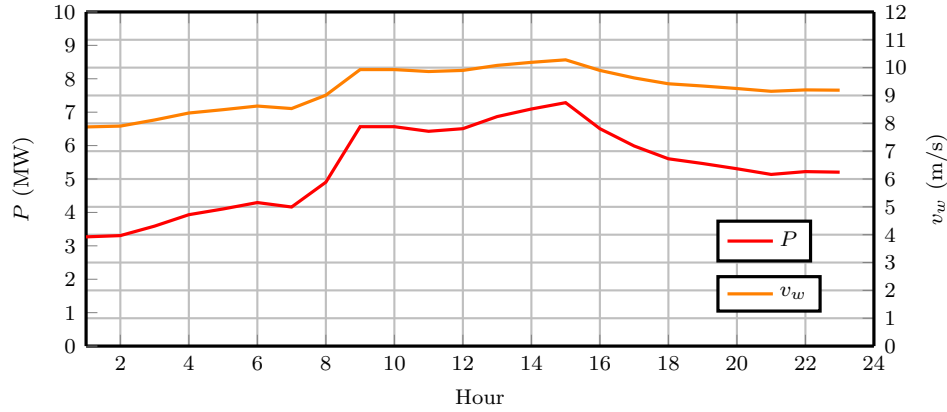


Figure 7. Wind speed and output power from the wind farm. Data from [15].

Notice the cubic relationship between the wind speed and the power. Small increases in wind speed provoke large variations in the output power.

4.3. Base case analysis

This base case analysis refers to the assessment of the influence the installation of renewables has on the results. It is compared to the system analyzed before with lines 6-10 and 6-13 permanently added. The goal is not to deduce if the grid meets the $N - 1$ criteria (most likely some other lines would have to be added), but rather compare if the voltages, the loadings of the lines and the losses suffer a certain improvement.

To perform the comparison, the most extreme values have been gathered. They are shown in Table 11 for both cases (with and without renewables).

Attributes	Without renewables	With renewables
V_{min} (p.u.)	0.962	0.968
V_{max} (p.u.)	1.050	1.050
Max. load (%)	41.65	40.76
Max. losses (MW)	14.54	14.43
Correct operation?	Yes	Yes

Table 11. Main results to compare between the grid with and without renewables

The results suggest that generally speaking there is little difference in installing or not renewables. The inclusion of the wind farm and the PV power plant cause the minimum voltage to rise a bit, the maximum loading of the lines to decrease about 1% (although without contingencies it is already low) and the maximum power losses experience a tiny reduction. In the two scenarios, the maximum voltage remains 1.05, which indicates there are no overvoltages. Since all magnitudes are inside the allowed limits, the system is operating correctly in both cases.

Adding renewables to the system comes at a cost. First, there has to be an investment of capital for deploying the wind turbines and the PV panels, apart from power electronics equipment and ancilliary components. Then, a couple of new power lines are added to interconnect them to the system. The slight improvement on the electrical magnitudes will most probably fail at justifying this investment.

However, it is important to note that the major advantage of installing renewables is in its environmental impact. If the power from the interconnection is assumed to come from coal and gas power plants, then installing renewables could become a sensible option. This is specially true when taking into account the actual costs of carbon emissions. Currently at 81.65 €/tonne, they have increased by a factor of 3 during the last year [16].

4.4. Contingency analysis

A different story would be the operation with contingencies. Here it is valuable to find out if the presence of distributed renewable generators can help at having to install less extra lines. Hence, the cost could be reduced.

The contingency analysis has been performed similarly to the ones in Tables 6, 8. We take a set of lines that can be potentially installed, and a set of initially powered lines. Contingencies are caused in this latter set to study which new lines have to be connected to meet the requirements. Then, the topologies that ensure the correct operation of the system in spite of which line fails, are selected and their associated costs are calculated. The top 10 most convenient configurations are presented in Table 12.

Identifier	New lines	Infraestructure cost (M€)
24	[8-9, 10-12]	402.71
12	[8-9, 9-6]	406.21
46	[11-12, 8-9]	406.21
8	[8-9, 8-12]	409.54
0	[11-12, 8-9, 10-12]	463.84
4	[8-9, 10-12, 9-6]	463.84
37	[11-12, 10-12, 9-6]	463.84
63	[8-9, 10-12, 8-12]	467.18
20	[11-12, 8-9, 9-6]	467.34
38	[11-12, 8-9, 8-12]	470.67

Table 12. Best configurations with the additional lines

Again, the optimal configuration is the one where apart from lines 6-10 and 6-13, lines 8-9 and 10-12 are added. This coincides with the conclusion we reached in Table 6. Nevertheless, the costs are now higher due to the addition of two new lines to connect the wind and the solar power plants to the system as such. Introducing renewables is not enough to avoid installing the same lines.

In case lines 8-9 and 10-12 are added, the operational costs would be practically zero because we would be meeting the $N - 1$ criteria. To summarize, installing renewables implies an additional cost for the system operator. With time, this could be compensated with the savings in carbon emissions.

tensively promoted. Apart from the direct impact on decarbonizing mobility, they can act as a source/sink of energy, which also has an appealing influence on power systems [18]. One of the largest barriers towards adopting batteries has to do with its high investment cost. Although the cost of batteries has been steadily declining for the last two decades [19], there is still a long way to go. Part of the intention regarding this section is to analyze if storage exerts a positive effect on the power flow of the power system under study.

