TORNO

80 mm delante la base de la mordaza y linea central ORIGEN DE SISTEMA DE REFERENCIA

Coordenadas en programas

S S

70

Offset para herramienta T0101 para el uso con G50

X162.775 Z110.024

CU 1/3/00

153

Centro de Automatización de Procesos

Torno - "offsets" de herramientas

Origen	en control:
80 mm	atrás do nio da mandana

Z X

ordaza					W-Shift	1 1 - 4/100	1,542
X	Z	R	T	zero X	zero Z	fecha	operario
0.000	0.000	0.4		162.775	110.024	01/03/00	CU
0,000	0,000	0,4		159,500	·110.024	02/10/00	IJ
A					1547 (p.Onto	Top No. of Control
22.179	ten kret		_			Jan 1963	5.07
Х	Z	R	Т	zero X	zero Z	fecha	operario
16.433	-0,277	0.4		146,342	110,301	01/03/00	CU
13,652	-0,27	0,4		201-8	4970.2	Terrior I	JJ
X	Z	R	Т	zero X	zero Z	fecha	operario
-0,325	-10,346	0.4		163,100	120,370	01/03/00	CU
7,849	-10,622	0,4					JJ
A.		- 10		11-7-2	2010		O.V
X	Z	R	Т	zero X	zero Z	fecha	operario
-6,705	45,616			1122.01		30/05/00	CU
-8,281	45,580				1 1 31		JJ
×							
X	Z	R	T	zero X	zero Z	fecha	operario
0,385	-4,877						CU
-1,200	-5,210				114,001	01700700	J 7
			_		-		· ·
			Т	zero X	zero Z	fecha	operario
						01/03/00	CU
-22,495	45,357	0,4					ŢŢ
X	Z	R	T	zero X	zero Z	fecha	operario
-0,502	-6,522						CU
11,662	-3,649						IJ
X	Z	R	Т	zero X	zero Z	fecha	operario
-19,649	44,310					08/03/00	CU
- 27,192	44,529						1]
1 1							
	X 0.000 0,000 X 16.433 /3,652 X -0,325 7,849 X -6,705 -8,281 X 0,385 -1,200 X -19,925 -22,495 X -0,502 ///,662	X Z 0.000 0.000 0,000 0,000 X Z 16.433 -0,277 13,652 -0,27 X Z -0,325 -10,346 7,849 -10,622 X Z -6,705 45,616 -8,281 45,580 X Z 0,385 -4,877 -1,200 -5,210 X Z -19,925 45,349 -22,495 45,357 X Z -0,502 -6,522 11,662 -3,649 X Z -19,649 44,310	X Z R 0.000 0.000 0.4 0.000 0.000 0.4 X Z R 16.433 -0.277 0.4 /3,652 -0.27 0.4 /3,652 -0.27 0.4 X Z R -0,325 -10,346 0.4 7,844 -10,622 0.4 X Z R -6,705 45,616 -8,281 45,580 X Z R 0,385 -4,877 -1,200 -5,210 X Z R -19,925 45,349 0.4 -22,495 45,357 0.4 X Z R -19,662 -3,649 X Z R -19,649 44,310	X Z R T 0.000 0.000 0.4 0.000 0.000 0.4 X Z R T 16.433 -0.277 0.4 //3,652 -0.27 0.4 //3,652 -0.27 0.4 X Z R T -0.325 -10.346 0.4 7,849 -10.622 0.9 X Z R T -6,705 45,616 -8,281 45,580 X Z R T 0.385 -4,877 -1,200 -5,210 X Z R T -19,925 45,349 0.4 -22,495 45,357 0.9 X Z R T -0,502 -6,522 //,662 -3,649 X Z R T -19,649 44,310	X Z R T zero X 0.000 0.000 0.4 162.775 0,000 0,000 0,4 162.775 0,000 0,000 0,4 163.750 X Z R T zero X 16.433 -0,277 0.4 146,342 /3,652 -0,27 0,4 163,100 7,849 -10,642 0,4 X Z R T zero X -6,705 45,616 -8,281 45,580 X Z R T zero X 0,385 -4,877 162,390 -/,200 -5,2/0 X Z R T zero X -1,200 -5,2/0 X Z R T zero X	X	X

