

# ENGG103 – Materials in Design

Week 5: Lecture 5 – Phase Diagrams



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**Consultation hours:** 

Monday 10:30 – 12:30

https://uow.webex.com/meet/ciara

Please email first for appointment.



#### Phase Diagrams

Phase diagrams are important for materials engineers

A phase diagram is a **graphical representation** of the phases that are present in a material at various temperatures and pressures and compositions.



#### Components and Phases

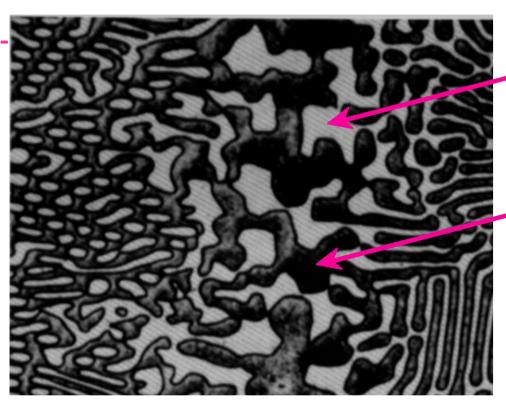
#### Components:

The elements or compounds that are mixed initially (AI and Cu).

#### • Phases:

A phase is a homogenous, physically distinct and mechanically separable portion of the material with a given chemical composition and structure ( $\alpha$  and  $\beta$ ).

Aluminum Copper Alloy



β (lighter phase) (Low Al content)

α (darker phase) (High Al content)



#### Phase Diagrams

Constitution of an alloy is described by

- 1. phases present
- 2. the weight fraction of each phase
- 3. the composition of each phase

Binary alloys: contain 2 components

Ternary alloys: contain 3 components

Quaternary: 4 components etc.



## Phase Diagrams – Binary (2 components)

- When we combine two elements...
   what is the resulting equilibrium state?
- In particular, if we specify...
  - -- the composition (e.g., wt% Cu wt% Ni), and
  - -- the temperature (T)

#### then we can determine the Constitution

- How many phases form?
- What is the composition of each phase?
- What is the amount of each phase?



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#### Phase Equilibria: Solubility Limit

- Solution solid, liquid, or gas solutions, single phase
- Mixture more than one phase

Adapted from Fig. 9.1, Callister & Rethwisch 8e.

#### Solubility Limit:

Maximum concentration for which only a single phase solution exists.

Question: What is the solubility limit for sugar in water at 20°C?

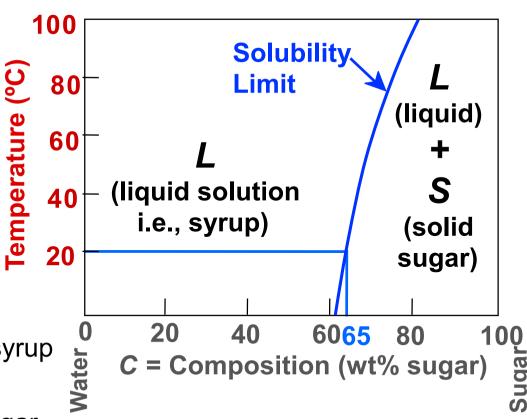
Answer: 65 wt% sugar.

At 20°C, if C < 65 wt% sugar: syrup

At 20°C, if C > 65 wt% sugar:

syrup + sugar

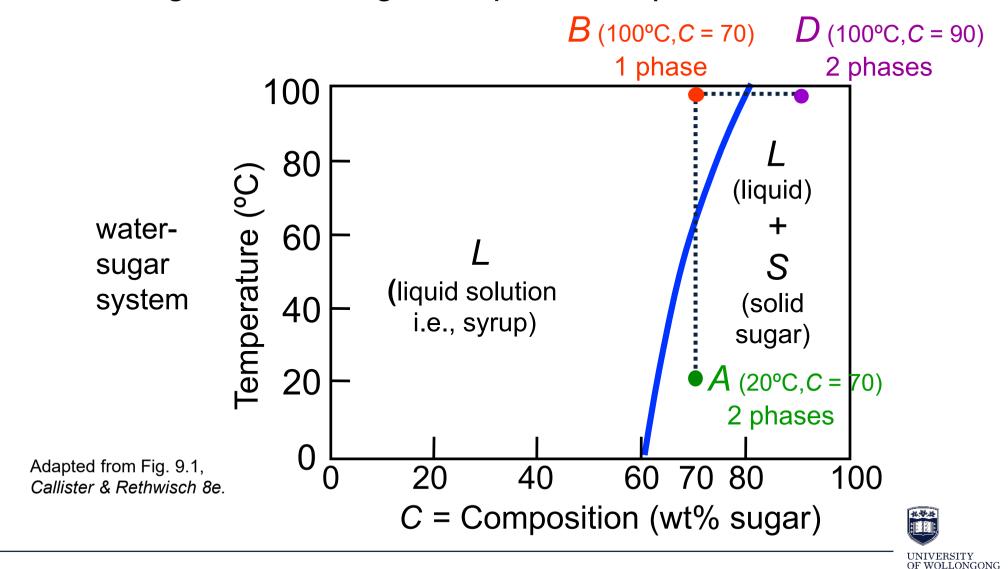
#### Sugar/Water Phase Diagram





### Effect of Temperature & Composition

- Altering T can change # of phases: path A to B.
- Altering C can change # of phases: path B to D.



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#### Criteria for Solid Solubility

Simple system (e.g., Ni-Cu solution)

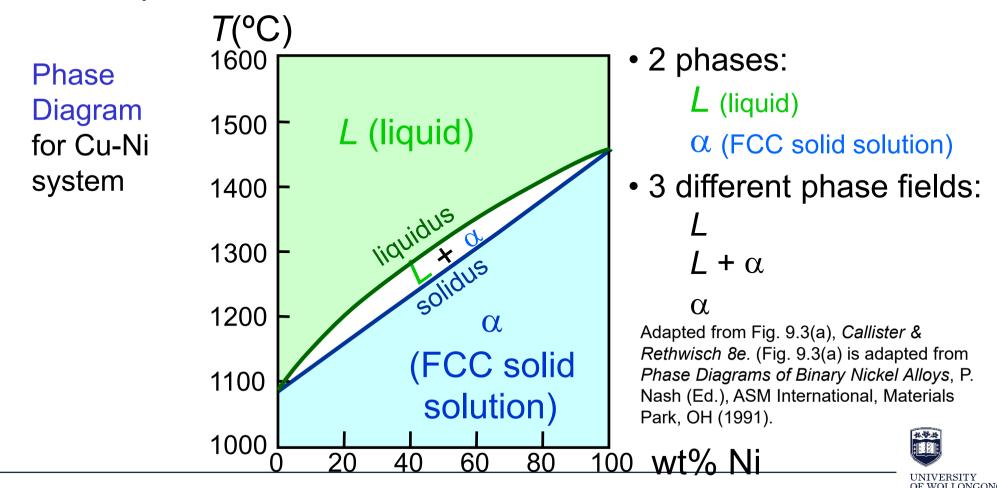
	Crystal Structure	electroneg	<i>r</i> (nm)
Ni	FCC	1.9	0.1246
Cu	FCC	1.8	0.1278

- Both have the same crystal structure (FCC) and have similar electronegativities and atomic radii (W. Hume – Rothery rules) suggesting high mutual solubility.
- Ni and Cu are totally soluble in one another for all proportions.



