

Now we have all the equations

Unknowns (15)

• Stress (6)

$$\begin{bmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ & \sigma_y & \tau_{yz} \\ sym. & \sigma_z \end{bmatrix} (x, y, z)$$

• Strain (6)

$$\begin{bmatrix} \varepsilon_{x} & \varepsilon_{xy} & \varepsilon_{xz} \\ & \varepsilon_{y} & \varepsilon_{yz} \\ sym. & \varepsilon_{z} \end{bmatrix} (x, y, z)$$

· Displacement (3)

Governing equations (field equations) (15)

• Equilibrium equations (3)

$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + f_x = 0 \quad (x, y, z)$$

• Strain-displacement (6)

$$\varepsilon_{x} = \frac{\partial u}{\partial x} \qquad \gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \quad (x, y, z; u, v, w)$$

(Compatibility equations(3/6))

· Stress-strain relations

$$\varepsilon_{x} = \frac{1}{E} \left(\sigma_{x} - v \left(\sigma_{y} + \sigma_{z} \right) \right) \quad \gamma_{xy} = \frac{1}{G} \tau_{xy}$$

$$\sigma_{x} = 2G\varepsilon_{x} + \lambda\varepsilon$$
 $\tau_{xy} = G\gamma_{xy} (x, y, z)$

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Solutions

The 15 equations can be reduced to 6 equations in terms of stress, or 3 in terms of displacement

Goals:

- Determination of stress, strain and displacement functions based on field equations
- Satisfying the boundary conditions
- Solution satisfying all conditions for a given problem is unique

Governing equations (field equations) (15)

• Equilibrium equations (3)

$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + f_x = 0 \quad (x, y, z)$$

• Strain-displacement (6)

$$\varepsilon_{x} = \frac{\partial u}{\partial x} \qquad \gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \quad (x, y, z; u, v, w)$$

(Compatibility equations(3/6))

· Stress-strain relations $\varepsilon_{x} = \frac{1}{E} \left(\sigma_{x} - \nu \left(\sigma_{y} + \sigma_{z} \right) \right) \quad \gamma_{xy} = \frac{1}{G} \tau_{xy}$

$$\sigma_x = 2G\varepsilon_x + \lambda\varepsilon$$
 $\tau_{xy} = G\gamma_{xy}$ (x, y, z)

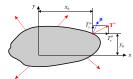
Boundary conditions

- Stress boundary:
 - Based on force equilibrium:

$$\begin{cases} T_{x}^{\mu} = \sigma_{x|0}\mu_{x} + \tau_{yx|0}\mu_{y} + \tau_{zx|0}\mu_{z} \\ T_{y}^{\mu} = \tau_{zy|0}\mu_{x} + \sigma_{y|0}\mu_{y} + \tau_{zy|0}\mu_{z} \\ T_{z}^{\mu} = \tau_{xz|0}\mu_{x} + \tau_{yz|0}\mu_{y} + \sigma_{z|0}\mu_{z} \end{cases}$$

· Displacement boundary:

$$\begin{cases} u(x_0, y_0, z_0) = u_b \\ v(x_0, y_0, z_0) = v_b \\ w(x_0, y_0, z_0) = w_b \end{cases}$$



Boundary point

$$\left(x_{\scriptscriptstyle 0},y_{\scriptscriptstyle 0},z_{\scriptscriptstyle 0}\right)$$
 Unit outward normal

Surface force (stress)

$$\left(T_x^{\mu}, T_y^{\mu}, T_z^{\mu}\right)$$

Direction cosines of μ with respect to x, y and z

 (μ_x, μ_y, μ_z)

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Boundary conditions

- Stress boundary
 - First boundary-value problem

$$T_x^\mu=\pm p,\,T_y^\mu=T_z^\mu=0$$



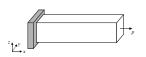
- Second boundary-value problem

$$u_b = v_b = w_b = 0$$

- · Stress & displacement boundary
 - Mixed boundary-value problem







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Plane strain problems

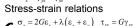
Displacements

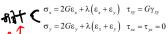
$$\begin{cases} u = u(x, y) \\ v = v(x, y) \\ w = 0 \end{cases}$$