CU 30/05/00

T0709	X	Z	R	T	zero X	zero Z	fecha	operario
erforar/cortar, izquierda	-0,502	-4,372					08/03/00	CU
			100					
1 2 2 2 5 5 5 5 7	75	4 4 5						
Τ0410	X	Z	R		zero X	zero Z	fecha	operario
proca D12.5 (max 52)		62,786	- '\	-	Zeiox	2010 2	30/05/00	CU
3100a B12.5 (11ax 32)	-5,882	02,700		-			00/00/00	
				-				
	-			-				
T0411	VI	Z	R		zero X	zero Z	fecha	operario
	X		- K	-	Zeio X	2010 2	30/05/00	CU
broca D13 (max 54)	-5,495	64,274	-	-		-	30/03/00	- 00
				_				
	No. VIII.		-	-				
T0440	VI	71	ы	-	zero X	zero Z	fecha	operario
T0412	X	Z	R	-	2610 /	2610 2	icciia	operano
mandril Dxx (max xx)		0.4.		-				ch 8/6/0
Stot Drill D6	-5.305	76.140		-				2-1 6/0/0
				-				
	-							
70440	X	Z	R		zero X	zero Z	fecha	operario
T0413	_^	- 4	-	-	2610 /	2010 2	lecila	operano
mandril Dxx (max xx)				-	-			
			-	-				
			-	-+				
	X	Z	R		zero X	zero Z	fecha	operario
Txx14			- 1	-	2010 X	2010 2	icciia	operano
				-				
				\dashv				
A STREET				-				
the competition of	100.5	100						
	- VI	Z	R	-	zero X	zero Z	fecha	operario
Txx15	X	- 4	-	-	Zelo A	2610 2	leciia	орегано
	-							
				-				
				\rightarrow				
	- UI		DI		TOTA VI	7022 71	footo	operacio
Txx16	X	Z	R	-	zero X	zero Z	fecha	operario
			\rightarrow	\rightarrow				
				\dashv				
1			- (- 1				

CU 30/05/00

(D)

Lista de los comandos del torno

Códigos G - Torno

G-Co G00 G01 G02 G03 G04	de. 0 1 1 1 1 0	Positioning (Rapid Traverse) Linear Interpolation (Feed) Circular Interpolation CW Circular Interpolation CCW Dwell
G10	0	Offset Value Setting By Program
G20 G21 G22 G23	6 6 9	Inch Data Input Metrie Data Input Stored Stroke Check On Stored Stroke Check Off
G27 G28 G29	0 0	Reference Point Return Check Reference Point Return Return From Reference Point
G30 G31 G32	0 0 1	Return To 2nd Reference Point Skip Function Thread Cutting
G34	1	Variable Lead Thread Cutting
G36 G37	0	Automatic Tool Compensation X Automatic Tool Compensation Z
G40 G41 G42	7 7 7	Tool Nose Radius Compensation Cancel Tool Nose Radius Compensation Left Tool Nose Radius Compensation Right
G50	0	Work Co-ord. Change/Max. Spindle Speed setting



CI 146/5/00

G65 G66	0 12	Macro Call Macro Modal Call
G67	12	Macro Modal Call Cancel
G70	4	Finishing Cycle
G71	4	Stock Removal in Turning
G72	0	Stock Removal in Facing
G73	0	Pattern Repeating
G74	0	Peck Drilling in Z Axis
G75	0	Grooving in X Axis
G76	0	Thread Cutting Cycil
G90	1	Cutting Cycle A
G92	1	Thread Cutting Cycle
G94	1	Cutting Cycle B
G96	2	Constant Surface Speed Control
G97	2	Constant Surface Speed Control Cancel
G98	11	Feed Per Minute
G99	11	Feed Per Revolution

G codes of group 0 represent those non modular and are effective to the designated block.

