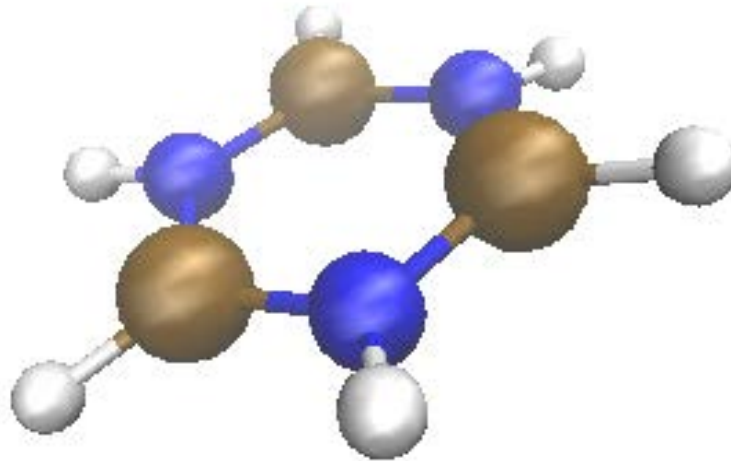


# MD Ensembles and Thermostats

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# Goal of MD simulations

- obtain ensemble average from trajectory

$$\langle A \rangle = \int P(p, t) A(p, r) dp dr = \int A(p(t), r(t)) dt$$

$P$ : probability

$p$ : momenta

$A$ : property

$r$ : position

- solve equations of motion

$$F_i = m_i \ddot{\mathbf{r}}_i$$

*Newton*

$$\mathcal{H}(\mathbf{r}, \mathbf{p}) = \frac{|\mathbf{p}|^2}{2m} + \mathcal{U}(r)$$

*Hamiltonian*

# Ensembles in MD

- ensemble: all microstates ( $\mathbf{r}, \mathbf{p}$ ) that are accessible to the simulation and provide probability of each microstate

particle number $N$	chemical potential $\mu$
volume $V$	pressure $P$
energy $E$	temperature $T$

- $NVE$  microcanonical
- $NVT$  canonical
- $NPT$  isothermal-isobaric

# Ensembles in MD

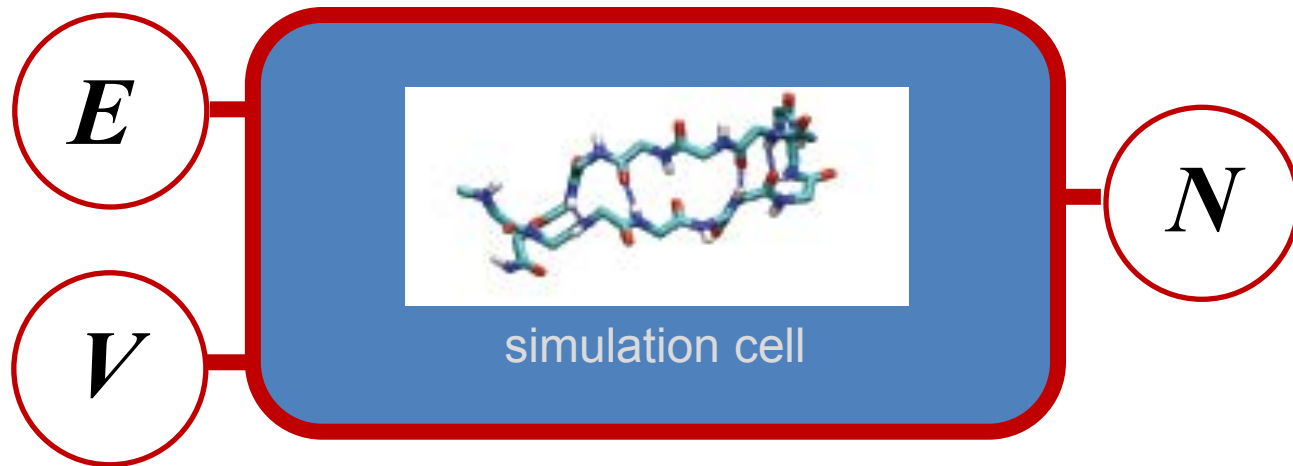
- ideal MD conserves energy and entropy: microcanonical ensemble ( $NVE$ )
- realistic systems change energy, volume and particles with external reservoirs → more difficult
- canonical ( $NVT$ ) most frequently used

$$P \propto e^{-\frac{E(\mathbf{r})}{k_b T}}$$

# NVE – microcanonical ensemble

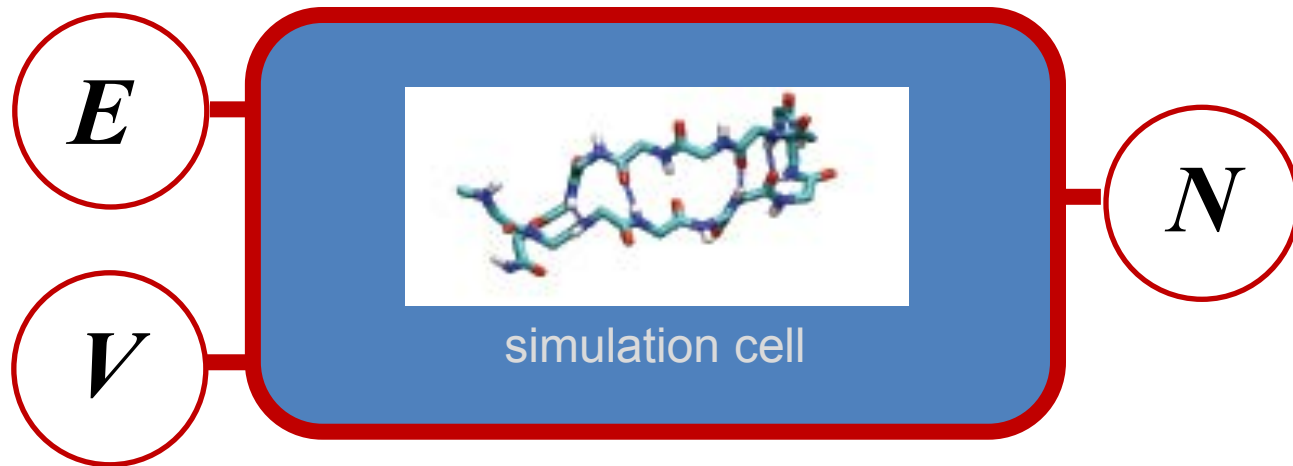
- system isolated with constant number of particles  $N$ , volume  $V$  and energy  $E$
- solving equations of motion without temperature or pressure control

