ENGG102 Fundamentals of Engineering Mechanics

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ENGG102

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Outline

- Characteristics of Dry Friction
- Problems Involving Dry Friction

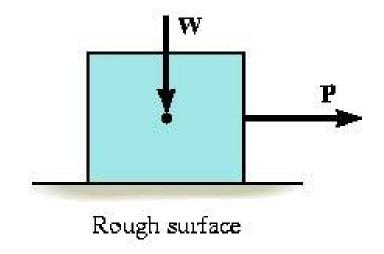
Friction: resistive force against movement

- or retards slipping of the body relative to a second body or surface which it is in contact
- Acts tangent to the surfaces at points of contact with other body
- Opposing possible or existing motion of the body relative to points of contact
- Two types of friction Fluid and Coulomb Friction

- Fluid friction exist when the contacting surfaces are separated by a film of fluid (gas or liquid); <u>parallel plates with fluid in between</u>
- Depends on velocity of the fluid and its ability to resist shear force
- Coulomb friction, also known as dry friction, occurs between contacting surfaces of bodies in the absence of a lubricating fluid

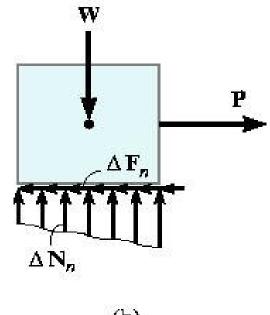
Theory of Dry Friction

- Consider the effects caused by pulling horizontally on a block of uniform weight W which is resting on a rough horizontal surface
- Consider the surfaces of contact to be nonrigid or deformable and other parts of the block to be rigid



Theory of Dry Friction

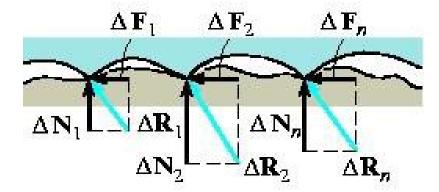
- FBD of the block
- The floor exerts a distribution of the normal force ΔN_n and frictional force ΔF_n along the contact surface



(b)

Theory of Dry Friction

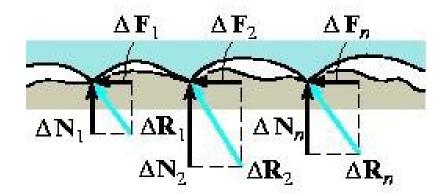
- Examining the contacting surfaces between the floor and the block, it can seen that many microscopic irregularities exist between the two surfaces
- Reactive forces $\Delta \mathbf{R}_n$ developed at each of the protuberances



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Theory of Dry Friction

• These forces act at all points of contact and each reactive force consist of both a frictional component $\Delta \mathbf{F}_n$ and a normal component $\Delta \mathbf{N}_n$

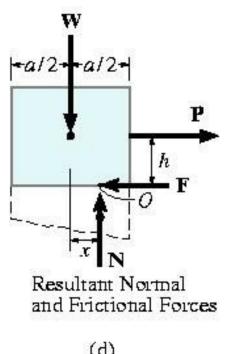


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Theory of Dry Friction

<u>Equilibrium</u>

- Effect of normal and frictional loadings are indicated by their resultant N and F
- Distribution of $\Delta \mathbf{F}_n$ indicates that \mathbf{F} is tangent to the contacting surface, opposite to the direction of **P**
- Normal force N is determined from the distribution of ΔN_n

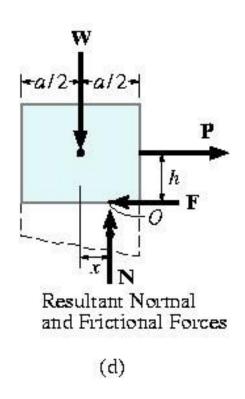


(d)

