

A Graph Theoretic Approach to Problem Formulation for Multidisciplinary Design Analysis and Optimization

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Abstract The formulation of multidisciplinary design, analysis, and optimization (MDO) problems has become increasingly complex as the number of analysis tools and design variables included in typical studies has grown. This growth in the scale and scope of MDAO problems has been motivated by the need to incorporate additional design disciplines and to expand the parametric design space to enable the exploration of unconventional design concepts. In this context, given a large set of disciplinary analysis tools, the problem of determining a feasible data flow between tools to produce a specified set of system-level outputs is combinatorically challenging. The difficulty is compounded in multi-fidelity problems, which are of increasing interest to the MDAO community. In this paper, we propose an approach for addressing this problem based on the formalism of graph theory. The approach begins by constructing the maximal connectivity graph (MCG) describing all possible interconnections between a set of analysis tools. Graph operations are then conducted to reduce the MCG to a fundamental problem graph (FPG) that describes the connectivity of analysis tools needed to solve a specified system-level design problem. The FPG does not predispose a particular solution procedure; any relevant MDO solution architecture

could be selected to implement the optimization. The approach is applied to an example problem to formulate an FPG for a commercial aircraft MDAO study.

1 Introduction

The number of analysis tools required in multidisciplinary design optimization (MDO) studies is growing in parallel with the increasing scope of typical problems. An example can be observed in the historical evolution of the disciplines involved in MDO problems in aircraft design. Multidisciplinary optimization emerged as a separate field from structural optimization through the need to introduce formal techniques for managing the coupling of aerodynamic loads and structural deformations, through the linking of aerodynamic vortex lattice or panel methods with structural finite element models [1]. Subsequently, flight performance and life cycle economics tools were integrated into MDO analysis workflows for conceptual and preliminary design studies [2]. Currently, MDO problems for aircraft design also often include tools for aircraft noise and emissions. In sum, it is now commonplace for 5–10 analysis tools to be employed for typical aircraft design optimization studies.

The number of analysis tools is expected to grow in the future as the scope of MDO problems continues to evolve, and as computing is increasingly commoditized. This expansion of scope will be driven, in part, by consideration of additional disciplines. Current trends on the horizon for aircraft MDO studies include incorporation of manufacturing analyses [3], subsystem performance [4,5], and models of emissions, noise, or economics [6–8].

The time and expense for setting up analysis models is growing in conjunction with the increasing scope of MDO problems. Multidisciplinary Design Analysis and Optimization (MDO) frameworks such as iSight®, ModelCenter®, ModeFrontier®, and OpenMDAO[9] and have enabled a new level of analysis tool integration and have paved the way for models with more analyses and increasing numbers of interdisciplinary couplings. This new capability has created a new challenge. Even models with tens of analyses could include hundreds or thousands of variables that are interdependent and must be linked in the framework. A common situation is that different analyses provide differing values for the same physical quantity, often in different data formats, and these conflicts need to be resolved. These occurrences are particularly acute in situations in which analysis tools have differing fidelities. For example, an abstracted aerodynamic analysis such as an empirical drag buildup model may return only integrated drag,

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whereas a CFD tool may return pressure and shear stress distributions across the entire surface grid. If an analysis downstream of the aerodynamics tool needs only integrated drag as an input, then the designer has a free choice of which of the two possible aerodynamics analysis tools to select to provide the drag estimate (presuming that drag can be computed from surface distributions by a simple integration algorithm). On the other hand, if a downstream analysis needs a pressure distribution in order to compute pitching moment, for example, then any feasible MDO problem formulation must include CFD or similar analysis in the data flow, regardless of whether the empirical drag buildup model is also included.