G codes of different groups can be commanded to the same block indefinitly. If more than one G code from the same group are commanded, the later becomes effective.

	* ** ** ** ** ** ** ** ** ** ** ** ** *
M40 M41	Parts catcher extend Parts catcher retract
M43 M44 M45	Swarf conveyor forward Swarf conveyor reverse Swarf conveyor stop
M48 M49	lock % f eed and % sbeed at 100 % Cancel M48 (default)
M50 M51 M52 M53 M54	Wait for axis in position signal (cancels continuous path) Cancel M50 (default) Pull-out in threading = 90 degrees (default) Cancel M52 Disable spindle fluctuation testing (def ault)
M56 M57	Select internal chucking (from PLC edition "F") Select external chucking (from PLC edition "F")
M62 M63 M64 M65 M66* M67* M68 M69	Auxiliary Output 1 On Auxiliary Output 2 On Auxiliary Output 1 Off Auxiliary Output 2 Off Wait for Auxiliary Output 1 On Input Wait for Auxiliary Output 2 On Input Only index with all axes at home position Index turret anywhere
M 70	Mirror in X On
M76 M77	Wait for Auxiliary Output 1 Off (from revision C) Wait for Auxiliary Output 2 Off (from revision C)
M80	Mirror in X Off
M98 M99	Sub Program Call Sub Program End

M codes marked with an * are executed at the end of a block, ie, after axis movement.

```
8 M66
        M39
        G99G97G40G21S2000
        G28U0W0
       M06T0101 M03
        G00X32Z0
        G01X-1F0.05
        z_1
   628U0W0
        M06T0303S2000
                                    0202
        G00X32Z2
        G71U1R0.05
        G71P102U0.05W0.1F0.05
        N1G00X0
       →G01Z0F0.05
      CG03X8Z-1.8R11.35F0.05
  Pendiente G01X5Z-17F0.05
     (G03X12Z-20R5.19F0.05
     ↔ G01Z-21F0.05
      (G03X28Z-27R10.32F0.05
      1 X32
        MO6TØ0X0X
   Perdiente GOOX28Z-27
     G01X12F0.05
      ⊃G02X8Z-32R6.18F0.05
  Pardienic G01X6Z-37F0.05
      CG03X12Z-39R4.59F0.05
    ↔ G01Z-40.5F0.05
      ( G03X18Z-42.5R3.66F0.05
    ←> G01Z-44F0.05
      CG03X24Z-45.5R2.55F0.05
    \longleftrightarrow G01<u>Z-47</u>.5F0.05
      $ G01X10F0.05
 Pero G01X8Z-54F0.05
      G02X14Z-60R8.36F0.05
Parliente G01X12Z-61F0.05
Padrate G01X30Z-67F0.05
    \leftrightarrow G01Z-70F0.05
        N2X34
        G70P1Q2
```

Página 1

Códigos M - Torno

	and the second of the second o
M00 M01* M02* M03 M04 M05* M06 M07 M08 M09*	Program Stop Optional Stop Program Reset Spindle Forward (clockwise) Spindle Reverse (counter clockwise) Spindle Stop Automatic Tool Change Coolant "B" On Coolant "A" On Coolant Off
M10 M11	Chuck Open Chuck Close
M13 M14 M15 M16	Spindle Forward and Coolant On Spindle Reverse and Coolant On Program Input using MIN P (special function) Special Tool Call (tool call ignores turret)
M19	Spindle Orientation
M20 M21 M22 M23	Spindle Index A Spindle Index 2A Spindle Index 3A Spindle Index 4A
M25 M26	Quill Extend Quill Retract
M29	Select DNC mode
M30 M31	Program Reset and Rewind Increment parts counter
M37 M38	Door open to stop Door Open Door Close

Reassessing power factors

Certain published data promotes inaccuracy when calculating horsepower for turning operations

Dr. Edmund Isakov Kennametal Inc.