Energy storage options can take many forms. For instance, fast-response devices such as super-capacitors provide peaks of power, yet their accumulated energy is rather low. The same characteristics apply to flywheels, although they store the energy mechanically, not electrically. Another option, likely the most favorable one, are batteries. They store the energy chemically, can provide energy for a sustained period of time, and tend to be easily controlled with power converters. This project conceives the storage unit as a lithium-ion battery, since it offers an attractive trade-off between lifetime, power and energy density, and flexibility of operation, despite its high cost.

Table 13 shows the most notorious characteristics of the chosen lithium-ion battery, along with the corresponding converter.

Magnitude	Units	Value
Capacity	MWh	50
Peak power	MW	10
Round-trip battery η	%	92
Maximum DOD	%	80
Converter η	%	96
Lifetime	cycles	3000
Working temperature	°C	-20/55
Specific energy	Wh/kg	133
Orientative LCOE	€/kWh	0.11/0.66

Table 13. Storage system characteristics. DOD: depth of discharge, LCOE: levelized cost of energy. Data from [20]–[22].

Having a lifetime of 3000 cycles means that it is not appropriate to charge and discharge the battery several times per day. If that were to be the case, the energy storage system would last for just a few years at most. On the contrary, if the battery is charged and discharged once per decade, its lifetime could approach a decade. For this reason, the proposed power profile to follow is represented in Figure 9.

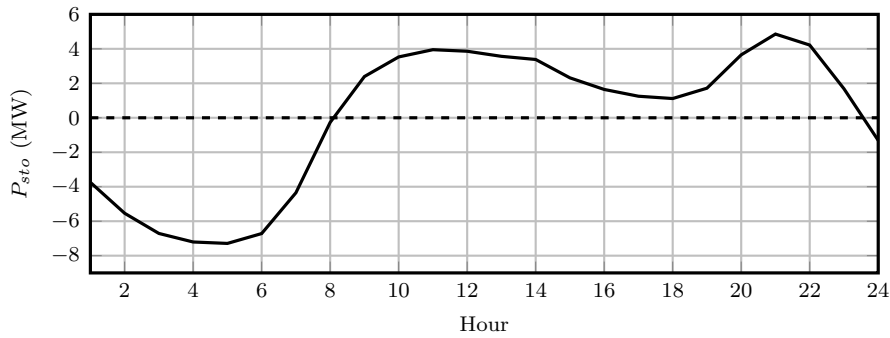


Figure 9. Daily charge and discharge profile for the battery system

This profile resembles the power demand of the loads. This dependence has been established intentionally. In previous analysis, it has been found that during peak hours (around 20:00 hours) the loading of lines is most extreme, and also, the voltages are closer to the lower limit of 0.9 p.u.. Therefore, in general terms, the battery should be discharged during the day and charged at night. According to the chosen sign criteria, positive powers indicate generation, while negative powers denote consumption.

Since the daily demand profile amongst consecutive days do not experience significant differences, it is convenient to always start and finish the day with the same state of charge (*SOC*). To achieve this, the accumulated area under the curve (in Figure 9, between the solid line and the dashed line) is kept at $E \cdot DOD = 40$ MWh. Besides, the sum of the positive and the negative area yields zero, as desired.

5.2. Dismantled plant

Another possibility to contemplate in order to reduce the dependence on the interconnection consists of employing the once dismantled power plant placed in bus 7 as indicated in Figure 8. The hypothesis is that this dismantled plant is powered by some kind of fossil fuel: coal, diesel, gas, etc. Thus, even if it could have a positive impact on the electrical magnitudes, its associated environmental impact has to be kept in check.

We start by exploring the diverse energy sources that could power it to extract conclusions regarding costs, emissions, and geopolitical aspects:

- Coal: it is the most polluting of the aforementioned fuels. Even though its emission factor largely depends on the type of coal (lignite, bituminous...), it is in the range of 300 to 360 g CO₂/kWh [23]. Coal power plants are mostly used in countries with availability of natural resources, which is not the case of Spain.
- Diesel: or more generally petroleum, these power plants are more a rarity than an actual common choice. They are suitable to be installed in microgrids or islanded systems thanks to their flexibility and suitability for hybrid systems where they act as backup units [24]. Since their chemical proportion between hydrogen and carbon is larger than in the case of coal, its emission factor becomes lower; it is around 270 g CO₂/kWh [23].
- Natural gas: the cleaner of the three options, with an emission factor of 180 g CO₂/kWh approximately [23]. Power plants powered by natural gas usually take the form of the so-called combined cycle gas turbine (CCGT) power plant. During the previous decades, Spain promoted the installation of combined cycle power plants, which nowadays are unused for the most part [25]. Probably the largest disadvantage of these power plants is the high cost of natural gas, which has fluctuated extensively during the last year [26].

When it comes to the implementation of the program, it makes no difference to consider one technology or another, as only the output power is relevant. However, this chapter also focuses on the emissions. Therefore, the results section analyzes the results for coal, diesel and natural gas.

