

3/4 (2. Halbttag) | Transistor und Transistorverstärker

Angelo Brade^{*1} and Jonas Wortmann^{†1}

¹Rheinische Friedrich–Wilhelms–Universität Bonn

September 7, 2024

^{*}s72abrad@uni-bonn.de

[†]s02jwort@uni-bonn.de

Contents

1	Introduction	1
2	Theory	1
3	Preliminary Tasks	2
3.1	G	2
3.2	H	2
3.3	I	2
3.4	J	2
3.5	K	2
3.6	L	2
3.7	M	2
3.8	N	2
4	Analysis	3
4.1	Voltageamplifier of the common collector	3
4.2	Common collector as buffer amplifier	3
4.3	Inverted amplifier	3
4.4	Alternating current cancellation of negative feedback	5
4.5	Frequency response of a cascode circuit	5
4.6	Amplifier with negative feedback	6
5	Conclusion	6

1 Introduction

In this experiment, the bipolar transistor is used, but here as an emitter sequence for voltage amplification and as an impedance converter (buffer). Also, the negative feedback of alternating current and the behavior of different frequencies will be observed via a cascode circuit.

2 Theory

The whole theory of different kinds of transistors is still needed.

An emitter follower is an electronic component, with which a current can be amplified (factor γ), without any change in voltage (factor ν).

$$\nu = \frac{dU_E}{dU_B} \approx 1 \quad \gamma = \frac{dI_E}{dI_B} \approx 100. \quad (2.1)$$

This is why sometimes an emitter follower is called an impedance changer.

The negative feedback factor k denotes, which fraction of the output voltage is used for the negative feedback

$$\frac{1}{\nu} = \frac{1}{\nu_0} + k. \quad (2.2)$$

Though the amplification with negative feedback ν is lower than the open-loop gain ν_0 , ν is only dependent on the circuit and not on the transistor itself. This amplification can be described as follows

$$\frac{d\nu}{\nu} = \frac{d\nu_0}{\nu_0} \frac{\nu}{\nu_0}. \quad (2.3)$$

The bandwidth of the amplifier circuit is the frequency band, in which the amplification is constant. To increase the bandwidth, one can use a cascode circuit. To achieve such an amplification, the alternating voltage feedback of the collector on the basis is reduced by utilizing a second transistor to prevent a voltage swing. Given an input signal, the resulting change in voltage will be significantly lower than the change in the output signal. This results in a higher bandwidth.

Stabilization of the operating point can be achieved by using negative feedback, in particular negative feedback of voltage.

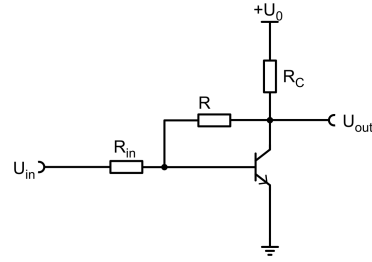


Figure 1: Transistor amplifier as common collector with negative feedback (voltage); figure 3/4.16 [?]

In this figure the resistor R sets the base potential as well as the operating point and couples the voltage from the collector back to the base. Due to this negative feedback the base current is reduced although the input current remains constant.

3 Preliminary Tasks

3.1 G

$\mathbb{Z} \nu = \frac{\gamma R_E}{r_{BE} + \gamma R_E}$ with $\gamma = \frac{dI_E}{dI_B}$ and $r_{BE} = \frac{dU_{BE}}{dI_B}$.

$$\begin{aligned}
 \nu &= \frac{dU_E}{dU_B} \\
 \Leftrightarrow &= \frac{dI_E R_E}{dU_{BE} + dU_E} \\
 \Leftrightarrow &= \frac{\frac{dI_E R_E}{dI_B}}{\frac{dU_{BE}}{dI_B} + \frac{dU_E}{dI_B}} \\
 \Leftrightarrow &= \frac{\gamma R_E}{r_{BE} + \gamma R_E}.
 \end{aligned} \tag{3.1}$$

3.2 H

The equation applies

$$\begin{aligned}
 \frac{r_{out}}{r_{in}} &= \frac{\frac{dU_E}{dI_E}}{\frac{dU_B}{dI_B}} \\
 \Leftrightarrow &= \frac{dU_E}{dI_E} \frac{dI_B}{dU_B} \\
 \Leftrightarrow &= \frac{dU_E}{dU_B} \frac{dI_B}{dI_E} \\
 \Leftrightarrow &\approx 1 \cdot \frac{1}{\gamma}.
 \end{aligned} \tag{3.3}$$