$$F_i = m_i \ddot{\mathbf{r}}_i$$



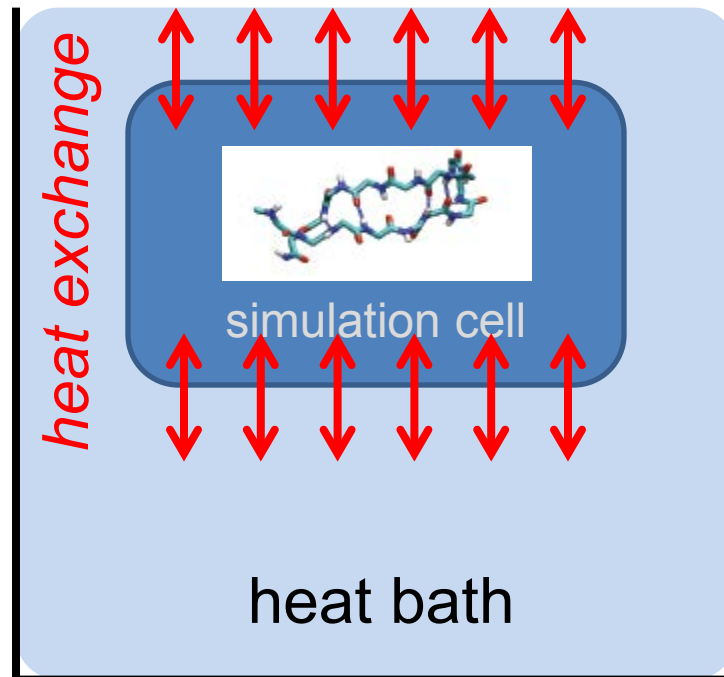
# NVE – microcanonical ensemble

- drift in  $E$  resulting from rounding and truncation errors
- time reversible
- dynamical variables well defined
- required initial conditions: position and velocity



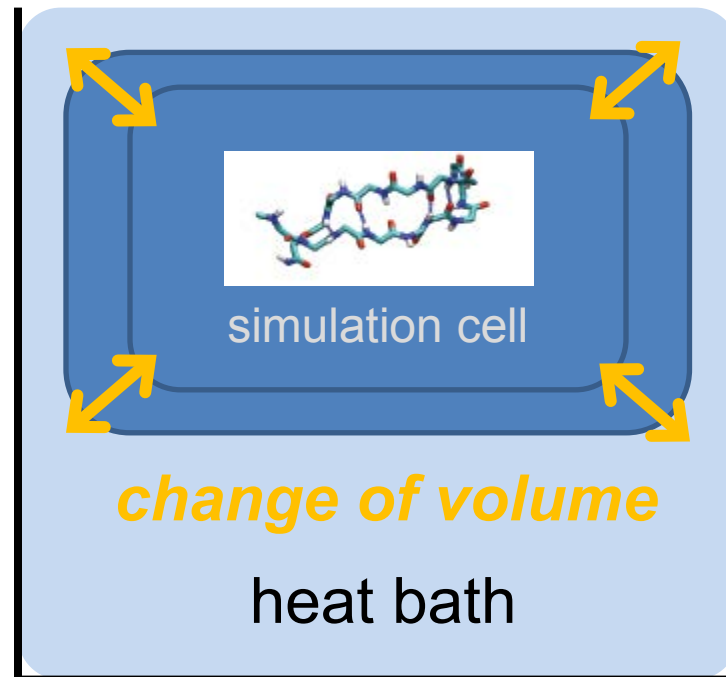
# NVT – canonical ensemble

- constant number of particles  $N$  and volume  $V$
- system in thermal contact with heat bath



# NPT – isothermal-isobaric ensemble

- constant number of particles  $N$ , pressure  $p$  and temperature  $T$
- use of thermostat and barostat





# Lagrangian equations of motion

- extended ensemble
- difference between kinetic and potential energy

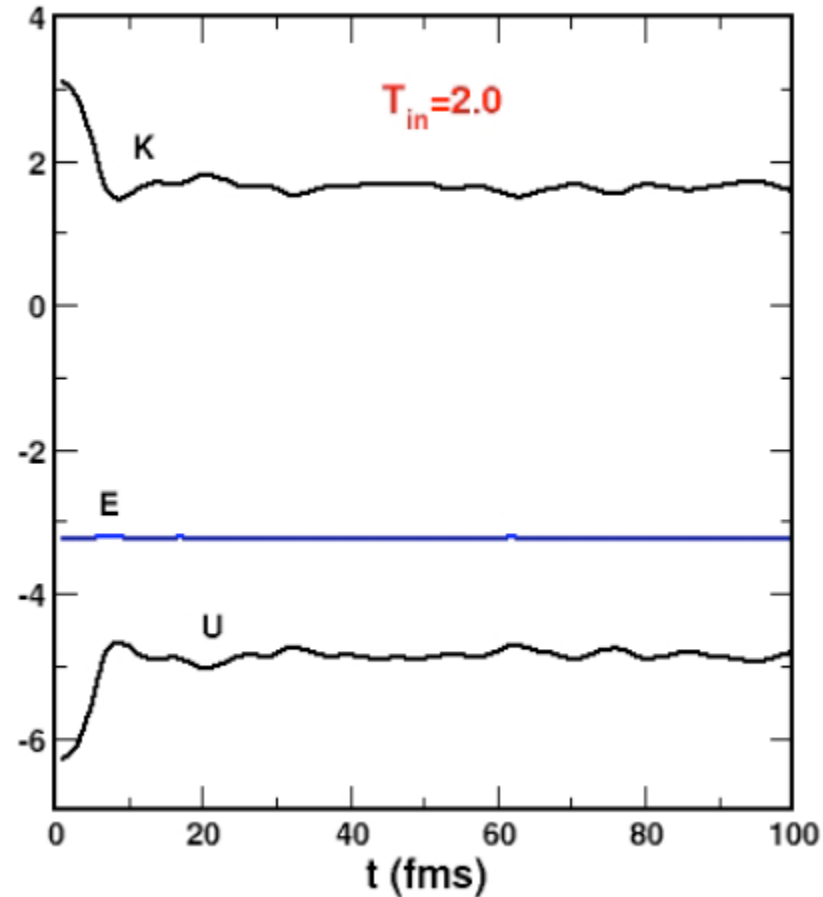
$$\mathcal{L}(\mathbf{r}^N, \mathbf{v}^N) = K(\mathbf{v}^N) - U(\mathbf{r}^N)$$

