

2. Übungsblatt

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1. Lösung: Delta Distribution

(a)

$$g(x) = x\theta(x) \quad (1)$$

$$g'(x) = x\theta'(x) + \theta(x) \quad (2)$$

$$g''(x) = 2\theta'(x) + x\theta''(x) \quad (3)$$

Da $\theta'(x) = \delta(x)$ kann man zeigen, dass

$$x\theta''(x) = x\delta'(x) = -\delta(x) \quad (4)$$

Man verwendet dafür, dass für alle Testfunktionen $h(x)$ gilt:

$$\int dx h(x)x\delta'(x) = - \int dx \delta(x) [h(x)x]' \quad (5)$$

$$= - \int dx \delta(x) [(h(x) + xh'(x))] \quad (6)$$

$$= - \int dx \delta(x)h(x) \quad (7)$$

(b) Sei $f(x)$ eine Testfunktion.

Angenommen $a > 0$:

$$\int_c^d dx f(x)\delta(ax) = \int_{c \cdot a}^{d \cdot a} \frac{dx}{dy} dy f\left(\frac{y}{a}\right) \delta(y) \quad (8)$$

$$= \frac{1}{a} \int_{c \cdot a}^{d \cdot a} dy f\left(\frac{y}{a}\right) \delta(y) \quad (9)$$

$$= \begin{cases} \frac{1}{a} f(0) & \text{falls } 0 \in [ac, ad] \\ 0 & \text{falls } 0 \notin [ac, ad] \end{cases} \quad (10)$$

Angenommen $a < 0$:

$$\int_c^d dx f(x) \delta(ax) = \int_{c \cdot a}^{d \cdot a} \frac{dx}{dy} dy f\left(\frac{y}{a}\right) \delta(y) \quad (11)$$

$$= \frac{1}{a} \int_{c \cdot a}^{d \cdot a} dy f\left(\frac{y}{a}\right) \delta(y) \quad (12)$$

$$= -\frac{1}{a} \int_{d \cdot a}^{c \cdot a} dy f\left(\frac{y}{a}\right) \delta(y) \quad (13)$$

$$= \begin{cases} -\frac{1}{a} f(0) & \text{falls } 0 \in [ad, ac] \\ 0 & \text{falls } 0 \notin [ad, ac] \end{cases} \quad (14)$$

(c) Sei $\epsilon > 0$ so klein, dass in $[x_i - \epsilon, x_i + \epsilon]$ nur eine Nullstelle x_i liegt. Dann ist

$$f(x) = f(x_i) + f'(x_i)(x - x_i) + \dots \quad (15)$$

$$= f'(x_i)(x - x_i) + \dots \quad (16)$$

und

$$\int_{x_i - \epsilon}^{x_i + \epsilon} dx \delta(f(x)) g(x) = \int_{x_i - \epsilon}^{x_i + \epsilon} dx \delta(f'(x_i)(x - x_i)) g(x) \quad (17)$$

$$= \int_{-\epsilon}^{\epsilon} dy \delta(f'(x_i)y) g(y + x_i) \quad (18)$$

$$= \int_{-\epsilon}^{\epsilon} dy \frac{1}{|f'(x_i)|} \delta(y) g(y + x_i) \quad (19)$$

$$= \frac{g(x_i)}{|f'(x_i)|} \quad (20)$$

Daraus folgt, dass

$$\int dx \delta(f(x)) g(x) = \sum_i \frac{g(x_i)}{|f'(x_i)|} \quad (21)$$

(d) (i) Es gilt

$$\lim_{\epsilon \rightarrow 0} f_\epsilon(x) = 0 \quad \text{für } x \neq 0 \quad (22)$$

und

$$\int_{-\infty}^{\infty} dx f_\epsilon(x) g(x) = \int_{-\epsilon}^{\epsilon} dx \frac{1}{2\epsilon} g(x) \quad (23)$$

$$= \int_{-\epsilon}^{\epsilon} dx \frac{1}{2\epsilon} [g(0) + g'(0)x + \dots] \quad (24)$$

$$= g(0) + \mathcal{O}(\epsilon^2) \xrightarrow{\epsilon \rightarrow 0} 0 \quad (25)$$