3.3 I

The equation applies

$$\begin{aligned}
 \nu &= \frac{dU_C}{dU_B} \\
 \Leftrightarrow &= \frac{dI_C R_C}{dU_{BE} + dU_E} \\
 \Leftrightarrow &= \frac{\frac{dI_C R_C}{dI_B}}{\frac{dU_{BE}}{dI_B} + \frac{dU_E}{dI_B}} \\
 \Leftrightarrow &= \frac{\beta R_C}{r_{BE} + \gamma R_E}.
 \end{aligned} \tag{3.5}$$

3.4 J

The equation applies

$$\begin{aligned}
 \frac{1}{\nu} &= \frac{1+k\nu_0}{\nu_0} \\
 \Leftrightarrow \nu &= \frac{\nu_0}{1+k\nu_0} \\
 \Leftrightarrow \frac{d\nu}{d\nu_0} &= \frac{1}{(1+k\nu_0)^2} \\
 \Leftrightarrow &= \frac{\nu}{\nu_0} \frac{1}{1+k\nu_0} \\
 \Leftrightarrow \frac{d\nu}{\nu} &= \frac{d\nu_0}{\nu_0} \frac{1}{1+k\nu_0} \\
 \Leftrightarrow &= \frac{d\nu_0}{\nu_0} \frac{\nu}{\nu_0}.
 \end{aligned} \tag{3.7}$$

3.5 K

The parallel capacitor with capacitance C_{CB} and transistor form a high-pass filter. This means that high frequency signals will run through the capacitor and not the transistor, resulting in them not being amplified.

3.6 L

There is no voltage change at point P, because the input signal to the transistor T2 is constant. The change in current $dI_E(T_2)$ is in return also zero.

3.7 M

For any transit frequency the equation holds $f_{\text{grenz gk}} \nu(f=0) = f_{\text{grenz}} \nu_0$. Thus $f_{\text{grenz gk}} = f_{\text{grenz}} \frac{\nu_0}{\nu(f=0)}$.

3.8 N

For increasing base current I_B , the collector voltage U_C and the voltage across the resistor U_{R_C} also increases. Because U_0 should be constant, the voltage drops across the resistor R , which in turn stabilizes the operating point.

4 Analysis

4.1 Voltage amplifier of the common collector

On circuit board I (Fig. 2) we construct a common collector with $dU_B = 2.1 V_{PP}$ and $U_B \approx 2 V$. To test the voltage amplification we chose a variety of different resistor combinations. The measurements are displayed in Tab. 1. We expect no change for different R_E .

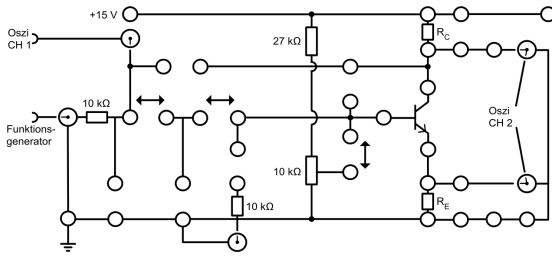


Figure 2: Circuit board 1[?]

R_C	R_E	amplification ν
360 Ω	1 k Ω	1.000(25)
360 Ω	22 k Ω	1.025(25)
360 Ω	47 k Ω	1.015(25)
1 k Ω	360 Ω	0.945(25)
22 k Ω	360 Ω	0.114(25)
47 k Ω	360 Ω	0.120(25)

Table 1: Voltage amplification for different resistor combinations

As we see, there is no significant variation of the amplification for different R_E . Though we can clearly see a lowering of the amplification for higher R_C , which is plausible since we have less current that can be amplified.

4.2 Common collector as buffer amplifier

Here we are tasked to match the impedance of a speaker, so we are able to hear an output. For this we firstly construct an Inverted Amplifier and test the speaker solely without a common collector. We observe, that the speaker does not produce any sound, because we haven't matched the impedance. Now we add a common collector as a buffer amplifier, which in theory should be able to match the impedance of the speaker. Unfortunately we could not get the circuit running and test the hypothesis.

4.3 Inverted amplifier

Phase relationship between input and output

Now we build a common emitter on circuit board I with $R_C = R_E = 390 \Omega$, $dU_B = 0.5 V_{PP}$, $U_B = 1.5 V$ and we choose a capacitor prior to the input signal of $0.1 \mu F$. As we can see in the xy (CH1, CH2) configuration in fig. 3, the phase is not linear, but elliptic. Thus we have not the same phase. We found out through experimenting, that the multiple ellipses come from noise. The phase relationship and especially the noise is also visible in fig. 4, as the lines are rather thick. We can see that the phase difference is between $\frac{1}{2}\pi$ and 1π , because we now have coupled the capacitor.