The chosen power generation profile for the dismantled plant is depicted in Figure 10. Compared to storage or the demand, here the peaks are more exaggerated. The underlying idea is that the system is more in need of generation during peak hours. And if demand increases, generation should increase by preferably by a larger factor to keep the losses and loadings of the lines at satisfactory values. A peak power of 50 MW has been considered, which corresponds to the most critical hour of the day. The plant is supposed to stop operating at night, and its voltage is maintained at 1.02 p.u. since it acts as a PV node.

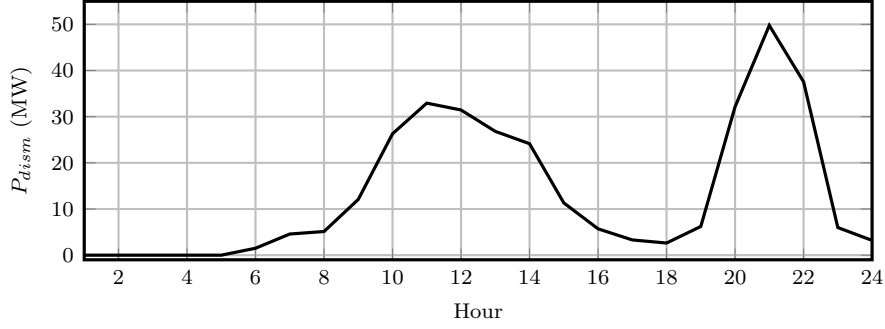


Figure 10. Daily generation profile of the dismantled plant

With storage and the generation of the dismantled plant defined, the simulation can be ran again. The next sections explore the results and draw conclusions from them.

5.3. Base case results

The base case considers the grid as shown in Figure 8, with the black lines representing actual connections. The red lines are only taken into account for the contingency analysis. In any case, it is expected that the presence of the battery and an additional plant should contribute to improving the electrical magnitudes, at least slightly. Table 11 shows this is precisely the case.

Attributes	Phase 2	Phase 3	Phase 4
V_{min} (p.u.)	0.962	0.968	0.971
V_{max} (p.u.)	1.050	1.050	1.050
Max. load (%)	41.65	40.76	39.63
Max. losses (MW)	14.54	14.43	13.89
Correct operation?	Yes	Yes	Yes

Table 14. Main results to compare between the grid without renewables, with renewables, and with storage and the dismantled plant

The results tend to be the ones we could already expect. The minimum voltage rises a bit thanks to the inclusion of more generation sources, which control the voltages at their respective buses and hence ensure the operation around nominal voltages. Similarly, the loadings of the lines are reduced a bit, being the most loaded line at only 39.63%. There could be reasons to think that the system is oversized, because lines do not approach their limits of 80%. While these claims would be full of validity, faults have to be taken into account as well. Redundant connections are a must if the criteria $N - 1$ has to be met.

The maximum losses are again reduced. A clear pattern can be spotted from comparing the results

in the three phases. Going from phase 2 to phase 4, results improve each time the grid becomes stronger and more decentralized. These are in essence some of the core characteristics of smart grids. Another central goal of smart grids has to do with decarbonizing the system, which is described below.

Regarding emissions, it is known beforehand that storage, renewables and nuclear do not emit CO₂ gases or equivalent during their operation. The only generation sources to account for emissions are the interconnection and the dismantled plant. In this base case, the dismantled plant produced 332 MWh, whereas the interconnection provided 4686 MWh. The interconnection can be assumed to have an emission factor of 190 kg CO₂-eq/MWh as in the case of Spain [27], [28].

With this, the total emissions for a full-day operation are gathered in Table 15 depending on the technology of the dismantled power plant.

Fuel	Dismantled	Interconnection	Total
	(tCO ₂ -eq)	(tCO ₂ -eq)	(tCO ₂ -eq)
Coal	108.56	890.34	998.90
Diesel	89.64	890.34	979.98
Gas	59.76	890.34	950.10

Table 15. Total daily emissions depending on the scenario

The conclusion we reach is that even if there is a non-negligible difference in the emissions caused by the dismantled plant, its overall influence is not that relevant. The interconnection accounts for 90 to 95% of the total CO₂ emissions. The only fix to that is the integration of nuclear and renewable power plants, which produce about 10.06 GWh daily. This is about twice the energy imported from the slack bus, so in proportion, about 2/3 of the total energy come from clean sources. This is equivalent to saying that the electricity emissions factor of the whole system is roughly 63 kg CO₂-eq/MWh. This is a more than acceptable value that most European countries do not reach (see [29]).

5.4. Contingency analysis

Just as in previous phases, a contingency analysis is performed to verify if new lines are required, and if so, which ones should be. The marked red lines shown in Figure 8 are the potentially added lines, while the black ones are the already established ones. Table 16 presents the top 10 best configurations under faults.

The results indicate that, contrary to previous configurations, installing only the additional line from buses 8 to 9 is enough to meet the $N - 1$ criteria. This is certainly a positive result, because in all other cases, at least two lines had to be added. Notice, however, that most configurations are the same as in Table 12. This makes sense since the topology is basically identical, with just minor variations due to the having added storage and the dismantled plant.