- assumption:  $K$  only dependent on  $v$ ,  $U$  only on  $r$

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \mathbf{v}_i} - \frac{\partial \mathcal{L}}{\partial \mathbf{r}_i} = 0$$

- Hamiltonian  $\mathcal{H} = \sum_i \mathbf{p}_i \cdot \mathbf{v}_i - \mathcal{L} = \boxed{\sum_i \mathbf{p}_i \cdot \mathbf{v}_i} + \boxed{\mathcal{U}}$   
*kinetic energy*      *potential energy*

# Lagrangian equations of motion



$$\mathcal{H} = \sum_i \mathbf{p}_i \cdot \mathbf{v}_i - \mathcal{L} = \sum_i \mathbf{p}_i \cdot \mathbf{v}_i + \mathcal{U}$$

# Calculation of temperature

$$\langle K \rangle = \frac{N_f}{2} k_B T$$

$K$ : kinetic energy

$$K = \sum_i \frac{p_i^2}{2m_i}$$

$$T = \sum_{i=1}^N \frac{p_i^2}{m_i k_B N_f} = \sum_{i=1}^N \sum_{\alpha} \frac{m_i v_{i\alpha}^2(t)}{k_B N_f}$$

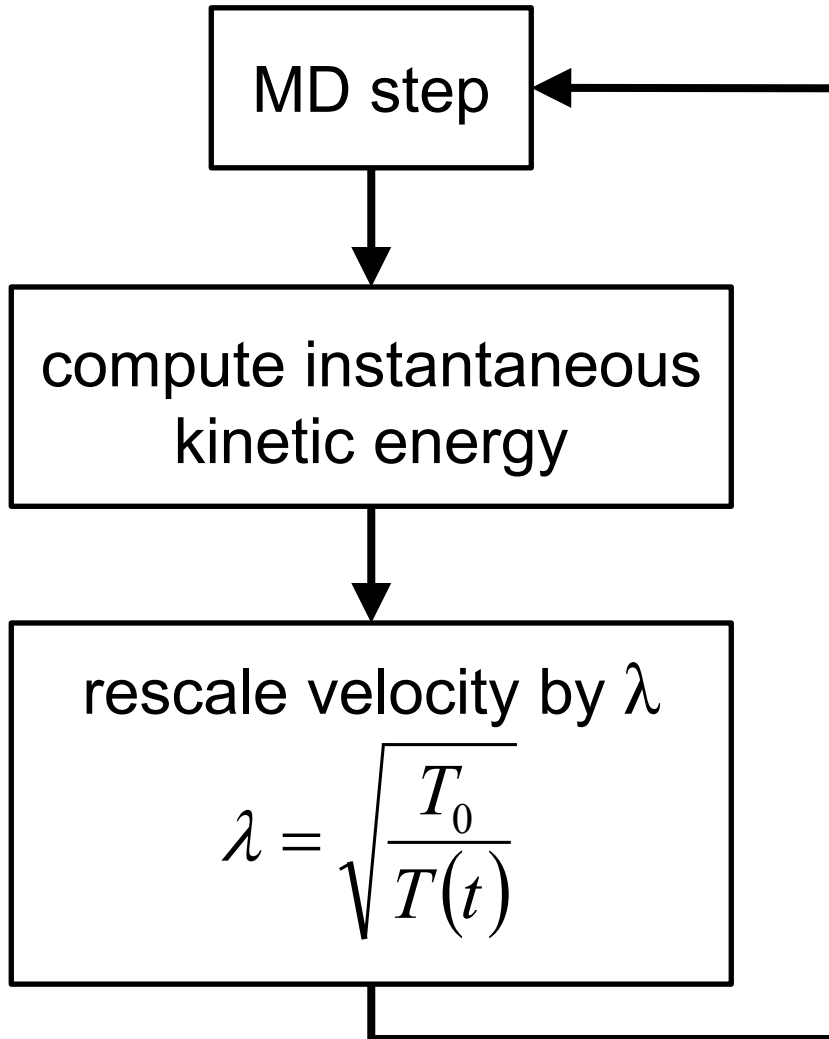
# Velocity rescaling

- multiply velocities by a factor  $\lambda$  to obtain desired temperature  $T_0$

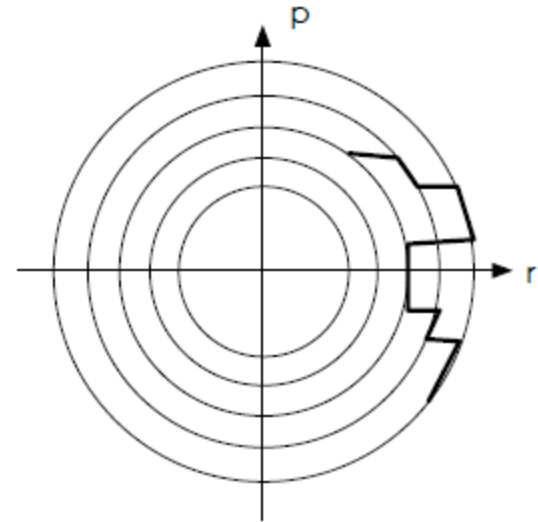
$$\Delta T = \frac{1}{2} \sum_{i=1}^N \frac{2}{3} \frac{m_i (\lambda v_i)^2}{N k_B} - \frac{1}{2} \sum_{i=1}^N \frac{2}{3} \frac{m_i v_i^2}{N k_B} = (\lambda^2 - 1) T(t)$$

$$\lambda = \sqrt{\frac{T_0}{T(t)}}$$

# Velocity rescaling



- straight forward
- does not correspond to any ensemble



# Berendsen thermostat

- system weakly coupled to heat bath with temperature  $T_{\text{bath}}$

$$\frac{dT(t)}{dt} = \frac{1}{\tau} (T_{\text{bath}} - T(t)) \quad \tau : \text{coupling parameter}$$

- rescaling at each step, with temperature change

$$\Delta T = \frac{\partial t}{\tau} (T_{\text{bath}} - T(t))$$

- scaling factor

$$(\lambda^2 - 1)T(t) = \frac{\partial t}{\tau} (T_{\text{bath}} - T(t))$$

# Berendsen thermostat

- smoother than velocity rescaling
- suppresses fluctuations in kinetic energy
  - no ensemble
- global thermostat
- for large systems good approximation