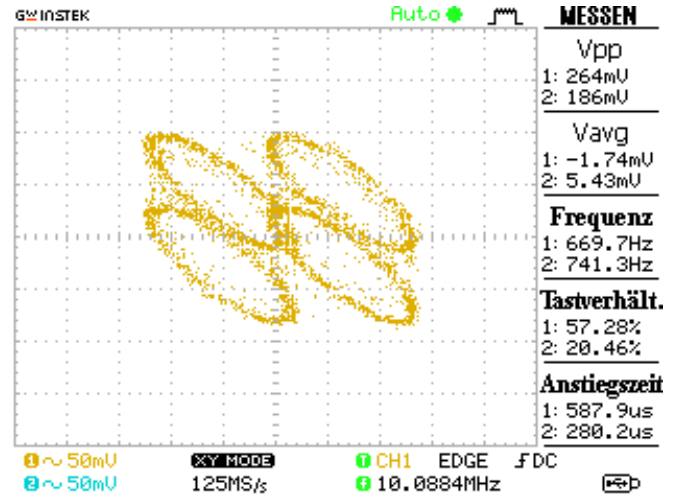


Figure 3: Phase relationship in phase space

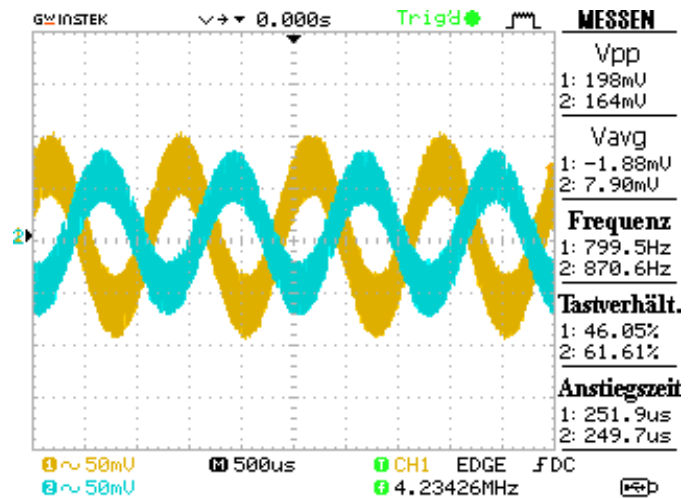


Figure 4: Phase relationship in voltage/time space

Voltage amplification of the inverted amplifier

We measure the voltage amplification with different values for the resistors R_E and R_C . The results are display in tab. 2.

R_C	R_E	amplification ν	$\nu = -\frac{R_C}{R_E}$
360 Ω	470 Ω	-0.686(24)	-0.830
360 Ω	1 k Ω	-0.437(24)	-0.390
360 Ω	4.7 k Ω	-0.250(25)	-0.083
360 Ω	33 k Ω	-0.196(25)	-0.012
360 Ω	47 k Ω	-0.180(25)	-0.008
470 Ω	360 Ω	-0.857(24)	-1.205
1 k Ω	360 Ω	-1.491(25)	-2.564
4.7 k Ω	360 Ω	-2.284(22)	-12.05
33 k Ω	360 Ω	-0.234(27)	-84.62
47 k Ω	360 Ω	-0.234(27)	-120.5

Table 2: Voltage amplification for different resistor combinations

We notice, where R_C stays constant, the experimental values for the amplification follow the theoretical ones in their general trend, but are not exactly the same. Where R_E stays constant we observe that first the data follows the calculations, but to the end, with the highest resistance, they just drop. It seems that there is a sweetspot for an optimal amplification. Then it should have to do something with resonance, so the amplification is frequency dependent. But since we expect that the formula for the theoretical values is correct, we assume we have made some mistake for the last two experimental values.

