

**Metric Prefixes:**

peta	P	$10^{15}$	1 000 000 000 000 000
tera	T	$10^{12}$	1 000 000 000 000
giga	G	$10^9$	1 000 000 000
mega	M	$10^6$	1 000 000
kilo	k	$10^3$	1 000
hecto	h	$10^2$	100
deca	da	$10^1$	10
one		$10^0$	1
deci	d	$10^{-1}$	0.1
centi	c	$10^{-2}$	0.01
milli	m	$10^{-3}$	0.001
micro	$\mu$	$10^{-6}$	0.000 001
nano	n	$10^{-9}$	0.000 000 001
pico	p	$10^{-12}$	0.000 000 000 001
femto	f	$10^{-15}$	0.000 000 000 000 001

**Ohm's Law:**  $V = IR$ ,  $I = \frac{V}{R}$ ,  $R = \frac{V}{I}$ **Power:**  $P = IV = I^2R = \frac{V^2}{R}$ **Energy:**

- $W = \int_0^t P(s) ds$
- Unit: Watts,  $W = \frac{J}{s} = \frac{V^2}{\Omega} = VA = A^2\Omega$

**KCL: Kirchoff's Current Law:**

- All currents out of (or into) a point sum to 0
- be careful with signs with this!

**KVL: Kirchoff's Voltage Law:**

- The sum of voltages around a fixed loop is 0
- be careful with signs with this one too!

**Exam 1 stuff:****Source Transformation:**

- When you have a current source with a resistor in

parallel to its load or a voltage source with a resistor in series to its load, you can use Ohm's Law to transform it into the opposite source type.

- The resistor value stays constant, the source type and value changes

**Nodal Analysis:**

- use KCL to sum all currents at each node to 0
- when in doubt, use more nodes
- remember to have a ground node for reference
- convention is to count current out of the node as positive
  - current sources pointing into the node are counted negative

**Superposition:**

- evaluate the circuit many times, killing all but one source each time
- sum the results to get the final result (be careful with signs)
- superposition only applies for linear circuits
  - which nearly all are. Notable exception: stuff with diodes

**Mesh:(current loop method)**

- use KVL to sum all the voltages in each loop to 0
- convention is to loop clockwise
- when you hit a voltage terminal, use the sign of that terminal; e.g. hit negative terminal of  $V_x$  means append " $-V_x$ " to equation. (does not matter if  $V_s$  is source or component)
- When you hit a resistor, use  $V = IR$  to find voltage drop

**Thevenin: Independent Only:**

- always remove the load resistor (if present) first
- find  $V_{th}$  by assuming  $AB$  is an open circuit
- find  $R_{th}$ :
  - first deactivate all sources in the circuit
  - then determine the equivalent resistance from  $A$  to  $B$

**Thevenin: Dependent and Independent:**

- Note: you can't kill independent sources
- find  $V_{th}$  the same way
- find  $R_{th}$ :
  - kill all independent sources
  - put a 1Amp independent current source across  $AB$
  - find voltage across new independent source
  - use  $R_{th} = \frac{V}{I} = \frac{V}{1\text{Amp}}$

**Thevenin: Dependent Only:**

- can't find  $V_{th}$  regular way, so use 1Amp source method
- This means you will get  $R_{th} = \frac{V_{th}}{1\text{Amp}}$

**Norton Equivalent:**

- just use Ohm's Law on the Thevenin Equivalent

**Exam 2 stuff:****Ideal Op Amp:**

- The output tries to do whatever is necessary to make the difference between the input voltages zero.
- Zero current in/out from the input pin
- For a real op amp, the output voltage is limited to  $\pm V_{CC}$ 
  - Saturated when  $|V_{out}| = V_{CC}$

**Op Amp - Inverting:**

- $V_o \rightarrow R_f \rightarrow -\text{input}$   
 $-\text{input} \rightarrow R_s \rightarrow V_s$   
 $+\text{input} \rightarrow \text{ground}$

•  $R_f$ : feedback resistor

$R_s$ : source resistor

•  $V_o = -\frac{R_f}{R_s} V_s$

• linear region:  $\left| \frac{R_f}{R_s} \right| \leq \left| \frac{V_{CC}}{V_s} \right|$

### Op Amp - Summing:

- Adds voltages
- Similar to inverting op amp except that each input is wired as  $V_x \rightarrow R_x \rightarrow -\text{input}$ . (Only one  $R_f$ , but one  $R_s = R_x$  for each input)
- $V_o = -\left( \frac{R_f}{R_a} V_a + \frac{R_f}{R_b} V_b + \dots \right)$
- If  $R_f = R_a = R_b \dots$  then  $V_o = -(V_a + V_b + \dots)$

