3/4 (2. Halbtag) | Transistor und Transistorverstärker

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Contents

1 Introduction

In this experiment, the bipolar transistor is used, but here as an emitter sequence for voltage amplification and as an impedance converter (buffer). Also, the negative feedback of alternating current and the behavior of different frequencies will be observed via a cascode circuit.

2 Theory

The whole theory of different kinds of transistors is still needed.

An emitter follower is an electronic component, with which a current can be amplified (factor γ), without any change in voltage (factor ν).

$$\nu = \frac{\mathrm{d}U_E}{\mathrm{d}U_B} \approx 1 \qquad \gamma = \frac{\mathrm{d}I_E}{\mathrm{d}I_B} \approx 100. \tag{2.1}$$

This is why sometimes an emitter follower is called an impedance changer.

The negative feedback factor k denotes, which fraction of the output voltage is used for the negative feedback

$$\frac{1}{\nu} = \frac{1}{\nu_0} + k. \tag{2.2}$$

Though the amplification with negative feedback ν is lower than the open–loop gain ν_0, ν is only dependent on the circuit and not on the transistor itself. This amplification can be described as follows

$$\frac{\mathrm{d}\nu}{\nu} = \frac{\mathrm{d}\nu_0}{\nu_0}\frac{\nu}{\nu_0}. \tag{2.3}$$

The bandwidth of the amplifier circuit is the frequency band, in which the amplification is constant. To increase the bandwidth, one can use a cascode circuit. To achieve such an amplification, the alternating voltage feedback of the collector on the basis is reduced by utilizing a second transistor to prevent a voltage swing. Given an input signal, the resulting change in voltage will be significantly lower than the change in the output signal. This results in a higher bandwidth.

Stabilization of the operating point can be achieved by using negative feedback, in particular negative feedback of voltage.

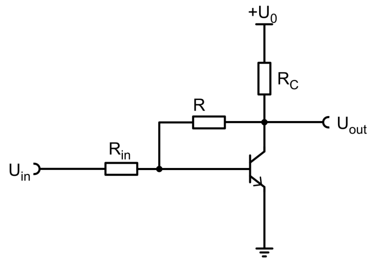

Figure 1: Transistor amplifier as common collector with negative feedback (voltage); figure 3/4.16 [1]

In this figure the resistor R sets the base potential as well as the operating point and couples the voltage from the collector back to the base. Due to this negative feedback the base current is reduced although the input current remains constant.

3 Preliminary Tasks

3.1 G

Zz $\nu = \frac{\gamma R_E}{r_{BE}+\gamma R_E}$ with $\gamma = \frac{\mathrm{d}I_E}{\mathrm{d}I_B}$ and $r_{BE} = \frac{\mathrm{d}U_{BE}}{\mathrm{d}I_B}$.

$$\nu = \frac{\mathrm{d}U_E}{\mathrm{d}U_B} \tag{3.1}$$

$$\Leftrightarrow \quad = \frac{\mathrm{d}I_E R_E}{\mathrm{d}U_{BE} + \mathrm{d}U_E}$$

$$\Leftrightarrow \quad = \frac{\frac{\mathrm{d}I_E R_E}{\mathrm{d}I_B}}{\frac{\mathrm{d}U_{BE}}{\mathrm{d}I_B} + \frac{\mathrm{d}U_E}{\mathrm{d}I_B}}$$

$$\Leftrightarrow \quad = \frac{\gamma R_E}{r_{BE} + \gamma R_E}. \tag{3.2}$$

3.2 H

The equation applies

$$\frac{r_{\text{out}}}{r_{\text{in}}} = \frac{\frac{\mathrm{d}U_E}{\mathrm{d}I_E}}{\frac{\mathrm{d}U_B}{\mathrm{d}I_B}} \tag{3.3}$$

$$\Leftrightarrow \quad = \frac{\mathrm{d}U_E}{\mathrm{d}I_E}\frac{\mathrm{d}I_B}{\mathrm{d}U_B}$$

$$\Leftrightarrow \quad = \frac{\mathrm{d}U_E}{\mathrm{d}U_B}\frac{\mathrm{d}I_B}{\mathrm{d}I_E}$$

$$\Leftrightarrow \quad \approx 1 \cdot \frac{1}{\gamma}. \tag{3.4}$$

3.3 I

The equation applies

$$\nu = \frac{\mathrm{d}U_C}{\mathrm{d}U_B} \tag{3.5}$$

$$\Leftrightarrow \quad = \frac{\mathrm{d}I_C R_C}{\mathrm{d}U_{BE} + \mathrm{d}U_E}$$