Theory of Dry Friction

Example

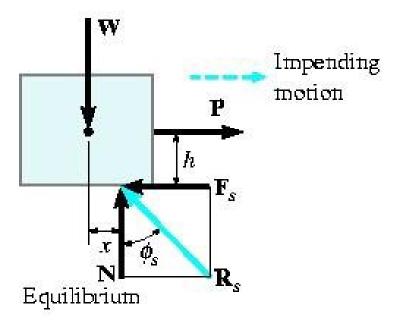
- P is applied at a height h from the surface
- Moment equilibrium about point O is satisfied if W x = Ph or x = Ph/W
- The block is on the verge of tipping if N acts at the right corner of the block, x = a/2



Theory of Dry Friction

 Limiting static frictional force F_s is directly proportional to the resultant normal force N

$$F_s = \mu_s N$$



(e)

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Theory of Dry Friction

- Constant of proportionality μ_s is known as the coefficient of static friction
- When the block is on the verge of sliding, the normal force ${\bf N}$ and the frictional force ${\bf F}_s$ combine to form a resultant ${\bf R}_s$
- Angle Φ_s that \mathbf{R}_s makes with \mathbf{N} is called the angle of static friction

$$\phi_s = \tan^{-1}\left(\frac{F_s}{N}\right) = \tan^{-1}\left(\frac{\mu_s N}{N}\right) = \tan^{-1}\mu_s$$

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Theory of Dry Friction (Project 2)

Typical Values of μ_s	Coefficient of Static
Contact Materials	Friction µ _s
Metal on ice	0.03 - 0.05
Wood on wood	0.30 - 0.70
Leather on wood	0.20 - 0.50
Leather on metal	0.30 - 0.60
Aluminum on aluminum	

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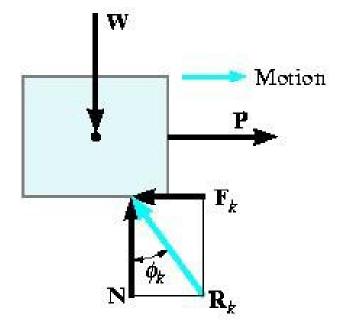
Theory of Dry Friction

Motion

• If the magnitude of <u>P acting</u> on the block is increased so that it is greater than F_s , the frictional force at the

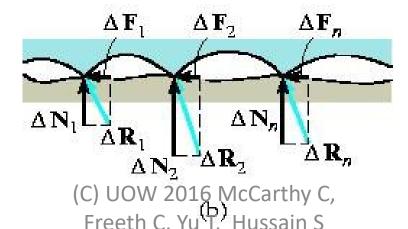
contacting surfaces drops slightly to a smaller value F_s, called **kinetic** frictional force

 The block will not be held in equilibrium (P > F_s) but slide with increasing speed



Theory of Dry Friction: why $F_k < F_s$?

- The <u>reduction made in the frictional force magnitude</u>, from F_s (static) to F_k (kinetic), can by explained by examining the contacting surfaces
- When P > F_s, P has the <u>capacity to shear off the peaks</u> at the <u>contact surfaces</u>, causing the blocks to lift and ride on top of these peaks



Theory of Dry Friction

 Resultant frictional force F_k is directly proportional to the magnitude of the resultant normal force N

$$F_k = \mu_k N$$

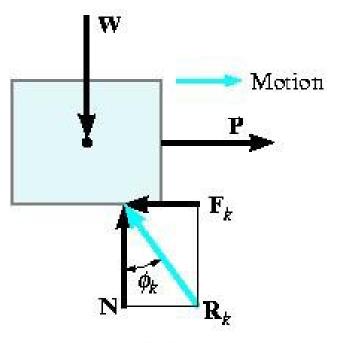
- Constant of proportionality μ_k is called the coefficient of kinetic friction
- μ_k are typically 25% smaller than μ_s

Theory of Dry Friction

• Resultant \mathbf{R}_k has a line of action defined by Φ_k , angle of kinetic friction

$$\phi_k = \tan^{-1}\left(\frac{F_k}{N}\right) = \tan^{-1}\left(\frac{\mu_k N}{N}\right) = \tan^{-1}\mu_k$$

