

Project Cantilever Beam
Rev. 001
Module Group Design E2
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1 Design of a Cantilever Beam

The analysis and design of a cantilever beam with a range of assumptions and scenarios, multiple variations are included for comparison.

1.1 Definition

The problem as stated is a cantilevered beam is to be designed to support a 10kN load acting at 1.5m from the fixed wall it is attached to. An optimized solution is to be found and a range of cross sectional geometries and materials are to be compared and considered.

The primary goals are to design a beam that, with no more than 2mm deflection, can support the 10kN load.

Secondary goals include cost and weight considerations, and simulations to be carried out using Solid works simulations and Ansys finite element packages, I will also endeavour to produce a calculator for the relevant formulas using Excel.

1.2 Assumptions made

It is to be assumed for ease of calculation and within the scope of this project that the beam will be of uniform geometry and uniform material, however the geometry and material chosen will be selected after a range of comparisons.

1.3 Summary of findings

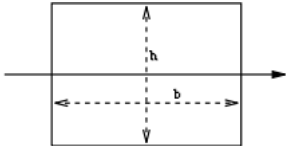
Please read on for detailed analysis.

All units are
[SI]

2 Comparison of various geometries

2.1 Cantilever beam of square cross section

For square geometry second moment of area is equal to $\frac{bd^3}{12}$ however for a square $b=d$, thus second moment of area $I = \frac{d^4}{12}$



2.1.1 Material 1: Steel BS 4360 grade 43A

Dimensions

Using Steel BS 4360 grade 43A with a strength of 255 N/mm^2 up to 25mm thick and 245 N/mm^2 over 50mm thick.

$$\sigma = \frac{My}{I} \text{ with } y \text{ being } \frac{d}{2} \text{ and } I \text{ being } \frac{d^4}{12}$$

thus simplifying to $\sigma = \frac{6M}{d^3}$

$$M = 1.5 \times 10 \times 10^3 = 15000 \text{ Nm} \quad \sigma = 245 \times 10^6 \frac{\text{N}}{\text{m}^2}$$

$$\text{Thus } d = \sqrt[3]{\frac{6M}{\sigma}} = \sqrt[3]{\frac{6 \times 15000}{245 \times 10^6}} = 71.62 \text{ mm}$$

Therefore a load of 15kN acting at 1.5m for the fixing point of the cantilever beam must have dimensions of cross section of 71.62mm high and wide i.e square.

For a safety factor of 2 assume σ is now half i.e 122.5 N/mm^2 , repeating the calculation yields d to be 90.23mm

Selected safety factors are given in the table below:

Safety factor	value of d (mm)	volume mm^3	Cost(\$)	Mass(kg)
1	71.62	7.69×10^6	39.24	60.36
2	90.23	1.22×10^7	62.25	95.77
3	103.29	1.60×10^7	81.64	125.6
4	113.69	1.94×10^7	98.99	152.29

Density = $7.85 \times 10^{-6} \frac{\text{kg}}{\text{m}^3}$, Price = \$650 per Ton (1000kg), i.e \$0.65 per kg. As you can see the safety factor dimensions are non-linear and it may be cost effective to implement a factor of 3 or even 4 given the difference in material costs.

In units of $\frac{\text{N}}{\text{mm}^2}$

Deflection

Specification dictates a limiting stiffness of 2mm, in order to calculate deflection this equation is used: $\delta = \frac{Fl^3}{3EI}$ for our scenario this becomes a rearrangement for d following on from the fact I is $\frac{d^4}{12}$

Thus we get: $d = \sqrt[4]{\frac{4FL^3}{E\delta}}$

$$d = \sqrt[4]{\frac{4 \times 10000 \times 1.5^3}{200 \times 10^9 \times 2 \times 10^{-3}}} \times 1000 = 135.54mm$$

Which gives a design stress safety factor of 6.78.

Safety factor	value of d(mm)	volume mm^3	Cost(\$)	Mass(kg)
6.78	135.54	2.76×10^7	140.83	140.83

2.1.2 Material 2: Alloy Steel B.S. CDS 110

Dimensions

Using Steel BS 4360 grade 43A with a strength of 1034 N/mm^2

$$\sigma = \frac{My}{I} \text{ with } y \text{ being } \frac{d}{2} \text{ and } I \text{ being } \frac{d^4}{12}$$

$$\text{thus simplifying to } \sigma = \frac{6M}{d^3}$$

$$M = 1.5 \times 10 \times 10^3 = 15000 \text{ Nm} \quad \sigma = 1034 \times 10^6 \frac{\text{N}}{\text{m}^2}$$

$$\text{Thus } d = \sqrt[3]{\frac{6M}{\sigma}} = \sqrt[3]{\frac{6 \times 15000}{1034 \times 10^6}} = 44.32 \text{ mm}$$

Therefore a load of 15kN acting at 1.5m for the fixing point of the cantilever beam must have dimensions of cross section of 44.32mm high and wide i.e square.