With the added complexity from larger models, it is plausible that the task of combining all the analyses into a consistent system model capable of solving a relevant engineering design problem could approach the cost and time requirements of creating any of the discipline analyses themselves. For these large scale MDO problems, the couplings between the analyses begin to dominate the effort required in setting up the model. It is this problem of determining sets of analysis tools and their inter-connectivities to form realistic multidisciplinary problems that is the subject of this paper. We are motivated by the following notional but realistic problem of organizing an MDO study for a complex system:

A new system is being designed for which there is little or no historical precedent. The system is complex, as measured by the number of coupled disciplines and/or components involved in the analysis. A general optimization problem statement has been formulated based on system-level objectives and constraints; however, it is unclear which engineering analysis tools should be interconnected in order to solve the optimization problem. A team of disciplinary and/or component design engineers has been formed in which each engineer has expertise in a particular analysis tool or component model. The engineers meet to discuss the approach to interconnecting their tools to achieve the required system-level MDO model.

Our goal is to develop formalism for expressing analysis interconnectivity and for determining feasible analysis tool sets to assist an engineering team conducting this task. Because the problem deals with interconnectivity, we base our approach on the representations and techniques of graph theory. The approach begins by constructing the *maximal connectivity graph (MCG)* describing all possible interconnections between

the analysis tools proposed by the engineers. Graph operations are then conducted to reduce the MCG to a *fundamental problem graph (FPG)* that describes the set of analysis tools needed to solve the specified system-level design problem. The concept of the FPG and the identification of feasible FPGs from an MCG are the main contributions of the paper.

This information in an FPG represents the engineering design problem that needs to be solved, but it is not itself sufficient to actually run a design optimization. It does not provide information about how to solve the problem. Even after the problem is defined an integration platform or framework needs to be selected and appropriate optimization methods identified. This last step essentially involves taking the FPG and turning it into a usable model. We briefly consider methods to further manipulate the FPG into a *problem solution graph (PSG)* which could be useful in this task, but that is not the focus of this paper. The work is primarily concerned with applying graph theory to the creation of an FPG and the benefits to the design process by doing so.

The paper is organized as follows. First, we describe the differences between a fundamental problem formulation, which is based only on the system-level optimization problem statement that the engineers desire to solve and on the available analysis tools, and a specific problem formulation, which additionally presumes a specific MDO solution approach to the problem. Next, we survey the literature related to graph theoretic and formal language approaches to multidisciplinary design problem formulation. We then discuss our graph syntax and representation of MDO problems and describe the procedures for determining the MCG and FPG. Finally, we present an example problem based on an MDO analysis of a commercial aircraft.

2 Background

2.1 Specific vs Fundamental Problem Formulation

The Fundamental Problem Formulation (FPF) is our terminology for a statement of the overall system-level optimization problem that contains only information about analysis tools, design variables, objectives, and constraints without reference to a solution approach. In particular, the FPF does not depend on the choice of solution-specific elements such as the MDAO framework, optimization algorithm, iterative solver, or execution sequence. This description represents the problem from the point of view of an engineer specifying the design problem that he/she desires to solve without specifying how the problem should be solved. The lack of solution information in the FPF contrasts with

optimization problem statements that are written with reference to a specific solution strategy or with implication of a specific execution sequence. For example, consider the Sellar test problem [10], with an FPF given as follows:

$$\begin{aligned}
&\text{given } y_1 = D_1(x_1, y_2, z_1, z_2) \\
&\quad y_2 = D_2(y_1, z_1, z_2) \\
&\text{min. } F(x_1, y_1, y_2, z_2) \\
&\text{w.r.t. } x_1, y_1, y_2, z_1, z_2 \\
&\text{s.t. } G_1(y_1) \geq 0 \\
&\quad G_2(y_2) \geq 0
\end{aligned} \tag{1}$$

In Eq. 1, y_1 is an output of D_1 as well as an input to D_2 . Similarly, y_2 is an output of D_2 as well as an input to D_1 . This implies that D_1 and D_2 are coupled together by means of their mutual dependence. However no information is given as to whether D_1 or D_2 should be run before the other. Given Eq. 1, it would be equally valid to run D_1 first, D_2 first, or both simultaneously. Any MDAO root finding method or compatibility constraint formulation could be implemented to achieve consistency between D_1 and D_2 .