## Phase Diagrams

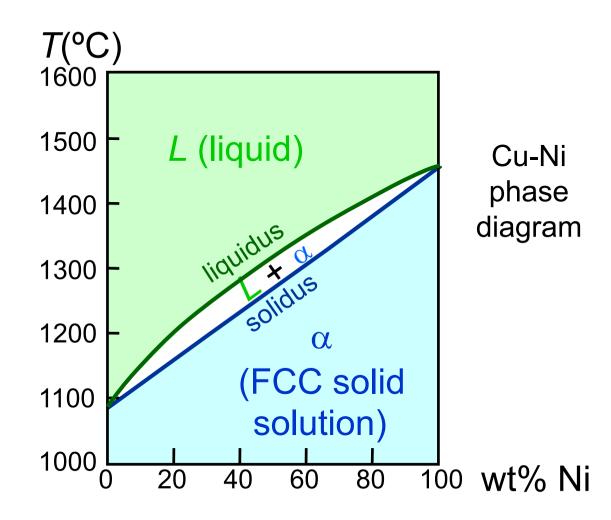
- Indicate phases as a function of T, C, and P.
- For this course:
  - binary systems: just 2 components.
  - independent variables: T and C (P = 1 atm is almost always used).



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# Isomorphous Binary Phase Diagram

- Phase diagram:
   Cu-Ni system.
- System is:
  - -- binary
    i.e., 2 components:
    Cu and Ni.
  - -- isomorphous
    i.e., complete
    solubility of one
    component in
    another; α phase
    field extends from
    0 to 100 wt% Ni.



Adapted from Fig. 9.3(a), Callister & Rethwisch 8e. (Fig. 9.3(a) is adapted from Phase Diagrams of Binary Nickel Alloys, P. Nash (Ed.), ASM International, Materials Park, OH (1991)

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#### Phase Diagrams:

### Determination of phase(s) present

- Rule 1: If we know T and  $C_0$ , then we know:
  - -- which phase(s) is (are) present.

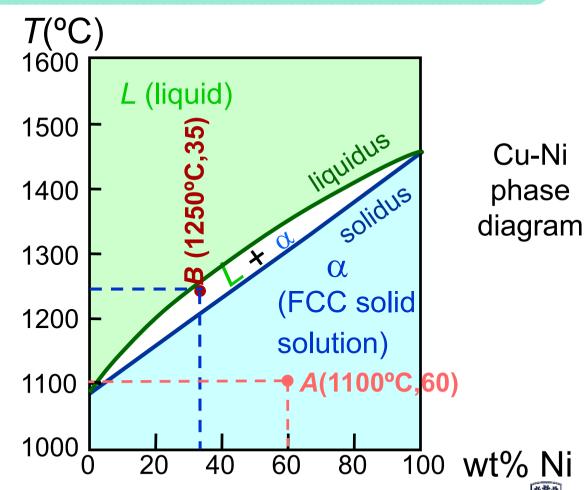
#### • Examples:

A(1100°C, 60 wt% Ni): 1 phase:  $\alpha$ 

B(1250°C, 35 wt% Ni):

2 phases:  $L + \alpha$ 

Adapted from Fig. 9.3(a), Callister & Rethwisch &e. (Fig. 9.3(a) is adapted from Phase Diagrams of Binary Nickel Alloys, P. Nash (Ed.), ASM International, Materials Park, OH (1991).



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#### Phase Diagrams:

### Determination of phase compositions

- Rule 2: If we know *T* and *C*<sub>0</sub>, then we can determine:
  -- the composition of each phase.

  Cu-Ni
- Examples:

```
Consider C_0 = 35 wt% Ni
```

At 
$$T_A = 1320$$
°C:

Only Liquid (L) present

$$C_L = C_0$$
 ( = 35 wt% Ni)

At  $T_D = 1190^{\circ}C$ :

Only Solid ( $\alpha$ ) present

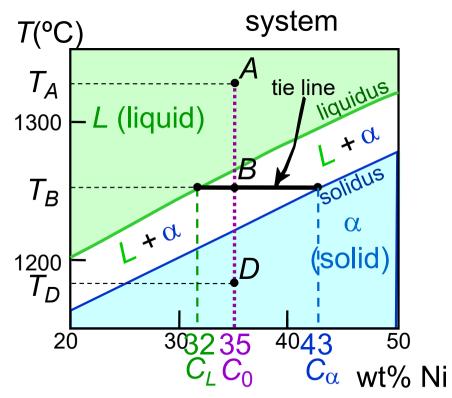
$$C_{\alpha} = C_0$$
 ( = 35 wt% Ni)

At 
$$T_B = 1250$$
°C:

Both  $\alpha$  and L present

$$C_L = C_{\text{liquidus}} (= 32 \text{ wt}\% \text{ Ni})$$

$$C_{\alpha} = C_{\text{solidus}}$$
 (= 43 wt% Ni)



Adapted from Fig. 9.3(a), Callister & Rethwisch 8e. (Fig. 9.3(a) is adapted from Phase Diagrams of Binary Nickel Alloys, P. Nash (Ed.), ASM International, Materials Park, OH (1991).

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#### Phase Diagrams:

### Determination of phase weight fractions

- Rule 3: If we know T and  $C_0$ , then can determine: -- the weight fraction of each phase. Cu-Ni
- Examples:

Consider  $C_0 = 35$  wt% Ni

At  $T_A$ : Only Liquid (L) present

$$W_L = 1.00, W_{\alpha} = 0$$

At  $T_D$ : Only Solid ( $\alpha$ ) present

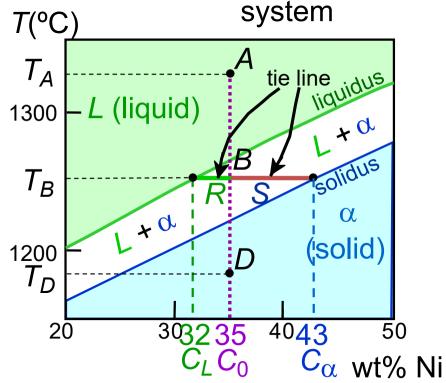
$$W_L = 0$$
,  $W_{\alpha} = 1.00$ 

At  $T_R$ : Both  $\alpha$  and L present

$$W_L = \frac{S}{R + S}$$

$$W_L = \frac{S}{R+S} = \frac{43-35}{43-32} = 0.73$$

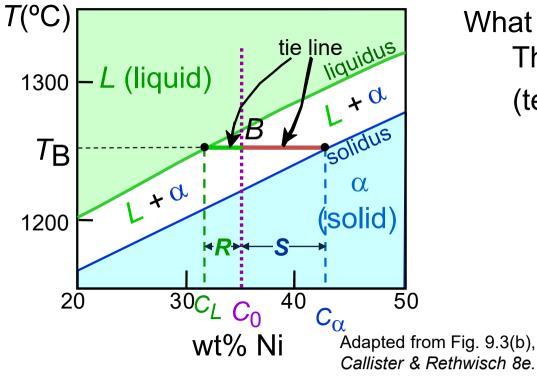
$$W_{\alpha} = \frac{R}{R + S} = 0.27$$



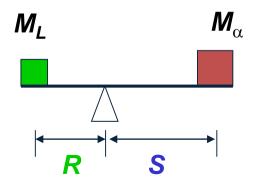
Adapted from Fig. 9.3(a), Callister & Rethwisch 8e. (Fig. 9.3(a) is adapted from Phase Diagrams of Binary Nickel Alloys, P. Nash (Ed.), ASM International, Materials Park, OH (1991).