$$\Leftrightarrow \quad = \frac{\frac{\mathrm{d}I_C R_C}{\mathrm{d}I_B}}{\frac{\mathrm{d}U_{BE}}{\mathrm{d}I_B} + \frac{\mathrm{d}U_E}{\mathrm{d}I_B}}$$

$$\Leftrightarrow \quad = \frac{\beta R_C}{r_{BE} + \gamma R_E}. \tag{3.6}$$

3.4 J

The equation applies

$$\frac{1}{\nu} = \frac{1+k\nu_0}{\nu_0} \tag{3.7}$$

$$\Leftrightarrow \quad \nu = \frac{\nu_0}{1+k\nu_0}$$

$$\Leftrightarrow \quad \frac{\mathrm{d}\nu}{\mathrm{d}\nu_0} = \frac{1}{(1+k\nu_0)^2}$$

$$\Leftrightarrow \quad = \frac{\nu}{\nu_0}\frac{1}{1+k\nu_0}$$

$$\Leftrightarrow \quad \frac{\mathrm{d}\nu}{\nu} = \frac{\mathrm{d}\nu_0}{\nu_0}\frac{1}{1+k\nu_0}$$

$$\Leftrightarrow \quad = \frac{\mathrm{d}\nu_0}{\nu_0}\frac{\nu}{\nu_0}. \tag{3.8}$$

3.5 K

The parallel capacitor with capacitance C_{CB} and transistor form a high–pass filter. This means that high frequency signals will run through the capacitor and not the transistor, resulting in them not being amplified.

3.6 L

There is no voltage change at point P, because the input signal to the transistor T2 is constant. The change in current $\mathrm{d}I_E\,(T_2)$ is in return also zero.

3.7 M

For any transit frequency the equation holds $f_{\text{grenz gk}}\nu\,(f=0) = f_{\text{grenz}}\nu_0$. Thus $f_{\text{grenz gk}} = f_{\text{grenz}}\frac{\nu_0}{\nu(f=0)}$.

3.8 N

For increasing base current I_B, the collector voltage U_C and the voltage across the resistor U_{R_C} also increases. Because U_0 should be constant, the voltage drops across the resistor R, which in turn stabilizes the operating point.

4 Analysis

4.1 Voltageamplifier of the common collector

On circut board I (Fig. 2) we construct a common collector with $\mathrm{d}U_B = 2.1\,\mathrm{V_{PP}}$ and $U_B \approx 2\,\mathrm{V}$. To test the voltage ampilification we chose a variety of diffrent resistor combinations. The messurements are displayed in Tab. 1. We expect no change for diffrent R_E.

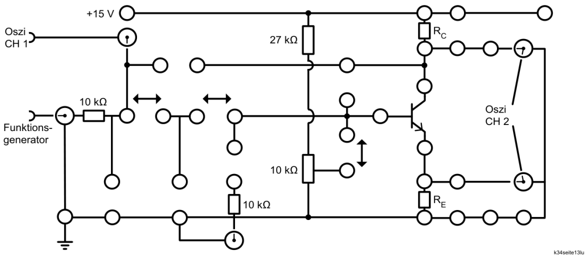

Figure 2: Circut board 1[1]

R_C	R_E	amplification ν
$360\,\Omega$	$1\,\mathrm{k\Omega}$	1.000(25)
$360\,\Omega$	$22\,\mathrm{k\Omega}$	1.025(25)
$360\,\Omega$	$47\,\mathrm{k\Omega}$	1.015(25)
$1\,\mathrm{k\Omega}$	$360\,\Omega$	0.945(25)
$22\,\mathrm{k\Omega}$	$360\,\Omega$	0.114(25)
$47\,\mathrm{k\Omega}$	$360\,\Omega$	0.120(25)

Table 1: Voltage amplification for diffrent resistor combinations

As we see, there is no significant variation of the amplification for diffrent R_E. Though we can clearly see a lowering of the amplification for higher R_C, wich is plausible since we have less current that can be amplified.

4.2 Common collector as buffer amplifier

Here we are tasked to match the impedance of a speaker, so we are able to hear an output. For this we firstly construct an Inverted Amplifiert and test the speaker solely without a common collector. We observe, that the speaker does not produce any sound, because we havent matched the impedance. Now we add a common collecter as a buffer amplifier, wich in theroy should be able to match the impedance of the speaker. Unfortunatly we could not get the circut running and test the hypothisis.

