

**Metric Prefixes**

peta	P	$10^{15}$	1 000 000 000 000 000
tera	T	$10^{12}$	1 000 000 000 000
giga	G	$10^9$	1 000 000 000
mega	M	$10^6$	1 000 000
kilo	k	$10^3$	1 000
hecto	h	$10^2$	100
deca	da	$10^1$	10
one		$10^0$	1
deci	d	$10^{-1}$	0.1
centi	c	$10^{-2}$	0.01
milli	m	$10^{-3}$	0.001
micro	$\mu$	$10^{-6}$	0.000 001
nano	n	$10^{-9}$	0.000 000 001
pico	p	$10^{-12}$	0.000 000 000 001
femto	f	$10^{-15}$	0.000 000 000 000 001

**Complex Numbers**

- $z = x + iy = re^{i\theta} = r[\cos(\theta) + i\sin(\theta)]$
- $[r(\cos(\theta) + i\sin(\theta))]^n = r^n[\cos(n\theta) + i\sin(n\theta)]$
- $z^n = (re^{i\theta}) = r^n e^{in\theta}$
- $\frac{1}{i} = -i$
- $\sqrt[n]{z} = \sqrt[n]{r} e^{\frac{\theta}{n} + \frac{2k\pi}{n}}$  for  $n \in \mathbb{N}^*$  (ints  $\geq 0$ )
- $e^{j\theta} = \cos(\theta) + j\sin(\theta)$
- $e^{-j\theta} = \cos(\theta) - j\sin(\theta)$
- $\cos(\theta) = \frac{1}{2}(e^{j\theta} + e^{-j\theta})$
- $\sin(\theta) = \frac{1}{2j}(e^{j\theta} - e^{-j\theta})$
- normalized:  $\text{sinc}(t) = \frac{\sin(\pi t)}{\pi t}$

**Trig**

- $\cos^2(a) + \sin^2(a) = 1$
- $\cos(2a) = \cos^2(a) - \sin^2(a) = 2\cos^2(a) - 1 = 1 - 2\sin^2(a)$
- $\sin(2a) = 2\sin(a)\cos(a)$
- $\cos^2(a) = \frac{1}{2}(1 + \cos(2a))$
- $\sin^2(a) = \frac{1}{2}(1 - \cos(2a))$

**Signals****• Even/Odd**

even:  $x(-t) = x(t)$  for all  $t$   
 odd:  $x(-t) = -x(t)$  for all  $t$

- **Auto Correlation:** compare signal with a time-delayed version of itself

$$\phi(\tau) = \int_{-\infty}^{\infty} x(t) * x(t + \tau) dt$$

\* peaks will be at multiples of the period

- **Cross Correlation:** like autocorrelation, but for two different signals

$$\phi(\tau) = \int_{-\infty}^{\infty} x_1(t) * x_2(t + \tau) dt$$

\* to easily tell if one signal is a shifted version of another

- Shifting and scaling: just always remember you're replacing **just**  $t$  with an expression involving  $t$
- **Unit Step Signal**  
 $* u(t) = \begin{cases} 0, & t < 0 \\ 1, & t > 0 \end{cases}$
- **Discrete Unit Impulse Signal**

$$\delta[n] = \begin{cases} 0, & n \neq 0 \\ 1, & n = 0 \end{cases}$$

\* any discrete signal can be represented as a sum of shifted unit impulse signals

$$* \delta[n] = u[n] - u[n - 1]$$

- **Continuous Unit Impulse Signal**

$$x(t) = \delta(t) = \begin{cases} 0, & t \neq 0 \\ \infty, & t = 0 \end{cases}$$

\* discontinuous at  $t = 0$

$$* \int_{-\infty}^{\infty} \delta(t) dt = 1$$

\* pick out values from discrete function: (shifting property)

$$\int_{-\infty}^{\infty} \delta(t) * f(t) dt = f(0)$$

$$\int_{-\infty}^{\infty} \delta(t - a) * f(t) dt = f(a)$$

- **Shifting Property:**  $\int_{-\infty}^{\infty} x(t)\sigma(t - t_0) dt = x(t_0)$

