Improved VoF algorithm to simulate multiphase flows

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Introduction

Modeling of immiscible two phase flows

- VoF methods suffer from spurious currents unphysical currents that appear without external forcing
- Reduction of spurious currents / improvement of interface tracking a hot research topic
- CLS-VoF, geometric reconstruction, ...
- Here: Algorithm presented in Journal of Computational Physics, April 2012, by Raeini, Blunt, Bijelijc
 - SSF = sharp surface forces

It looks like you're having problems with VoF.

Would you like help?

- Get help with spurious currents
- Just continue without help
- Don't show me this tip again





Outline

Modeling of immiscible two phase flows

- Combatting numerical diffusion in VoF methods
- Problems in determining interface curvature with a "sharp"
 VoF interface
- Combination of smoothing and sharpening in the SSF formulation
- Treatment of the capillary pressure
- Semi-implicit coupling of the volume fraction and momentum solution
- Static test case spherical bubble equilibrium
- Dynamic test case Thermocapillary driven cavity



Introduction

The Volume of Fluid method (VoF)

| 0 | 0 | 0 | 0 Air |
|---|-------------|----|----------|
| | |) | 0 |
| 1 | 1 | L | |
| 1 | Liquid 1 | 1. | 1, |

$$\frac{\partial \alpha}{\partial t} + \nabla \cdot (U\alpha) = 0$$



Cells of interface liquid-air with 0 < C < 1

VoF field is directly coupled to flow field via advection term



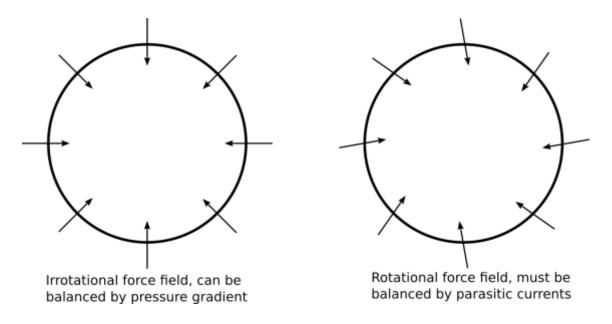
Artificial diffusion of the sharp interface

- A perfect solution to a volume tracking problem will retain a sharp interface shape
 - This is important e. g. to accurately determine drag force on a bubble
 - Strong diffusion would eventually to result in mixing, completely changing the physics
- Pure advection problems will always be accompanied by numerical diffusion
- This can be countered by sophisticated advection schemes incorporating downwinding, and artificial compression
- Dilemma: Too much sharpening will lead to noise in the curvature calculation



Noise in curvature due to sharp interface

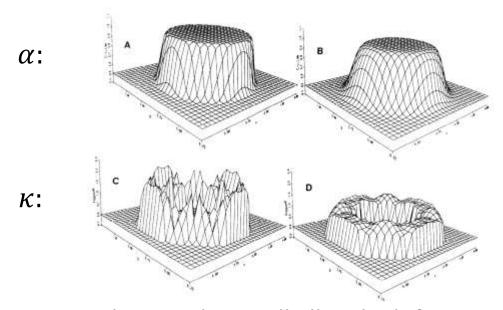
- Flow field is coupled to VoF through surface tension forces $\sigma \kappa |\nabla \alpha|$
- Inaccuracies in curvature determination lead to force field not balanced by pressure gradient => rotational velocity field





Noise in curvature due to sharp interface

Noise can be mitigated by smoothing the volume fraction field



 Dilemma: Too much smoothing will allow high frequency capillary waves to persist unphysically



Smoothing in interFoamSSF (the new algorithm)

- Compute VoF field
- Determine curvature from smoothed volume fraction field
- Amount of smoothing determined by a blending coefficient
- Smooth curvature away from interface

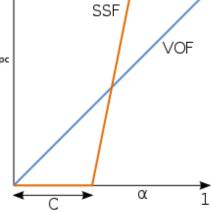


interFoamSSF – sharp surface formulation

- Compute VoF field
- Determine curvature from smoothed volume fraction field
- Amount of smoothing determined by a blending coefficient
- Smooth curvature away from interface
- Apply the resulting surface tension force to a sharpened interface (sharp surface formulation SSF) α_i

