ENGG102 Fundamentals of Engineering Mechanics

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UNIVERSITY OF WOLLONGONG



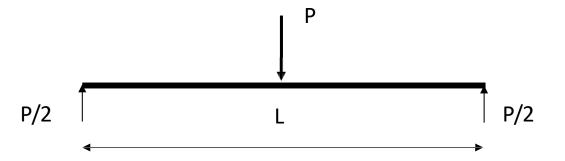
Outline:

- 1. Recap on last lecture
- 2. Revision of Internal Forces in Structural Members
- Shear and Bending Moment Equations and Diagrams
- 4. Relationship between Shear and Bending Moment



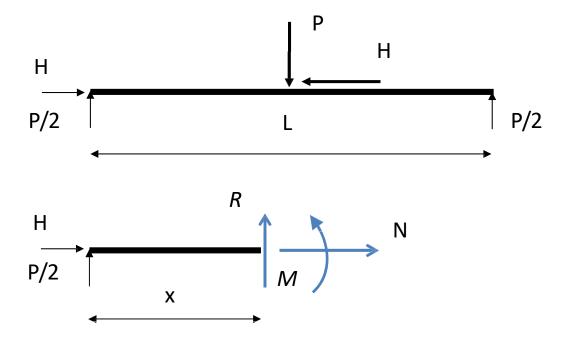
Recap on Lecture 3

- Making FBD of part of the beam
- Allows us to determine INTERNAL forces and moments





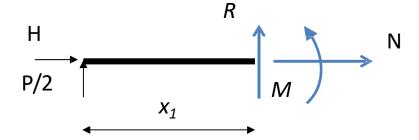
General Case



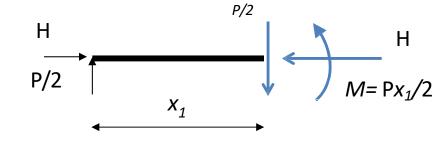
- When we cut a solid beam element we replace the right hand part by THREE actions
- Axial Force, Moment and a transverse force R



Solving FBD

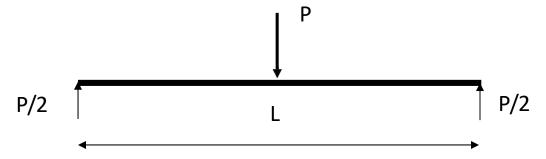


- $\Sigma F_x = 0$: H + N = 0 implies N = -H
- $\Sigma F_v = 0$: P/2 + R = 0 implies R = -P/2
- $\Sigma M_{x1} = 0$: $-(P/2).x_1 + M = 0$ implies $M = Px_1/2$
- The N and R arrows are in the incorrect sense
- M is correct
- Final FBD

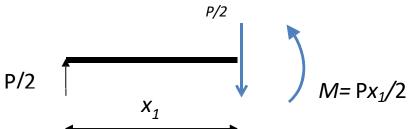




Our Balsa Beam

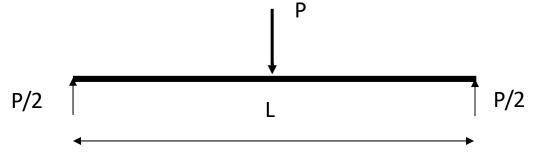


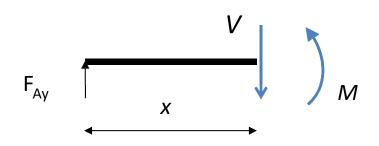
- $\Sigma F_x = 0$: H = N = 0
- $\Sigma F_v = 0$: P/2 + R = 0 implies R = -P/2
- $\Sigma M_{x1} = 0$: $-(P/2).x_1 + M = 0$ implies $M = Px_1/2$
- Final FBD
- At $x_1 = L/2$
- M = PL/4