#### The Lever Rule

 Tie line – connects the phases in equilibrium with each other – also sometimes called an isotherm



What fraction of each phase?
Think of the tie line as a lever
(teeter-totter)

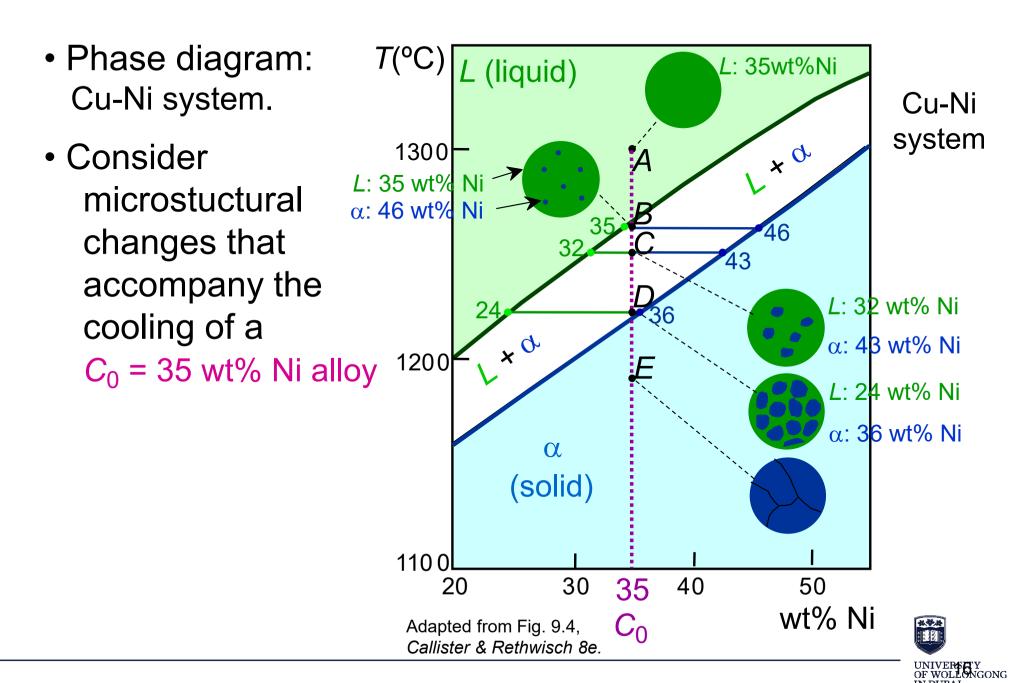


$$M_{\alpha} \times S = M_{L} \times R$$

$$W_{L} = \frac{M_{L}}{M_{L} + M_{\alpha}} = \frac{S}{R + S} = \frac{C_{\alpha} - C_{0}}{C_{\alpha} - C_{L}}$$

$$W_{\alpha} = \frac{R}{R+S} = \frac{C_0 - C_L}{C_{\alpha} - C_{\alpha}}$$

#### Ex: Cooling of a Cu-Ni Alloy



### Mechanical Properties: Cu-Ni System

- Effect of solid solution strengthening on:
  - -- Tensile strength (*TS*)

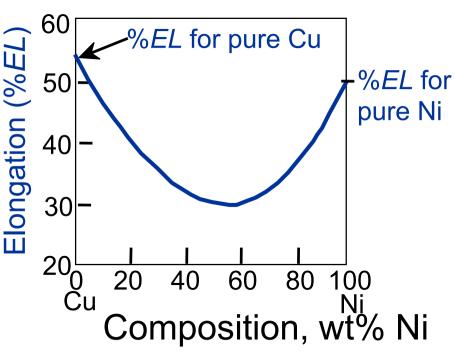
TS for pure Cu

Cu

Composition, wt% Ni

Adapted from Fig. 9.6(a), Callister & Rethwisch 8e.

-- Ductility (%*EL*)



Adapted from Fig. 9.6(b), Callister & Rethwisch 8e.



- The phase(s) present at a given temperature and composition
- 2. The chemical composition of each phase present
- 3. The mass fraction (%) of each phase present

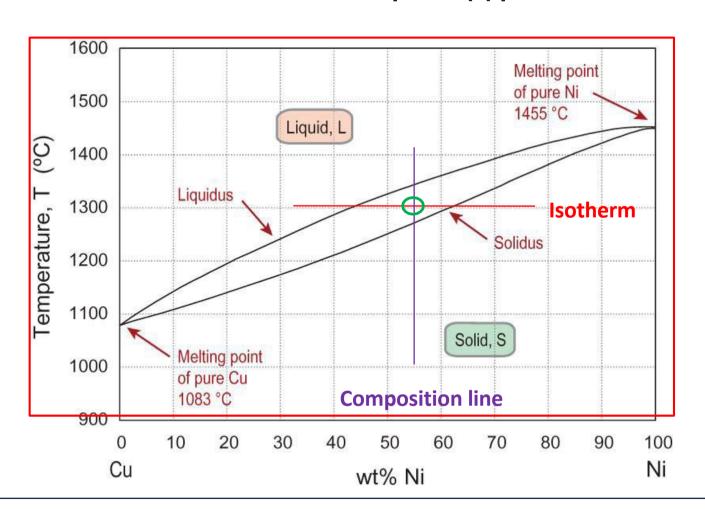
### These three rules are of the utmost importance.

You need to make sure that you understand the rules the implications thereof and the application off these three rules



#### 1. The phase(s) present at a given temperature and composition

The intersection of the isotherm with the composition line define the phase(s) present



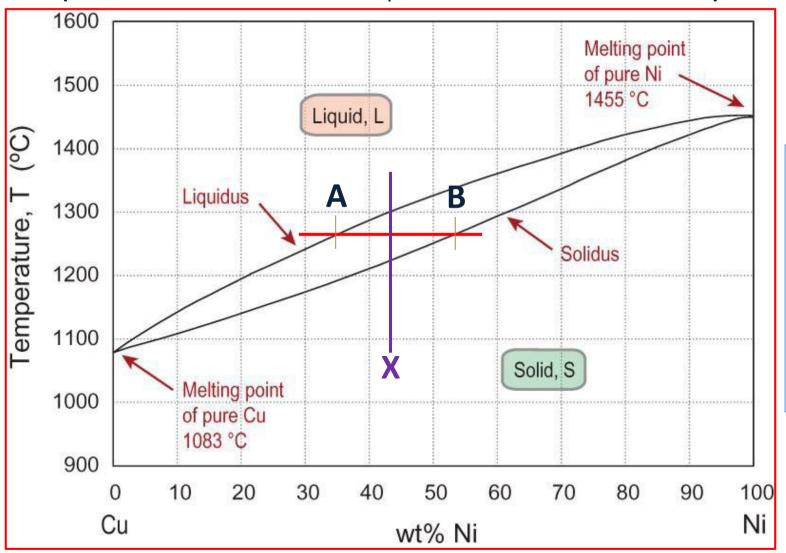
# Phases present at 1300C

Liquid and Solid



#### For composition X, the line A-B is called a tie-line

(The isotherm intersects the liquidus in A and the solidus in B)