The total installation cost increases a bit respect to the case where only renewables were added. Of course, new lines have been included to connect the storage unit to the system. Yet, the conclusion has not changed. Moving towards a smart grid, which includes a larger penetration of renewables,

Identifier	New lines	Infraestructure cost (M€)
33	[8-9]	419.49
24	[8-9, 10-12]	477.12
12	[8-9, 9-6]	480.62
46	[11-12, 8-9]	480.62
8	[8-9, 8-12]	483.96
57	[8-9, 6-8]	505.94
0	[8-9, 10-12]	538.25
4	[8-9, 10-12, 9-6]	538.25
37	[11-12, 10-12, 8-12]	538.25
63	[8-9, 10-12, 8-12]	541.59

Table 16. Best configurations with the additional lines with storage and a dismantled plant

batteries, and other elements, supposes a large investment cost. The question is if this investment ends up being worth it. Multiple reasons could be added into the equation, but what is for sure is that there is a climate emergency to combat.

6. CODE

```

1 import pandapower as pp
2 import pandas as pd
3 import numpy as np
4 import pandapower.control as control
5 import pandapower.networks as nw
6 import pandapower.timeseries as timeseries
7 from pandapower.timeseries.data_sources.frame_data import DFData
8 from pandapower.plotting import simple_plot
9
10 from line_param_calc import calc_line
11
12
13
14 pd.set_option('display.max_rows', 500)
15 pd.set_option('display.max_columns', 500)
16 pd.set_option('display.width', 1000)
17
18 def initialize_net(path_bus, path_geodata, path_line, path_demand, path_busload, path_generation
    , path_busgen, path_trafo):
19     """
20     initialize the grid from the .csv files
21
22     :param path_bus: path to the bus .csv file
23     :param geodata: path to the geodata .csv file
24     :param path_line: path to the line .csv file
25     :param path_demand: path to the normalized demand .csv file
26     :param busload: path to the bus-load look up table .csv file
27     :param path_generation: path to the normalized generation .csv file
28     :param busgen: path to the bus-generator look up table .csv file
29     :param trafo: path to the trafo .csv file
30     :return: the net class
31     """
32
33     def create_bus(path_bus, path_geodata):
34         """
35         adapts the data from the bus file (if needed)
36
37         :param path_bus:
38         :param path_geodata:
39         :return: the net with the buses added
40         """
41
42         df_bus = pd.read_csv(path_bus)
43         df_geodata = pd.read_csv(path_geodata)
44
45         net.bus = df_bus
46
47         # adapt geodata
48         for ll in range(len(df_geodata)):
49             indx_bus = pp.get_element_index(net, "bus", df_geodata['name'][ll])
50             df_geodata['name'][ll] = indx_bus
51
52         net.bus_geodata = df_geodata
53
54         return net
55
56
57     def create_line(path_line):
58         """
59         adapts the data from the line file
60
61         :param path_line:
62         :return: the net with the lines added
63         """
64
65         df_line = pd.read_csv(path_line)

```

```

66     for _, line in df_line.iterrows():
67         from_bus = pp.get_element_index(net, "bus", line.from_bus)
68         to_bus = pp.get_element_index(net, "bus", line.to_bus)
69
70         rr, xx, cc, imax = calc_line(line.a,
71                                     line.b,
72                                     line.c,
73                                     line.d,
74                                     line.e,
75                                     line.max_i,
76                                     int(line.parallel))
77
78         pp.create_line_from_parameters(net,
79                                       from_bus,
80                                       to_bus,
81                                       length_km=line.length,
82                                       r_ohm_per_km=rr,
83                                       x_ohm_per_km=xx,
84                                       c_nf_per_km=cc,
85                                       max_i_ka=imax,
86                                       name=line.name_l,
87                                       parallel=line.parallel)
88
89     return net
90
91
92 def create_load(path_demand, path_busload, path_bus):
93     """
94     adapts the load files
95
96     :param path_demand:
97     :param path_busload:
98     :param path_bus:
99     :return: the net with the loads added
100    """
101
102    df_demand = pd.read_csv(path_demand)
103    df_busload = pd.read_csv(path_busload)
104    df_bus = pd.read_csv(path_bus)
105
106    # create basic load dataframe
107    # find the bus index of each load
108    load_indx = []
109    for _, load in df_busload.iterrows():
110        bus_load = pp.get_element_index(net, "bus", load.bus)
111        load_indx.append(bus_load)
112
113    load_indx = pd.DataFrame(load_indx)
114    load_indx = load_indx.rename(columns={0: "bus"})
115
116    # load name and peak power
117    load_name = df_busload['bus']
118    load_pmw = df_busload['p_mw']
119    load_qmvar = df_busload['q_mvar']
120
121    # merge in a full dataframe
122    headers = ["name", "bus", "p_mw", "q_mvar"]
123    df_load = pd.concat([load_name, load_indx, load_pmw, load_qmvar], axis=1)
124    df_load.columns.values[0] = "name"
125
126    # create time series from the basic load df
127    Nt = len(df_demand)
128    Nl = len(df_load)
129    pmw_ts = np.zeros((Nt, Nl), dtype=float)
130    qmvar_ts = np.zeros((Nt, Nl), dtype=float)
131    for i in range(Nt): # number of time periods
132        pmw_ts[i,:] = df_load['p_mw'][:,i] * df_demand['norm'][i]