General FBD for Beam with point load

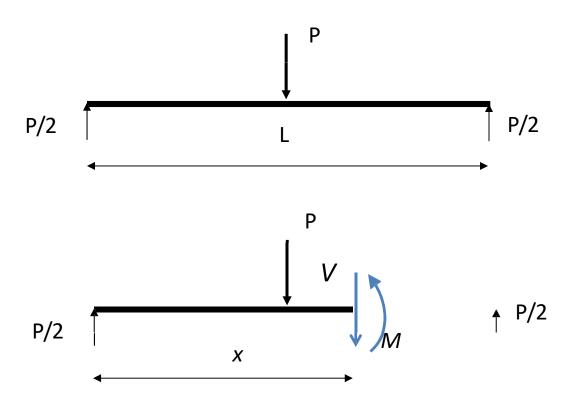




We have a special name for the internal moment: We call it the BENDING MOMENT because it makes the beam bend

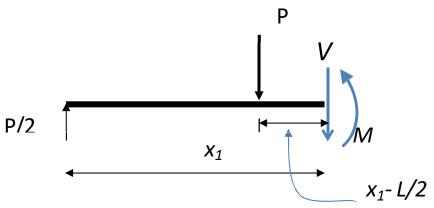


What if we made out cut to right of P?





What if we made out cut to right of P?



- $\Sigma F_x = 0$: N = 0
- $\Sigma F_v = 0$: P/2 P V = 0 implies V = -P/2 (direction wrong)
- $\Sigma M_{x1} = 0$: $-(P/2).x_1 + P(x_1-L/2) + M = 0$

implies
$$M = PL/2 - Px_1/2$$
 Note When $x_1 = L/2$ $M = PL/2-PL/4 = PL/4$

• These equations are true $\forall x \in [L/2 < x \le L]$



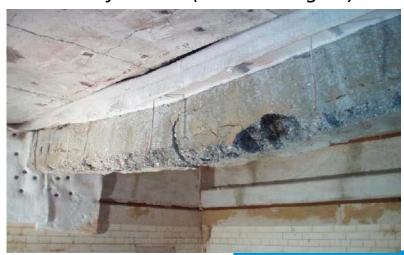
Bending Moment Diagram is **important** because:

- 1. Failure occurs where the bending moment is maximum
- 2. Deflection can be predicted by means of bending moment diagrams

Beam failure from bending under snow overload.



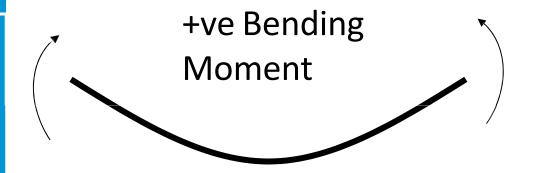
Beam failure – (in middle again)



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www.structurearchives.org

Sign convention for **Bending Moment Diagram**:



Sagging moment

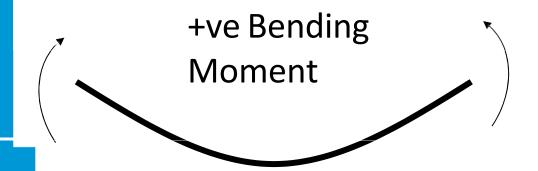
BMD is always a pair of equal but opposite moments



Hogging moment



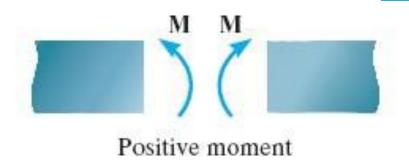
You should not confuse the sign convention for Bending Moment Diagram with the sign convention in equilibrium equations.



Sagging moment

In equilibrium equations, the left end moment is normally considered negative as it has a clockwise direction.

In the textbook:

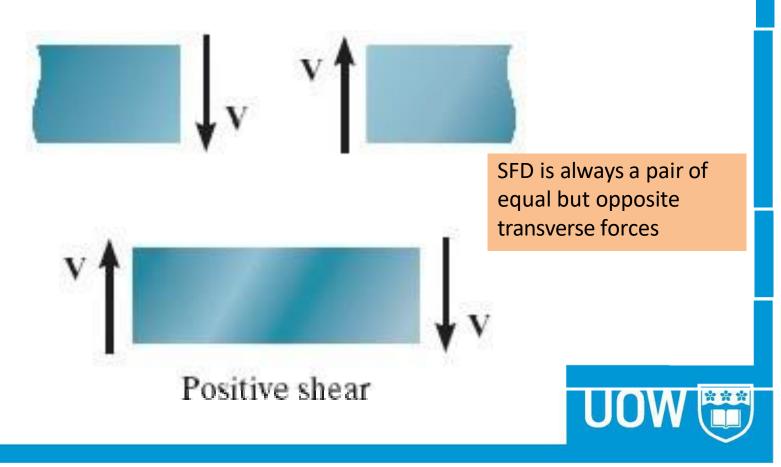


Sagging moment





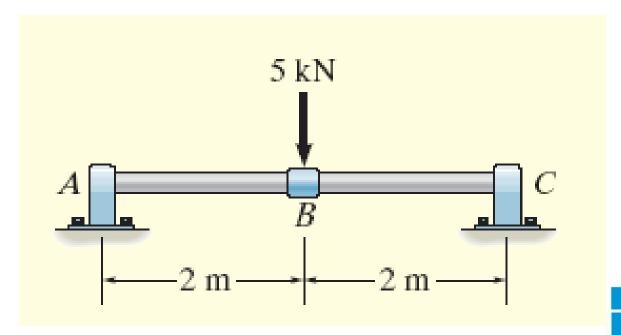
Sign convention for **Shear Force Diagram**:





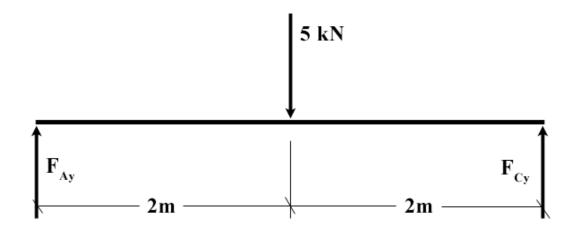
In equilibrium equations, the right end shear force is normally considered negative as it has a downward direction.

Draw the shear and bending moments diagrams for the shaft. The supports at A and C do not resist any moment.





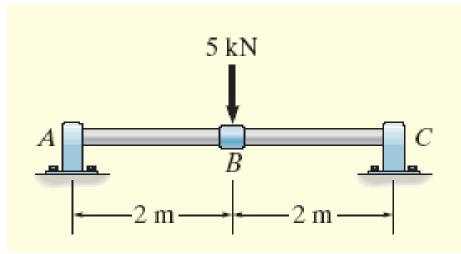
Draw free body diagram and calculate reactions:

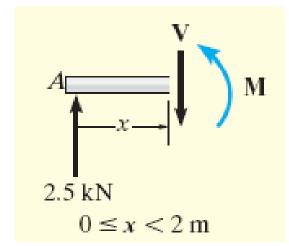


$$\Sigma M_A = -(5 \text{ kN})(2 \text{ m}) + F_{Cy}(4 \text{ m}) = 0$$
: $F_{Cy} = 2.5 \text{ kN} (\uparrow)$

$$\Sigma F_{V} = F_{AV} - 5 \text{ kN} + F_{CV} = 0$$
: $F_{AV} = 2.5 \text{ kN} (\uparrow)$







We can also see that due to symmetry, the vertical reaction at A must be half the applied load, i.e. 2.5 kN upwards.

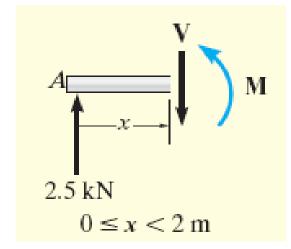
Looking at the FBD above for $0 \le x < 2$ m:

$$\sum F_{y} = 2.5 \text{ kN} - V = 0 \Rightarrow V = 2.5 \text{ kN}(\downarrow)$$



$$\sum F_y = 2.5 \text{ kN} - V = 0 \Rightarrow V = 2.5 \text{kN}(\downarrow)$$

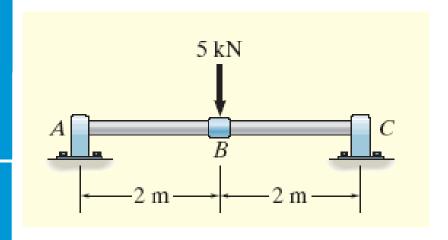


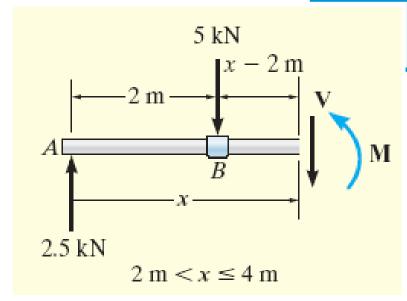


Note: When adding all the forces we do not include M – because it is not a force!