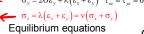
· Strain-displacement

$$\varepsilon_x = \frac{\partial u}{\partial x}$$
 $\varepsilon_y = \frac{\partial v}{\partial y}$ $\gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial z}$

 $\varepsilon_z = \gamma_{yz} = \gamma_{xz} = 0$









$\frac{\partial \sigma_x}{\partial x}$ +	$-\frac{\partial \tau_{yx}}{\partial y} + f_x = 0$
$\frac{\partial \tau_{xy}}{\partial x}$ +	$\frac{\partial \sigma_y}{\partial y} + f_y = 0$



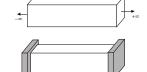


 ϵ_z vanishes, but σ_z does not

Plane strain problems



- **Boundary conditions**
 - Surface forces must be independent of \boldsymbol{z}
 - The body in z direction may be either infinite or finite length with fixed ends



Stress boundary condition:

$$\begin{cases} T_{x}^{\mu} = T_{x}^{\mu}(x_{0}, y_{0}) \\ T_{y}^{\mu} = T_{y}^{\mu}(x_{0}, y_{0}) \end{cases} \longrightarrow \begin{cases} T_{x}^{\mu} = \sigma_{x|0}\mu_{x} + \tau_{yx|0}\mu_{y} \\ T_{y}^{\mu} = \tau_{xy|0}\mu_{x} + \sigma_{y|0}\mu_{y} \end{cases}$$

The only boundary conditions required for plane strain problems are those specified on the lateral surfaces

Displacement boundary condition:

$$\begin{cases} u(x_0, y_0) = u_b \\ v(x_0, y_0) = v_b \end{cases}$$

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Solution of plane strain problems - displacement formulation

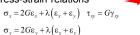
• Displacements

$$\begin{cases} u = u(x, y) \\ v = v(x, y) \end{cases}$$

· Strain-displacement

$$\varepsilon_x = \frac{\partial u}{\partial x}$$
 $\varepsilon_y = \frac{\partial v}{\partial y}$ $\gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$

· Stress-strain relations



• Equilibrium equations

$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + f_x = 0$$
$$\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + f_y = 0$$

 $G\nabla^2 u + (\lambda + G)\frac{\partial}{\partial x} \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}\right) + f_x = 0$ $G\nabla^{2}v + (\lambda + G)\frac{\partial}{\partial y}\left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}\right) + f_{y} = 0$

where
$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$$

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Solution of plane strain problems - stress formulation

• Displacements

$$\begin{cases} u = u(x, y) \\ v = v(x, y) \end{cases}$$

• Strain-displacement

$$\varepsilon_x = \frac{\partial u}{\partial x}$$
 $\varepsilon_y = \frac{\partial v}{\partial y}$ $\gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$



Stress-strain relations

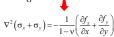
$$\sigma_{x} = 2G\varepsilon_{x} + \lambda(\varepsilon_{x} + \varepsilon_{y}) \quad \tau_{xy} = G\gamma_{xy}$$

ress-strain relations
$$\begin{aligned} & \varepsilon_x = \frac{1}{E} \left((1 - v^2) \sigma_x - v (1 + v) \sigma_y \right) \\ & \sigma_y = 2G \varepsilon_x + \lambda \left(\varepsilon_x + \varepsilon_y \right) \end{aligned} \quad \tau_{xy} = G \gamma_{xy} \\ & \varepsilon_y = \frac{1}{E} \left(\left(1 - v^2 \right) \sigma_y - v (1 + v) \sigma_x \right) \end{aligned}$$

· Equilibrium equations

$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + f_x = 0$$

$$\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + f_y = 0$$



Compatibility equation in terms of stress

Solution of plane strain problems

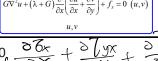
• Equilibrium equations

$$\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yx}}{\partial x} + f_x = 0 \ (x, y)$$

