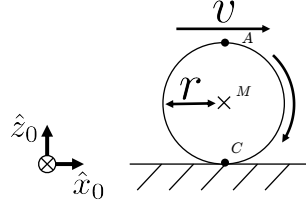


1. **(7 points)** A cylinder rolls without slipping in the \hat{x}_0 direction. The cylinder has a radius of r and a constant forward speed of v . What is the spatial acceleration of this cylinder expressed in $\{o\}$, ${}^o\mathcal{A}$ and expressed in $\{C\}$, ${}^C\mathcal{A}$, where frame $\{C\}$ has the same orientation as frame $\{o\}$ and its origin is at the contact point C .



Solution: In frame $\{o\}$

We know that

$${}^o\mathcal{V}_{body} = [0 \quad v/r \quad 0 \quad 0 \quad 0 \quad vC_x(t)/r]^T \quad (1)$$

so

$$\begin{aligned} {}^o\mathcal{A}_{body} &= {}^o\dot{\mathcal{V}}_{body} \\ &= [0 \quad \dot{v}/r \quad 0 \quad 0 \quad 0 \quad (\dot{v}C_x(t) + v^2)/r]^T \\ &= [0 \quad 0 \quad 0 \quad 0 \quad 0 \quad v^2/r]^T \end{aligned} \quad (2)$$

In frame $\{C\}$

We know that

$${}^C\mathcal{V}_{body} = [0 \quad v/r \quad 0 \quad 0 \quad 0 \quad 0]^T \quad (3)$$

so

$$\begin{aligned} {}^C\mathcal{A}_{body} &= {}^C\dot{\mathcal{V}}_{body} + {}^C\mathcal{V}_C \times {}^C\mathcal{V}_{body} \\ &= \begin{bmatrix} 0 \\ \dot{v}/r \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} \mathbf{0} & \mathbf{0} \\ [{}^Cv_C] & \mathbf{0} \end{bmatrix} \begin{bmatrix} 0 \\ v/r \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \end{aligned} \quad (4)$$

That is

$$\begin{aligned} {}^C\mathcal{A}_{body} &= [0 \quad \dot{v}/r \quad 0 \quad 0 \quad 0 \quad v^2/r]^T \\ &= [0 \quad 0 \quad 0 \quad 0 \quad 0 \quad v^2/r]^T \end{aligned} \quad (5)$$

Or you can use adjoint transformation

$${}^C\mathcal{A}_{body} = {}^CX_o {}^o\mathcal{A}_{body} \quad (6)$$

□

2. **(7 points)** Let ${}^O T_A = (R, p)$ be the pose of frame A . Suppose A is moving with velocity ${}^O \mathcal{V}_A = (\omega, v)$. Show that

$$\frac{d}{dt} [{}^O X_A^*] = \begin{bmatrix} [\omega] & [v] \\ 0 & [\omega] \end{bmatrix} {}^O X_A^*$$

Solution:

$${}^O X_A^* = \begin{bmatrix} R & [p]R \\ 0 & R \end{bmatrix} \quad (7)$$

$$\frac{d}{dt} [{}^O X_A^*] = \begin{bmatrix} \dot{R} & \frac{d}{dt} [p]R \\ 0 & \dot{R} \end{bmatrix} \quad (8)$$

We know that $\dot{R} = [\omega]R$ and

$$\begin{aligned} \frac{d}{dt} [p]R &= [\dot{p}]R + p\dot{R} \\ &= [\dot{p}R] + [p][\omega]R \\ &= [v + \omega \times p]R + [p][\omega]R \\ &= [v]R + [\omega][p]R - [p][\omega]R + [p][\omega]R \\ &= [v]R + [\omega][p]R \end{aligned} \quad (9)$$

So

$$\begin{aligned} \frac{d}{dt} [{}^O X_A^*] &= \begin{bmatrix} [\omega]R & [v]R + [\omega][p]R \\ 0 & [\omega]R \end{bmatrix} \\ &= \begin{bmatrix} [\omega] & [v] \\ 0 & [\omega] \end{bmatrix} \begin{bmatrix} R & [p]R \\ 0 & R \end{bmatrix} \\ &= \begin{bmatrix} [\omega] & [v] \\ 0 & [\omega] \end{bmatrix} {}^O X_A^* \end{aligned} \quad (10)$$

□

3. **(7 points)** A rigid body is a collection of point masses m_i at location p_i . Given a reference point o , the angular momentum of point mass i is $\overrightarrow{op_i} \times m_i v_i$. Given the definition of the angular momentum of the rigid body $\phi_o = \sum_i \overrightarrow{op_i} \times m_i v_i$, show that for any reference point o and q , we have

$$\phi_q = \phi_o + \overrightarrow{qo} \times L \quad (11)$$

where L is the linear momentum of the rigid body.

Solution:

$$\phi_q = \sum_i \overrightarrow{qp_i} \times m_i v_i \quad (12)$$

Since $\overrightarrow{qp_i} = \overrightarrow{qo} + \overrightarrow{op_i}$, we have

$$\begin{aligned}
\phi_q &= \sum_i \vec{op_i} \times m_i v_i + \sum_i \vec{q\delta} \times m_i v_i \\
&= \phi_o + \vec{q\delta} \times \sum_i m_i v_i
\end{aligned} \tag{13}$$

Given $L = \sum_i m_i v_i$, we have

$$\phi_q = \phi_o + \vec{q\delta} \times L \tag{14}$$

□

4. **(7 points)** Given our derivation in class, we have $M(\theta) = \sum_i J_i^T \mathcal{I}_i J_i$ and $c(\theta, \dot{\theta}) = \sum_i J_i^T (\mathcal{I}_i \dot{J}_i + \mathcal{I}_i V_i \times J_i + V_i \times^* \mathcal{I}_i J_i)$. Prove that $\dot{M} - 2c$ is skew symmetric.

Solution: We have

$$\dot{M} = \dot{J}_i \mathcal{I}_i J_i + J_i^T \mathcal{I}_i \dot{J}_i \tag{15}$$

which leads

$$\dot{M} - 2c = \dot{J}_i \mathcal{I}_i J_i - J_i^T \mathcal{I}_i \dot{J}_i - 2J_i^T (\mathcal{I}_i [\mathcal{V}_i \times] + [\mathcal{V}_i \times^*] \mathcal{I}_i) J_i \tag{16}$$

Using $\mathcal{I}_i^T = \mathcal{I}_i$ and $[\mathcal{V}_i \times^*] = -[\mathcal{V}_i \times]^T$

$$\left(\dot{J}_i \mathcal{I}_i J_i - J_i^T \mathcal{I}_i \dot{J}_i \right)^T = - \left(\dot{J}_i \mathcal{I}_i J_i - J_i^T \mathcal{I}_i \dot{J}_i \right) \tag{17}$$

and

$$\begin{aligned}
(\mathcal{I}_i [\mathcal{V}_i \times] + [\mathcal{V}_i \times^*] \mathcal{I}_i)^T &= [\mathcal{V}_i \times]^T \mathcal{I}_i - \mathcal{I}_i [\mathcal{V}_i \times] \\
&= -(\mathcal{I}_i [\mathcal{V}_i \times] + [\mathcal{V}_i \times^*] \mathcal{I}_i)
\end{aligned} \tag{18}$$

So $\dot{M} - 2c$ is skew-symmetric.

□