# Andersen thermostat

- random collisions of molecules with an imaginary heat bath (randomize velocities)

$$P(p_1, p_2, \dots) \propto \exp\left(-\frac{p_1^2}{2k_B T m_1}\right) \times \exp\left(-\frac{p_2^2}{2k_B T m_2}\right) \times \dots$$

$$p_{new} = \sqrt{mk_B T} R$$

random Gaussian number



# Andersen thermostat

- canonical ensemble ( $NVT$ )
- stochastic
- local thermostat
- **destroys momentum transport** (true molecular kinetics are not preserved)
  - cannot be used to calculate transport properties (diffusion coefficient)

# Langevin thermostat

- velocity corrected by random force and constant friction

$$m\ddot{\mathbf{r}}_i = -\frac{\partial U}{\partial \mathbf{r}_i} - m\Gamma\dot{\mathbf{r}}_i + \mathbf{W}_i(t)$$

$\Gamma$  : friction coefficient  
 $\mathbf{W}$ : random force

- relation between magnitude of force and friction

$$\langle \mathbf{W}_i(t), \mathbf{W}_j(t') \rangle = \partial_{ij} \delta(t - t') 6m \Gamma k_B T$$

# Langevin thermostat

- canonical ensemble ( $NVT$ )
- local thermostat
- ergodic
- allows the use of large time steps
- destroys momentum transport → cannot be used to calculate transport properties (diffusion coefficient)

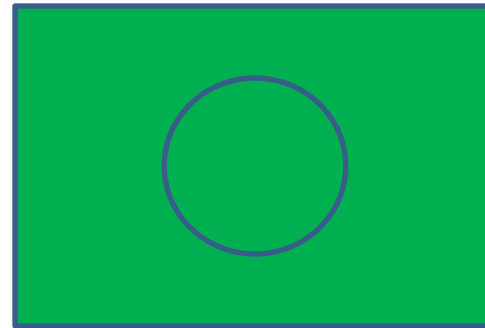
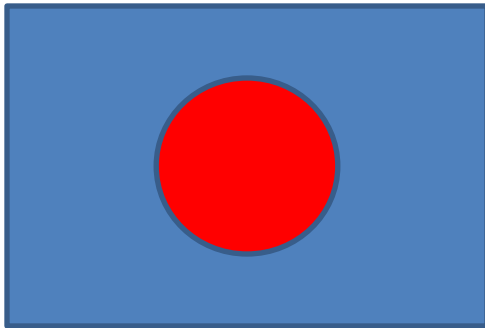
# Local and global thermostats

Berendsen (global)

$$\dot{p}_i = -\gamma p_i = -\left[\frac{1}{2\tau}\left(\frac{\bar{K}}{K}-1\right)\right]p_i$$

Langevin (local)

$$\dot{p}_i = -\gamma p_i + \sqrt{2m_i k_B T \gamma} \eta_i$$



if needed: different thermostats for different atoms

# Nosé thermostat

- add two additional degrees of freedom the system:
  - $s$  – position of imaginary heat reservoir
  - $p_s$  – conjugate momentum of imaginary heat reservoir

- additional parameter

$Q$  – effective mass

$$p_s = \frac{\partial \mathcal{L}}{\partial \dot{s}} = Q\dot{s}$$

- momenta conjugate to  $\mathbf{r}_i$

$$\mathbf{p}_i = \frac{\partial \mathcal{L}}{\partial \dot{\mathbf{r}}_i} = m_i s^2 \dot{\mathbf{r}}_i$$

- Hamiltonian

$$H_N = \sum_i \frac{\mathbf{p}_i^2}{2m_i s^2} + \mathcal{U}(\mathbf{r}^N) + \frac{p_s^2}{2Q} + gk_B T \ln s$$

# Nosé thermostat

- canonical ensemble ( $NVT$ )
  - smooth
  - deterministic
  - time-reversible
- 
- fluctuation of real time step resulting from scaling factor  $s$

$$dt' = s dt$$

# Nosé-Hoover thermostat

- eliminate problem of “real”-time averages

$$H_{NH} = \sum_i \frac{\mathbf{p}_i^2}{2m_i} + \mathcal{U}(\mathbf{r}^N) + \frac{1}{2} Q \xi^2 - g k_B T \ln s$$

$$g = 3N$$

- friction coefficient  $\dot{\xi} = \frac{1}{Q} \left( \sum_i \frac{\mathbf{p}_i^2}{m_i} - g k_B T \right)$

$$\xi = \frac{\dot{s}}{s} = \frac{d \ln s}{dt}$$

# Nosé-Hoover thermostat

- second order equation on  $K$
- proper sampling
- deterministic (can be non-ergodic)
- second order  $\rightarrow$  can be oscillating



# Nosé-Hoover chains

- canonical ensemble ( $NVT$ )

$$\dot{\xi}_1 = \frac{1}{Q_1} \left( \sum_i \frac{\mathbf{p}_i^2}{m_i} g k_B T \right) - \xi_1 \xi_2$$

$$\dot{\xi}_j = \frac{1}{Q_j} (Q_{j-1} \xi_{j-1}^2 - k_B T) - \xi_j \xi_{j+1}$$

$$\dot{\xi}_M = \frac{1}{Q_M} (Q_{M-1} \xi_{M-1}^2 - k_B T)$$

# Nosé-Hoover chains

- higher order equation on  $K$
- canonical
- ergodic
- additional equations for chaotic behavior

# Basic input in CP2K

```
&GLOBAL
  PROJECT   MD_NVE
  RUN_TYPE  MD
  PRINT_LEVEL LOW
  WALLTIME  600
&END GLOBAL

&MOTION
  &MD
    ENSEMBLE NVE
    STEPS    1000
    TIMESTEP 0.5
    TEMPERATURE 300.0
  &END MD
&END MOTION
```