```

```

133         qmvar_ts[i,:] = df_load['q_mvar'][:] * df_demand['norm'][i]
134
135     # form loads as a static picture (initial time)
136     for ll in range(len(df_busload)):
137         pp.create_load(net, bus=load_indx['bus'][ll], p_mw=pmw_ts[0, ll], q_mvar=qmvar_ts[0,
138         ll], name=load_name[ll], index=int(ll))
139
140     # timeseries
141     df_pload_ts = pd.DataFrame(pmw_ts, index=list(range(Nt)), columns=net.load.index)
142     df_qload_ts = pd.DataFrame(qmvar_ts, index=list(range(Nt)), columns=net.load.index)
143     ds_pload_ts = DFData(df_pload_ts)
144     ds_qload_ts = DFData(df_qload_ts)
145     const_load = control.ConstControl(net, element='load', element_index=net.load.index,
146     variable='p_mw', data_source=ds_pload_ts, profile_name=net.load.index)
147     const_load = control.ConstControl(net, element='load', element_index=net.load.index,
148     variable='q_mvar', data_source=ds_qload_ts, profile_name=net.load.index) # add the
149     reactive like this?
150
151     return net
152
153 def create_generator(path_generation, path_busgen, path_bus):
154     """
155     adapts the generation files
156
157     :param path_generation:
158     :param path_busgenerator:
159     :param path_bus:
160     :return: the net with the generators added
161     """
162
163     df_generation = pd.read_csv(path_generation)
164     df_busgen = pd.read_csv(path_busgen)
165     df_bus = pd.read_csv(path_bus)
166
167     # create basic generator dataframe
168     # find the bus index of each gen
169     gen_indx = []
170     for _, gen in df_busgen.iterrows():
171         bus_gen = pp.get_element_index(net, "bus", gen.bus)
172         gen_indx.append(bus_gen)
173
174     gen_indx = pd.DataFrame(gen_indx)
175     gen_indx = gen_indx.rename(columns={0: "bus"})
176
177     # load name and peak power
178     gen_name = df_busgen['bus']
179     gen_pmw = df_busgen['p_mw']
180     gen_vpu = df_busgen['vm_pu']
181
182     # merge in a full dataframe
183     headers = ["name", "bus", "p_mw", "vm_pu"]
184     df_gen = pd.concat([gen_name, gen_indx, gen_pmw, gen_vpu], axis=1)
185     df_gen.columns.values[0] = "name"
186
187     # create time series from the basic load df
188     Nt = len(df_generation)
189     Ng = len(df_gen)
190     pmw_ts = np.zeros((Nt, Ng), dtype=float)
191     for i in range(Nt): # number of time periods
192         pmw_ts[i,:] = df_gen['p_mw'][:] * df_generation['norm'][i]
193
194     # gen structure for 1 t
195     for ll in range(len(df_busgen)):
196         pp.create_gen(net, bus=gen_indx['bus'][ll], p_mw=pmw_ts[0, ll], vm_pu=gen_vpu[ll],
197         name=gen_name[ll], index=int(ll))

```

```

195
196     # timeseries
197     df_gen_ts = pd.DataFrame(pmw_ts, index=list(range(Nt)), columns=net.gen.index)
198     ds_gen_ts = DFData(df_gen_ts)
199     const_gen = control.ConstControl(net, element='gen', element_index=net.gen.index,
200     variable='p_mw', data_source=ds_gen_ts, profile_name=net.gen.index)
201
202     return net
203
204 def create_intercon(path_bus):
205     """
206     defines the interconnection (slack bus)
207
208     :param path_bus:
209     :return: the net with the interconnection added
210     """
211
212     df_bus = pd.read_csv(path_bus)
213
214     # find the slack index
215     slack_indx = 0
216     for ll in range(len(df_bus)):
217         # slack_indx = pp.get_element_index(net, "bus", bb.name)
218         if df_bus['name'][ll] == 'intercon':
219             slack_indx = pp.get_element_index(net, "bus", df_bus['name'][ll])
220
221     pp.create_ext_grid(net, slack_indx, vm_pu=1.0, va_degree=0)
222
223     return net
224
225
226 def create_trafo(path_trafo):
227     """
228     defines the transformers
229
230     :param path_trafo:
231     :return: the net with the transformers added
232     """
233
234     df_trafo = pd.read_csv(path_trafo)
235
236     # for trafo in df_trafo:
237     for _, trafo in df_trafo.iterrows():
238         hv_bus = pp.get_element_index(net, "bus", trafo.hv_bus)
239         lv_bus = pp.get_element_index(net, "bus", trafo.lv_bus)
240
241         pp.create_transformer_from_parameters(net,
242                                             hv_bus,
243                                             lv_bus,
244                                             trafo.sn_mva,
245                                             trafo.vn_hv_kv,
246                                             trafo.vn_lv_kv,
247                                             trafo.vkr_percent,
248                                             trafo.vk_percent,
249                                             trafo.pfe_kw,
250                                             trafo.i0_percent)
251
252     return net
253
254
255
256
257
258
259 # create empty network
260 net = pp.create_empty_network()