We call the line that intersects an isotherm at the phase boundaries a Tie-Line



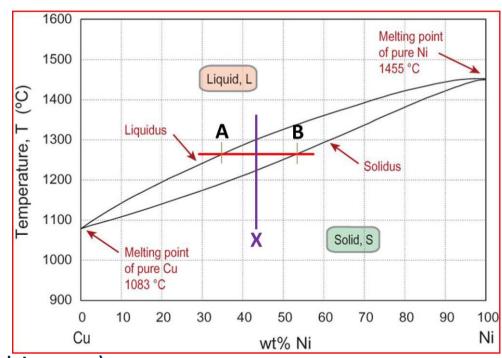
#### 2. The chemical composition of each phase present

For a given composition, the intersections of the tie-line with the phase boundaries define the chemical composition of the respective phases

#### For composition X

The **tie-line** intersect the phase boundaries:

- The liquidus in A
- The solidus in B

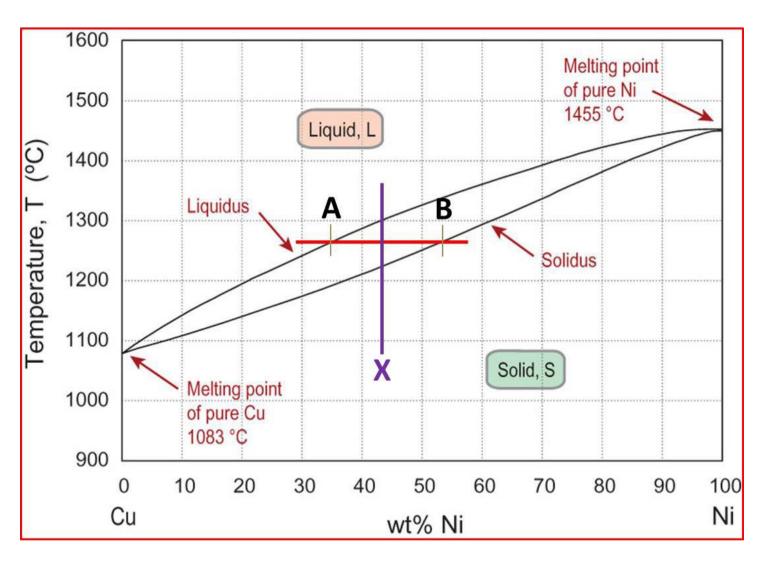


A gives the composition of the liquid (35% in this case)

**B** gives the chemical composition of the solid (53% in this case)



#### 3. The mass fraction (%) of each phase present



The lever rule is a tool used to determine the mole fraction of each phase of a binary equilibrium phase diagram.

This rule gives the **fraction** of a phase by the **ratio of the lengths** of the tie line between C<sub>o</sub> and composition of the other phase to the total length of the tie line.

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# Stop and check video on moodle

**Lecture 5: Distance Learning Resources folder – Phase Diagrams video** 



## Eutectic alloy systems

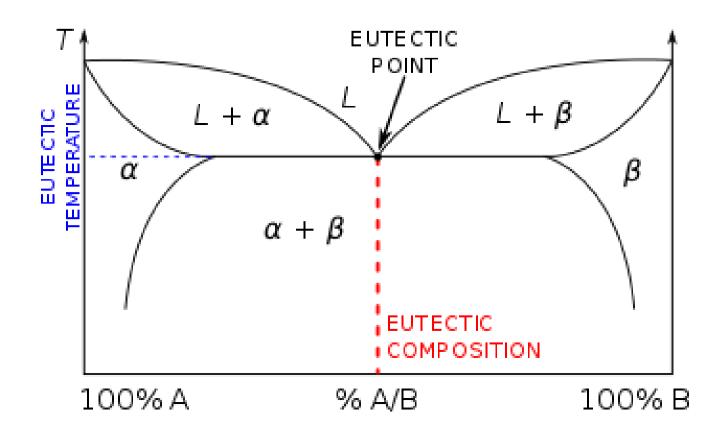
In the Cu-Ni system we dealt with two elements that display complete solubility in the liquid as well as in the solid state.

Not all metals display complete solid solubility

An important alloy system of this type is the **eutectic system** of which the Pb-Sn (Lead – Tin) system is an example



#### Phase Diagrams II



**Eutectics** and **Eutectoids** are important and common in engineering alloys and allow the production of special, strong microstructure.

# Binary-Eutectic Systems has a sp components with a m

has a special composition with a min. melting *T*.

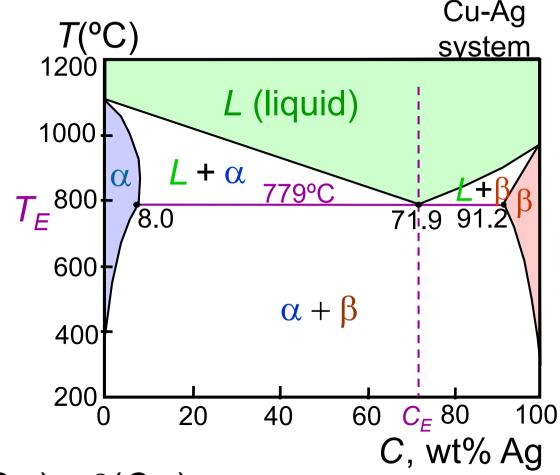
Ex.: Cu-Ag system

- 3 single phase regions
   (L, α, β)
- Limited solubility:

α: mostly Cu

β: mostly Ag

- $T_E$ : No liquid below  $T_E$
- $C_E$ : Composition at temperature  $T_E$



Eutectic reaction

$$L(C_E) \implies \alpha(C_{\alpha E}) + \beta(C_{\beta E})$$

Adapted from Fig. 9.7, Callister & Rethwisch 8e.

$$L(71.9 \text{ wt\% Ag}) \stackrel{\text{cooling}}{====} \alpha(8.0 \text{ wt\% Ag}) + \beta(91.2 \text{ wt\% Ag})$$



### EX 1: Pb-Sn Eutectic System

• For a 40 wt% Sn-60 wt% Pb alloy at 150°C, determine:

-- the phases present

Answer:  $\alpha + \beta$ 

-- the phase compositions

Answer:  $C_{\alpha}$  = 11 wt% Sn  $C_{\beta}$  = 99 wt% Sn

-- the relative amount of each phase

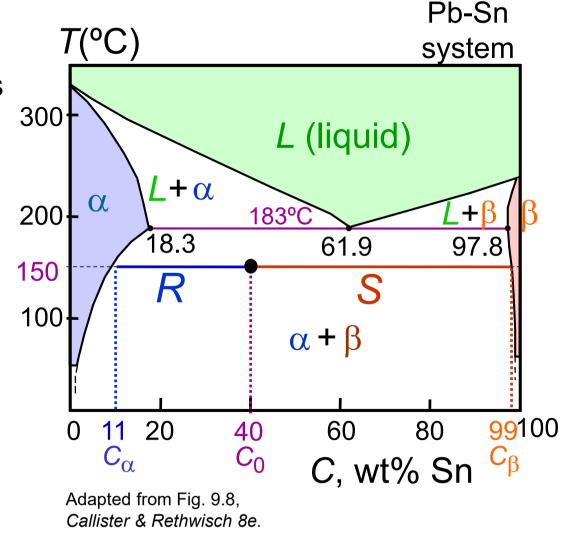
#### **Answer:**

$$W_{\alpha} = \frac{S}{R+S} = \frac{C_{\beta} - C_{0}}{C_{\beta} - C_{\alpha}}$$

$$= \frac{99 - 40}{99 - 11} = \frac{59}{88} = 0.67$$

$$W_{\beta} = \frac{R}{R+S} = \frac{C_{0} - C_{\alpha}}{C_{\beta} - C_{\alpha}}$$

$$= \frac{40 - 11}{99 - 11} = \frac{29}{88} = 0.33$$





### EX 2: Pb-Sn Eutectic System

For a 40 wt% Sn-60 wt% Pb alloy at 220°C, determine:

-- the phases present:

Answer:  $\alpha + L$ 

-- the phase compositions

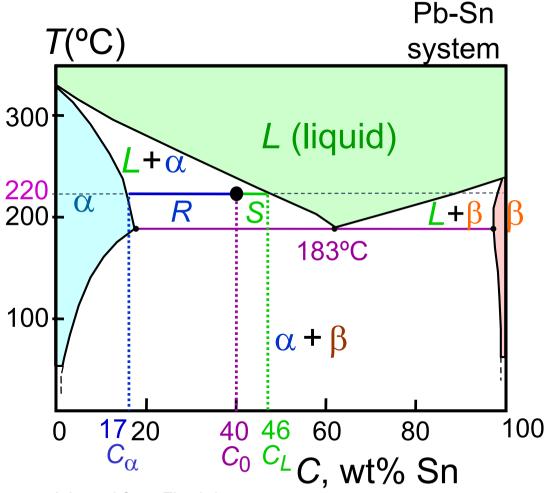
Answer:  $C_{\alpha} = 17$  wt% Sn  $C_{I} = 46$  wt% Sn

-- the relative amount of each phase

#### **Answer:**

$$W_{CL} = \frac{C_L - C_0}{C_L - C_{\alpha}} = \frac{46 - 40}{46 - 17}$$
$$= \frac{6}{29} = 0.21$$

$$W_L = \frac{C_0 - C_{\alpha}}{C_L - C_{\alpha}} = \frac{23}{29} = 0.79$$

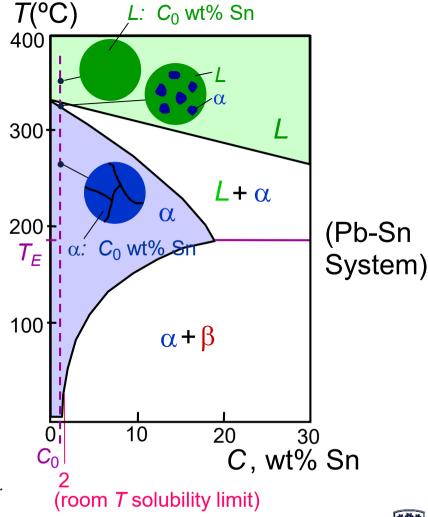


Adapted from Fig. 9.8, Callister & Rethwisch 8e.



# Microstructural Developments in Eutectic Systems I

- For alloys for which  $C_0 < 2$  wt% Sn
- Result: at room temperature
   -- polycrystalline with grains of
   α phase having
   composition C<sub>0</sub>



Adapted from Fig. 9.11, Callister & Rethwisch 8e.



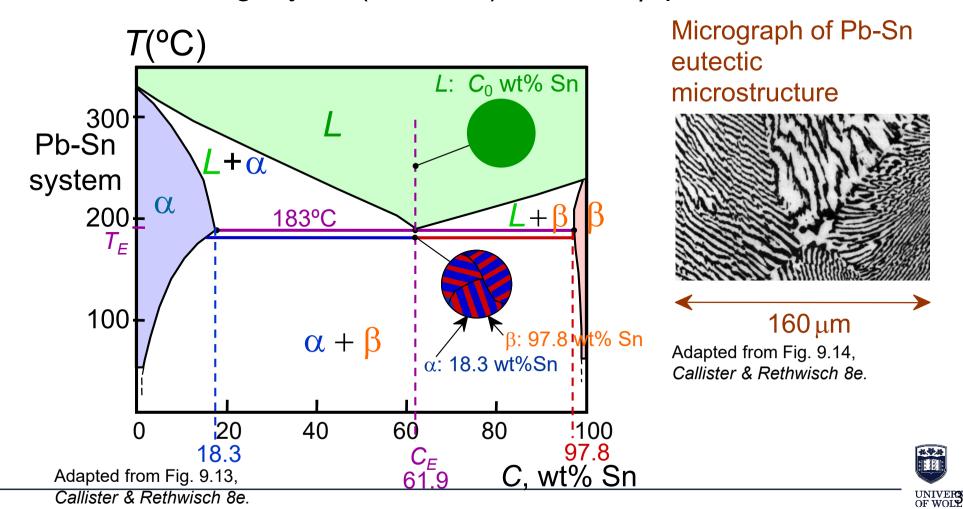
# Microstructural Developments in Eutectic Systems II

*L: C*<sub>0</sub> wt% Sn  $T(^{\circ}C)$  For alloys for which 400 2 wt% Sn <  $C_0$  < 18.3 wt% Sn • Result: at temperatures in  $\alpha$  +  $\beta$  range<sup>300</sup> -- polycrystalline with  $\alpha$  grains C₀ wt% Sn and small β-phase particles 200 T<sub>E</sub> 100  $\alpha + \beta$ Pb-Sn system 20 10 30 Adapted from Fig. 9.12, C, wt% Sn Callister & Rethwisch 8e. (sol. limit at  $T_{room}$ ) (sol. limit at  $T_{E}$ )

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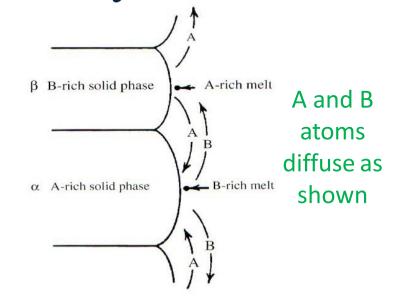
# Microstructural Developments in Eutectic Systems III

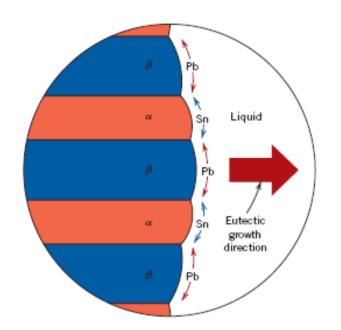
- For alloy of composition  $C_0 = C_E$
- Result: Eutectic microstructure (lamellar structure)
  - -- alternating layers (lamellae) of  $\alpha$  and  $\beta$  phases.