4.3 Inverted amplifier

4.3.1 Phasere relationship between input and output

Now we build a common emitter on circuit board I with $R_C = R_E = 390\,\Omega$, $\mathrm{d}U_B = 0.5\,\mathrm{V_{PP}}$, $U_B = 1.5\,\mathrm{V}$ and we choose a capacity prior to the input signal of $0.1\,\mathrm{\mu F}$. As we can see in the xy (CH1, CH2) configuration in fig. 3, the phase is not linear, but eliptic. Thus we have not the same phase. We found out through experimenting, that the multiple elipsis come from noise. The phase relationship and especially the noise is also visible in fig. 4, as the lines are rather thicc. We can see that the phase diffrence is between $\frac{1}{2}\pi$ and 1π, because we now have coupled the capacitor.

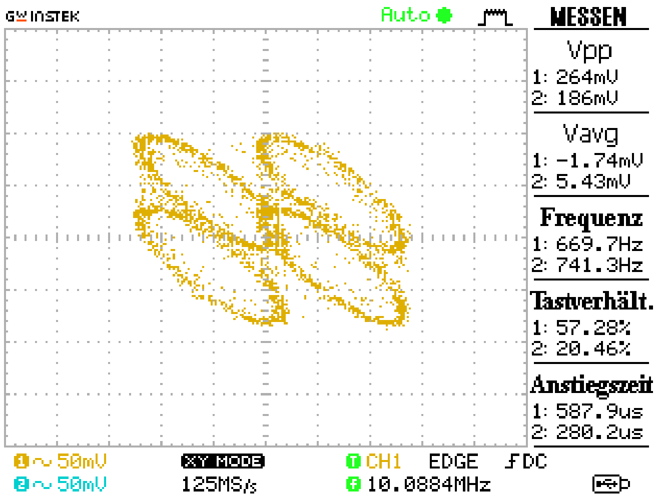

Figure 3: Phase relationship in phase space

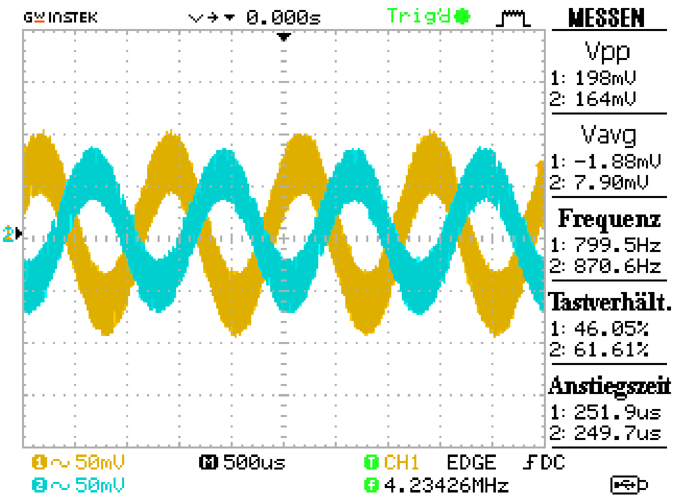

Figure 4: Phase relationship in voltage/time space

4.3.2 Voltage amplification of the inverted amplifier

We measure the voltage amplification with diffrent values for the resistors R_E and R_C. The results are display in tab. 2.

R_C	R_E	amplification ν	$\nu = -\frac{R_C}{R_E}$
$360\,\Omega$	$470\,\Omega$	$-0.686(24)$	-0.830
$360\,\Omega$	$1\,\mathrm{k}\Omega$	$-0.437(24)$	-0.390
$360\,\Omega$	$4.7\,\mathrm{k}\Omega$	$-0.250(25)$	-0.083
$360\,\Omega$	$33\,\mathrm{k}\Omega$	$-0.196(25)$	-0.012
$360\,\Omega$	$47\,\mathrm{k}\Omega$	$-0.180(25)$	-0.008
$470\,\Omega$	$360\,\Omega$	$-0.857(24)$	-1.205
$1\,\mathrm{k}\Omega$	$360\,\Omega$	$-1.491(25)$	-2.564
$4.7\,\mathrm{k}\Omega$	$360\,\Omega$	$-2.284(22)$	-12.05
$33\,\mathrm{k}\Omega$	$360\,\Omega$	$-0.234(27)$	-84.62
$47\,\mathrm{k}\Omega$	$360\,\Omega$	$-0.234(27)$	-120.5

Table 2: Voltage amplification for diffrent resistor combinations

We notice that the part, where R_C stays constant, the experimental values follow the theoretical ones in thier generall trend, but are not exactly the same. For the part where R_E stays constant we observe that first the data follows the calculations, but to the end, with the highest restance, just drop. It seems that there is a sweetspot for an optimal amplification. Then it should have to do something with resonace, so the amplification is frequency dependent.