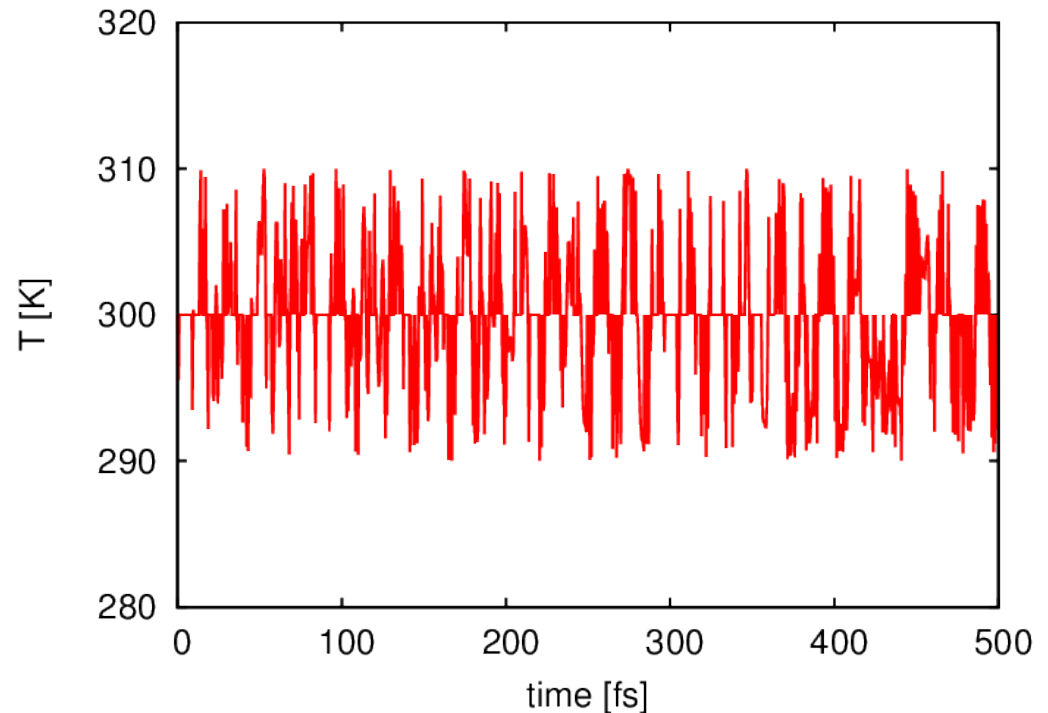
# Ensembles in CP2K

```
&MOTION
  &MD
    ENSEMBLE NVE
    STEPS 1000
    TIMESTEP 0.5
    TEMPERATURE 300.0
  &END MD
&END MOTION
```

- microcanonical: **NVE**
- canonical: **NVT**
- canonical using Langevin: **LANGEVIN**
- isobaric-isothermic: **NPT\_F**
- isobaric-isothermic in isotropic cell: **NPT\_I**
- constant pressure: **NPE\_F**
- constant pressure in isotropic cell: **NPE\_I**
- constant kinetic energy: **ISOKIN**
- HYDROSTATICSHOCK, MSST, MSST\_DAMPED, NVT\_ADIABATIC,...

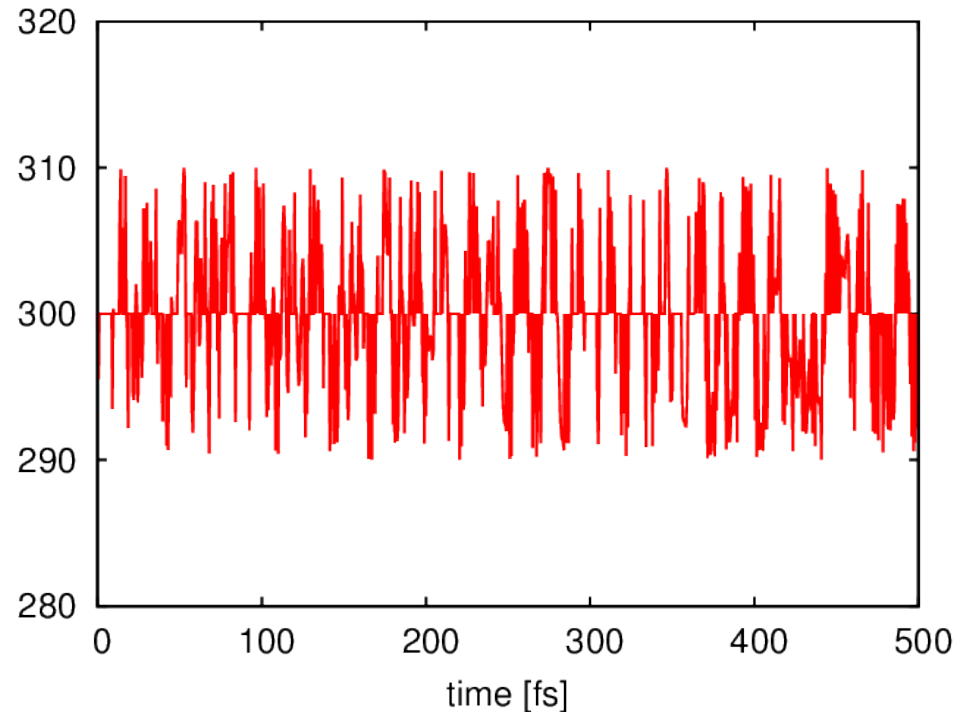
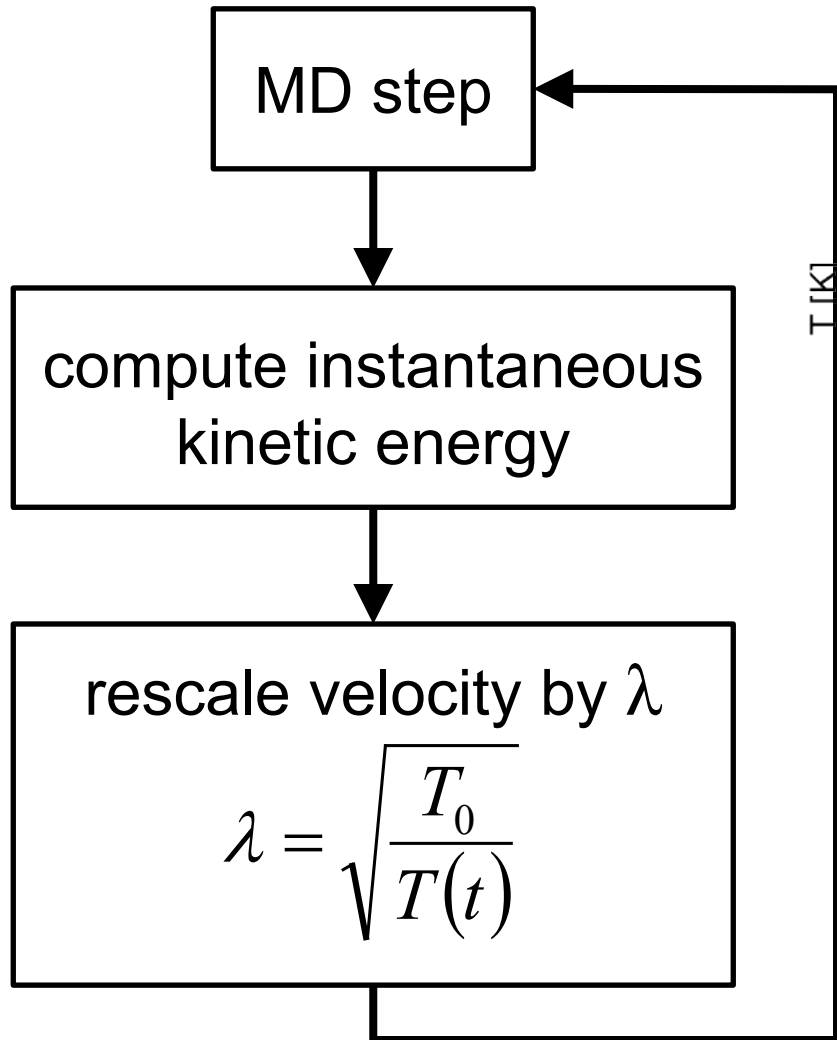
# Ensembles in CP2K

```
&MOTION
  &MD
    ENSEMBLE NVE
    STEPS 1000
    TIMESTEP 0.5
    TEMPERATURE 300.0
    TEMP_TOL 10
  &END MD
&END MOTION
```