### Op Amp - Non-inverting:

- $+\text{input} \rightarrow R_s \rightarrow V_g \rightarrow \text{ground}$   
 $-\text{input} \rightarrow R_s \rightarrow \text{ground}$   
 (two different resistors each with value  $R_s$ )  
 same  $R_f$  feedback resistor as inverting amp  
 $R_f$  and  $R_s$  form an unloaded voltage divider across  $-\text{input}$
- $V_o = \frac{R_s + R_f}{R_s} V_g$
- Linear region:  $\frac{R_s + R_f}{R_s} < \left| \frac{V_{CC}}{V_g} \right|$

### Op Amp - Difference:

- regular feedback resistor  $R_b$   
 $R_a$ : from  $V_a$  to  $-\text{input}$   
 $R_c$ : from  $V_b$  to  $+\text{input}$   
 $R_d$ : from  $+\text{input}$  to ground
- $V_o = \frac{R_d(R_a + R_b)}{R_a(R_c + R_d)} V_b - \frac{R_b}{R_a} V_a$
- if  $\frac{R_a}{R_b} = \frac{R_c}{R_d}$  then  $V_o = \frac{R_b}{R_a} (V_b - V_a)$

### Op Amp - Integrator:

- Circuit: just like inverting op-amp except with a

capacitor instead of the feedback resistor ( $R_f$ )

- The only resistor is  $R_s$ , between the source and the  $-\text{input}$  of the op amp
- $V_o = -\frac{1}{R_s C} \int V_{in} dt$
- can be used to turn square wave into sawtooth wave

### Op Amp - Differentiator:

- Circuit: just like inverting op-amp except with a capacitor instead of the input resistor ( $R_s$ )
- $V_o = -R_f C \frac{dV_{in}}{dt}$
- Can be used to turn sawtooth wave into square wave

### Inductors:

- Series and parallel is the same as resistors
- Voltage:  $V_L(t) = -L \frac{di_L(t)}{dt}$   
 Energy:  $W(t) = \frac{1}{2} L * i(t)^2$
- $\tau = \frac{L}{R}$
- RL Charging:  $i(t) = i_f + (i_o - i_f)e^{-tR/L}$
- RL Discharging:  $i(t) = i_o e^{-tR/L}$

### Capacitors:

- Series and parallel is the opposite as resistors
- Current:  $I_c(t) = C \frac{dV_C(t)}{dt}$   
 Energy:  $W(t) = \frac{1}{2} C * V_C(t)^2$
- $\tau = RC$   
 $V_f$  = final voltage  
 $V_o$  = initial voltage
- RC Charging:  $V(t) = V_f + (V_o - V_f)e^{-t/(RC)}$
- RC Discharging:  $V(t) = V_o e^{-t/(RC)}$

### Exam 3 stuff:

#### RLC Circuits - Parallel:

- $s_{1,2} = \frac{1}{2/RC} \pm \sqrt{\left( \frac{1}{2RC} \right)^2 - \frac{1}{LC}}$   
 $s_{1,2} = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2}$
- $\alpha = \frac{1}{2RC}$
- resonant frequency:  $\omega_0 = \frac{1}{\sqrt{LC}}$

### damping:

- $\omega_0 < \alpha$ : over damped  
 $* V(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t}$
- $\omega_0 = \alpha$ : critically damped  
 $* V(t) = B_1 t e^{\alpha t} + B_2 e^{\alpha t}$
- $\omega_0 > \alpha$ : under damped  
 $* V(t) = B_1 t e^{\alpha t} \cos(\omega_0 t) + B_2 e^{\alpha t} \sin(\omega_0 t)$
- $\omega_d = \sqrt{\omega_0^2 - \alpha^2}$  damped frequency (only relevant for under damped)

### Impedance:

- $V = IZ$
- $Z_R = R$   
 $\phi_R = 0^\circ$
- $Z_L = j\omega L$   
 • Current lags  $90^\circ$  behind voltage  
 $\phi_L = -90^\circ$
- $Z_C = \frac{1}{j\omega C}$   
 • Current leads voltage by  $90^\circ$   
 $\phi_C = 90^\circ$

### Reactance:

- $X_L = \frac{V_L}{I_L} = \omega L = 2\pi f L$
- $X_C = -\frac{1}{\omega C} = -\frac{1}{2\pi f C}$

### Complex Power:

- $S = P + jQ = \frac{(V_{RMS})^2}{Z^*}$   
 $\bar{Z}$  is complex conjugate of  $Z$
- $P = \frac{V_m I_m}{2} \cos(\theta_v - \theta_i)$
- $Q = \frac{V_m I_m}{2} \sin(\theta_v - \theta_i)$
- $S = VI^*$   
 $*$  also means conjugate

### Maximum Power Transfer:

- unrestricted:  $Z_L = \bar{Z}_{Th}$
- restricted:  $|Z_L| = |\bar{Z}_{Th}|$