- **Bounded:**  $x(t) \leq M$  for all  $t$ , some  $M$

\* unbounded signals typically are infinite at some time instant

- **Causal** iff  $x(t) = 0$  for all  $t < 0$

- **Energy:**  $E_x = \int_{-\infty}^{\infty} |x(t)|^2 dt$

\* signal is an energy signal if  $0 < E_x < \infty$

- **Power:**  $P_x = \frac{1}{T} \int_T |x(t)|^2 dt$

\* (for periodic signals)

\* signal is a power signal if  $0 < P_x < \infty$

**Convolution**

- $\sum_{k=-\infty}^{\infty} x(k)h(n - k)$  or  $\int_{-\infty}^{\infty} x(\tau)h(t - \tau) d\tau$

- graphically:

\* choose one function to be  $h$

\* flip around origin with  $t \rightarrow -t$

\* shift back and forth on form  $h(t - \tau)$

\* shift is reversed because the negative

\* multiply by  $x(t)$  and then sum

- if the system is LTI invariant, then the convolution of  $x(t)$  with the impulse response  $h(t)$  is the same as if  $x(t)$  were the input of the system

- convolution with shifted unit impulse is the same as shifting the original system:  $h(t) * \sigma(t - a) = h(t - a)$

- Step response is just convolution with impulse response. worked out:  $u(t) * h(t) = \int_{-\infty}^t h(\tau) d\tau$   
 \* only works for LTI systems!

**Geometric Series**

- $\sum_{k=0}^{\infty} ar^k = \frac{a}{1-r}$

- $a$  is first term of the series

$r$  is ratio between terms:  $r = \frac{a_1}{a_0} = \frac{a_2}{a_1} \dots$

**Systems**

- A system is an operation that transforms an input signal into an output signal

\* you can add/subtract signals

\* composing signals (one input to another) is convolution

(easier to just shift if input is shifted unit step (because LTI))

- **BIBO stability:** output is stable iff input signal is stable

\* also if impulse response  $\int_{-\infty}^{\infty} |h(t)| dt < \infty$  (for LTI systems)

- \* bounded:  $h(t) < M$  for all  $t$  and some  $M$
- **Memory:** iff the system depends on past or future values of the input
- **Causality:** iff the output depends only on the current or past values of the input
  - \* (cannot depend on future values of input)
- **Invertibility:** iff the system's input can be recovered from the output
- **Time Invariance:** iff shifting the input signal shifts the output
  - \* integral is time invariant
- **Superposition:** additive commutativity
  - \*  $H\{x_1(t) + x_2(t)\} = H\{x_1(t)\} + H\{x_2(t)\}$
- **Homogeneity:**
  - \*  $H\{ax(t)\} = aH\{x(t)\}$
- **Linearity:** iff satisfies Superposition and Homogeneity
  - \*  $H\{ax_1(t) + bx_2(t)\} = aH\{x_1(t)\} + bH\{x_2(t)\}$
  - \* averaging filter is linear
- **LTI:** both Linear and Time Invariant
  - \* simplest systems
- system from block diagram:
  - \* add/subtract signals just like you would
  - \* for signals  $h_1(t) \rightarrow h_2(t)$  (in series), you get  $y(t) = h_1(t) * h_2(t)$  (convolution of the two signals)
  - \* basic method is to keep combining adjacent signal blocks using convolution, scaling, and addition until you get a single block
- system from differential equation:
  - \* solve equation for  $y(t)$
  - \* stuff in terms of input goes on the left; output on the right
  - \* add constants scaling to each output, and sum it all together

## Linearity

- system is linear if it satisfies superposition (additive) and homogeneity (scalable)
  - \* superposition:  $h(a) + h(b) = h(a + b)$
  - \* homogeneity:  $ah(b) = h(ab)$

## Noise

- unwanted signals generated externally or internally
- thermal noise is a thing

## Impulse Response

- output of a system when the input is  $\sigma(t)$ 
  - memoryless if  $h(t) = c\sigma(t)$
  - causal if  $h(t) = 0$  for  $t < 0$
- BIBO stable if  $\int_{-\infty}^{\infty} |h(t)| dt < \infty$
- invertible if  $h(t) * h^{inv}(t) = \sigma(t)$ 
  - \* same for discrete time