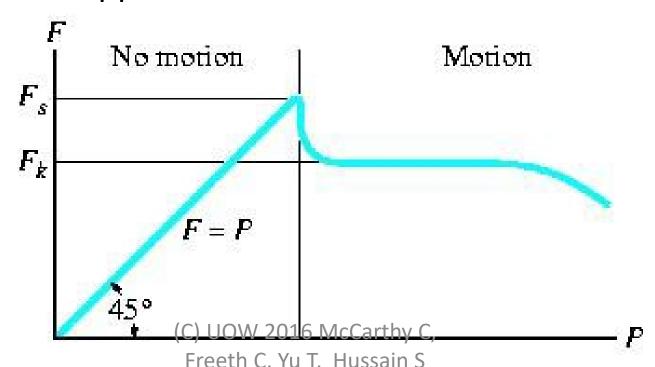
• $\Phi_s \ge \Phi_k$



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Theory of Dry Friction

 The graph summarizes the effects regarding friction and shows the variation of frictional force F versus applied load P

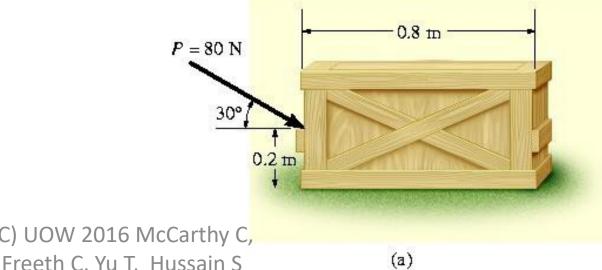


Theory of Dry Friction

- Frictional force is categorized into three ways
 - -<u>F is a static-frictional</u> force if equilibrium is maintained
 - -<u>F is a limiting static-frictional</u> force F_s when it reaches the <u>maximum value</u> needed to maintain equilibrium
 - <u>F is a kinetic-frictional</u> force F_k when sliding occurs at the contact surface

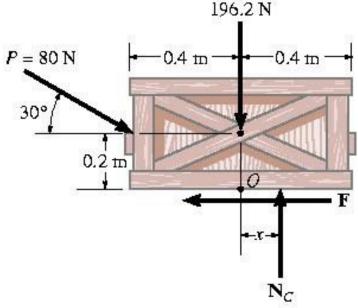
Example 1

The uniform crate has a mass of 20kg. If a force P = 80N is applied on to the crate, <u>determine</u> if it remains in equilibrium. The coefficient of static friction is $\mu = 0.3$.



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- Resultant normal force Nc act a distance x from the crate's center line in order to counteract the tipping effect caused by P
- 3 unknowns to be determined by 3 equations of equilibrium



Solution

$$+ \rightarrow \sum F_x = 0;$$

$$80\cos 30^{\circ} - F = 0$$

$$+\uparrow\sum F_{y}=0;$$

$$-80\sin 30^{\circ} + N_C - 196.2 = 0$$

$$\sum M_O = 0;$$

$$80\sin 30^{\circ} (0.4m) - 80\cos 30^{\circ} (0.2m) + N_C(x) = 0$$

Solving

$$F = 69.3N, Nc = 236N, x = -0.00908 = -9.08mm$$

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Solution

- Since x is negative, the resultant force acts (slightly) to the left of the crate's center line
- No tipping will occur since $x \le 0.4$ m
- Maximum frictional force which can be developed at the surface of contact

$$F_{\text{max}} = \mu_s N_C = 0.3(236N) = 70.8N$$

 Since F = 69.3N < 70.8N, the crate will not slip although it is close to doing so