Edited by Thomas J. Grasson

vailable power on turning equipment places limits on cut size. Thus it is important to calculate horsepower properly when developing specifications for new equipment or optimizing existing operations.

This raises concern about the accuracy of the p values used in calculating horsepower requirements since many of the published values are not precise enough for accurate calculations.

The p value, also known as power unit or K factor, is an experimentally determined constant and is equal to the horsepower required to cut a material at a rate of one in.3/min. The unit of measure of p is hp/in.3/min.

The common method of estimating horsepower in turning is based on metal removal rate (Q) and p for workpiece materials. Horsepower at the cutting tool (Pc) is found from: $P_c = Q \times p$

The metal removal rate is calculated by the formula:

 $Q = 12 \times d \times f \times V_c$

where d is the depth of cut in inches; f is the feed rate in in/rev. (ipr); V_c is the cutting speed in sur-

Dr. Isakov is senior staff engineer at Metalworking Systems Engineering, Kennametal Inc., Raleigh.

	Workpiece			p values at machining conditions			
Material	Designation	Brinell hardness	General purpose	Finishing	Roughing		
Carbon	AISI 1018	141	0.62	0.70	0.66		
Carbon steel	AISI 1045	195	0.72	0.74	0.70		
Alloy steel	AISI 4140	194	0.73	0.79	0.74		
Alloy steel	AISI 4340	214	0.73	0.76	0.72		
Alloy steel	AISI 4140	258	0.79	0.85	0,77		
Alloy steel	AISI 4142	277	0.75	0.84	0.77		
Alloy steel	AISI 4340	485	1.05	1.31	1.00		
Tool steel	AISI HII	205	0.76	0.78	0.73		
Stainless steel	AISI 316L	147	0.73	0.81	0.73		
Stainless steel	AISI 410	243	0.74	0.81	0.71		
Stainless steel	AISI 17-4PH	294	0.72	0.99	0.70		
Gray cast iron	SAE G3000	195	0.47	0.53	0.48		
Ductile cast iron	ASTM 65-45-12	165	0.51	0,58	0.55		
Titanium alloy	AMS Ti-6Al-4V	287	0.62	0,64	0,62		
Nickel alloy	Inconel 718	277	1.02	1.20	1.01		
Aluminum alloy	AMS 2024	139	0.30	0.31	0.29		

The formula for horsepower at the motor (Pm) is:

where E = machine tool efficiency (typically, <math>E = 0.70-0.90).

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face ft/min. (sfm).

The p factors can be found in several handbook publications. However, different handbooks list different values for these power constants that vary by as much as 40 to 50% for the same material and Brinell hardness number. Aggravating this situation, p factors are based on using sharp tools only with no consideration given for type of cut, such as rough, finish, or general purpose.

While many in the metal cutting

industry think of these handbooks as bibles of machining practices, the p factors vary so broadly that people find selecting the proper factor difficult. To correct this situation, special lab tests were conducted to determine actual power-constant values for machining common work materials at various cutting conditions.

A three-force component dynamometer helped measure tangential (F_t) , feed (F_t) , and radial (F_t)

Cutting force components Ft = Tangential force Ff = Feed force Fr = Radial force R = Resultant cutting force

Calculating cutting force components

The cutting force components are tangential (F_d) , feed (F_d) , and radial (F_d) . Calculation of tangential force is important because this force produces torque at the spindle and accounts for the greatest portion of the machining power. Tangential force can be calculated by the general equation:

$$F_t = \frac{33,000 \cdot P_c}{V_c}$$

where 33,000 = conversion factor; 1 hp = 33,000 ft lb/min. Substitution for Pc and Q into the formula produces: $F_t = 396,000 \times d \times f \times p$

AISI	Hardness	Feed	Depth of Cut	Empirical
Steel	BHN	ipr	in.	Formula
1018, 316L,	140-200	0.008-0.010	0.060-0.300	$F_i = 0.581F_i - 18.3$
4140, 1045		0.012-0.020	0.060-0.300	$F_{\ell} = 0.458F_{\ell} - 6.6$
H11, 4340,	205-260	0.008-0.012	0.060-0.300	$F_c = 0.556F_c - 5.3$
410, 4140		0.015-0.020	0.060-0.300	$F_{\ell} = 0.477F_{\ell} + 7.3$

Feed forces calculated by the empirical formulas vary from measured values within ±10% in 82% of all data points and within ±15% in 99% of all data points.