For $0 \le x < 2$ m, i.e. between A and B, the internal shear force diagram is *positive*.







For 2 m < $x \le 4$ m, i.e. between B and C:

$$\sum F_{v} = 2.5 \text{ kN} - 5 \text{ kN} - V = 0 \Rightarrow V = -2.5 \text{ kN}(\uparrow)$$

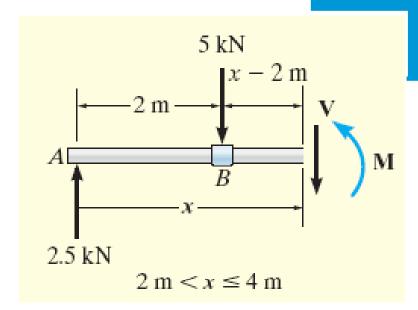


For 2 m < $x \le 4$ m:

$$\sum F_y = 2.5 \text{ kN} - 5 \text{ kN} - V = 0$$

$$V = -2.5 \text{ kN}(\uparrow)$$



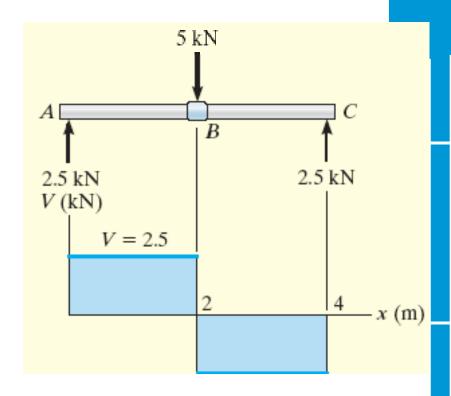


For 2 m < $x \le 4$ m, i.e. between B and C, the internal shear force diagram is *negative*.



For $0 \le x < 2$ m, i.e. between A and B, the internal shear force diagram is positive.

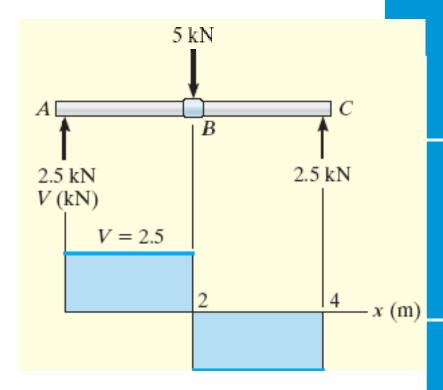
For 2 m $< x \le 4$ m, i.e. between B and C, the internal shear force diagram is negative.



Shear Force Diagram

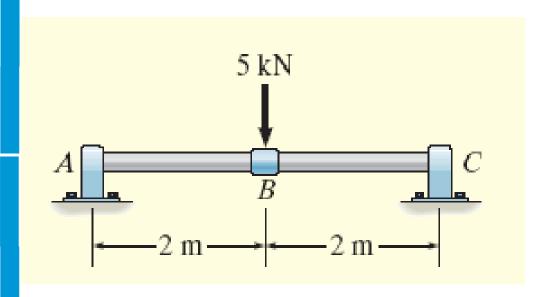


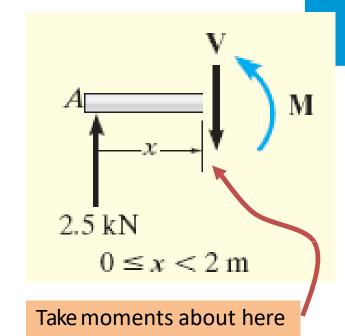
Note that, at B, the internal shear force abruptly changes from 2.5 k to -2.5 k, i.e. by the amount of the applied load of -5.0 kN.