For a safety factor of 2 assume σ is now half i.e 517 N/mm^2 , repeating the calculation yields d to be 55.84mm

Selected safety factors are given in the table below:

Safety factor	value of d(mm)	volume mm^3	Cost(\$)	Mass(kg)
1	44.32	2.95×10^6	39.24	60.36
2	55.84	4.67×10^6	62.25	95.77
3	63.92	6.13×10^6	81.64	125.6
4	70.34	7.42×10^6	98.99	152.29

Density = $8.03 \times 10^{-6} \frac{\text{kg}}{\text{m}^3}$, Price = \$4000 per Ton (1000kg), i.e \$4 per kg. As you can see the safety factor dimensions are non-linear and it may be cost effective to implement a factor of 3 or even 4 given the difference in material costs.

Deflection

Specification dictates a limiting stiffness of 2mm, in order to calculate deflection this

equation is used: $\delta = \frac{Fl^3}{3EI}$ for our scenario this becomes a rearrangement for d

following on from the fact I is $\frac{d^4}{12}$

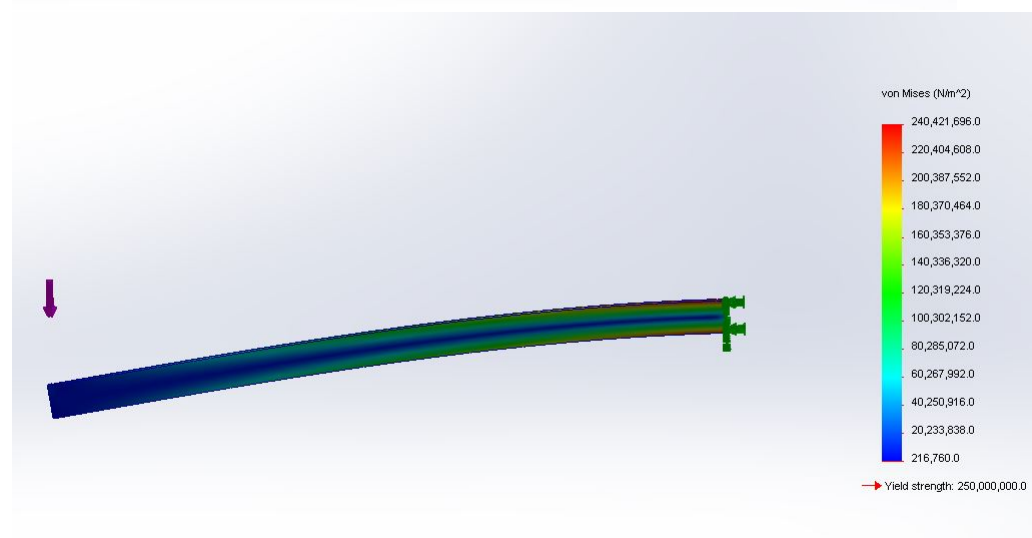
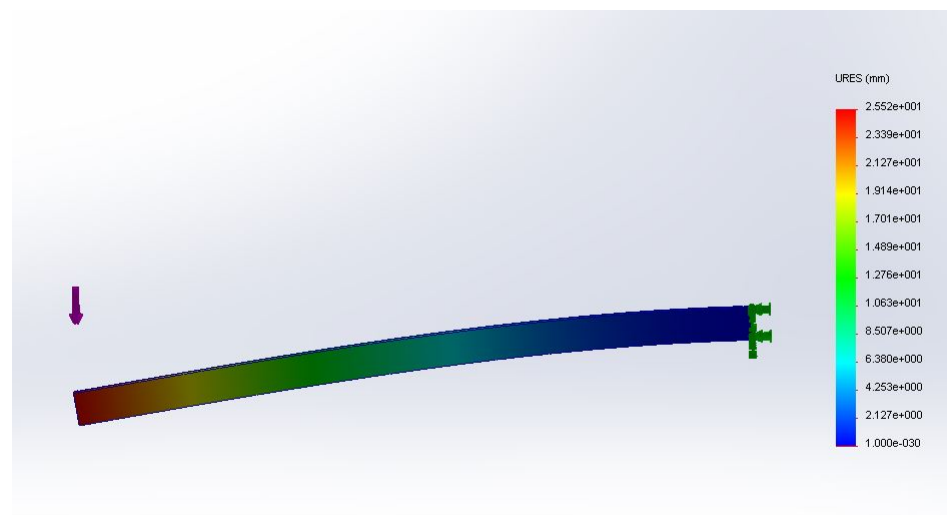
$$\text{Thus we get: } d = \sqrt[4]{\frac{4FL^3}{E\delta}}$$

$$d = \sqrt[4]{\frac{4 \times 10000 \times 1.5^3}{200 \times 10^9 \times 2 \times 10^{-3}}} \times 1000 = 135.54 \text{ mm}$$

Which gives a design stress safety factor of 6.78.