enable **velocity rescaling**  
when  $T < 290$  K or  $T > 310$  K

# Velocity rescaling



$T < 290 \text{ K}$  or  $T > 310 \text{ K}$

# Ensembles in CP2K - CSVR

Kinetic energy

$$dK = \sum_i \frac{f_i \cdot p_i}{m_i} dt + (\bar{K} - K) \frac{dt}{\tau} + 2 \sqrt{\frac{K\bar{K}}{N_f}} \frac{dW}{\sqrt{\tau}} \quad \left( \tau = \frac{1}{2\gamma} \right)$$

thermostat part

$$dK = \boxed{(\bar{K} - K) \frac{dt}{\tau}} + \boxed{2 \sqrt{\frac{K\bar{K}}{N_f}} \frac{dW}{\sqrt{\tau}}}$$

Berendsen  
thermostat

noise gives  
correct  
fluctuations

# Ensembles in CP2K - CSV

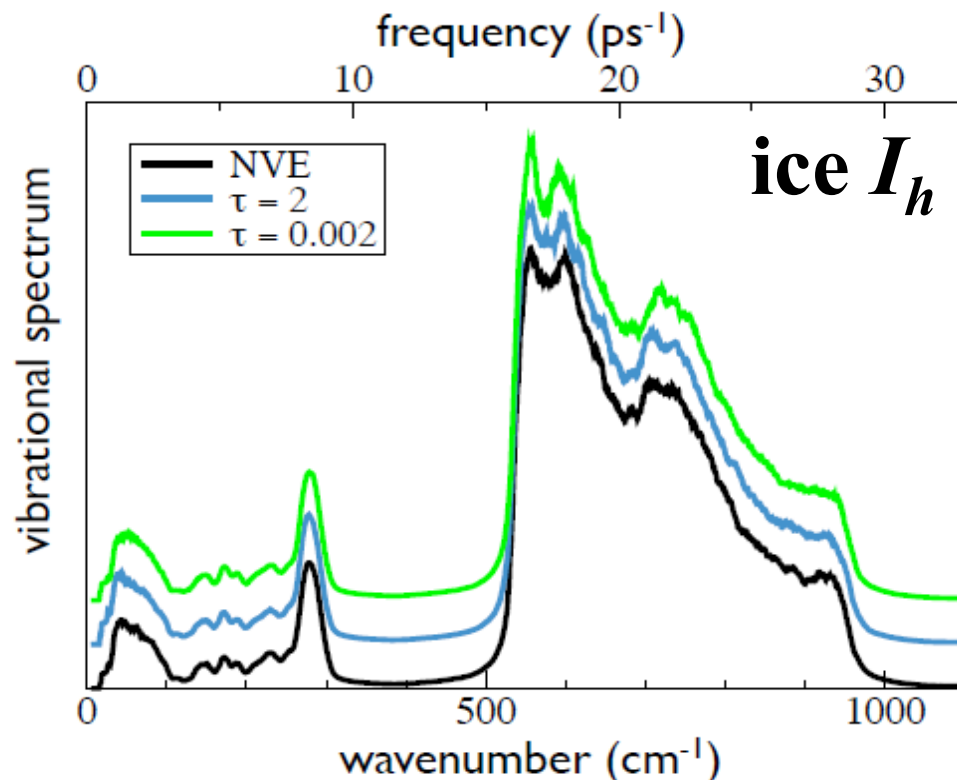
$$dK = (\bar{K} - K) \frac{dt}{\tau} + 2 \sqrt{\frac{K\bar{K}}{N_f}} \frac{dW}{\sqrt{\tau}}$$

- stochastic velocity rescaling for  $\tau = 0$
- global
- correct fluctuations
- preserves dynamic properties
- recovers Langevin for single degree of freedom



# Ensembles in CP2K - CSV

```
&MOTION
  &MD
    ENSEMBLE NVT
    STEPS 1000
    TIMESTEP 0.5
    TEMPERATURE 300.0
  &THERMOSTAT
    TYPE CSV
    REGION GLOBAL
  &CSV
    TIMECON 50.
  &END CSV
&END THERMOSTAT
&END MD
&END MOTION
```