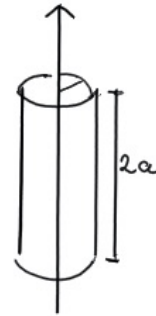
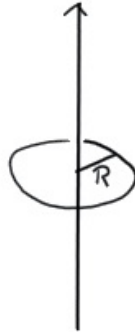
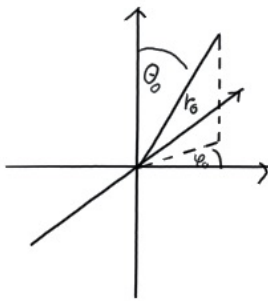


Abbildung 1: Ladungsverteilungen

(ii) Es gilt

$$\lim_{\epsilon \rightarrow 0} f_{\epsilon}(x) = \begin{cases} 0 & \text{für } x \neq 0 \\ \infty & \text{für } x = 0 \end{cases} \quad (26)$$

$$\int_{-\infty}^{\infty} dx f_{\epsilon}(x) g(x) = \int_{-\infty}^{\infty} dx \frac{1}{\sqrt{2\pi\epsilon}} e^{-\frac{x^2}{2\epsilon}} g(x) \quad (27)$$

$$= \int_{-\infty}^{\infty} dy \frac{1}{\sqrt{2\pi}} e^{-\frac{y^2}{2}} g(y\sqrt{\epsilon}) \quad (28)$$

$$\lim_{\epsilon \rightarrow 0} \int_{-\infty}^{\infty} dx f_{\epsilon}(x) g(x) = \lim_{\epsilon \rightarrow 0} \int_{-\infty}^{\infty} dy \frac{1}{\sqrt{2\pi}} e^{-\frac{y^2}{2}} g(y\sqrt{\epsilon}) \quad (29)$$

$$= g(0) \int_{-\infty}^{\infty} dy \frac{1}{\sqrt{2\pi}} e^{-\frac{y^2}{2}} \quad (30)$$

$$= g(0) \quad (31)$$

2. Lösung: Ladungsverteilungen

Kugelkoordinaten

$$\mathbf{x} = r \begin{pmatrix} \sin \theta \cos \phi \\ \sin \theta \sin \phi \\ \cos \theta \end{pmatrix} \quad d^3x = r^2 \sin \theta d\theta d\phi \quad (32)$$

Polarkoordinaten

$$\mathbf{x} = r \begin{pmatrix} \rho \cos \phi \\ \rho \sin \phi \\ z \end{pmatrix} \quad d^3x = \rho d\rho d\phi dz \quad (33)$$

(a)

$$\rho(\mathbf{x}) = N \cdot Q \cdot \delta(r - r_0) \delta(\phi - \phi_0) \delta(\theta - \theta_0) \quad (34)$$

Die Normierung N folgt aus:

$$Q = \int d^3x \rho(\mathbf{x}) \quad (35)$$

$$= \int dr d\theta d\phi r^2 \sin \theta \rho(r, \theta, \phi) \quad (36)$$

$$= \int d^3x \rho(\mathbf{x}) \quad (37)$$

$$= r_0^2 \sin \theta_0 \cdot N \cdot Q \quad (38)$$

$$\rightarrow N = \frac{1}{r_0^2 \sin \theta_0} \quad (39)$$

(b)

$$\rho(\mathbf{x}) = \frac{Q}{4\pi R^2} \delta(r - R) \quad (40)$$

Man erhält die Normierung wie in (a) mit

$$\int_0^\pi \int_0^{2\pi} \sin \theta d\theta d\phi = 4\pi \quad (41)$$

(c)

$$\rho(\mathbf{x}) = Q \cdot N \cdot \delta(z) \theta(R - r) \quad (42)$$

Die Normierung folgt aus:

$$\int dr d\phi dz \rho(r, \phi, z) r = \int_0^{2\pi} \int d\phi dr Q \cdot N \cdot \theta(R - r) r \quad (43)$$

$$= Q \cdot N \cdot \frac{R^2}{2} \cdot 2\pi \quad (44)$$

$$\rightarrow N = \frac{1}{R^2 \pi} \quad (45)$$

Hinweis:

$$\int dx \theta(x) x = \left[\theta(x) \frac{x^2}{2} \right] - \int dx \delta(x) \frac{x^2}{2} \quad (46)$$

$$= \frac{x^2}{2} \quad (47)$$

(d)

$$\rho(\mathbf{x}) = Q \cdot N \cdot \delta(r - b) \theta(a - |z|) \quad (48)$$

Normierung folgt aus:

$$Q = \int dr d\phi dz r \rho(r, \phi, z) \quad (49)$$

$$= b \int_0^{2\pi} \int_{-\infty}^{\infty} d\phi dz Q \cdot N \cdot \theta(a - |z|) \quad (50)$$

$$= b \cdot 2\pi \cdot Q \cdot N \cdot 2a \quad (51)$$

3. Lösung: Radialfeld

(a)

$$\partial_r = \frac{\partial x}{\partial r} \partial_x + \frac{\partial y}{\partial r} \partial_y + \frac{\partial z}{\partial r} \partial_z \quad (52)$$

$$= \sin \theta \cos \phi \partial_x + \sin \theta \sin \phi \partial_y + \cos \theta \partial_z \quad (53)$$

$$\frac{1}{r} \partial_\theta = \frac{1}{r} \left(\frac{\partial x}{\partial \theta} \partial_x + \frac{\partial y}{\partial \theta} \partial_y + \frac{\partial z}{\partial \theta} \partial_z \right) \quad (54)$$

$$= \cos \theta \cos \phi \partial_x + \cos \theta \sin \phi \partial_y - \sin \theta \partial_z \quad (55)$$

$$\frac{1}{r \sin \theta} \partial_\phi = \frac{1}{r \sin \theta} \left(\frac{\partial x}{\partial \phi} \partial_x + \frac{\partial y}{\partial \phi} \partial_y + \frac{\partial z}{\partial \phi} \partial_z \right) \quad (56)$$

$$= -\sin \phi \partial_x + \cos \phi \partial_y \quad (57)$$

Wenn wir nun die Einheitsvektoren der Kugelkoordinaten in kartesischen Einheitsvektoren ausdrücken folgt:

$$\hat{\mathbf{e}}_r \partial_r + \frac{1}{r} \hat{\mathbf{e}}_\theta \partial_\theta + \frac{1}{r \sin \theta} \hat{\mathbf{e}}_\phi \partial_\phi \quad (58)$$

$$\begin{aligned} &= [\sin \theta \cos \phi \hat{\mathbf{e}}_x + \sin \theta \sin \phi \hat{\mathbf{e}}_y + \cos \theta \hat{\mathbf{e}}_z] (\sin \theta \cos \phi \partial_x + \sin \theta \sin \phi \partial_y + \cos \theta \partial_z) \\ &\quad + [\cos \theta \cos \phi \hat{\mathbf{e}}_x + \cos \theta \sin \phi \hat{\mathbf{e}}_y - \sin \theta \hat{\mathbf{e}}_z] (\cos \theta \cos \phi \partial_x + \cos \theta \sin \phi \partial_y - \sin \theta \partial_z) \\ &\quad + [-\sin \phi \hat{\mathbf{e}}_x + \cos \phi \hat{\mathbf{e}}_y] (-\sin \phi \partial_x + \cos \phi \partial_y) \end{aligned} \quad (59)$$

$$\begin{aligned} &= [\sin^2 \theta \cos^2 \phi + \cos^2 \theta \cos^2 \phi + \sin^2 \phi] \hat{\mathbf{e}}_x \partial_x \\ &\quad + [\sin^2 \theta \sin^2 \phi + \cos^2 \theta \sin^2 \phi + \cos^2 \phi] \hat{\mathbf{e}}_y \partial_y \\ &\quad + [\cos^2 \theta + \sin^2 \theta] \hat{\mathbf{e}}_z \partial_z \\ &\quad + [\sin \theta \cos \theta \cos \phi - \sin \theta \cos \theta \cos \phi] (\hat{\mathbf{e}}_x \partial_z + \hat{\mathbf{e}}_z \partial_x) \\ &\quad + [\sin \theta \cos \theta \sin \phi - \sin \theta \cos \theta \sin \phi] (\hat{\mathbf{e}}_y \partial_z + \hat{\mathbf{e}}_z \partial_y) \\ &\quad + [\sin^2 \theta \cos \phi \sin \phi + \cos^2 \theta \cos \phi \sin \phi + \sin \phi \cos \phi] (\hat{\mathbf{e}}_x \partial_y + \hat{\mathbf{e}}_y \partial_x) \end{aligned} \quad (60)$$

$$= \hat{\mathbf{e}}_x \partial_x + \hat{\mathbf{e}}_y \partial_y + \hat{\mathbf{e}}_z \partial_z \quad (61)$$