```

```

261
262     # buses
263     net = create_bus(path_bus, path_geodata)
264
265     # lines
266     net = create_line(path_line)
267
268     # loads
269     net = create_load(path_demand, path_busload, path_bus)
270
271     # gens
272     net = create_generator(path_generation, path_busgen, path_bus)
273
274     # interconnection
275     net = create_intercon(path_bus)
276
277     # trafos
278     net = create_trafo(path_trafo)
279
280
281
282     return net
283
284
285 if __name__ == "__main__":
286     # load paths
287     path_bus = 'Datafiles/bus1.csv'
288     path_geodata = 'Datafiles/geodata1.csv'
289     path_line = 'Datafiles/line1.csv'
290     path_demand = 'Datafiles/demand1.csv'
291     path_busload = 'Datafiles/bus_load1.csv'
292     path_generation = 'Datafiles/generation1.csv'
293     path_busgen = 'Datafiles/bus_gen1.csv'
294     path_trafo = 'Datafiles/trafo1.csv'
295
296     # define net
297     net = initialize_net(path_bus, path_geodata, path_line, path_demand, path_busload,
298                          path_generation, path_busgen, path_trafo)
299
300     # run timeseries
301     ow = timeseries.OutputWriter(net, output_path="./Results/", output_file_type=".xlsx")
302     ow.log_variable('res_bus', 'vm_pu')
303     ow.log_variable('res_line', 'loading_percent')
304     timeseries.run_timeseries(net)
305
306     # run diagnostic
307     # pp.diagnostic(net)
308     print(net.bus)
309
310     # plot
311     # pp.plotting.simple_plot(net)
312     # simple_plot(net)

```

Listing 6.1. Main code in Python with the Pandapower library

```

1 import numpy as np
2
3 def calc_line(a, b, c, d, e, immax, npar, RCA, Dext, kgg):
4     """
5     calculate r, x, c, and return also Imax
6
7     :param a: horizontal distance between A1 and C2
8     :param b: horizontal distance between B1 and B2
9     :param c: horizontal distance between C1 and A2
10    :param d: vertical distance between A1 and B1
11    :param e: vertical distance between B1 and C1
12    :param immax: max current in A

```

```

13 :param npar: number of parallel lines (1 or 2)
14 :param Rca: ac resistance in ohm/km
15 :param Dext: external diameter in mm
16 :param kg: factor of roughly 0.8
17 :return: r, x, c, imax
18 """
19
20 def single_line(a, b, immax, Rca, Dext, kgg):
21     """
22     calculate the R, X, C parameters, also return Imax
23
24     :param a: horizontal distance between A and C
25     :param b: vertical distance between A and B
26     :param immax: max current in A
27     :param Rca: ac resistance in ohm/km
28     :param Dext: external diameter in mm
29     :param kg: factor of roughly 0.8
30
31     :return: R, X, C, Imax, in the units desired by pandapower
32     """
33
34     # cardinal: https://www.elandcables.com/media/38193/acsr-astm-b-aluminium-conductor-steel-reinforced.pdf
35     # 54 Al + 7 St, Imax = 888.98 A
36
37     w = 2 * np.pi * 50 # rad / s
38     Imax = immax * 1e-3 # kA
39     # Stot = 547.3 * 1e-6 # m2, the total section
40     # R_ac_75 = 0.07316 * 1e-3 # ohm / m
41     # kg = 0.809 # from the slides in a 54 + 7
42
43     R_ac_75 = Rca * 1e-3 # ohm / m, should we correct by temperatures?
44     Stot = np.pi * Dext ** 2 / 4 * 1e-6 # m2, the total section
45     kg = kgg
46
47     r = np.sqrt(Stot / np.pi) # considering the total section
48
49     dab = np.sqrt((a / 2) ** 2 + b ** 2)
50     dbc = np.sqrt((a / 2) ** 2 + b ** 2)
51     dca = a
52
53     GMD = (dab * dbc * dca) ** (1 / 3)
54     GMR = kg * r
55     RMG = r
56
57     L = 4 * np.pi * 1e-7 / (2 * np.pi) * np.log(GMD / GMR) # H / m
58
59     C = 2 * np.pi * 1e-9 / (36 * np.pi) / np.log(GMD / RMG) # F / m
60
61     # in the units pandapower wants
62     R_km = R_ac_75 * 1e3 # ohm / km
63     X_km = L * w * 1e3 # ohm / km
64     C_km = C * 1e9 * 1e3 # nF / km
65
66     return R_km, X_km, C_km, Imax
67
68
69 def double_line(a, b, c, d, e, immax, Rca, Dext, kgg):
70     """
71     calculate the R, X, C parameters, also return Imax
72
73     :param a: horizontal distance between A1 and C2
74     :param b: horizontal distance between B1 and B2
75     :param c: horizontal distance between C1 and A2
76     :param d: vertical distance between A1 and B1
77     :param e: vertical distance between B1 and C1
78     :param immax: max current in A