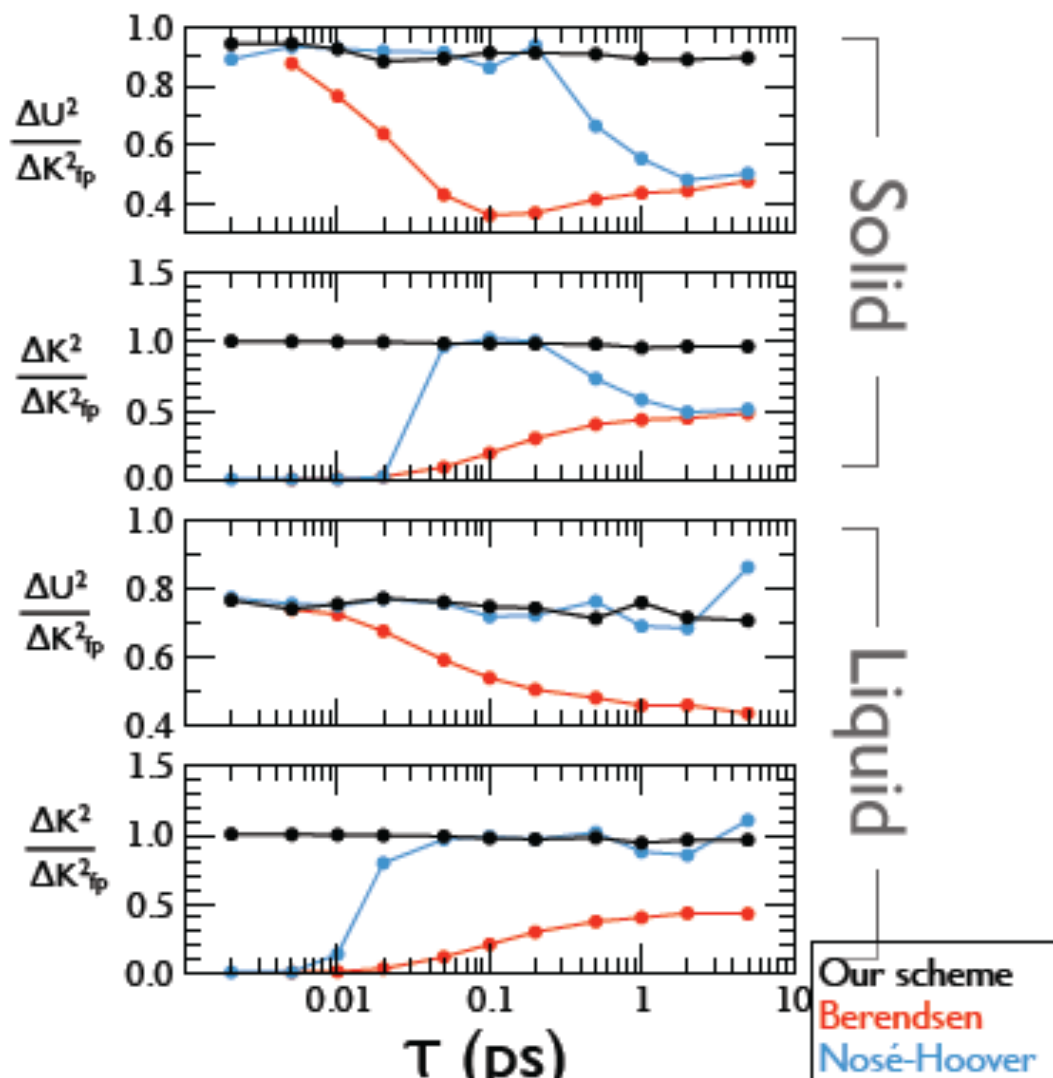


# Ensembles in CP2K - CSVr

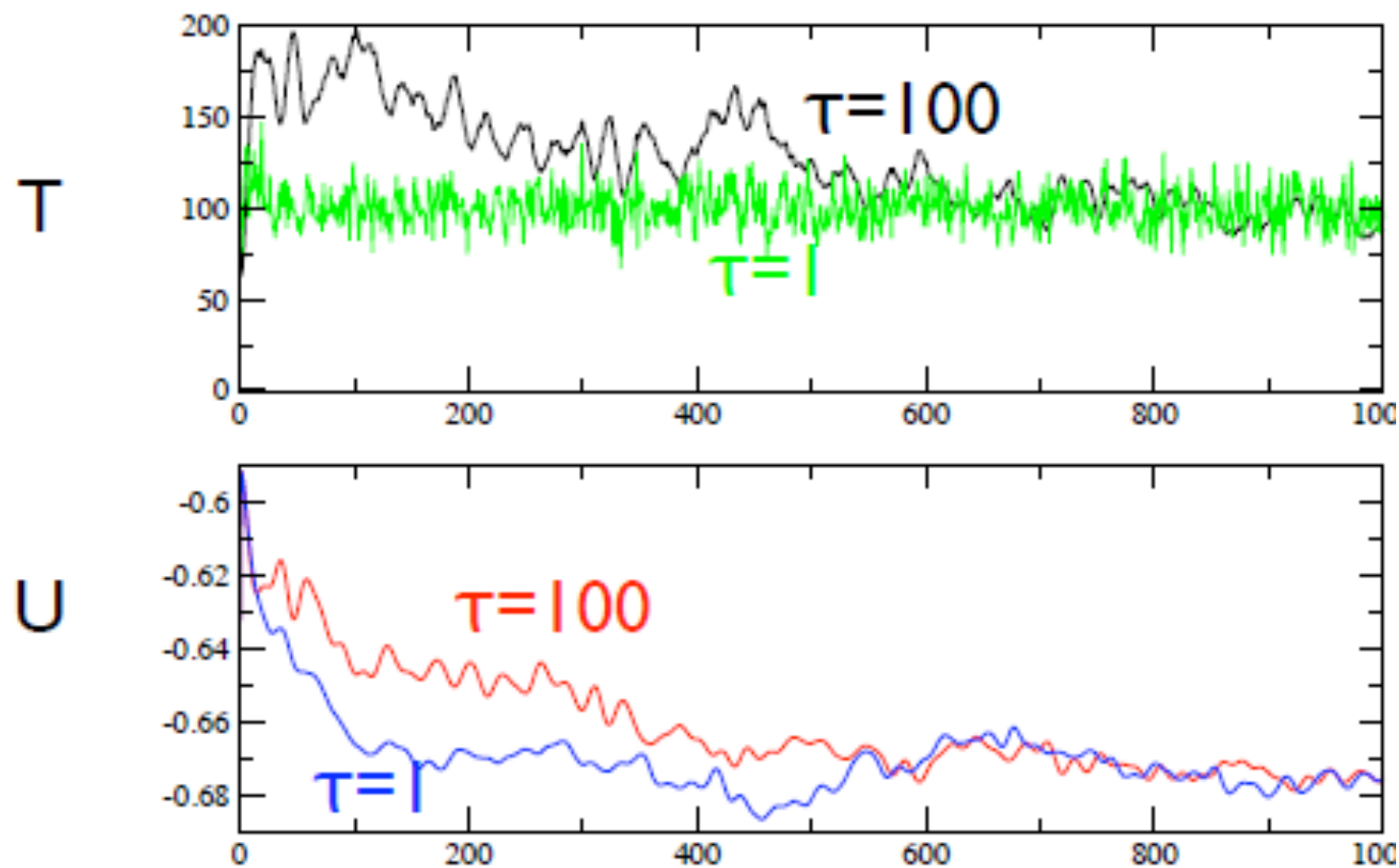
Energy fluctuations  
(in units of  $N_f k_b^2 T^2 / 2$ )  
from a 1.0 ns run.