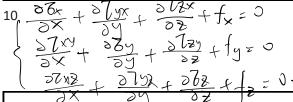
- Hooke's law
- Strain-displacement
- unknowns

Displacement formulation

- 1. Strain-displacement
- 2. Stress-strain relations
- 3. Equilibrium equations (displacement)
- Stress formulation
- Strain-stress relations
- Compatibility equation (stress)
- Equilibrium equations







Solution of 3D problems displacement formulation

Governing equations

• Strain-displacement (6)

$$\varepsilon_x = \frac{\partial u}{\partial x}$$
 $\gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$ $(x, y, z; u, v, w)$

- Stress-strain relations (6)
 - $\sigma_x = 2G\varepsilon_x + \lambda\varepsilon$ $\tau_{xy} = G\gamma_{xy} (x, y, z)$
- Equilibrium equations (3)

$$\frac{\partial \sigma_{x}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + f_{x} = 0 \quad (x, y, z)$$

Substitute strain into Hooke's law

$$\begin{split} &\sigma_{x}=2G\frac{\partial u}{\partial x}+\lambda\epsilon & &\tau_{xy}=G\left(\frac{\partial u}{\partial y}+\frac{\partial v}{\partial x}\right) \\ &\sigma_{y}=2G\frac{\partial v}{\partial y}+\lambda\epsilon & &\tau_{yz}=G\left(\frac{\partial v}{\partial z}+\frac{\partial w}{\partial y}\right) \\ &\sigma_{z}=2G\frac{\partial w}{\partial z}+\lambda\epsilon & &\tau_{z}=G\left(\frac{\partial w}{\partial z}+\frac{\partial u}{\partial y}\right) \end{split}$$

Substitute stress into equilibrium equations

$$\begin{cases} \left(\lambda + G\right)\frac{\partial \varepsilon}{\partial x} + G\nabla^2 u + f_x = 0 \\ \left(\lambda + G\right)\frac{\partial \varepsilon}{\partial y} + G\nabla^2 v + f_y = 0 \end{cases} & \text{Navier's equations} \\ \left(\lambda + G\right)\frac{\partial \varepsilon}{\partial z} + G\nabla^2 w + f_z = 0 \\ & \text{where} & \nabla^2 u = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial x^2}$$

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Solution of 3D problems - displacement formulation

Displacement boundary condition:

$$\begin{cases} u(x_0, y_0) = u_b \\ v(x_0, y_0) = v_b \\ w(x_0, y_0) = w_b \end{cases}$$

Stress boundary conditions: The disperement fight

$$\begin{cases} T_x^{\mu} = \sigma_{x|0} \mu_x + \tau_{yx|0} \mu_y + \tau_{zx|0} \mu_z \\ T_y^{\mu} = \tau_{xy|0} \mu_x + \sigma_{y|0} \mu_y + \tau_{zy|0} \mu_z \end{cases}$$





Solution of 3D problems - stress formulation

Governing equations

• Stress-strain relations (6)

$$\varepsilon_x = \frac{1}{E} \left(\sigma_x - v \left(\sigma_y + \sigma_z \right) \right) \quad \gamma_{xy} = \frac{1}{G} \tau_{xy}$$

• Compatibility equations (3)

$$\frac{\partial^2 \varepsilon_x}{\partial y^2} + \frac{\partial^2 \varepsilon_y}{\partial x^2} = \frac{\partial^2 \gamma_{xy}}{\partial x \partial y}$$

$$2\frac{\partial^{2} \varepsilon_{x}}{\partial y \partial z} = \frac{\partial}{\partial x} \left(-\frac{\partial \gamma_{yz}}{\partial x} + \frac{\partial \gamma_{zx}}{\partial y} + \frac{\partial \gamma_{xy}}{\partial z} \right)$$

• Equilibrium equations (3)

$$\frac{\partial \sigma_{x}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + f_{x} = 0 \quad (x, y, z)$$

- Substitute strain into compatibility equations
- Together with the three equilibrium equations form the final six equations in terms of stress