Shear Force Diagram







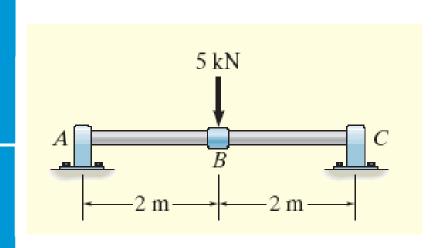
For $0 \le x < 2$ m, i.e. between A and B:

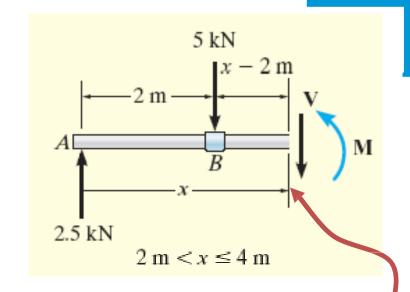
$$\sum M_x = -2.5 \text{ kN}(x) + M = 0 \Rightarrow M = 2.5x \text{ kN.m}$$

Note: When adding up the moments, forces times distance = moment. We must add in M at the cut because it is one of the moments in the diagram



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For 2 m < $x \le 4$ m:

Take moments about here

$$\sum M_x = M + 5 \text{ kN}(x - 2\text{m}) - 2.5 \text{ kN}(x) = 0$$

 $M = (10 - 2.5x) \text{ kN.m}$

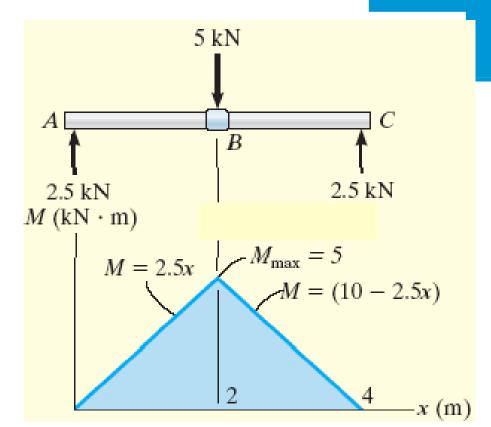


For $0 \le x < 2$ m, i.e. between A and B:

•

For 2 m < $x \le 4$ m, i.e. between B and C:

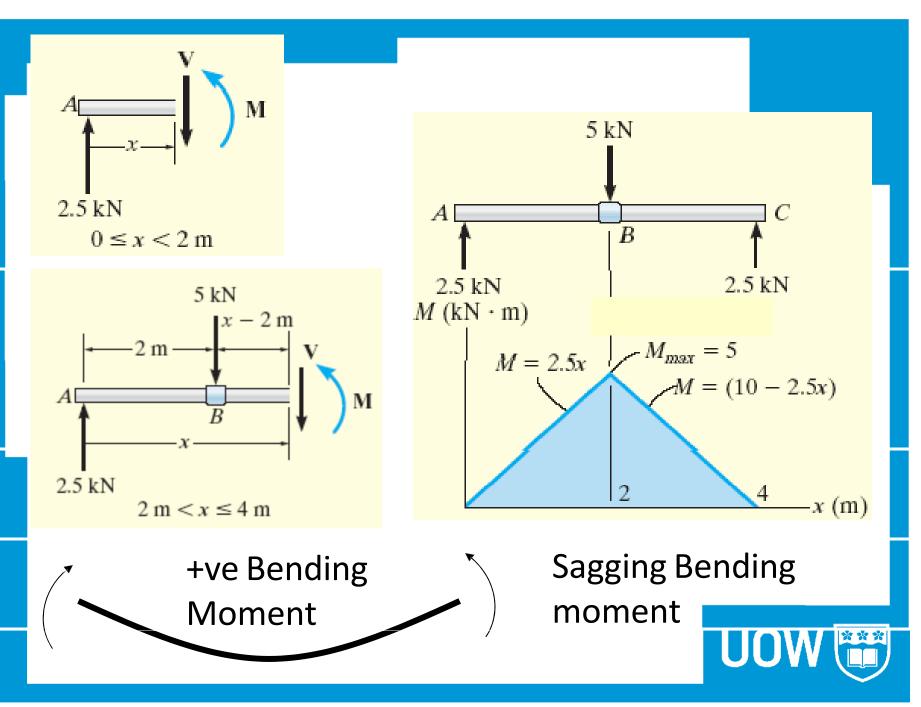
$$M = (10 - 2.5x) \text{ kN.m}$$



+ve Bending
Moment

Sagging Bending moment

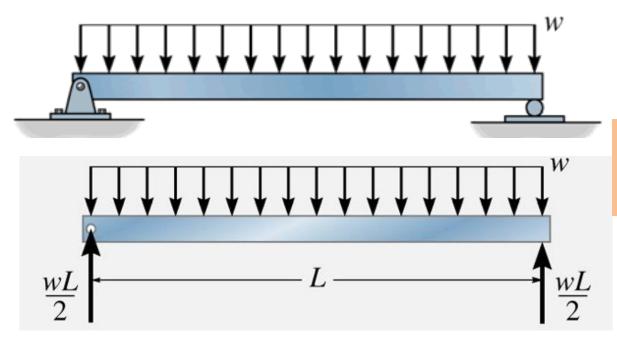




Shear and Bending Moment Equations and Diagrams In practice, beams are commonly subject to distributed loads.



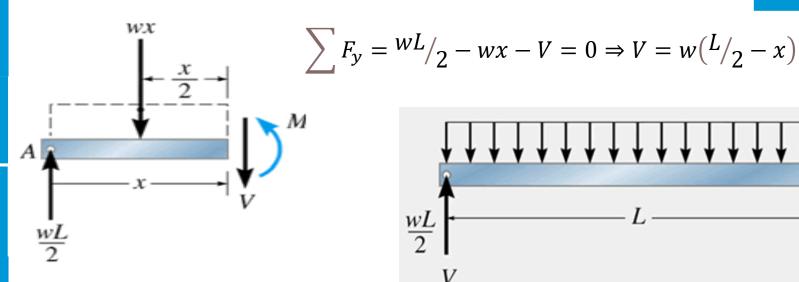




Units for w are usually N/m or kN/m

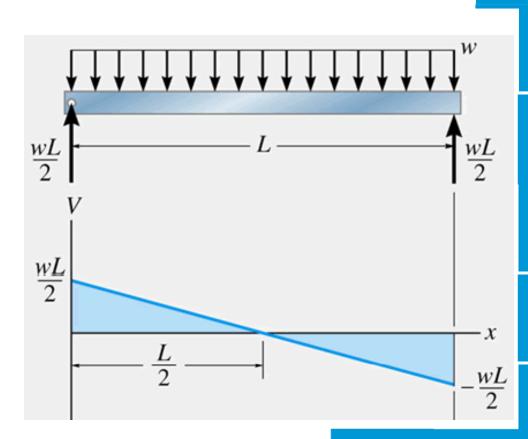
Due to symmetry, we know that the vertical reaction at A must be half the applied load, i.e. $w^L/_2$ upwards.



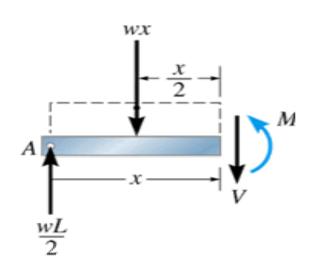




Shear Force Diagram

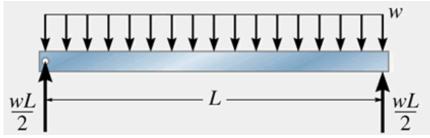






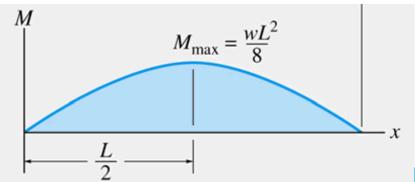
$$\sum M_x = -\frac{wL}{2}(x) + wx\left(x/2\right) + M = 0$$

$$M = \frac{w}{2} \left(Lx - x^2 \right)$$



Sagging moment

+ve Moment



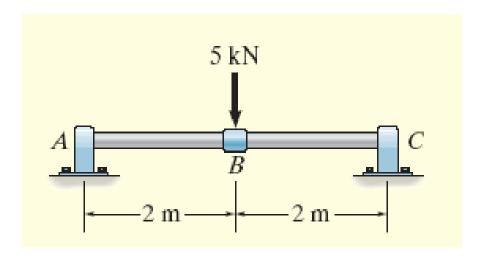


Bending moment diagram calculators

http://beamguru.com/online/beam-calculator/
https://bendingmomentdiagram.com/free-calculator/

NOT allowed in exams/quizzes.