## even/odd signals

- $f(t) = f_e(t) + f_o(t)$
- $f_e(t) = \frac{1}{2}(f(t) + f(-t))$
- $f_o(t) = \frac{1}{2}(f(t) - f(-t))$

## Fourier Series

- Harmonic:  $e^{jk2\pi F_0 t}$
- Synthesis:  $f(t) = \sum_{k=-\infty}^{\infty} X[k]e^{jk2\pi F_0 t}$
- Analysis:  $X[k] = \frac{1}{T_p} \int_0^{T_p} x(t)e^{-jk2\pi F_0 t} dt$ 
  - \* note the different sign!
- $X[k] = C_k$
- Parseval's theorem: (energy of a signal)
 
$$\int_{-\infty}^{\infty} |x(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |X(j\omega)|^2 d\omega$$
- FT of fraction of two polynomials: use partial fraction decomposition

## Fourier Transform

- $x(t) = \int_{-\infty}^{\infty} X(j\omega)e^{j\omega t} d\omega$
- $X(j\omega) = \int_{-\infty}^{\infty} x(t)e^{-j\omega t} dt$

## Fourier Properties

- linearity:
 
$$z(t) = ax(t) + by(t) \leftrightarrow Z(k) = aX(k) + bY(k)$$
- time shift:  $x(t - t_0) \leftrightarrow X(k)e^{-jk\omega_0 t_0}$
- frequency shift:  $x(t)e^{jk_0\omega_0 t} \leftrightarrow X(k - k_0)$
- time scaling: same coefficients,  $x(at) \rightarrow \omega = a\omega_0$  (for  $a > 0$ )
- time reversal:  $x(-t) \leftrightarrow X(-k)$
- convolution:  $x(t) * z(t) \leftrightarrow TX(k)Z(k)$
- multiplication:  $x(t)z(t) \leftrightarrow \sum_{l=-\infty}^{\infty} X(k)Z(k - l)$ 
  - \* similar to convolution
- derivative:  $\frac{d}{dt}(x(t)) \leftrightarrow jk\omega_0 X(k)$
- integral:  $\int_{-\infty}^t x(t) dt \leftrightarrow \frac{1}{jk\omega_0} X(k)$
- Symmetry: if  $x(t) = x_r(t) + jx_i(t)$  then
 
$$x^*(t) = x_r(t) - jx_i(t)$$
- if  $x(t)$  is real and even,  $X(k)$  is real and even
- if  $x(t)$  is real and odd,  $X(k)$  is imaginary and odd
- unnormalized sinc:  $\text{sinc}(t) = \frac{\sin(t)}{t}$
- normalized sinc:  $\text{sinc}(t) = \frac{\sin(\pi t)}{\pi t}$

## Frequency Response

- how the system will respond to a particular frequency
- the Fourier Transform of the impulse response (we don't have to convolve it here, just multiply since it's frequency domain)
- find using  $H(\omega) = \frac{Y(\omega)}{X(\omega)}$ 
  - \* if the starting equation is expressed as a differential equation, you can (usually) derive this from that.
- usually represented as  $H(\omega) = |H(\omega)|e^{j\theta_H(\omega)}$  (magnitude and phase)
  - \* magnitude:  $|H(\omega)|$ , phase:  $\theta_H(\omega)$
- magnitude and phase can be linearly combined

## Sampling

- sampling: independent variable (input); continuous  $\rightarrow$  discrete
- quantization: dependent variable (output); continuous  $\rightarrow$  discrete
- aliasing: different signals being indistinguishable after sampling due to sampling rate.
- $F_{CT}$ : continuous time frequency;  $f_{DT}$ : discrete time frequency,  $F_s$ : sampling frequency
- $F_{CT} \rightarrow f_{DT}$  is a many to one mapping
  - \* Folding Frequency =  $F_s/2$ , where frequency

wraps-around

\* restrict to one-to-one: satisfy  $|F| < F_s/2$

- **Nyquist Rate:** signal with maximum frequency  $f_{max}$  can be recovered exactly if it is sampled at least  $f_s > 2f_{max}$
- continuous to discrete:
  - \*  $x[n] = x_a(n/F_s)$
  - \*  $X(f) = F_s \sum_{k=-\infty}^{\infty} \infty X_a[(f - k)F_s]$
- sampling is equivalent to convolving with a delta chain (dirac comb)
- under-sampling:  $f_s < 2f_{max}$ . Generally bad