```



```

79     :param Rca: ac resistance in ohm/km
80     :param Dext: external diameter in mm
81     :param kgg: factor of roughly 0.8
82     :return: R, X, C, Imax, in the units desired by pandapower
83     """
84
85     # cardinal: https://www.elandcables.com/media/38193/acsr-astm-b-aluminium-conductor-steel-reinforced.pdf
86     # 54 Al + 7 St, Imax = 888.98 A
87
88     w = 2 * np.pi * 50 # rad / s
89     Imax = immax * 1e-3 * 2 # kA, for the full line, x2
90     # Stot = 547.3 * 1e-6 # m2, the total section
91     # Rac_75 = 0.07316 * 1e-3 # ohm / m
92     # kg = 0.809 # from the slides in a 54 + 7
93
94     Rac_75 = Rca * 1e-3 # ohm / m, should we correct by temperatures?
95     Stot = np.pi * Dext ** 2 / 4 * 1e-6 # m2, the total section
96     kg = kgg
97
98
99
100    r = np.sqrt(Stot / np.pi) # considering the total section
101
102    da1b1 = np.sqrt((b / 2 - a / 2) ** 2 + d ** 2)
103    da1b2 = np.sqrt((a / 2 + b / 2) ** 2 + d ** 2)
104    da2b1 = np.sqrt((c / 2 + b / 2) ** 2 + e ** 2)
105    da2b2 = np.sqrt((b / 2 - c / 2) ** 2 + e ** 2)
106
107    db1c1 = np.sqrt((b / 2 - c / 2) ** 2 + e ** 2)
108    db1c2 = np.sqrt((b / 2 + a / 2) ** 2 + d ** 2)
109    db2c1 = np.sqrt((b / 2 + c / 2) ** 2 + e ** 2)
110    db2c2 = np.sqrt((b / 2 - a / 2) ** 2 + d ** 2)
111
112    dc1a1 = np.sqrt((a / 2 - c / 2) ** 2 + (d + e) ** 2)
113    dc1a2 = c
114    dc2a1 = a
115    dc2a2 = np.sqrt((a / 2 - c / 2) ** 2 + (d + e) ** 2)
116
117    dab = (da1b1 * da1b2 * da2b1 * da2b2) ** (1 / 4)
118    dbc = (db1c1 * db1c2 * db2c1 * db2c2) ** (1 / 4)
119    dca = (dc1a1 * dc1a2 * dc2a1 * dc2a2) ** (1 / 4)
120
121    rp = kg * r
122
123    da1a2 = np.sqrt((a / 2 + c / 2) ** 2 + (d + e) ** 2)
124    db1b2 = b
125    dc1c2 = np.sqrt((c / 2 + a / 2) ** 2 + (d + e) ** 2)
126
127    drap = np.sqrt(rp * da1a2)
128    drbp = np.sqrt(rp * db1b2)
129    drcp = np.sqrt(rp * dc1c2)
130
131    dra = np.sqrt(r * da1a2)
132    drb = np.sqrt(r * db1b2)
133    drc = np.sqrt(r * dc1c2)
134
135    GMD = (dab * dbc * dca) ** (1 / 3)
136    GMR = (drap * drbp * drcp) ** (1 / 3)
137    RMG = (dra * drb * drc) ** (1 / 3)
138
139    L = 4 * np.pi * 1e-7 / (2 * np.pi) * np.log(GMD / GMR) # H / m
140
141    C = 2 * np.pi * 1e-9 / (36 * np.pi) / np.log(GMD / RMG) # F / m
142
143    # in the units pandapower wants
144    Rkm = Rac_75 / 2 * 1e3 # ohm / km, like 2 resistances in parallel

```

```
145     X_km = L * w * 1e3 # ohm / km
146     C_km = C * 1e9 * 1e3 # nF / km
147
148     return R_km, X_km, C_km, Imax
149
150     if npar == 1:
151         rr, xx, cc, imm = single_line(a, b, immax, Rca, Dext, kgg)
152     elif npar == 2:
153         rr, xx, cc, imm = double_line(a, b, c, d, e, immax, Rca, Dext, kgg)
154     else:
155         print('Error: number of parallel lines is not 1 nor 2')
156
157     return rr, xx, cc, imm
158
159 # rr, xx, cc, ii = double_line(11, 2, 4, 5, 6, 1000)
160 # print(rr, xx, cc, ii)
```