For $0 \le x < 2$ m (between A and B):

$$M = 2.5x \text{ kN.m}$$

$$V = 2.5 \text{ kN}$$

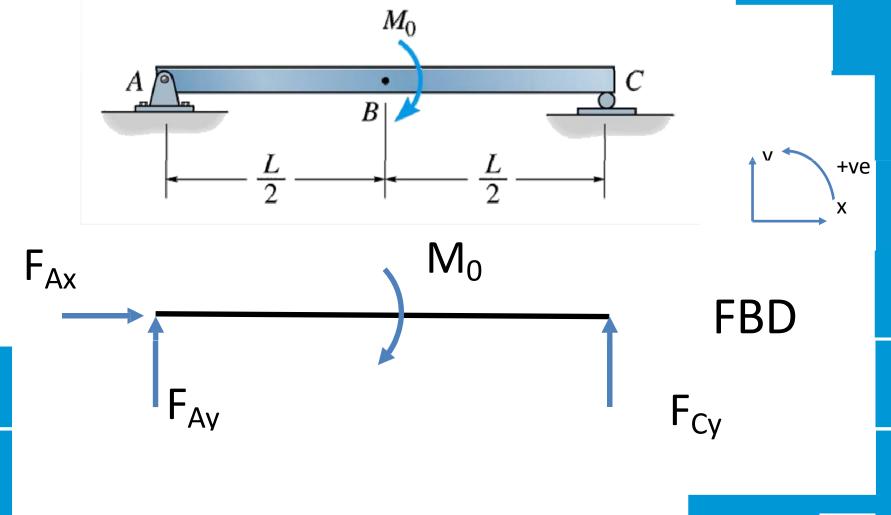
For 2 m < $x \le 4$ m (between B and C):

$$M = (10 - 2.5x)$$
kN.m

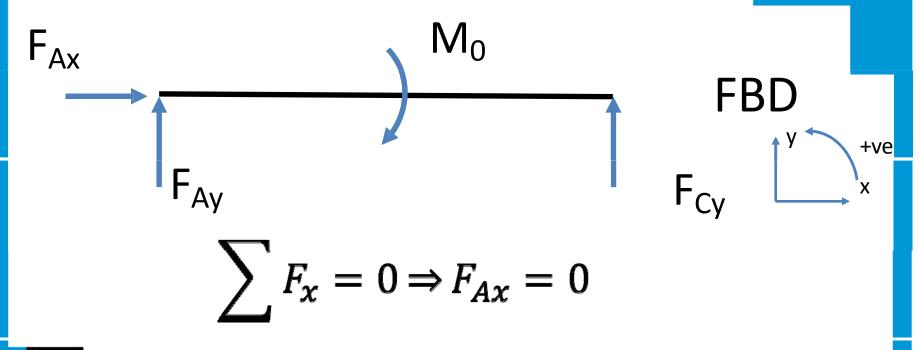
$$V = -2.5 \text{ kN}$$

Notice any pattern between V and M equations?