## DFT

- discrete in both time domain and frequency domain
- zero padding (on the right) increases frequency domain resolution
- frequency domain is on range  $[0, 2\pi)$
- TODO

## DTFT

- Discrete Time Fourier Transform
- Discrete in time, continuous in frequency
- $X(e^{j\Omega}) = \sum_{n=-\infty}^{\infty} x[n]e^{-j\Omega n}$
- $x[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\Omega})e^{j\Omega n} d\Omega$
- frequency domain is **periodic**, range  $[-\pi, \pi]$  is repeated
  - \* if aliasing happens ( $F_s < 2f_{max}$ ) then parts will overlap, and won't work right
- maximum frequency  $\rightarrow \pi$ ; sampling frequency  $\rightarrow 2\pi$

## Laplace Transform

- $X(s) = \int_0^{\infty} x(t)e^{st} dt$
- $s = \sigma - j\omega$
- relation to Fourier Transform:  $X(j\omega) = X(s)|_{s=j\omega, \sigma=0}$
- zeros: numerator is 0, so value is 0
- poles: denominator is 0, so value is  $+$  or  $-\infty$ 
  - \* effect on impulse response on  $t > 0$ :
    - poles left of  $s = 0$ : decaying exponential
    - poles right of  $s = 0$ : increasing exponential (reversed on  $t < 0$ )
- Specified on a Region of Convergence (ROC)
- ROC must contain no poles
- Unilateral: integral starts from 0
  - \* assumes signals is 0 before  $t = 0$
  - \* i.e. multiplied by  $u(t)$
- Bilateral: starts from  $-\infty$ 
  - \* same as unilateral iff  $x(t) = 0$  for  $t < 0$
- Shifting:
  - \*  $x(t - T) \leftrightarrow e^{-sT} X(s)$
  - \*  $T$  such that  $x(t - T)u(t) = x(t - T)u(t - T)$ 
    - i.e. doesn't shift any non-zero part of the signal left of  $t = 0$
  - (Doesn't apply for Bilateral transform)
- Initial Value Theorem:
  - \*  $\lim_{s \rightarrow \infty} sX(s) = \lim_{t \rightarrow 0^+} x(t) = x(0^+)$
  - \* order of numerator  $<$  denominator

\*  $x(t) = 0$  for  $t < 0$

## Final Value Theorem:

- \*  $\lim_{s \rightarrow 0} sX(s) = \lim_{t \rightarrow \infty} x(t) = x(\infty)$
- \*  $x(t) = 0$  for  $t < 0$ ,  $x(t)$  finite as  $t \rightarrow \infty$
- \* all poles on left of plane with at most one at  $s = 0$

## System Response:

- \* take Laplace Transform to get equation in form  $a(s)Y(s) - c(s) = b(s)X(s)$
- \* solve  $Y(s) = \frac{b(s)X(s)}{a(s)} + \frac{c(s)}{a(s)} = Y^{(f)}(s) + Y^{(n)}(s)$
- \*  $Y^{(f)}(s)$ : forced response;  $Y^{(n)}(s)$ : natural response
- \* Frequency Response (transfer function):
$$H(\omega) = \frac{Y(\omega)}{X(\omega)}$$