# Growth mechanism for a plate-like (lamellar) eutectic alloy

- Two phases grow cooperatively from the liquid
- Normal eutectics grow as alternate lamellae or as rods of the minor phase embedded in the other
- Both phases grow simultaneously behind a planar solid/liquid interface

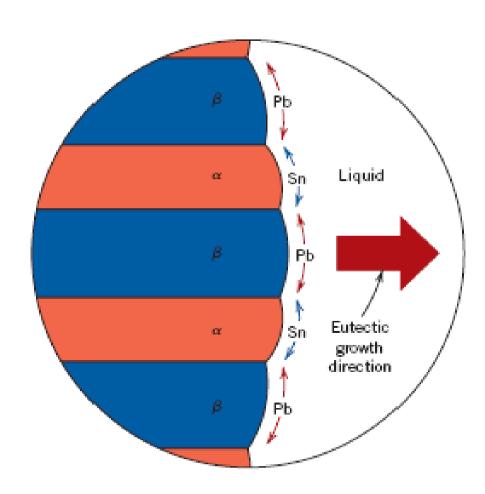




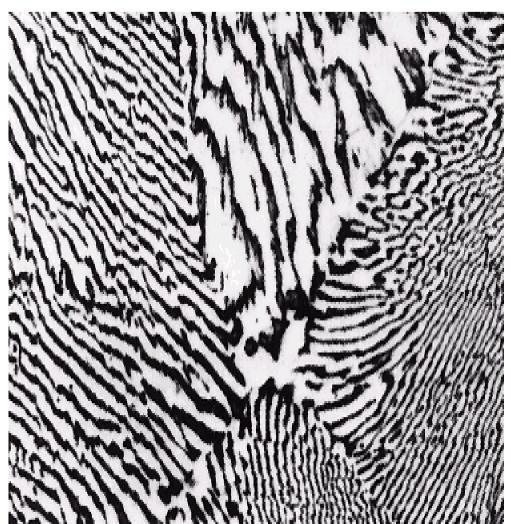
As the A-rich  $\alpha$  phase solidifies, excess B atoms diffuse a short distance in the liquid laterally where it is incorporated into the B-rich  $\beta$ -phase

The A atoms rejected ahead of the  $\beta$  -lamellae diffuse in the liquid to the tips of the adjacent  $\alpha$ -lamellae

#### Lamellar Eutectic Structure



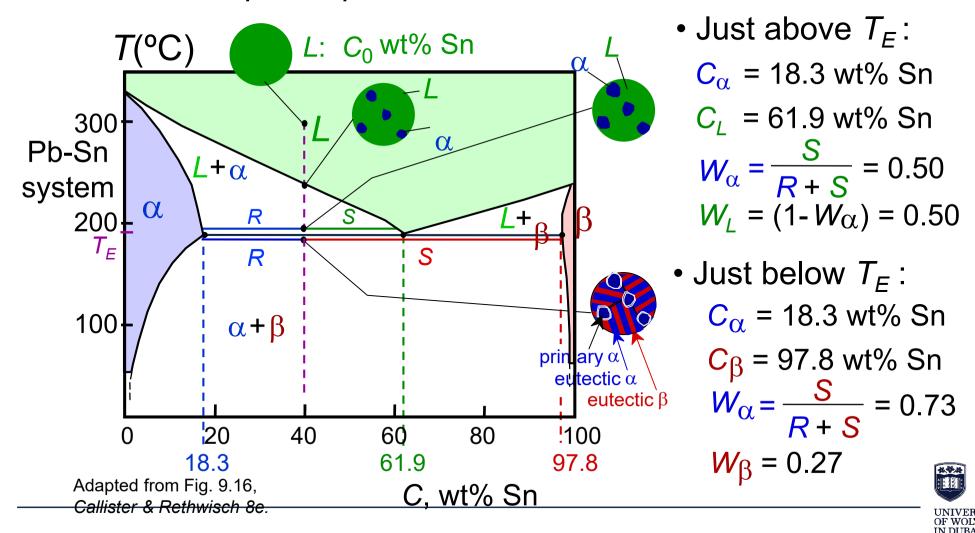
Adapted from Figs. 9.14 & 9.15, *Callister & Rethwisch 8e.* 





# Microstructural Developments in Eutectic Systems IV

- For alloys for which 18.3 wt% Sn  $< C_0 < 61.9$  wt% Sn
- Result:  $\alpha$  phase particles and a eutectic microconstituent



### Eutectic, Eutectoid, & Peritectic

- Eutectic liquid transforms to two solid phases  $\frac{\text{cool}}{\text{heat}}$   $\Delta + \beta$  (For Pb-Sn, 183°C, 61.9 wt% Sn)
- Eutectoid one solid phase transforms to two other solid phases

intermetallic compound 
$$S_2 \Longrightarrow S_1 + S_3$$
 - cementite  $\gamma \in \frac{\text{cool}}{\text{heat}} \alpha + \text{Fe}_3 C$  (For Fe-C, 727°C, 0.76 wt% C)

 Peritectic - liquid and one solid phase transform to a second solid phase

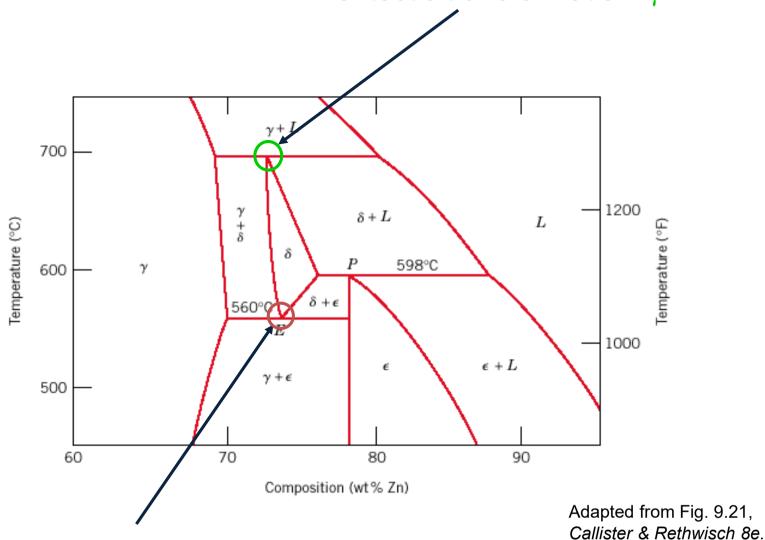
$$S_1 + L \Longrightarrow S_2$$
  
 $\delta + L \stackrel{\text{cool}}{\rightleftharpoons} \gamma$  (For Fe-C, 1493°C, 0.16 wt% C)



#### **Eutectoid & Peritectic**

Cu-Zn Phase diagram

Peritectic transformation  $\gamma + L \Longrightarrow \delta$ 



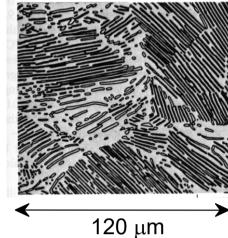
Eutectoid transformation  $\delta \Longrightarrow \gamma + \epsilon$ 