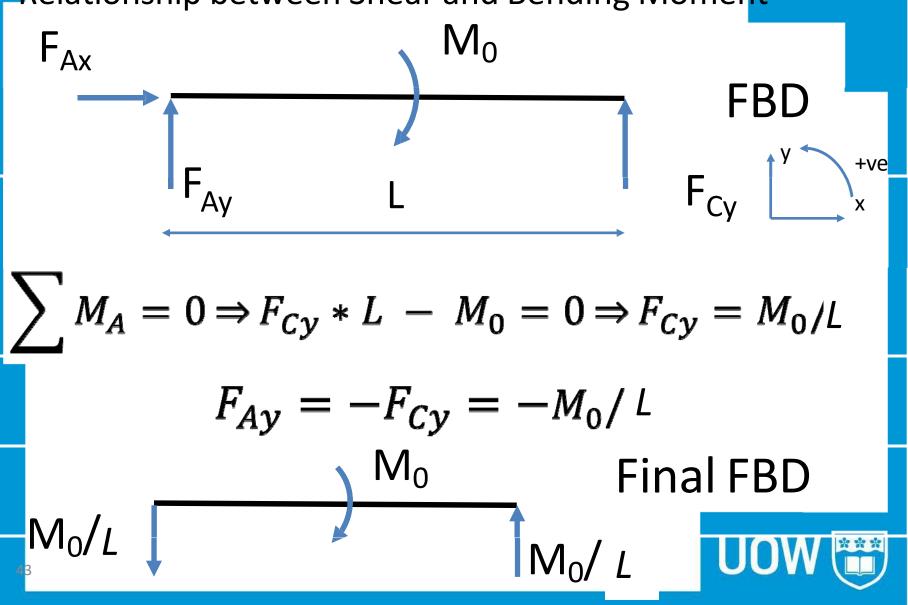


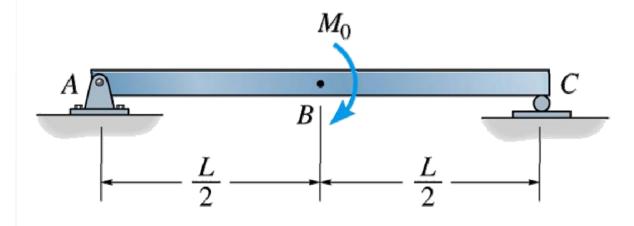




$$\sum_{A} F_{y} = 0 \Rightarrow F_{Ay} + F_{Cy} = 0 \Rightarrow F_{Ay} = -F_{Cy}$$







For $0 \le x < \frac{L}{2}$ (between A and B):

$$M = -\frac{M_o x}{L}$$

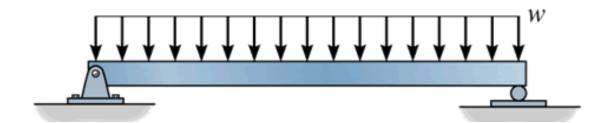
$$V = {M_o/L}$$

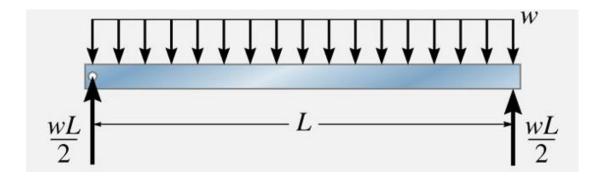
For $L/2 < x \le L$ (between B and C): $M = M_o(1 - x/L)$

$$M = M_o (1 - x/L)$$

$$V = -\frac{M_o}{L}$$







$$M = \frac{w}{2} \left(Lx - x^2 \right)$$

$$V = w(L/2 - x) = \frac{w}{2}(L - 2x)$$



Do you notice a pattern?

$$M = 2.5x \text{ kN.m}$$
 $M = (10 - 2.5x) \text{ kN.m}$
 $V = 2.5 \text{ kN}$ $V = -2.5 \text{ kN}$

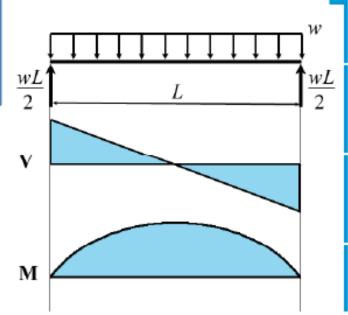
$$M = -\frac{M_0 x}{L} \qquad M = M_0 \left(1 - \frac{x}{L}\right)$$

$$V = -\frac{M_0}{L} \qquad V = -\frac{M_0}{L}$$

$$M = \frac{w}{2} (Lx - x^2)$$

$$V = w \left(\frac{L}{2} - x \right)$$

$$V = w \left(\frac{L}{2} - x \right)$$





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07_PH05

In order to design the beam used to support these power lines, it is important to first draw the shear and moment diagrams for the beam.

YOUR Beam: stress and strength

FAST FORWARD TO SECOND YEAR ENGG251

- Maximum tensile stress allowed in BALSA is for you to find
- In this case the beam will break (mostly) because it is bending
- In that case stress on the bottom fibres in the middle will be $\sigma_{\rm max} = M_{\rm max} h/(2I)$