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$$\frac{\partial^{3} \varepsilon_{x}}{\partial y^{2}} + \frac{\partial^{2} \varepsilon_{y}}{\partial x^{2}} = \frac{\partial^{2} \gamma_{xy}}{\partial x \partial y}$$

$$\frac{\partial^{2} \varepsilon_{y}}{\partial z^{2}} + \frac{\partial^{2} \varepsilon_{z}}{\partial y^{2}} = \frac{\partial^{2} \gamma_{yz}}{\partial y \partial z}$$

$$\frac{\partial^{2} \varepsilon_{x}}{\partial z^{2}} + \frac{\partial^{2} \varepsilon_{x}}{\partial z^{2}} = \frac{\partial^{2} \gamma_{xx}}{\partial z \partial x}$$

$$\begin{cases} \varepsilon_{z} = \frac{1}{E} (\sigma_{x} - v(\sigma_{y} + \sigma_{z})) \\ \varepsilon_{y} = \frac{1}{E} (\sigma_{y} - v(\sigma_{z} + \sigma_{x})) \\ \varepsilon_{z} = \frac{1}{E} (\sigma_{z} - v(\sigma_{z} + \sigma_{y})) \end{cases}$$

$$\gamma_{yz} = \frac{1}{G} \tau_{yz}$$

$$\gamma_{zz} = \frac{1}{G} \tau_{zz}$$

Compatibility equations in terms of stress

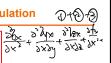
$$\frac{\partial^{2} \sigma_{x}}{\partial y^{2}} - v \frac{\partial^{2} \left(\sigma_{y} + \sigma_{z}\right)}{\partial y^{2}} + \frac{\partial^{2} \sigma_{y}}{\partial x^{2}} - v \frac{\partial^{2} \left(\sigma_{x} + \sigma_{z}\right)}{\partial x^{2}} = 2(1 + v) \frac{\partial^{2} \tau_{xy}}{\partial x \partial y}$$

$$\frac{\partial^{2} \sigma_{y}}{\partial z^{2}} - v \frac{\partial^{2} \left(\sigma_{x} + \sigma_{z}\right)}{\partial z^{2}} + \frac{\partial^{2} \sigma_{z}}{\partial y^{2}} - v \frac{\partial^{2} \left(\sigma_{x} + \sigma_{y}\right)}{\partial y^{2}} = 2(1 + v) \frac{\partial^{2} \tau_{yz}}{\partial y^{2}}$$

$$\frac{\partial^{2} \sigma_{z}}{\partial x^{2}} - v \frac{\partial^{2} \left(\sigma_{x} + \sigma_{y}\right)}{\partial x^{2}} + \frac{\partial^{2} \sigma_{x}}{\partial x^{2}} - v \frac{\partial^{2} \left(\sigma_{y} + \sigma_{z}\right)}{\partial x^{2}} = 2(1 + v) \frac{\partial^{2} \tau_{yz}}{\partial y \partial x}$$

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Solution of 3D problems – stress formulation



Eliminate shear stresses using equilibrium equations

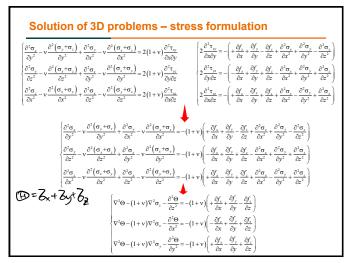
$$\begin{cases} \frac{\partial \sigma_{x}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + f_{x} = 0 \\ \frac{\partial \tau_{yy}}{\partial x} + \frac{\partial \sigma_{y}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} + f_{y} = 0 \\ \frac{\partial \tau_{zx}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_{z}}{\partial z} + f_{z} = 0 \end{cases}$$



$$2\frac{\partial^{2} \tau_{xz}}{\partial x \partial z} = -\left(+\frac{\partial f_{x}}{\partial x} - \frac{\partial f_{y}}{\partial y} + \frac{\partial f_{z}}{\partial z} + \frac{\partial^{2} \sigma_{x}}{\partial x^{2}} - \frac{\partial^{2} \sigma_{y}}{\partial y^{2}} + \frac{\partial^{2} \sigma_{z}}{\partial z^{2}}\right)$$