The Sellar problem is simple, with only a single coupling interaction between the two disciplines and a very limited set of variables. However, for larger and more complex problems, it is much more difficult to identify the fundamental problem formulation. Interdisciplinary couplings are not always apparent and the set of analysis tools and variables are much larger.

An example of a more specific problem statement for the Sellar problem is presented in Eq. 2. In this formulation, the implication is that D_1 must be run first. A new variable, \hat{y}_2 , is introduced to break the direct dependence of D_1 on D_2 , and a new coupling constraint, H , is added to enforce consistency. Equation 2 is an equally valid expression of the Sellar problem that could be generated based on a preferred solution approach.

$$\begin{aligned}
&\text{given } y_1 = D_1(x_1, \hat{y}_2, z_1, z_2) \\
&\quad y_2 = D_2(y_1, z_1, z_2) \\
&\text{min. } F(x_1, y_1, y_2, z_2) \\
&\text{w.r.t. } x_1, y_1, \hat{y}_2, z_1, z_2 \\
&\text{s.t. } H(y_2, \hat{y}_2) = 0 \\
&\quad G_1(y_1) \geq 0 \\
&\quad G_2(y_2) \geq 0
\end{aligned} \tag{2}$$

2.2 Background in Graph-Based Descriptions of MDAO Problems

As indicated in the examples in Sec. 2.1, the mathematical language for specifying optimization problem formulations is very general and can be used both for fundamental and specific problem formulations. Tedford and Martins used this syntax to specify the FPF for a set of test problems and also to describe specific formulations for solving them with a number of optimization architectures [11]. By solving different specific problem statements corresponding to the same FPF, they were able to benchmark the performance of different optimization architectures against a fixed set of problems. Gray et al. also benchmarked the performance of a set of MDAO architectures with a similar approach [12]. This work examined a larger set of architectures and proposed the use of OpenMDAO as a platform to build a larger community-developed set of test problems and architectures. Both of these benchmarking efforts demonstrate how multiple specific problem formulations can relate to a common FPF and indicate the value of a common problem description. The challenge with this traditional syntax is that it is not easily manipulated or analyzed with automatic procedures to explore alternate problem formulations.

A number of graph-based methods have been used successfully to translate the mathematical syntax into a more useful computational form. Steward's Design Structure Matrix (DSM) is a square adjacency matrix which captures the relationship between analysis tools. Off-diagonal elements of the matrix indicate coupling [13]. Since a DSM describes a square adjacency matrix, it can be represented in an equivalent directed graph in which nodes represent analysis tools and edges represent information dependence between those tools. The ordering of elements in a DSM can be used to indicate execution order. For more complex problems, choosing the proper order to run analysis tools is a challenging task. Rogers et al. developed DeMAID to manipulate a DSM to find an ordering for analysis tools that reduces the cost of solving highly coupled systems [14, 15]. This re-ordering is done through operations on the DSM matrix and yields multiple specific problem formulations which all solve the same FPF.

A DSM itself is insufficient to describe complete optimization problem formulations because it captures only information about data dependency between analyses; objective and constraint information is missing from the DSM description of the problem. An alternative matrix-based syntax, called a Functional Dependency Table (FDT), was proposed by Wagner and Papalambros. The FDT represents the relationship be-

tween functions, including objectives and constraints, and specific variables that affect them [16]. Similar to DSM, FDT also describes an adjacency matrix of a graph. Unlike the DSM graph, however, the FDT graph is undirected and nodes can represent analysis tools, objectives, or constraints. Edges between nodes represent a dependence on the same variable. Michelena and Papalambros made use of the FDT to solve a graph partitioning problem that yielded more efficient optimization problem decompositions [17]. Allison extended this work to incorporate adjacency matrix information with the FDT to account for system coupling in an automated partitioning scheme [18].

