

**Metric Prefixes**

peta	P	$10^{15}$	1 000 000 000 000 000
tera	T	$10^{12}$	1 000 000 000 000
giga	G	$10^9$	1 000 000 000
mega	M	$10^6$	1 000 000
kilo	k	$10^3$	1 000
hecto	h	$10^2$	100
deca	da	$10^1$	10
one		$10^0$	1
deci	d	$10^{-1}$	0.1
centi	c	$10^{-2}$	0.01
milli	m	$10^{-3}$	0.001
micro	$\mu$	$10^{-6}$	0.000 001
nano	n	$10^{-9}$	0.000 000 001
pico	p	$10^{-12}$	0.000 000 000 001
femto	f	$10^{-15}$	0.000 000 000 000 001

**RC Filter**

- Transmission Function:  $T(s) = \frac{V_o(s)}{V_i(s)}$
- Corner frequency: frequency  $s$  at which  $T(s) = \frac{1}{\sqrt{2}}$
- for simple circuit: ground  $\rightarrow$  source  $\rightarrow R \rightarrow C \rightarrow$  ground
  - \*  $T(s) = \frac{1}{1+RCs}$
  - $|T(j\omega)| = \frac{1}{\sqrt{1+R^2C^2\omega^2}}$
  - $|\angle T(j\omega)| = \frac{1}{\sqrt{1+R^2C^2\omega^2}}$

**Bode Plots**

- magnitude is plotted in dB:
  - $|T(j\omega)|_{dB} = 20 \log_{10} |T(j\omega)|$
- starts on y-axis at DC offset with slope 0
- just add together the bode plots of each individual pole, zero, and the DC offset
- poles always slope down, zeros slope up (applies for both magnitude and phase)
- $dec$ =decade, e.g. from  $10^0$  to  $10^1$
- magnitude:
  - \* Pole/Zero at origin: constant slope  $\pm 20db/dec$  for all  $\omega$ ;  $0dB$  at  $\omega = 10^0 = 1$
  - \* Pole/Zero at  $\omega_0$ : 0 for  $\omega < \omega_0$  slope  $\pm 20 \frac{db}{dec}$  after
  - \* Constant  $C$ : constant line at  $20 \log_{10}(|C|)$
- phase:
  - \* Pole at origin: constant  $-\frac{\pi}{2}$  or  $-90^\circ$
  - \* Zero at origin: constant  $+\frac{\pi}{2}$  or  $+90^\circ$
  - \* Pole/Zero at  $\omega_0$ : 0 for  $\omega < \frac{\omega_0}{10}$  slope linearly ( $\pm 45^\circ/dec$ ) until  $10\omega_0$  0 slope for  $\omega > 10\omega_0$
  - \* Constant  $C$ : no effect (0 for all  $\omega$ )

**Solving systems with Op Amps**

- step 0: if the op amp is ideal, write out ideal properties:
  - \*  $V_+ = V_-$
  - \*  $I_- = 0, I_+ = 0$
- avoid doing KCL/KVL directly on the output node of the op amp
- ignore resistors from a point at  $0V$  to ground

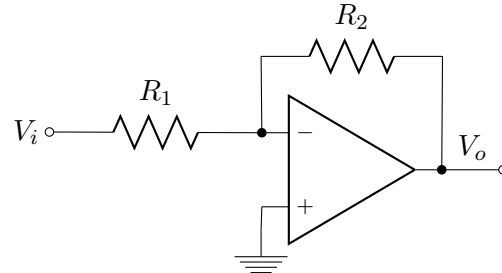
**Op Amp Equations**

- general form:  $T(s) = \frac{K_0}{1+\frac{s}{\omega_0}}$ 
  - \*  $T(0) = K_0$ : DC offset. For these simple ones, it's equal to ideal response
  - \*  $\omega_0 = \frac{\omega_t}{1+R_2/R_1}$

**inverting op amp:**

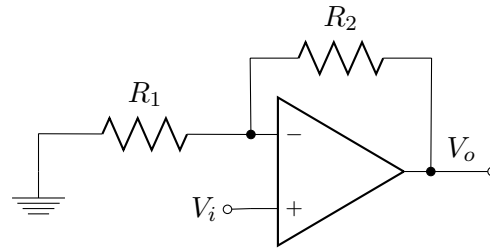
$$\text{* ideal: } T(s) = \frac{V_o}{V_i} = -\frac{R_2}{R_1}$$

$$\text{* non-ideal: } T(s) = \frac{V_o}{V_i} = \frac{-R_2/R_1}{1+\frac{1+R_2/R_1}{A(s)}} = \frac{-R_2/R_1}{1+\frac{\omega_t}{1+R_2/R_1}}$$

**non-inverting op-amp:**

$$\text{* ideal: } T(s) = \frac{V_o}{V_i} = 1 + \frac{R_2}{R_1}$$

$$\text{* non-ideal: } T(s) = \frac{V_o}{V_i} = \frac{1+R_2/R_1}{1+\frac{1+R_2/R_1}{A(s)}} = \frac{1+R_2/R_1}{1+\frac{\omega_t}{1+R_2/R_1}}$$

**Non-Ideal Op Amps**

- open-loop gain dependent on frequency:  $A(s) = \frac{A_0}{1-\frac{s}{\omega_b}}$ 
  - \* open-loop response drops off after  $\omega_b$  (usually  $2\pi \leq \omega_b \leq 2\pi 100$ )
  - \*  $A_0$ : DC gain
  - \*  $\omega_t$ : unity gain frequency:  $dB(T(\omega_t)) = 1$ 
    - $\omega_t \approx A_0 \omega_b$
    - AKA gain bandwidth product
  - \* in this case, we still assume  $I_- = I_+ = 0$  and  $V_- = V_+$ ?
- slew rate
  - \* max rate at which the output can change
  - \* for a sinusoidal signal: ( $V_{pk}$ : peak voltage)
    - $SR > 2\pi f V_{pk}$  or  $SR > \omega V_{pk}$