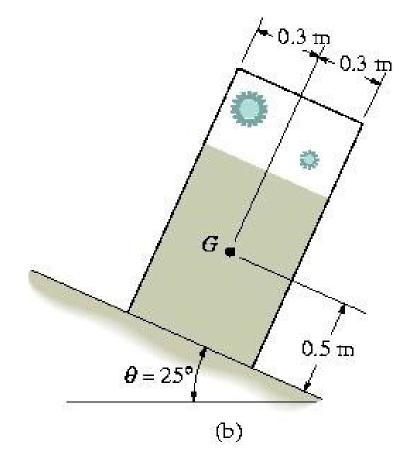
Example 2

It is observed that when the bed of the dump truck is raised to an angle of $\theta = 25^{\circ}$ the vending machines begin to slide off the bed. Determine the static of coefficient of friction between them and the surface of the truck

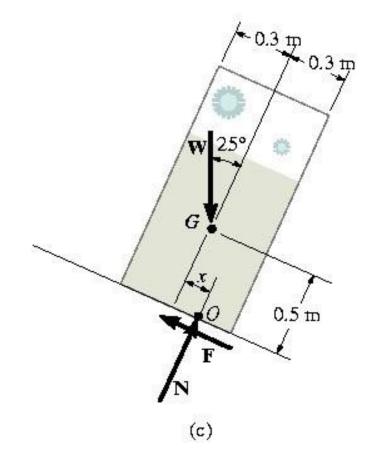


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- Idealized model of a vending machine lying on the bed of the truck
- Dimensions measured and center of gravity located
- Assume machine weighsW



- Dimension x used to locate position of the resultant normal force
 N
- 4 unknowns



$$\sum F_x = 0;$$

$$W \sin 25^\circ - F = 0$$

$$\sum F_y = 0;$$

$$N - W \cos 25^\circ = 0$$

$$\sum M_o = 0; \text{ (if checking for tipping)}$$

$$-W \sin\theta (0.5m) + W \cos\theta (x) = 0$$
Slipping occurs at $\theta = 25^\circ$

$$F_s = \mu_s N; \quad W \sin 25^\circ = \mu_s (W \cos 25^\circ) \quad ; \quad \mu_s = \tan 25^\circ = 0.466$$

- Angle $\theta = 25^{\circ}$ is referred as the angle of repose
- By comparison, $\theta = \Phi_s$
- θ is independent of the weight of the vending machine so knowing θ provides a method for finding coefficient of static friction
- $\theta = 25^{\circ}$, x = 0.233m
- Since 0.233m < 0.3m the vending machine will slip before it can tip as observed

Example 3

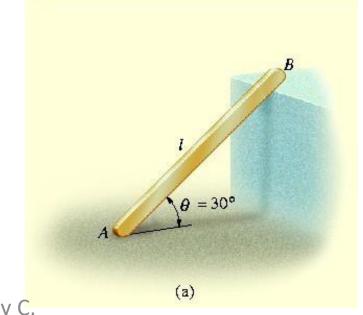
The uniform rod having a weight of W and length I is supported at its ends against the surfaces A and B. If the rod is

on the <u>verge of slipp</u>ing when

 $\theta = 30^{\circ}$, determine the coefficient

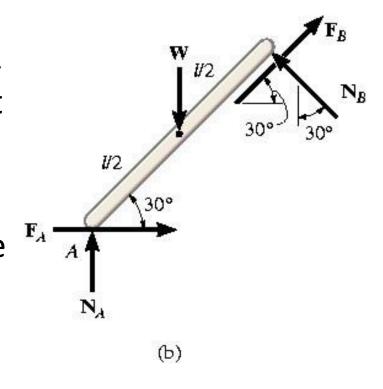
of static friction μ_s at A and B.

Neglect the thickness of the rod for calculation.