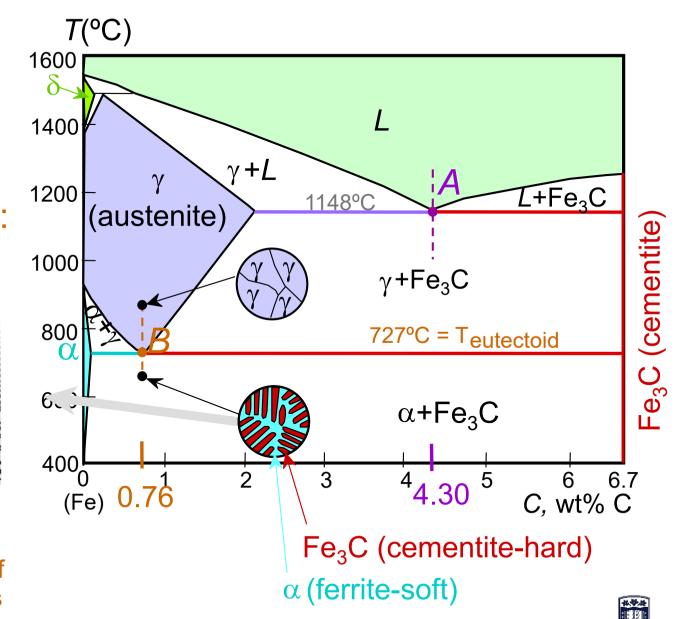
## Iron-Carbon (Fe-C) Phase Diagram

- 2 important points
  - Eutectic (A):  $L \Rightarrow \gamma + \text{Fe}_3\text{C}$
  - Eutectoid (B):

$$\gamma \Rightarrow \alpha + \text{Fe}_3\text{C}$$



Result: Pearlite = alternating layers of  $\alpha$  and Fe<sub>3</sub>C phases



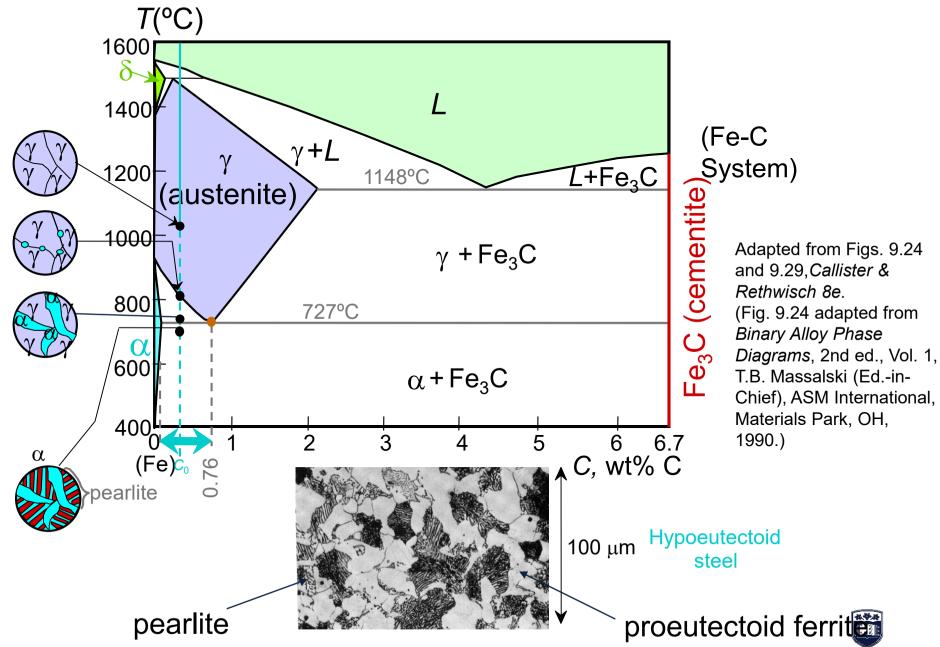
(Adapted from Fig. 9.27,

Adapted from Fig. 9.24,

Callister & Rethwisch 8e.)

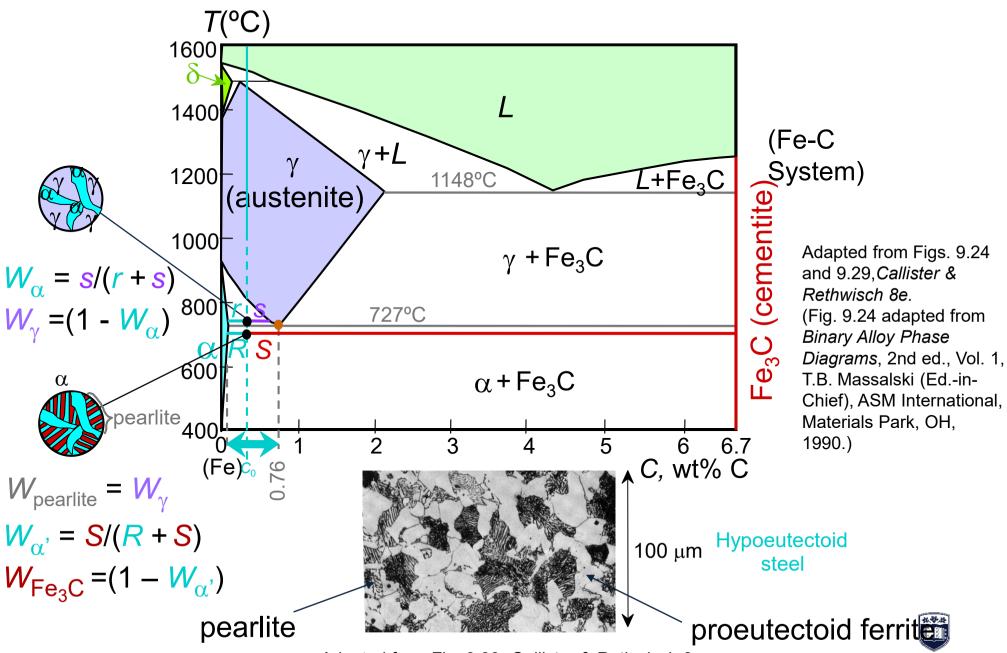
Callister & Rethwisch 8e.

# Hypoeutectoid Steel



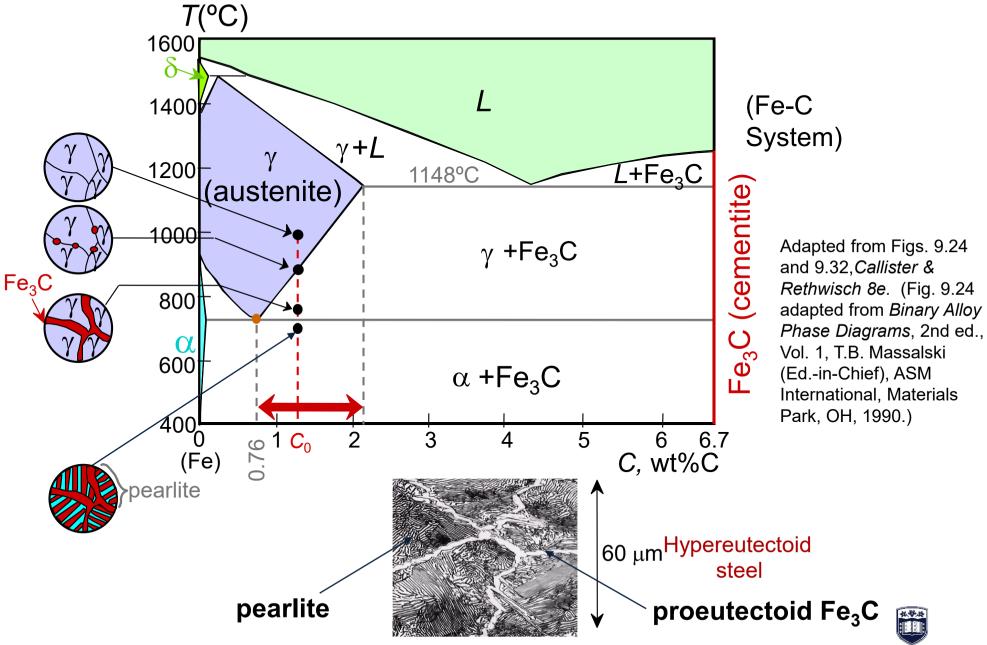
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# **Hypoeutectoid Steel**