•
$$f_{c,f} = \sigma k_f \nabla_f (\alpha_{SSF})$$

•
$$\alpha_{SSF} = \frac{1}{1-2C} \left[\min(\max(\alpha, C), 1-C) - C \right]$$



- C=0 will give original field, C=0.5 a very sharp transition
- ~0.48 good for static problems, ~0.25 good for dynamic problems



Notes on pressure

- It is important to determine the surface force at cell faces if the pressure is solved there (already done in interFoam)
 - Using cell values will not balance pressure
- Reference goes a step further and separates capillary pressure and gravity from total pressure
 - $p = p_d + p_c + \rho g$
- Remaining pressure field p_d will be smooth! p_c is calculated explicitly from the normal surface tension force



Are we done yet? Not quite.

- Standard VoF implementations have explicit coupling of VoF field and velocity
 - Compute VoF field for a given time
 - Update velocity field for this time step based on new transport properties
 - Advance to next time step
- Updated velocity doesn't directly couple back to VoF equation!
- Severe time step criterion: $\Delta t = \sqrt{\rho/\sigma} \, \Delta x^{3/2} \approx O(10^{-6} s)$



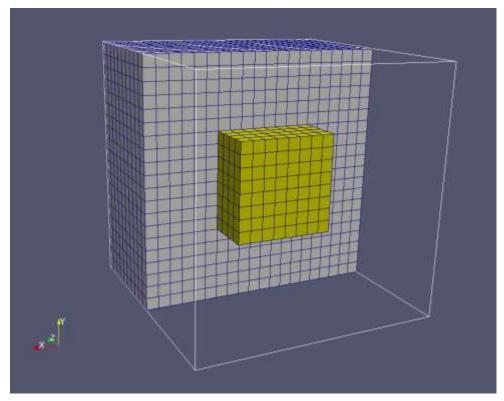
Semi-implicit solution

- Compute VoF field for time $t = t^{n-1} + \Delta t/2$
- For i
 - Update VoF field for time tⁿ
 - Update velocity and pressure
 - Relax velocity and surface force, EXCEPT for last iteration
 - Loop
- One loop: Half time step only for VoF field => computational efficiency
- Multiple loops: Semi-implicit update of the VoF field
- Larger time steps possible



Relaxing droplet

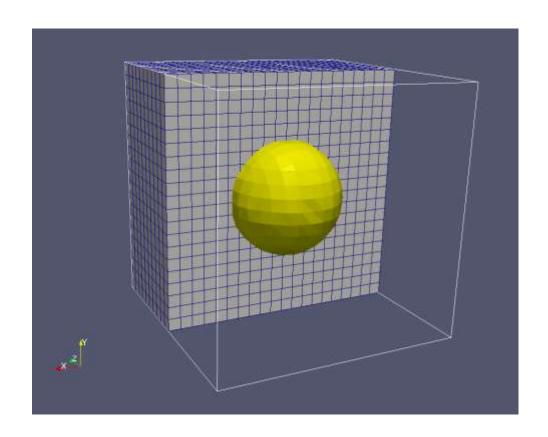
- 100 μm domain, 40 μm droplet diameter
- t=0s