While FDT succeeds at capturing the information about objectives and constraints, its lack of directed edges implies that it cannot describe the coupled data dependency that a DSM captures. Figure 1 shows the FDT for the Sellar problem described by Eq. 1. The FDT shows that D_1 is dependent on y_2 and that D_2 is dependent on y_1 , but the coupled dependence cannot be inferred from that information alone. This missing information implies that, although FDT is very useful for partitioning problems, it is not sufficient to completely describe the data flows in a problem formulation.

	x_1	y_1	y_2	z_1	z_2
D_1	1		1	1	1
D_2		1		1	1
F	1	1	1		1
G_1		1			
G_2			1		

Fig. 1: Functional Dependency Table (FDT) for Eq. 1

Alexandrov and Lewis introduced a graph based syntax called Reconfigurability in MDO Problem Synthesis (REMS) which incorporates objectives and constraints into a graph, effectively combining FDT and DSM [19]. REMS retains the square adjacency matrix form from DSM, but by adding the objectives and constraints, it partially combines a traditional DSM with an FDT. This formulation allows REMS to represent data dependency between multiple analysis tools as well as between analysis tools and objective/constraint functions. Additionally, REMS addresses the need to transition between multiple solution strategies while maintaining a single consistent graph representation of the fundamental problem formulation. However REMS does not provide a mechanism for inclusion of solvers or optimizers in the graph. This fundamentally limits REMS from describing the specifics of a different solution strategies as applied to a specific problem.

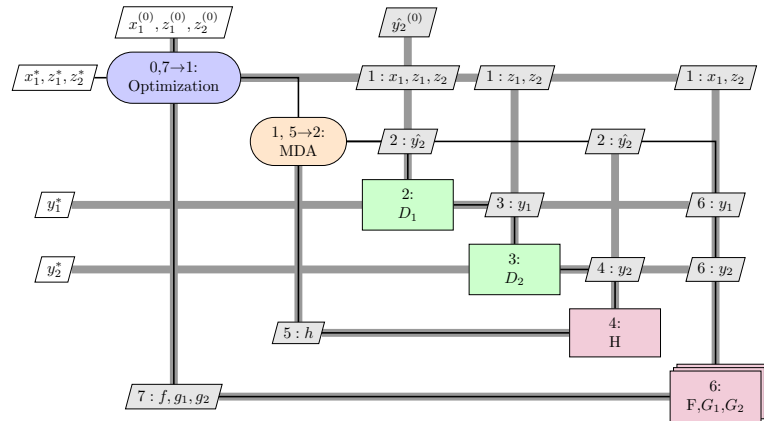


Fig. 2: XDSM for Eq. 2, with a Gauss-Seidel iteration and MDF solution architecture.

Lamb and Martins also included objectives and constraint functions as nodes in an Extended DSM (XDSM) in order to capture a more complete description of solution strategies for MDAO problems [20]. Unlike REMS, XDSM also includes nodes for solvers and optimizers to enable complete definition of MDAO architectures. Martins uses XDSM to describe 13 different optimization architectures in a survey paper that provides a novel classification of the different techniques [21]. With the additional information included in an XDSM, Lu and Martins applied both ordering and partitioning algorithms to an MDAO test problem termed the Scalable Problem [22].

Although XDMS captures many of the functional aspects of FDT, it requires the use of solver and optimizer blocks to represent the relationship between design variables and objectives/constraints. By introducing solver or optimizer blocks, XDMS automatically implies a solution strategy. The XDMS for Eq. 2 is given in Figure 2. This diagram is shown with an assumed Gauss-Seidel iteration scheme and an MDF solution architecture.

In this paper, we propose a new graph syntax that combines certain features of REMS and XDMS. Despite sharing some features with both of these other graph based approaches, the syntax proposed here has a fundamentally different goal which is complimentary to both of them. REMS and XDMS provide excellent human readable formats for an MDAO problem description. This syntax is designed to provide a more effective machine readable format for MDAO problem definition. In the interest of making it easier to algorithmically operate on the graphs, the specified format is both more verbose and less visually informative. The benefit is a

more consistent and easily utilized graph from an algorithm perspective.