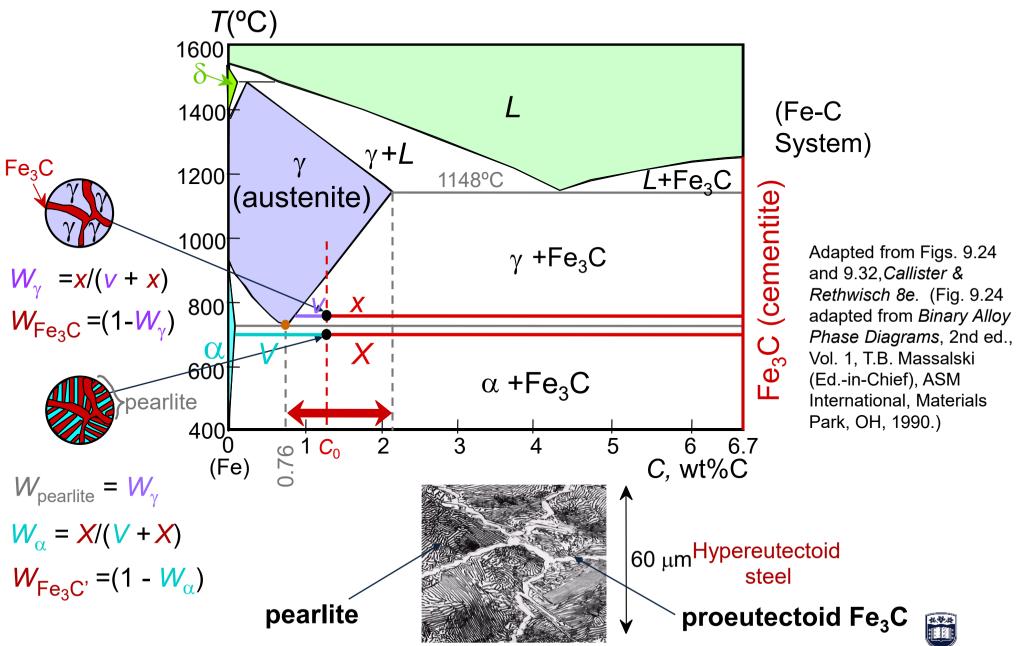
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# Hypereutectoid Steel



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# Hypereutectoid Steel



#### **Example Problem**

For a 99.6 wt% Fe-0.40 wt% C steel at a temperature just below the eutectoid, determine the following:

- a) The compositions of Fe<sub>3</sub>C and ferrite ( $\alpha$ ).
- b) The amount of cementite (in grams) that forms in 100 g of steel.
- c) The amounts of pearlite and proeutectoid ferrite ( $\alpha$ ) in the 100 g.



## Solution to Example Problem

a) Using the RS tie line just below the eutectoid

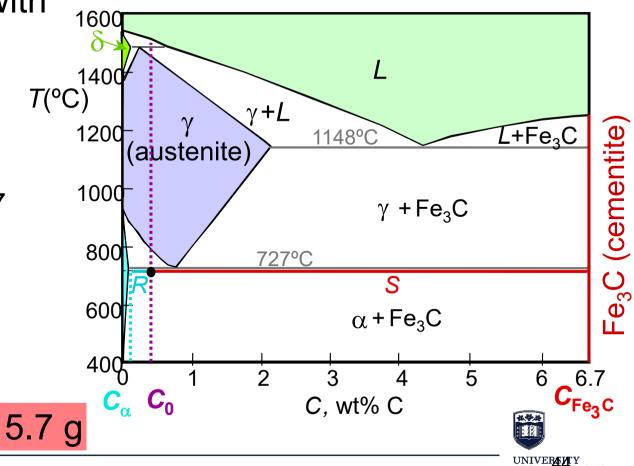
$$C_{\alpha} = 0.022 \text{ wt% C}$$
  
 $C_{\text{Fe}_{3}\text{C}} = 6.70 \text{ wt% C}$ 

b) Using the lever rule with the tie line shown

$$W_{\text{Fe}_3\text{C}} = \frac{R}{R+S} = \frac{C_0 - C_\alpha}{C_{\text{Fe}_3\text{C}} - C_\alpha}$$
$$= \frac{0.40 - 0.022}{6.70 - 0.022} = 0.057$$

Amount of  $Fe_3C$  in 100 g =  $(100 \text{ g})W_{Fe_3C}$ 

$$= (100 g)(0.057) = 5.7 g$$



## Solution to Example Problem (cont.)

### Using the VX tie line just above the eutectoid and realizing that

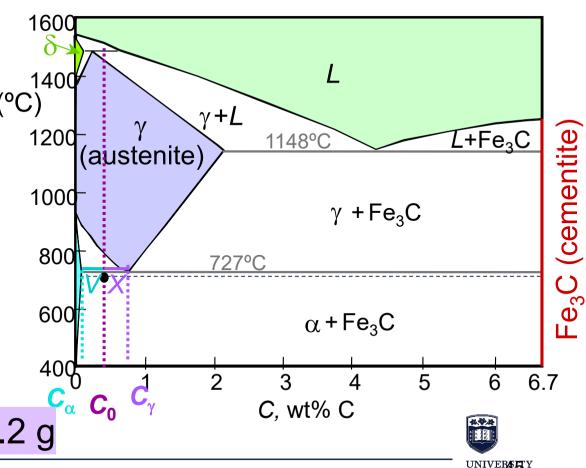
$$C_0 = 0.40 \text{ wt\% C}$$
  
 $C_{\alpha} = 0.022 \text{ wt\% C}$   
 $C_{\text{pearlite}} = C_{\gamma} = 0.76 \text{ wt\% C}$ 

$$W_{\text{pearlite}} = \frac{V}{V + X} = \frac{C_0 - C_{\alpha}}{C_{\gamma} - C_{\alpha}}$$
$$= \frac{0.40 - 0.022}{0.76 - 0.022} = 0.512$$

Amount of pearlite in 100 g

= 
$$(100 \text{ g})W_{\text{pearlite}}$$

$$= (100 g)(0.512) = 51.2 g$$



#### **Summary**

- Phase diagrams are useful tools to determine:
  - -- the number and types of phases present,
  - -- the composition of each phase,
  - -- and the weight fraction of each phase given the temperature and composition of the system.
- The microstructure of an alloy depends on
  - -- its composition, and
  - -- whether or not cooling rate allows for maintenance of equilibrium.
- Important phase diagram phase transformations include eutectic, eutectoid, and peritectic.