4.3.3 Resistance of a Transistor

Now with the special case, that $R_E = 0\,\Omega$ and $E_C = 390\,\Omega$, we can read the peak-to-peak voltage from oscillogramm and calculate the amplification and $\beta = \frac{I_C}{I_E}$ with $I = \frac{U}{R}$.

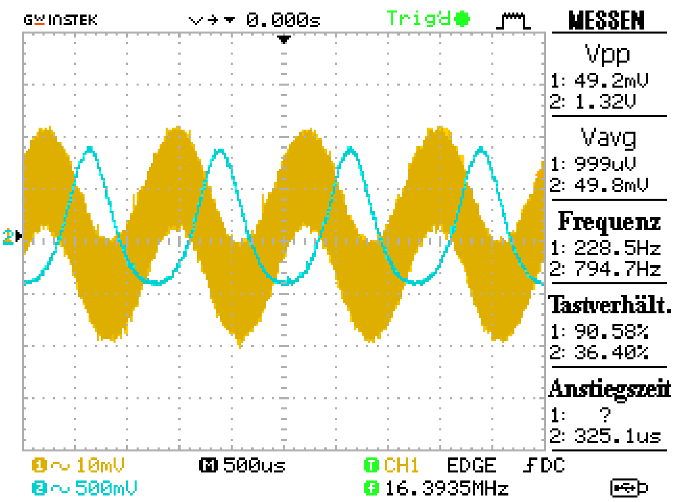

Figure 5: Phase relationship in phase space

4.4 Common Collector as Buffer Amplifier

Here we are tasked to match the impedance of a speaker, so we are able to hear an output. For this we firstly construct an Inverted Amplifiert and test the speaker solely without a Common Collector. We observe, that the speaker does not produce any sound, because we havent matched the impedance. Now we add a Common Collecter as a Buffer Amplifier, wich in theroy should be able to match the impedance of the speaker. Unfortunatly we could not get the circut running and test the hypothisis.

4.5 Inverted Amplifier

4.5.1 Phasere Relationship between input and output

Now we build a Common Emitter on Circut Board I

4.6 Alternating current cancellation of negative feedback

In this task, the noise visible on the oszillograph is reduced by increasing the voltage of the input signal.

Changing R_E to be zero, the amplification $|\nu|$ is maximised. The range in which the transistor has enough voltage to output a sinusoidal signal, meaning the signal lies within the dynamic range, is between $R_P \in [1.359\,\mathrm{k}\Omega, 3.161\,\mathrm{k}\Omega]$. R_P is the potentiometer changing the offset voltage. For $R_E = 390\,\Omega$ (which is $|\nu| = 1$), the potentiometer has a range of $R_P \in [1.178\,\mathrm{k}\Omega, 10\,\mathrm{k}\Omega = \max(R_P)]$.

Now a capacitor with capacitance $C = 0.1\,\mu\mathrm{F}$ is connected in parallel with R_E. The previous amplification of around 10 is achieved for a signal with frequency 44 kHz. This makes sense, because the capacitor in parallel acts as a low pass, letting frequencies below 44 kHz pass through it, such that no amplification of 10 is achieved. The resistance above 44 kHz is high enough so that the signal passes through the transistor and gets amplified.

4.7 Frequency response of a cascode circuit

A transistor amplifier circuit is constructed on circuit board 2. Output 2 is used here.

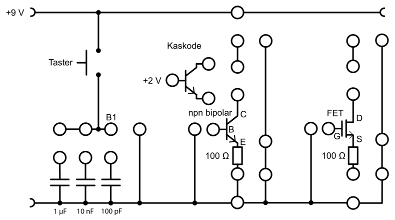

Figure 6: Circuit board 2; Abb. 3.5[1]

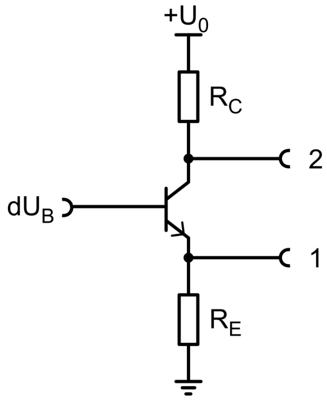

Figure 7: Transistor amplifier circuit using output 2; Abb. 3/4.15[1]

To achieve an amplification of 10, the emitter and collector resistors are chosen to be $R_E = 100\,\Omega$ and $R_C = 1\,\mathrm{k}\Omega = 10 \cdot R_E$. The input signal is a sinusoidal wave of 100 Hz with $U_{PP} = 200\,\mathrm{mV}$. The DC–offset is set via a voltage divider.