Resistance of a Transistor

Now with the special case, that $R_E = 0 \Omega$ and $E_C = 390 \Omega$, we can read the peak-to-peak voltage from oscillogramm in fig. 5 and calculate the amplification. We calculate the amplification to be $\nu_0 = -26.8(10)$. $\beta = 547(27)$ has already been determined in the last lab course. Now we can calculate the differential resistance of the Emitter-Base-Diode r_{BE} :

$$\begin{aligned}\nu_0 &= -\beta \frac{R_C}{r_{BE}} \\ \Leftrightarrow r_{BE} &= -\beta \frac{R_C}{\nu_0} \\ &= 7.96(49) \text{ k}\Omega\end{aligned}$$

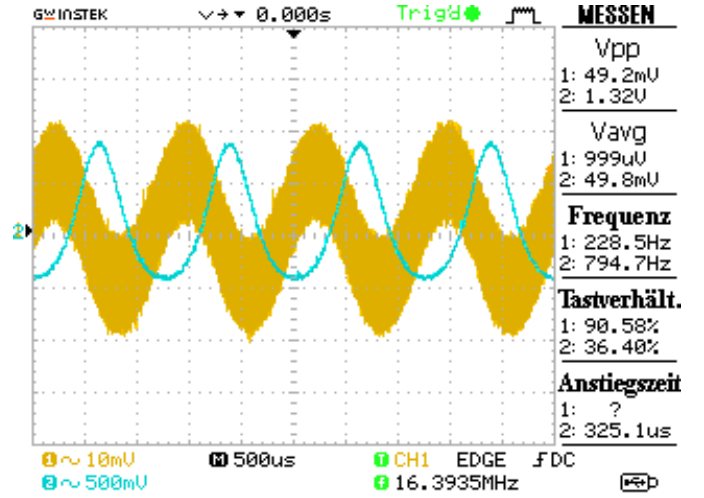


Figure 5: Voltage amplification

We now plot the data from tab. 2 in fig. 6 and 7. At this point we are tasked to display the theoretical line in the figures, however they diverge to the extent, that one of them would not be readable anymore. So we choose not to display the theoretical line, but rather the fit we have done to our data. As mentioned previously, the two last data points are probably not representative in any way, so they will be left out.

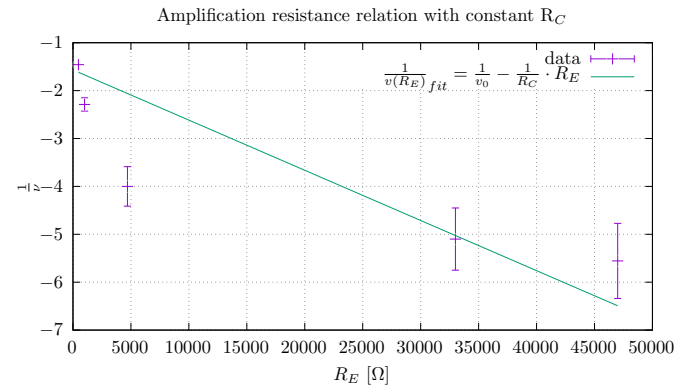


Figure 6: Amplification-Resistance-Relation for constant R_C

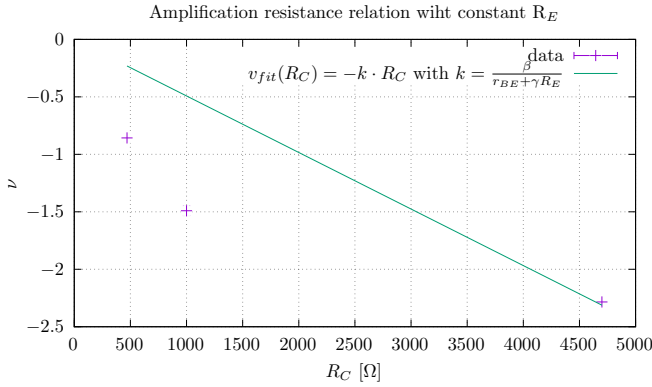


Figure 7: Amplification-Resistance-Relation for constant R_E

Parameter	Value
ν_0	-0.639(95)
R_C	9.5(47) kΩ

Table 3: Fit-Parameter und Werte

Parameter	Value
k	492(58) $\mu\frac{1}{\Omega}$

Table 4: Fit-Parameter und Werte

We have got the values for the parameters presented in tab. 3 and 4. Here we use

$$\frac{1}{\nu}(R_E) = \frac{1}{\nu_0} - \frac{1}{R_C} \cdot R_E \text{ and}$$

$$\nu(R_C) = -k \cdot R_C$$

$$\text{with } k = \frac{\beta}{r_{BE} + \gamma R_E}.$$

When comparing ν_0 , R_C and k to the previous calculated/set values, it is obvious that no fitted values are anywhere near the expected range or order. This is probably a consequence of bad execution of the experiment. Now, without the constructed circuit, it is not easy to tell afterwards where exactly our mistake took place. We noticed a lot of noise throughout the whole lab course, that sometimes could be fixed, or at least fixed to an extent, by moving our connections or holding them in specific but seemingly random places. So another source of error could have been the equipment, though we think with the right execution we would have gotten significant better results.