Solution of 3D problems – stress formulation $\begin{vmatrix} \frac{\partial^2 \sigma_i}{\partial \rho^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial \rho^2} + \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} = 2(1+v) \frac{\partial^2 \tau_{iv}}{\partial x^2 i} \\ \frac{\partial^2 \sigma_i}{\partial x^2 i} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} = 2(1+v) \frac{\partial^2 \tau_{iv}}{\partial x^2 i} \\ \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} = 2(1+v) \frac{\partial^2 \tau_{iv}}{\partial y^2 i} \\ \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} = 2(1+v) \frac{\partial^2 \tau_{iv}}{\partial y^2 i} \\ \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} - v \frac{\partial^2 (\sigma_i + \sigma_i)}{\partial x^2} = 2(1+v) \frac{\partial^2 \tau_{iv}}{\partial x^2 i} \\ \frac{\partial^2 \tau_{iv}}{\partial x^2 i} = -\left(-\frac{\partial f_i}{\partial x} + \frac{\partial f_i}{\partial y} + \frac{\partial f_i}{\partial x} - \frac{\partial^2 \sigma_i}{\partial y^2} + \frac{\partial^2 \sigma_i}{\partial x^2} - \frac{\partial^2 \sigma_i}{\partial y^2} + \frac{\partial^2 \sigma_i}{\partial x^2} \right)$ $\frac{\partial^2 \sigma_i}{\partial x^2} + v \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial y^2} - v \left(\frac{\partial^2 (2\sigma_i + \sigma_j + \sigma_i)}{\partial x^2} + \frac{\partial^2 (\sigma_i + 2\sigma_j + \sigma_i)}{\partial y^2} + \frac{\partial^2 (\sigma_i + \sigma_j + 2\sigma_i)}{\partial x^2} \right)$ $= -(1+v) \left(\frac{\partial f_i}{\partial x} + \frac{\partial f_i}{\partial y} + \frac{\partial f_i}{\partial x} + \frac{\partial f_i}{\partial y} + \frac{\partial f_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial y^2} + \frac{\partial^2 \sigma_i}{\partial y^2} + \frac{\partial^2 \sigma_i}{\partial x^2} \right)$ $\nabla^2 \Theta = -\left(\frac{1+v}{1-v} \right) \left(\frac{\partial f_i}{\partial x} + \frac{\partial f_j}{\partial y} + \frac{\partial f_i}{\partial x} \right)$ $\Theta = \sigma_i + \sigma_j + \sigma_i$ $\nabla^2 = \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2} + \frac{\partial^2 \sigma_i}{\partial x^2}$

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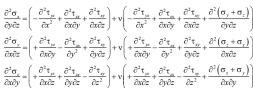
Solution of 3D problems – stress formulation $\nabla^2\Theta = -\left(\frac{1+\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right)$ $\nabla^2\Theta = -\left(\frac{1+\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right)$ $\nabla^2\Theta - (1+\mathbf{v})\nabla^2\sigma_s - \frac{\partial^2\Theta}{\partial z^2} = -(1+\mathbf{v})\left(-\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right)$ $\nabla^2\Theta - (1+\mathbf{v})\nabla^2\sigma_s - \frac{\partial^2\Theta}{\partial y^2} = -(1+\mathbf{v})\left(-\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right)$ $\nabla^2\Theta - (1+\mathbf{v})\nabla^2\sigma_s - \frac{\partial^2\Theta}{\partial y^2} = -(1+\mathbf{v})\left(-\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right)$ $\nabla^2\Theta - (1+\mathbf{v})\nabla^2\sigma_s - \frac{\partial^2\Theta}{\partial y^2} = -(1+\mathbf{v})\left(-\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial z}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial z^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial^2\Theta}{\partial y^2} = -\left(\frac{\mathbf{v}}{1-\mathbf{v}}\right)\left(\frac{\partial f_s}{\partial x} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z}\right) - 2\frac{\partial f_s}{\partial x}$ $\nabla^2\sigma_s + \frac{1}{1+\mathbf{v}}\frac{\partial f_s}{\partial y} = -\frac{\mathbf{v}}{1+\mathbf{v}}\frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z} - 2\frac{\partial f_s}{\partial y}$ $\nabla^2\sigma_s + \frac{\partial f_s}{\partial x} = -\frac{\mathbf{v}}{1+\mathbf{v}}\frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z} - 2\frac{\partial f_s}{\partial y}$ $\nabla^2\sigma_s + \frac{\partial f_s}{\partial x} = -\frac{\mathbf{v}}{1+\mathbf{v}}\frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial z} - 2\frac{\partial f_s}{\partial y}$ $\nabla^2\sigma_s + \frac{\partial f_s}{\partial x} = -\frac{\mathbf{v}}{1+\mathbf{v}}\frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial y} + \frac{\partial f_s}{\partial y} - \frac{\partial f_s}{\partial y} + \frac{\partial f$