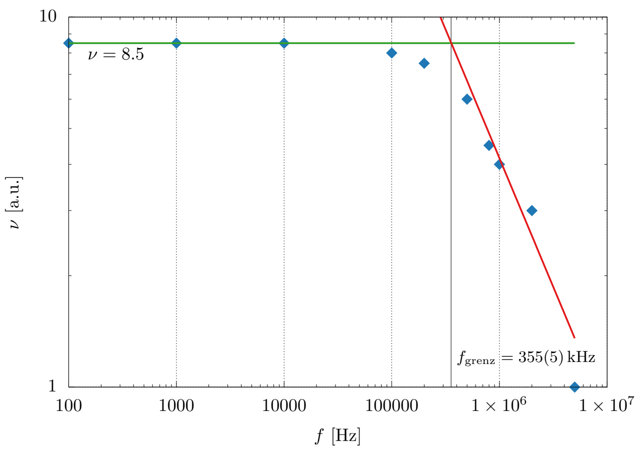

Figure 8: Bode–diagram of a transistor amplifier circuit

The fit curve is given by $f(x) = x^m \cdot b$, with $m = -0.695\,813(246300)\,\mathrm{Hz}^{-1}$ and $b = 62\,123.800(2149) \times 10^5$. As expected, the amplification stays the same until the cutoff frequency $f_{\mathrm{grenz}} = 355(5)\,\mathrm{kHz}$ is reached. After that, the amplification decreases exponentially. At an amplification of $\nu = 1$ the input voltage of 200 mV is reached. The transit frequency is calculated via

$$f_T = f_{\mathrm{grenz}} \nu_0 = 355(5)\,\mathrm{kHz} \cdot 8.5 = 3017.5(425)\,\mathrm{kHz}. \tag{4.1}$$

To calculate the bandwidth one can solve for x in

$$1 = x^m \cdot b \quad \Leftrightarrow \quad x = B = 7.73(61)\,\mathrm{MHz}. \tag{4.2}$$

Due to lack of time, it was not possible to construct the cacode circuit and measure the amplification–frequency relation again. Though it was expected to see a decline in amplification for an increase in bandwidth. The transit frequency would have still been the same.

4.8 Amplifier with negative feedback

Due to time contrains it was not possible to complete the final task.

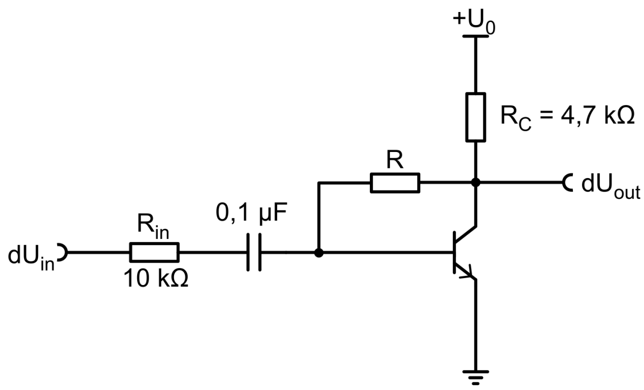

Figure 9: Amplifier with negative feedback; Abb. 4.1[1]

With $R = 100\,\mathrm{k}\Omega$ as well as $R = 33\,\mathrm{k}\Omega$ the voltage amplification $\frac{\mathrm{d}U_{\mathrm{out}}}{\mathrm{d}U_{\mathrm{in}}}$ should have been measured for an input frequency of $f = 1\,\mathrm{kHz}$.

Because R_{in} reduces the amplification, measurements have to be taken after R_{in} as well. One would expect an increase in amplification because no voltage can drop across R_{in}.

List of Figures

List of Tables

Source

[1] Fabian Hügging. *Elektronik–Praktikum Versuchsanleitung*. Universität Bonn, kurs b edition, 2024.