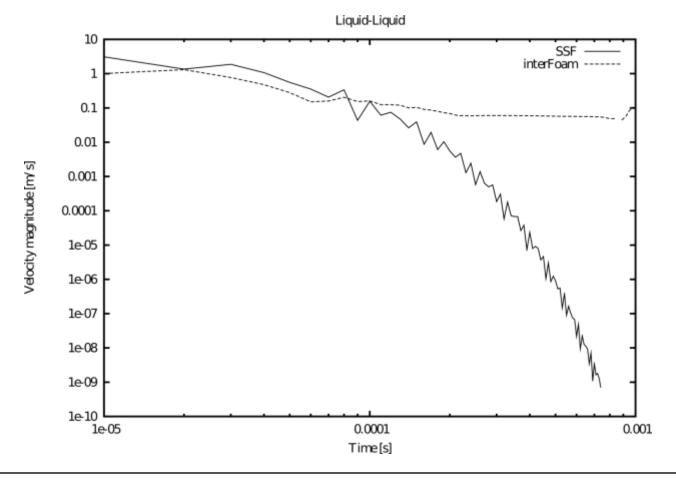
Relaxing droplet

• t=0.001s



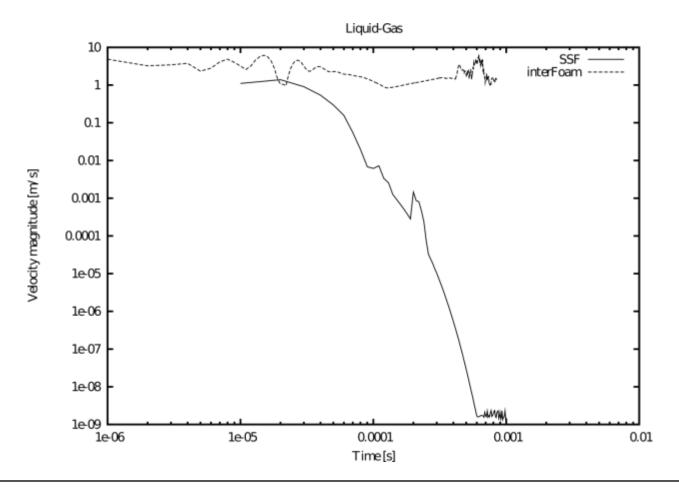


Relaxing droplet



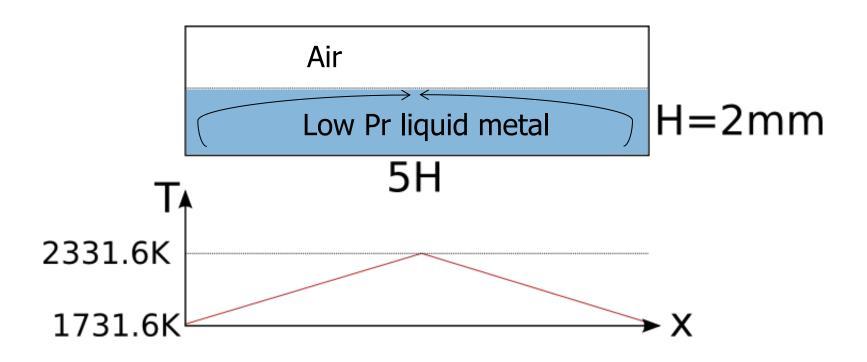


Relaxing bubble



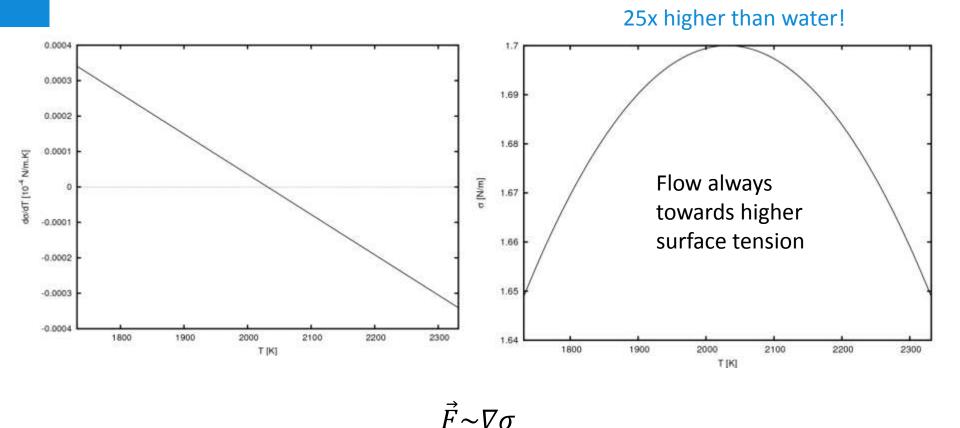


Thermocapillary cavity



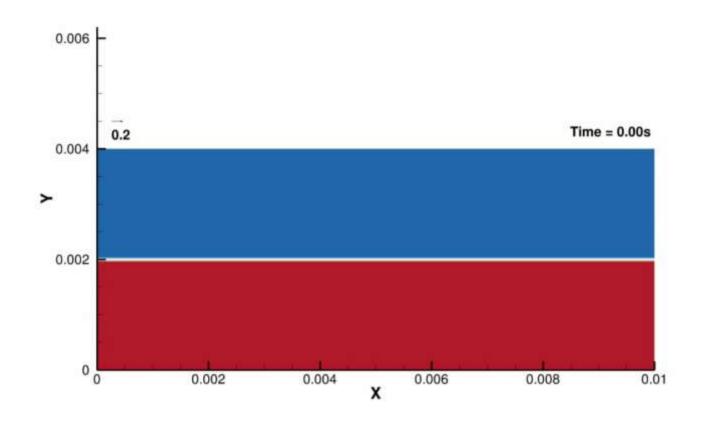


Thermocapillary cavity



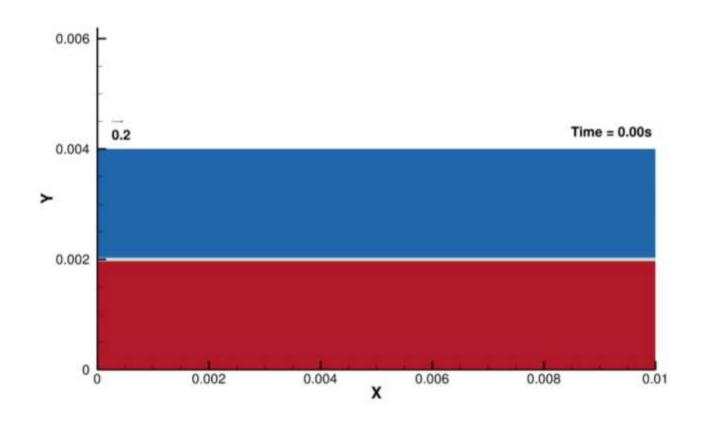


Thermocapillary cavity results - interFoam



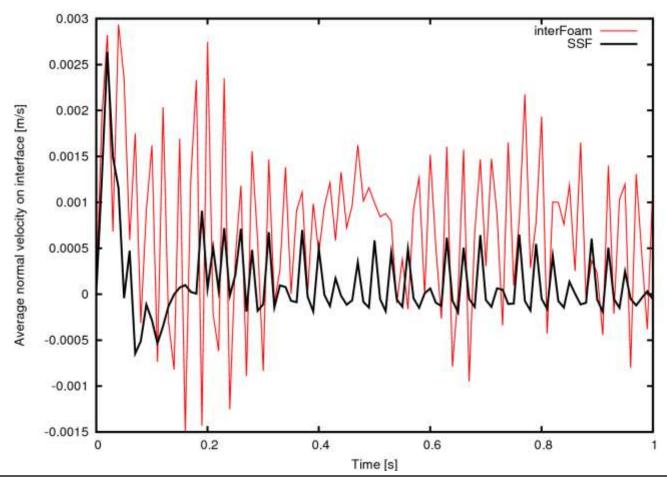


Thermocapillary cavity results - SSF





Thermocapillary cavity – spurious currents





Conclusion

Modeling of immiscible two phase flows

- VoF can be enhanced by a few relatively simple modifications
 - Smoothing
 - Sharp-Surface-Force
 - Explicit capillary pressure
 - Semi-implicit coupling of equations
- If you'd like to test the solver, check out my OpenFOAM version at http://code.google.com/p/interfoamssf/
- The official solver is available here:
 http://www3.imperial.ac.uk/earthscienceandengineering/rese
 arch/perm/porescalemodelling/software/porefoam