Solution of 3D problems - stress formulation

$$\begin{split} &2\frac{\partial^{2} \mathbf{c}_{x}}{\partial y \partial z} = \frac{\partial}{\partial x} \left(-\frac{\partial \gamma_{xx}}{\partial x} + \frac{\partial \gamma_{xx}}{\partial y} + \frac{\partial \gamma_{xy}}{\partial z} \right) \\ &2\frac{\partial^{2} \mathbf{c}_{y}}{\partial x \partial z} = \frac{\partial}{\partial y} \left(\frac{\partial \gamma_{yz}}{\partial x} - \frac{\partial \gamma_{xx}}{\partial y} + \frac{\partial \gamma_{xy}}{\partial z} \right) \\ &2\frac{\partial^{2} \mathbf{c}_{x}}{\partial x \partial y} = \frac{\partial}{\partial z} \left(\frac{\partial \gamma_{yz}}{\partial x} + \frac{\partial \gamma_{xx}}{\partial y} - \frac{\partial \gamma_{xy}}{\partial z} \right) \end{split}$$

$$\begin{cases} \varepsilon_x = \frac{1}{E} (\sigma_x - v(\sigma_y + \sigma_z)) & \qquad \gamma_{xy} = \frac{1}{G} \tau_{xy} \\ \varepsilon_y = \frac{1}{E} (\sigma_y - v(\sigma_z + \sigma_x)) & \gamma_{yz} = \frac{1}{G} \tau_{yz} \\ \varepsilon_z = \frac{1}{E} (\sigma_z - v(\sigma_z + \sigma_y)) & \gamma_{zz} = \frac{1}{G} \tau_{zz} \end{cases}$$

Compatibility equations in terms of stress



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Solution of 3D problems - stress formulation

Eliminate normal stresses using equilibrium equations

$$\begin{cases} \frac{\partial \sigma_{x}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} + f_{x} = 0 \\ \frac{\partial \tau_{yy}}{\partial x} + \frac{\partial \sigma_{y}}{\partial y} + \frac{\partial \tau_{yy}}{\partial z} + f_{y} = 0 \\ \frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_{z}}{\partial z} + f_{z} = 0 \end{cases}$$



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Solution of 3D problems - stress formulation



$$\begin{split} \frac{\partial^{1}\left(\sigma_{i}+\sigma_{j}\right)}{\partial \phi^{2}} &= \left(\frac{\partial^{2}\tau_{in}}{\partial \alpha^{2}} + \frac{\partial^{2}\tau_{in}}{\partial \tau^{2}} + \frac{\partial^{2}\tau_{in}}{\partial \alpha^{2}} + \frac{\partial^{2}\tau_{in}}{\partial \tau^{2}} + \frac{$$