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- 5 unknowns
- 3 equilibrium equations and 2 frictional equations applied at A and B
- Frictional forces must be drawn with their correct sense so that they oppose the tendency for motion of the rod



Solution

Frictional equations

$$F = \mu_s N;$$

$$F_A = \mu_s N_A$$
, $F_B = \mu_s N_B$

Equilibrium equations

$$+ \rightarrow \sum F_x = 0;$$

$$\mu_s N_A + \mu_s N_B \cos 30^{\circ} - N_B \sin 30^{\circ} = 0$$

$$+\uparrow \sum F_{y}=0;$$

$$N_A - W + N_B \cos 30^\circ + \mu_s N_B \sin 30^\circ = 0$$

$$\sum M_A = 0;$$

$$N_B \ell - W\left(\frac{\ell}{2}\right) \cos 30^\circ = 0$$

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Solution

Solving

$$N_B = 0.4330W$$

$$\mu_s N_A = 0.2165W - (0.3750W)\mu_s$$

$$N_A = 0.6250W - (0.2165W)\mu_s$$

By division

$$0.6250\mu_s - 0.2165\mu_s^2 = 0.2165 - 0.375\mu_s$$
$$\mu_s^2 - 4.619\mu_s + 1 = 0$$

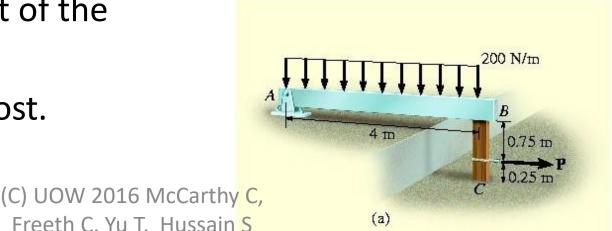
Solving for the smallest root

$$\mu_{s} = 0.228$$

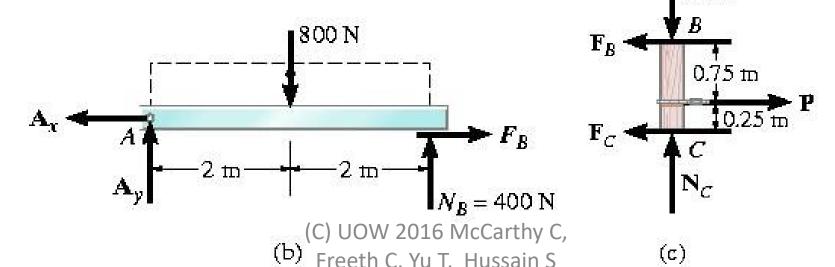
Example 4

Beam AB is subjected to a uniform load of 200N/m and is supported at B by post BC. If the coefficients of static friction at B and C are μ_B =0.2 and μ_C = 0.5, determine the force **P** needed to pull the post out from under the beam.

Neglect the weight of the members and the thickness of the post.



- FBD of beam AB and the post
- Apply $\sum M_A = 0$, $N_B = 400N$
- 4 unknowns
- 3 equilibrium equations and 1 frictional equation applied at either B or C



Solution

$$+ \rightarrow \sum F_x = 0; \qquad P - F_B - F_C = 0$$

$$+ \uparrow \sum F_y = 0; \qquad N_C - 400N = 0$$

$$\sum M_c = 0; \quad -P(0.25m) + F_B(1m) = 0$$
Post cline only at P

Post slips only at B

$$F_C \le \mu_C N_C$$

 $F_B = \mu_B N_B; F_B = 0.2(400N) = 80N$

Solving

$$P = 320N, F_C = 240N, N_C = 400N$$

 $F_C = 240N > \mu_C N_C = 0.5(400N) = 200N$ (Post is also slipping at C)

Solution

Post slips only at C

$$\sum M_B = 0$$
; $P(0.75m) - F_C(1m) = 0$

$$F_B \leq \mu_B N_B$$

$$F_C = \mu_C N_C$$
; $F_C = 0.5N_C = 0.5(400) = 200N$

Solving

$$P = 267N, N_C = 400N, F_C = 200N, F_B = 66.7N$$

Choose second case as it requires a smaller value of P