4.4 Alternating current cancellation of negative feedback

In this task, the noise visible on the oscilloscope is reduced by increasing the voltage of the input signal.

Changing R_E to be zero, the amplification $|\nu|$ is maximised. The range in which the transistor has enough voltage to output a sinusoidal signal, meaning the signal lies within the dynamic range, is between $R_P \in [1.359 \text{ k}\Omega, 3.161 \text{ k}\Omega]$. R_P is the potentiometer changing the offset voltage. For $R_E = 390 \Omega$ (which is $|\nu| = 1$), the potentiometer has a range of $R_P \in [1.178 \text{ k}\Omega, 10 \text{ k}\Omega = \max(R_P)]$.

Now a capacitor with capacitance $C = 0.1 \mu\text{F}$ is connected in parallel with R_E . The previous amplification of around 10 is achieved for a signal with frequency 44 kHz. This makes sense, because the capacitor in parallel acts as a low pass, letting frequencies below 44 kHz pass through it, such that no amplification of 10 is achieved. The resistance above 44 kHz is high enough so that the signal passes through the transistor and gets amplified.

4.5 Frequency response of a cascode circuit

A [transistor amplifier circuit](#) is constructed on [circuit board 2](#). Output 2 is used here.

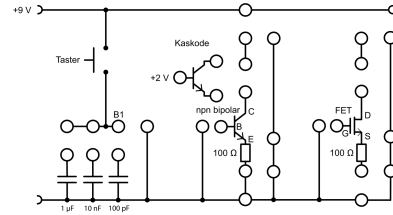


Figure 8: Circuit board 2; Abb. 3.5[?]

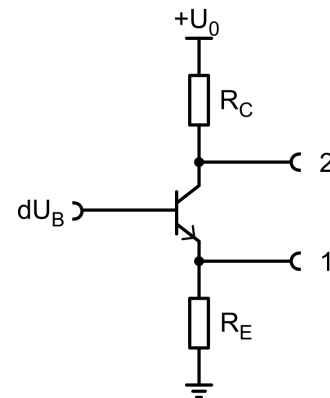


Figure 9: Transistor amplifier circuit using output 2; Abb. 3/4.15[?]

To achieve an amplification of 10, the emitter and collector resistors are chosen to be $R_E = 100 \Omega$ and $R_C = 1 \text{ k}\Omega = 10 \cdot R_E$. The input signal is a sinusoidal

wave of 100 Hz with $U_{PP} = 200$ mV. The DC-offset is set via a voltage divider.

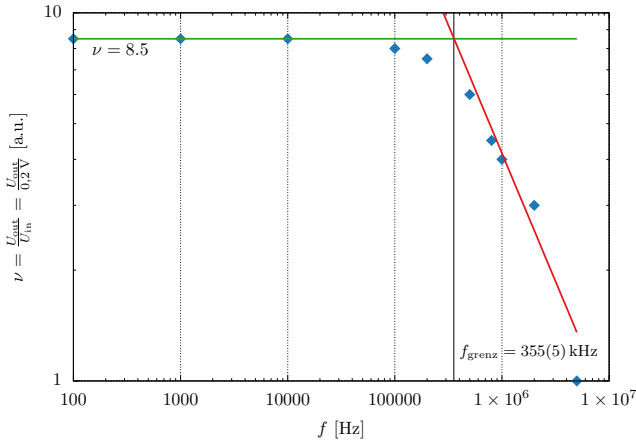


Figure 10: Bode-plot of a transistor amplifier circuit

frequency [Hz]	voltage [V]	ν [a.u.]
100	1.7	8.5
1000	1.7	8.5
10000	1.7	8.5
100000	1.6	8.0
200000	1.5	7.5
500000	1.2	6.0
800000	0.9	4.5
1000000	0.8	4.0
2000000	0.6	3.0
5000000	0.2	1.0