Equilibrium equations

Compatibility equations



 $\frac{\partial^2 \sigma_4}{\partial \phi^2} + \frac{\partial^2 (\sigma_2 + \sigma_2)}{\partial \phi^2} = \left(-\frac{\partial^2 \tau_w}{\partial x^2} + \frac{\partial^2 \tau_w}{\partial x^2} + \frac{\partial^2 \tau_w}{\partial x^2} \right) + \sqrt{\left(-\frac{\partial^2 \tau_w}{\partial x^2} + \frac{\partial^2 \tau_w}{\partial x^2} + \frac{\partial^2 \tau_w}{\partial x^2} + \frac{\partial^2 \tau_w}{\partial y^2} + \frac{\partial^2 (\sigma_2 + \sigma_2)}{\partial y^2} \right)} + \frac{\partial^2 (\sigma_2 + \sigma_2)}{\partial y^2} + \frac{\partial^2 (\sigma_2 + \sigma_2)}{$

$$\frac{\partial^2 \mathbf{c}_{-}}{\partial k^2 \mathbf{c}_{-}} = \frac{\partial^2 \mathbf{c}_{-}}{\partial k^2 \mathbf{c}_{-}} = \left(\frac{\partial^2 \mathbf{c}_{-}}{\partial \mathbf{c}_{-}} - \frac{\partial^2 \mathbf{c}_{-}}{\partial \mathbf{c}_{-}} - \frac{\partial^2 \mathbf{c}_{-}}{\partial \mathbf{c}_{-}} + \frac{\partial^2 \mathbf{c}_{-}}{\partial \mathbf{c}_{-}} \right) - \frac{\partial^2 \mathbf{c}_{-}}{\partial \mathbf{c}_{-}} + \frac{\partial^2 \mathbf{c}_{-}}{\partial \mathbf$$

Solution of 3D problems - stress formulation

$$\frac{\partial^2 \sigma_z}{\partial \phi_z} = \left(-\frac{\partial^2 \tau_w}{\partial x^2} + \frac{\partial^2 \tau_w}{\partial \phi_z} + \frac{\partial^2 \tau_w}{\partial x^2} +$$

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Solution of 3D problems - stress formulation

Compatibility equations in terms of stress Or Beltrami-Michell compatibility equations

Compatibility equations in terms of normal stress

Compatibility equations in terms of shear stress

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Solution of 3D problems

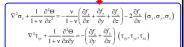
- Equilibrium equations (3) $\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} + f_z = 0 \ (x, y, z)$
- Hooke's law (6) $\sigma_x = 2G\varepsilon_x + \lambda(\varepsilon_x + \varepsilon_y + \varepsilon_z)(x, y, z)$ $\tau_{xy} = G\gamma_{xy}$
- Strain-displacement (6) $\varepsilon_x = \frac{\partial u}{\partial x}$ $\gamma_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$
- Unknowns (15) $\sigma_x, \sigma_y, \sigma_z, \tau_{xy}, \tau_{xz}, \tau_{yz}, \epsilon_x, \epsilon_y, \epsilon_z, \gamma_{xy}, \gamma_{xz}, \gamma_{yz}, u, v, w$

Displacement formulation

- Strain-displacement
 1. Str
- 2. Stress-strain relations
- 3. Equilibrium equations (displacement)
- $G\nabla^{2}u + (\lambda + G)\frac{\partial \varepsilon}{\partial x} + f_{x} = 0 \ (u, v, w)$ u, v, w

Stress formulation

- 1. Strain-stress relations
- 2. Compatibility equation (stress)
- 3. Equilibrium equations



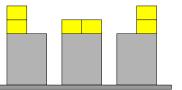
Miscellaneous

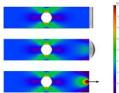
- · Principal of superposition
 - Two or more stresses fields may be superposed to yield the results for combined loads
 - Only when displacements and strains are small and the strain-displacement, stress-strain equations are linear
- · Uniqueness of elasticity solutions
 - For a given surface force and body force distribution, there is only one solution for the stress components consistent with equilibrium and compatibility

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Saint-Venant's principle

- The stresses due to two statically equivalent loadings applied over a small area are significantly different only in the vicinity of the area on which the loadings are applied
- At distance which are large in comparison with the linear dimension of the area on which the loadings are applied, the effects due to these two loadings are the same





Stress distribution around a hole

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