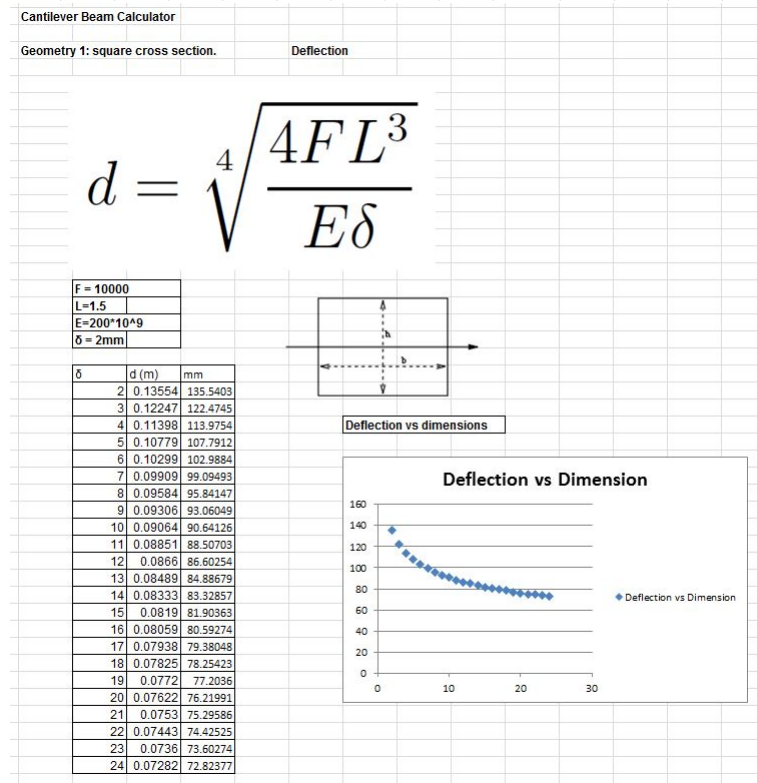
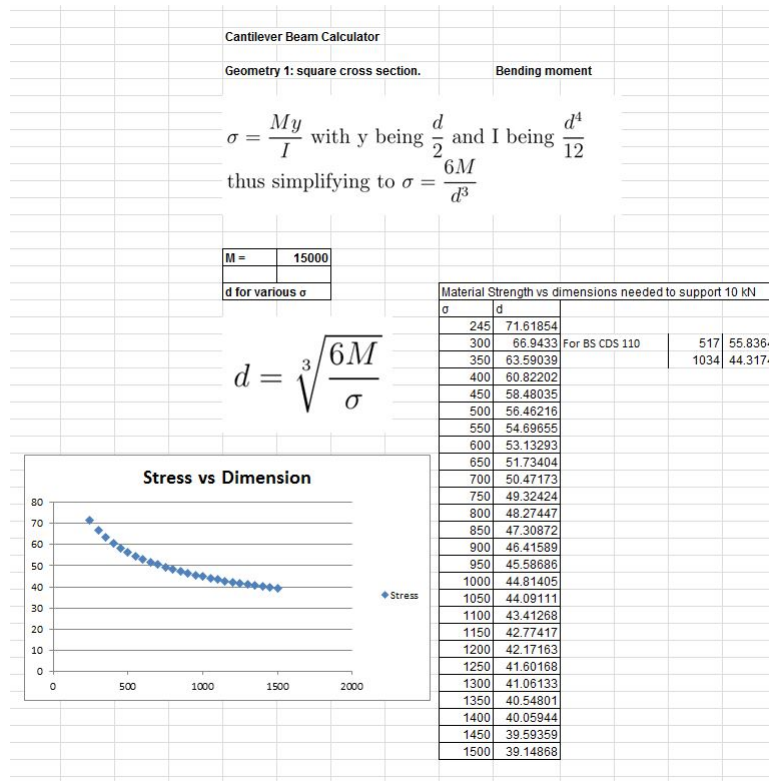
Safety factor	value of d(mm)	volume mm^3	Cost(\$)
6.78	135.54	2.76×10^7	

3 Solidworks simulation



4 Appendix 1

4.1 Calculators in Excel



4.2 Equations Used

Engineers theory of bending equation:

$$\sigma = \frac{My}{I}$$

Deflection equation:

$$\delta = \frac{Fl^3}{3EI}$$

Table of symbols:

- M= Bending Moment
- y = geometric depth /2
- I = second moment of area
- F = Force
- E = Youngs modulus
- σ = Yield Stress/Strength
- δ = Deflection