Listing 6.2. Code for the calculation of lines

BIBLIOGRAPHY

- [1] Red Eléctrica de España, *Sistema de información del operador del sistema (esios). perfiles de demanda y generación*. <https://www.esios.ree.es/es?locale=en>, Accessed: 2021-10-25.
- [2] Q. Wang and J. D. McCalley, "Risk and "n-1" criteria coordination for real-time operations," *IEEE Transactions on Power Systems*, vol. 28, no. 3, pp. 3505–3506, 2013.
- [3] A. Gourtani, H. Xu, D. Pozo, and T.-D. Nguyen, "Robust unit commitment with n-1 security criteria," *Mathematical Methods of Operations Research*, vol. 83, no. 3, pp. 373–408, 2016.
- [4] B. Stott, J. Jardim, and O. Alsac, "Dc power flow revisited," *IEEE Transactions on Power Systems*, vol. 24, no. 3, pp. 1290–1300, 2009.
- [5] F. Capitanescu, J. M. Ramos, P. Panciatici, D. Kirschen, A. M. Marcolini, L. Platbrood, and L. Wehenkel, "State-of-the-art, challenges, and future trends in security constrained optimal power flow," *Electric Power Systems Research*, vol. 81, no. 8, pp. 1731–1741, 2011.
- [6] L. Thurner, A. Scheidler, F. Schafer, J. H. Menke, J. Dollichon, F. Meier, S. Meinecke, and M. Braun, "Pandapower - an open source python tool for convenient modeling, analysis and optimization of electric power systems," *IEEE Transactions on Power Systems*, 2018, ISSN: 0885-8950. DOI: 10.1109/TPWRS.2018.2829021. [Online]. Available: <https://arxiv.org/abs/1709.06743>.
- [7] Agency for the Cooperation of Energy Regulators (ACER), *Uic report - electricity infrastructure. 2015*.
- [8] Autosolar, *Pallet paneles 405w deep blue 3.0 ja solar mono*, <https://autosolar.es/panel-solar-24-voltios/pallet-paneles-405w-deep-blue-30-ja-solar-mono>, Accessed: 2021-12-01.
- [9] European Comission, *Photovoltaic geographical information system (pvgis)*, <https://ec.europa.eu/jrc/en/pvgis>, Accessed: 2021-12-01.
- [10] N. Kumar, P. Yadav, and S. Chandel, "Comparative analysis of four different solar photovoltaic technologies," in *2015 International Conference on Energy Economics and Environment (ICEEE)*, IEEE, 2015, pp. 1–6.
- [11] Wind Turbine Models, *Gamesa g132-5.0mw*, <https://en.wind-turbine-models.com/turbines/768-gamesa-g132-5.0mw>, Accessed: 2021-12-01.
- [12] M. Ragheb, "Wind energy conversion theory, betz equation," *Wind Energie*, 2014.
- [13] J. Bartl, F. Pierella, and L. Sætrana, "Wake measurements behind an array of two model wind turbines," *Energy Procedia*, vol. 24, pp. 305–312, 2012.
- [14] V. Smil, *Power density: a key to understanding energy sources and uses*. MIT press, 2015.
- [15] NASA Prediction of Worldwide Energy Resources, *The power project*, <https://power.larc.nasa.gov/>, Accessed: 2021-12-01.
- [16] Investing, *Carbon emissions futures overview*, <https://www.investing.com/commodities/carbon-emissions>, Accessed: 2021-12-07.
- [17] B. P. Roberts and C. Sandberg, "The role of energy storage in development of smart grids," *Proceedings of the IEEE*, vol. 99, no. 6, pp. 1139–1144, 2011.
- [18] V. Monteiro, H. Gonçalves, and J. L. Afonso, "Impact of electric vehicles on power quality in a smart grid context," in *11th International Conference on Electrical Power Quality and Utilisation*, IEEE, 2011, pp. 1–6.
- [19] M. S. Ziegler and J. E. Trancik, "Re-examining rates of lithium-ion battery technology improvement and cost decline," *Energy & Environmental Science*, vol. 14, no. 4, pp. 1635–1651, 2021.

- [20] F. Díaz-González, A. Sumper, and O. Gomis-Bellmunt, *Energy storage in power systems*. John Wiley & Sons, 2016.
- [21] F. Lo Franco, A. Morandi, P. Raboni, and G. Grandi, “Efficiency comparison of dc and ac coupling solutions for large-scale pv+ bess power plants,” *Energies*, vol. 14, no. 16, p. 4823, 2021.
- [22] M. M. Rahman, A. O. Oni, E. Gemechu, and A. Kumar, “Assessment of energy storage technologies: A review,” *Energy Conversion and Management*, vol. 223, p. 113 295, 2020, ISSN: 0196-8904.
- [23] Catalan Office for Climate Change, *Practical guide for calculating greenhouse gas (ghg) emissions*, https://canviclimatic.gencat.cat/web/.content/04_ACTUA/Com_calcular_emissions_GEH/guia_de_calcul_demissions_de_co2/190301_Practical-guide-calculating-GHG-emissions_OCCC.pdf, Accessed: 2021-12-10.
- [24] M. S. Ismail, M. Moghavvemi, and T. Mahlia, “Techno-economic analysis of an optimized photovoltaic and diesel generator hybrid power system for remote houses in a tropical climate,” *Energy conversion and management*, vol. 69, pp. 163–173, 2013.
- [25] AleaSoft, *The combined cycle gas turbines and the wind energy in the spanish electricity mix*, <https://aleasoft.com/combined-cycle-gas-turbines-wind-energy-spanish-electricity-mix/>, Accessed: 2021-12-10.
- [26] Trading Economics, *Natural gas usd/mmbtu*, <https://tradingeconomics.com/commodity/natural-gas>, Accessed: 2021-12-10.
- [27] Red Eléctrica de España, *Emissions from the spanish electricity system have fallen by 30 million tonnes in the last 5 years*, <https://www.ree.es/en/press-office/news/featured-story/2020/06/emissions-spanish-electricity-system-have-fallen-30-million-tonnes-last-5-years>, Accessed: 2021-12-11.
- [28] C. C. Spork, A. Chavez, X. Gabarrell Durany, M. K. Patel, and G. Villalba Méndez, “Increasing precision in greenhouse gas accounting using real-time emission factors: A case study of electricity in spain,” *Journal of Industrial Ecology*, vol. 19, no. 3, pp. 380–390, 2015.
- [29] European Environmental Agency, *Greenhouse gas emission intensity of electricity generation in europe*, <https://www.eea.europa.eu/ims/greenhouse-gas-emission-intensity-of-1>, Accessed: 2021-12-11.