- Stability: system is stable  $\leftrightarrow$  all poles left of  $s = 0$

## Filters

- multiply signal by a filter to filter it
- pass: allow through (not filtered out)
- stop: filter out, remove
- *something* pass filter passes *something*; same for stop
- low pass filter: passes  $\omega$  lower than  $b$ , drops higher
$$H(\omega) = \begin{cases} 0: |\omega| > b \\ 1: |\omega| < b \end{cases}$$
- high pass filter: opposite of low pass filter
- band pass filter: pass a specific band of frequency.
  - \* That frequency is specified by magnitude, so it can be on the positive or negative side of the graph
- Notch filter: band stop filter with a narrow stop band
- An ideal filter has exact edges, but real filters don't
  - \* This is impossible in practice. Typically there is vertical variation inside the pass band and stop band, and also a trans band ( $\omega_s$ ), as transition between pass and stop band.
- series RC circuit with  $x(t)$  as input and  $y(t)$  on capacitor:  $RCy'(t) + y(t) = x(t)$  or  $y'(t) + \frac{1}{RC}y(t) = \frac{1}{RC}x(t)$ 
  - \* capacitor:  $I(t) = C * \frac{d}{dt}(V(t))$
  - \* inductor:  $V(t) = L * \frac{d}{dt}(I(t))$
- highpass and band-stop filters do not have bandwidth
- Absolute Bandwidth: width of passband
- 3-dB Bandwidth: (for low pass): width of passband where  $H(j\omega) \geq |H(0)|/\sqrt{2}$ 
  - \* because low pass has max at  $\omega = 0$ . Different for other filter types
  - \* AKA half power bandwidth
- Bode Plot: frequency response ( $H(s = j\omega, \sigma = 0)$ ) in dB as a function of logarithm of frequency
- ideal filter has linear phase response
  - \* so that the response to different frequencies is the same
  - \* constant delay is linear phase response (it's just  $H(j\omega) = e^{-j\omega a}$ )
- ideal filter magnitude response is 1 in passband and 0 in stopband
- real filter has  $E, \delta$  and transition band ( $\omega_p, \omega_s$ ) such that:

- \* passband:  $1 - E \leq H(j\omega) < 1$  for  $0 \leq |\omega| \leq \omega_p$
- \* stopband:  $|H(j\omega)| < \delta$  for  $\omega > \omega_s$
- FIR filter: Finite Impulse Response
  - \* finite memory (lower startup transient time)
  - \* always BIBO stable
  - \* desired magnitude response with exactly linear phase response
- IIR filter: Infinite Impulse Response
  - \* output governed by recursive linear constant coefficient differential equations
  - \* uses z transform
  - \* allows shorter (lower order?) filters
  - \* has phase distortion (nonlinear phase response)
  - \* non-finite transient startup
- Butterworth Filter
  - \* looks like a nice simple slope, relatively large transition band though
  - \*  $\omega_c$ : cutoff frequency
  - \*  $|H(j\omega)|^2 = 1/(1 + (\frac{\omega}{\omega_c})^{1/(2K)})$ ,  $K = 1, 2, 3, \dots$
  - $H(s)H(-s)|_{s=j\omega} = |H(j\omega)|^2$
  - \* passband:  $\omega_p = \omega_c(\frac{\epsilon}{1-\epsilon})^{1/(2K)}$
  - \* stopband:  $\omega_s = \omega_c(\frac{1-\delta}{\delta})^{1/(2K)}$
  - \* poles:  $\omega_c e^{i\pi(2k+1)/(2K)}$ ,  $k = 0, 1, \dots, (2K-1)$ 
    - never pure imaginary
    - left of  $s = 0$  belong to  $H(s)$ , right of  $s = 0$  belong to  $H(-s)$
  - \* to get transfer function, find poles and make fraction from there
- Chebyshev Filter
  - \* poles on ellipse in  $s$ -plane
  - \* ripples in either passband or stopband, not both
  - \* smaller transition band
- Elliptic Filter
  - \* smallest transition band
  - \* ripples in both passband and stopband

## Communication Systems

- frequency range: what frequencies are best transmitted, and what are lost
- modulation: embedding a signal inside a carrier signal that propagates better
- simultaneous transmission (multiplexing): use modulation to transmit more than one signal simultaneously

## Amplitude Modulation (AM)

- mix (convolve) payload and carrier in frequency domain (multiply in time domain)
- carrier is typically a high frequency cosine, which is two impulses in frequency domain, so the convolution makes two shifted copies of the input signals, each centered around  $\pm$  carrier frequency
- demodulation: recover original signal: shift it back to the origin and apply low-pass filter
- Frequency Modulation is another (different) kind of modulation