Berendsen:  
wrong ensemble

Nosé-Hoover:  
not-ergodic,  
especially in solid  
(NHC solve this)



# Ensembles in CP2K - CSVr



# Overview of thermostats

	tune	cont.	L/G	correct	ergodic	cons. q.	determ.	cp2k
Velocity rescaling			G		?		X	
Andersen	X		L	X	X			
Berendsen	X	X	G		?		X	
Nosé-Hoover	X	X	L/G	X		X	X	NOSE*
Nosé-Hoover chains	X	X	L/G	X	X	X	X	NOSE
Langevin	X	X	L	X	X	X		CSVR**
Stochastic velocity rescaling	X	X	L/G	X	X	X		CSVR

\*use "LENGTH=1"  
 \*\*use "MASSIVE"

# Recipes for MD calculations

- equilibration:
  - strong thermostat (small  $\tau$ )
  - local for ab initio; local or global for classical
- normal production:
  - global,  $\tau=1-100$  fs
- difficult temperature control:
  - local,  $\tau=1-100$  fs
- two or more “separate” subsystems (solid-liquid, QMMM,...)
  - global, one per subsystem
- always check energy conservation
- always check kinetic energy fluctuations

# Analysis of trajectories

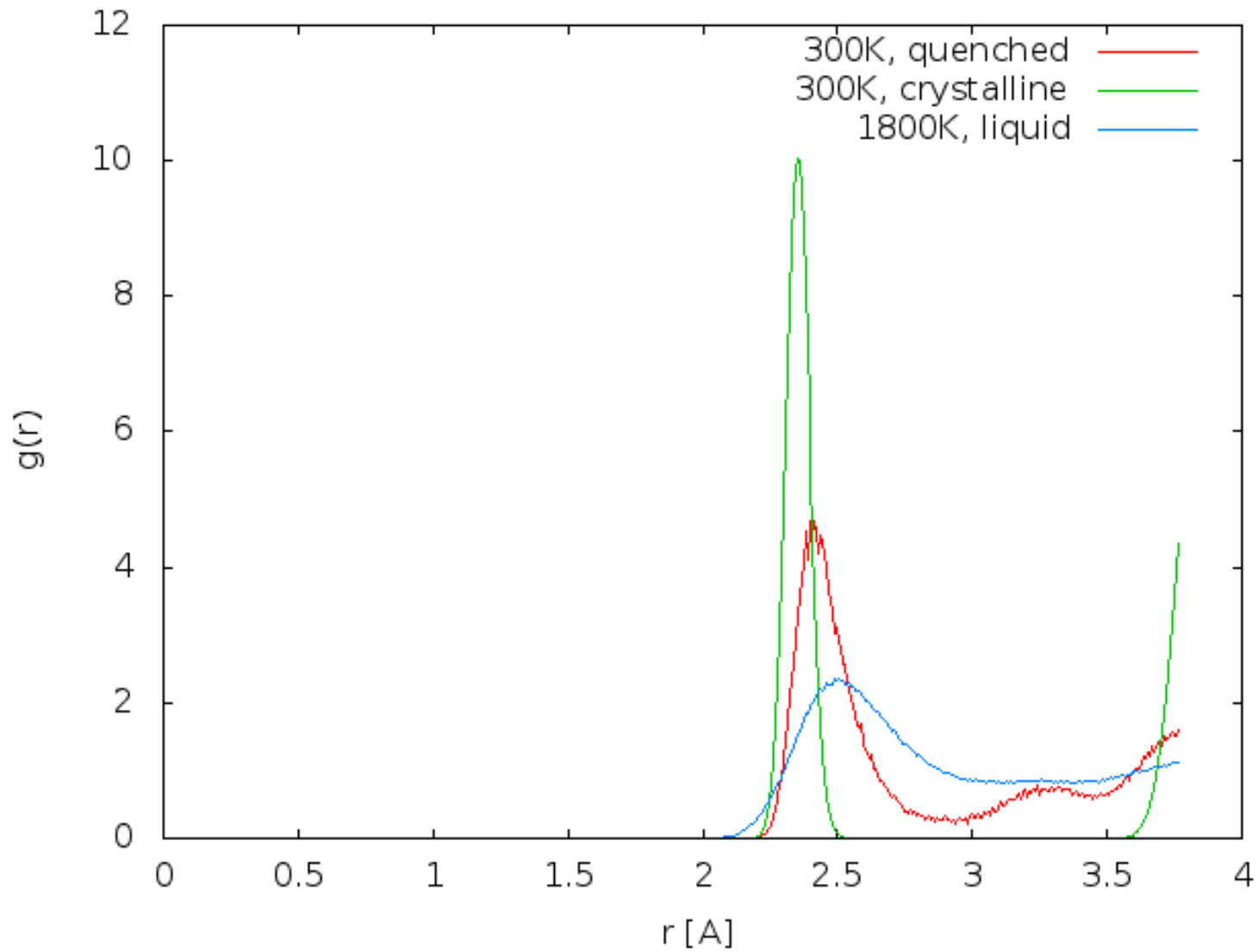
$$\langle A \rangle = \int P(p, t) A(p, r) dp dr = \int A(p(t), r(t)) dt$$

from trajectory file *[project]-pos-1.xyz*

**property A**

- *g* or *r*

# $g(r)$ of Si



# Analysis of trajectories

$$\langle A \rangle = \int P(p, t) A(p, r) dp dr = \int A(p(t), r(t)) dt$$

from trajectory file *[project]-pos-1.xyz*

## property A

- *g* or *r*
- mean square displacement (MSD)
- bond length
- coordination number
- .....



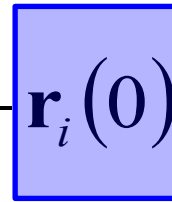
# REFTRAJ in CP2K

```
&MOTION
  &MD
    ENSEMBLE REFTRAJ
    STEPS 5
    &REFTRAJ
      TRAJ_FILE_NAME traj.xyz
      FIRST_SNAPSHOT 1
      LAST_SNAPSHOT 5
    &END REFTRAJ
  &END MD
&END MOTION
```

```
&SUBSYS
...
  &COLVAR
    &COORDINATION
      KINDS_FROM O
      KINDS_TO Si
      R_0 [angstrom] 1.8
    &END COORDINATION
  &END COLVAR
&END SUBSYS
```

# Mean square displacement

$$\text{MSD}(t) = \langle \Delta \mathbf{r}_i(t)^2 \rangle = \langle (\mathbf{r}_i(t) - \mathbf{r}_i(0))^2 \rangle$$



reference cell

```
&MOTION
  &MD
    ENSEMBLE REFTRAJ
    STEPS 5
    &REFTRAJ
      TRAJ_FILE_NAME traj.xyz
      FIRST_SNAPSHOT 1
      LAST_SNAPSHOT 5
      &MSD
        MSD_PER_KIND
        REF0_FILENAME ref0.xyz
      &END MSD
    &END REFTRAJ
  &END MD
&END MOTION
```

MSD