Table 5: Values to 10

The fit curve is given by $f(x) = x^m \cdot b$, with $m = -0.695\,813(246300) \text{ Hz}^{-1}$ and $b = 62\,123.800(2149) \times 10^5$. As expected, the amplification stays the same until the cutoff frequency $f_{\text{grenz}} = 355(5) \text{ kHz}$ is reached. After that, the amplification decreases exponentially. At an amplification of $\nu = 1$ the input voltage of 200 mV is reached. The transit frequency is calculated via

$$f_T = f_{\text{grenz}} \nu_0 = 355(5) \text{ kHz} \cdot 8.5 = 3017.5(425) \text{ kHz}. \quad (4.1)$$

To calculate the bandwidth one can solve for x in

$$1 = x^m \cdot b \quad \Leftrightarrow \quad x = B = 7.73(61) \text{ MHz}. \quad (4.2)$$

Due to lack of time, it was not possible to construct the cacode circuit and measure the amplification-frequency relation again. Though it was expected to see a decline in amplification for an increase in bandwidth. The transit frequency would have still been the same.

4.6 Amplifier with negative feedback

Due to time constraints it was not possible to complete the final task.

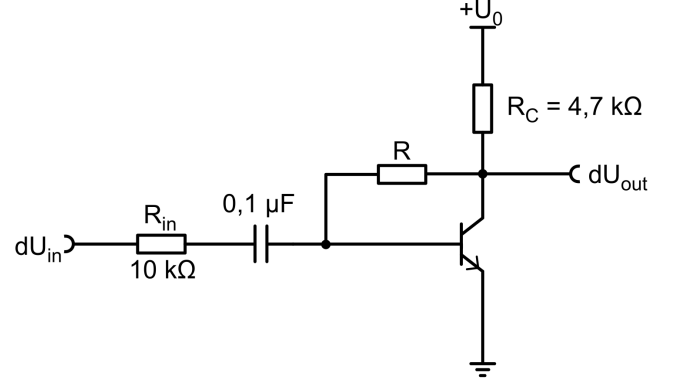


Figure 11: Amplifier with negative feedback; Abb. 4.1[?]

With $R = 100 \text{ k}\Omega$ as well as $R = 33 \text{ k}\Omega$ the voltage amplification $\frac{dU_{\text{out}}}{dU_{\text{in}}}$ should have been measured for an input frequency of $f = 1 \text{ kHz}$.

Because R_{in} reduces the amplification, measurements have to be taken after R_{in} as well. One would expect an increase in amplification because no voltage can drop across R_{in} .

5 Conclusion

In this lab course we have further explored the common collector as voltage amplifier. Furthermore we build a common collector as buffer amplifier with the example of a speaker. This was, due to some complications, sadly not possible to construct, but the theory was still understood. After the common collector, we build a common emitter, which acted as inverter amplifier. The inversion was nicely observed with Lissajous Figures. Afterwards we tried to measure the amplification, which was not quite possible. We took measurements but in the analysis it was quite quickly clear, that the results were not following the theory. But the measurements were still good enough to extract e.g. ν_0 and directly see the discrepancy ($\nu_0 = -26.8(10)$ in comparison to the $-0.639(95)$ through the fitting). Also one could demonstrate the effect of an high-pass used in an amplifier, by connecting a capacitor in parallel and comparing the frequencies at which a similar amplification is achieved.

The cutoff frequency of an amplifier circuit is demonstrated in a bode-plot (10). It can be seen that the amplification stays constant and suddenly falls at the cutoff frequency of $f_{\text{grenz}} = 355(5) \text{ kHz}$. One can now calculate the transit frequency to be $f_T = 3017.5(425) \text{ kHz}$ and the bandwidth $B = 7.73(61) \text{ MHz}$.

Due to lack of time the comparison with a cascode expected results have been discussed nevertheless. circuit as well as the last task couldn't be completed. The

List of Figures

1	Transistor amplifier as common collector with negative feedback (voltage); figure 3/4.16 [?]	1
2	Circuit board 1[?]	3
3	Phase relationship in phase space	3
4	Phase relationship in voltage/time space	3
5	Voltage amplification	4
6	Amplification-Resistance-Relation for constant R_C	4
7	Amplification-Resistance-Relation for constant R_E	5
8	Circuit board 2; Abb. 3.5[?]	5
9	Transistor amplifier circuit using output 2; Abb. 3/4.15[?]	5
10	Bode-plot of a transistor amplifier circuit	6
11	Amplifier with negative feedback; Abb. 4.1[?]	6

List of Tables

1	Voltage amplification for different resistor combinations	3
2	Voltage amplification for different resistor combinations	4
3	Fit-Parameter und Werte	5
4	Fit-Parameter und Werte	5
5	Values to 10	6