(b) Um die Rotation des Vektorfeldes auszurechnen benötigen wir die Ableitung von $\hat{\mathbf{e}}_r$.

$$\partial_r \hat{\mathbf{e}}_r = 0 \quad (62)$$

$$\partial_\theta \hat{\mathbf{e}}_r = \hat{\mathbf{e}}_\theta \quad (63)$$

$$\partial_\phi \hat{\mathbf{e}}_r = \sin \theta \hat{\mathbf{e}}_\phi \quad (64)$$

$$\nabla \times \mathbf{V} = (\hat{\mathbf{e}}_r \partial_r + \frac{1}{r} \hat{\mathbf{e}}_\theta \partial_\theta + \frac{1}{r \sin \theta} \hat{\mathbf{e}}_\phi \partial_\phi) \times V_r \hat{\mathbf{e}}_r \quad (65)$$

$$\begin{aligned} &= \hat{\mathbf{e}}_r \times (\hat{\mathbf{e}}_r \partial_r V_r + V_r \partial_r \hat{\mathbf{e}}_r) + \frac{1}{r} \hat{\mathbf{e}}_\theta \times (\hat{\mathbf{e}}_r \partial_\theta V_r + V_r \partial_\theta \hat{\mathbf{e}}_r) \\ &\quad + \frac{1}{r \sin \theta} \hat{\mathbf{e}}_\phi \times (\hat{\mathbf{e}}_r \partial_\phi V_r + V_r \partial_\phi \hat{\mathbf{e}}_r) \end{aligned} \quad (\text{Produktregel}) \quad (66)$$

$$\begin{aligned} &= \hat{\mathbf{e}}_r \times (\hat{\mathbf{e}}_r \partial_r V_r + 0) + \frac{1}{r} \hat{\mathbf{e}}_\theta \times (\hat{\mathbf{e}}_r \partial_\theta V_r + V_r \hat{\mathbf{e}}_\theta) \\ &\quad + \frac{1}{r \sin \theta} \hat{\mathbf{e}}_\phi \times (\hat{\mathbf{e}}_r \partial_\phi V_r + V_r \sin \theta \hat{\mathbf{e}}_\phi) \end{aligned} \quad (\text{Ableitung } \hat{\mathbf{e}}_r) \quad (67)$$

$$= \frac{1}{r} \hat{\mathbf{e}}_\theta \times \hat{\mathbf{e}}_r \partial_\theta V_r + \frac{1}{r \sin \theta} \hat{\mathbf{e}}_\phi \times \hat{\mathbf{e}}_r \partial_\phi V_r \quad \mathbf{a} \times \mathbf{a} = 0 \quad (68)$$

$$= -\frac{\partial_\theta V_r}{r} \hat{\mathbf{e}}_\phi + \frac{\partial_\phi V_r}{r \sin \theta} \hat{\mathbf{e}}_\theta \quad (69)$$

Während in unserem Spezialfall die meisten Terme verschwinden, lautet die allgemeine Form der Rotation in Kugelkoordinaten:

$$\nabla \times \mathbf{V} = \frac{1}{r \sin \theta} \left(\frac{\partial}{\partial \theta} (V_\phi \sin \theta) - \frac{\partial V_\theta}{\partial \phi} \right) \mathbf{e}_r + \frac{1}{r} \left(\frac{1}{\sin \theta} \frac{\partial V_r}{\partial \phi} - \frac{\partial}{\partial r} (r V_\phi) \right) \mathbf{e}_\theta + \frac{1}{r} \left(\frac{\partial}{\partial r} (r V_\theta) - \frac{\partial V_r}{\partial \theta} \right) \mathbf{e}_\phi$$