	Relationship between radial and tangential forces			orces
AISI Steel	Hardness BHN	Feed ipr	Depth of Cut in.	Empirical Formula
1018, 316L	140-200	0.010-0.020	0.060-0.150	F,=0.145 F,+ 32.0
4140, 1045		0.010-0.020	0.180-0.300	$F_r = 0.182 F_t - 9.3$
H11, 4340,	205-260	0.008-0.012	0.060-0.300	$F_r = 0.111 F_t + 40.7$
410, 4140		0.015-0.020	0.060-0.300	Fr=0.143 Ft+ 48.7

Radial forces calculated by the empirical formulas vary from measured values within $\pm 10\%$ in 74% of all data points and within $\pm 15\%$ in 93% of all data points.

cutting forces. The measurements were the basis for developing an equation to calculate p factors using the cutting force values. From this equation, actual p value numbers were developed for various materials and machine processes categorized as general purpose, finishing, and roughing.

Verification of p values took place by calculating feed force and radial force based on tangential force and determining the accuracy between the calculated and measured forces.

Recorded and calculated cutting forces

Using the indicated machining conditions, the chart shows recorded and calculated cutting forces when turning 4140 alloy steel with a hardness of 258 BHN.

Cutting force components were measured with a Kistler dynamometer, type 9263. After collection, the data was converted into digital form and recorded. Cutting force components were calculated using the same machining conditions.

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	input data i	n the shaded	cells only
Machining Conditions and Calculations	Symbol	Unit	Value
Workpiece Ma	iterial		
Diameter Hardness Power constant	D BHN P	in. hp/in³/min	4.0 258 0.77
Machining Con	ditions		
1. Depth of cut 2. Feed rate 3. Cutting speed 4. Spindle speed 5. Metal removal rate	d f V _c n Q	in. ipr sfm rpm in³/min	0.200 0.020 900 859 43.2
Calculations of Cut	ting Forces		
Tangential force Feed force Radial force Resultant force	Fr Fr R	lb lb lb lb	1219.7 589.1 223.1 1372.8
Horsepower Cal	culation		
Horsepower at the cutting tool Machine tool efficiency factor Horsepower at the motor	HP _c E HP _m	hp hp	33.3 0.80 41.6

Calculated feed forces varied from measured values within ±10% in 82% of all data points and within ±15% in 99% of all data points. Radial forces calculated by the formulas varied from measured values within ±10% in 74% of all data points and within ±15% in 93% of all data points.

Based on the accuracy of this data, the practical value of p fosters a high confidence factor and is a safe bet when estimating horsepower requirements for turning operations.■

Type of Drive	E
Direct belt drive	0.90
Back gear drive	0.75
Geared head drive	0.70-0.80
Oil-Hydraulic drive	0.60-0.90

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Depth of cut, in.	Feed rate, ipr	p factor	Tangential force, lb		Feed force, lb		Radial force, lb	
			recorded	calculated	recorded	calculated	recorded	calculated
0.080	0.008	0.85	224.7	215.4	130.7	114.5	63.3	64.6
0.080	0.012	0.85	309.2	323.1	149.9	174.3	82.7	76.6
0.140	0.015	0.79	653.8	657.0	365.4	320.7	158.6	142.7
0.200	0.010	0.77	621.9	609.8	347.0	333.7	106.7	108.4
0.200	0.020	0.77	1179.5	1219.7	565.9	589.1	250.6	223.1

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