2.3 Requirements for a New Graph Syntax

The goal of the graph-based syntax presented here is to enable the general structure of an MDAO problem to be described independently of any solution information, while still being able to accommodate the more specific case when a solution strategy is applied. In order to achieve this goal, the graph syntax needs to accommodate a number of MDAO problem constructs:

- Analysis tools and their interconnections
- Design variables, objectives, and constraints
- Coupling between analyses
- Multi-fidelity analyses

The syntax is intended to represent three phases of the design problem formulation process. In the initial problem definition phase, the specific analysis tools and design goals are identified. Next, a single formal problem formulation is identified that specifies design variables, constraints, objectives, analysis tools, and all other elements required to represent the overall MDAO problem. Lastly, a specific procedure for solving the problem is selected, e.g. selecting an MDAO optimization architecture. Using the proposed graph syntax, the outcome of these phases can be represented with the following graphs:

- Maximal Connectivity Graph (MCG)
- Fundamental Problem Graph (FPG)
- Problem Solution Graph (PSG)

The *maximal connectivity graph* represents the first phase of the problem formulation with all analysis tools being considered and all possible connections between them also present. The second phase of problem formulation results in the *fundamental problem graph*, which comprises only the analysis tools, objectives, constraints, and variables to solve the problem. The final phase results in a *problem solution graph* which includes additional edges and nodes to represent the solution strategy being employed to solve the problem. This paper focuses on the MCG and FPG and does not describe the PSG in detail.

Comparisons of the number and size of each of these graphs are depicted in Figs. 3(a) and 3(b). The tree diagram illustrates that it is generally possible to obtain multiple FPGs from a single maximal connectivity graph. The multiple FPGs may correspond to different down-selections of analysis tools, different connections between the tools, or both. Each down-selection reduces

the number of possible FPGs that could be reached until only one remains. For a given FPG, however, different PSGs may be obtained by implementing different solution strategies. Considering the size of a graph to be the sum of all of its edges and nodes, the hour-glass shape in Fig. 3(b) qualitatively illustrates how the FPG is obtained from the MCG by *removing* nodes and edges, and the PSG is obtained from the FPG by *adding* nodes and edges. These additions correspond to optimizers, solvers, and compatibility constraints required in particular MDAO solution architectures.

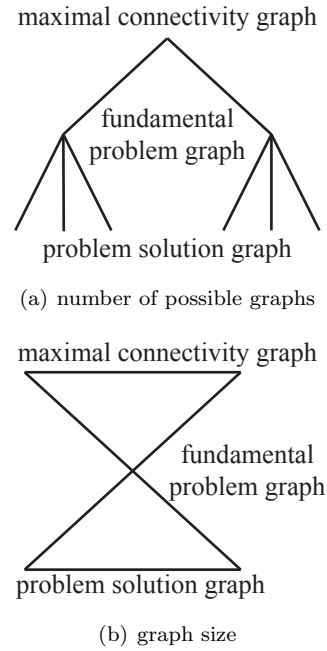


Fig. 3: The relationship between the MCG, FPG, and PSG.

2.4 Potential Applications

The syntax proposed here for defining graphs is partially motivated by the unique needs of working with very large problems that have thousands of design variables. Such problems are large enough that many traditional design methods stumble simply because the problems are so large that one person can not maintain a complete view of the problem. Hence as problems grow to that size, software tools become needed to manage the complexity of the problem itself.

Even for small problems, algorithmic exploration of problem structure can yield deeper understanding of problems and more effective solution methods, as

demonstrated by the work with the FDT. The syntax described here along with the rules for applying that syntax to the three phases of the design process provides a strong foundation to begin developing new algorithms for analyzing and modifying problem structure. This foundation makes it much easier to incorporate a standard view of problem definition into MDAO frameworks and by extension to implement any new algorithms inside those frameworks.

3 Graph-Based Syntax Definition and Formalisms

In this section we present our graph-based syntax, beginning with the necessary graph theoretic fundamentals to construct the graphs discussed in Sec. 2.3. The notation used in this paper is adapted from Diestel [23]. A *graph* is a pair $G = (V, E)$ of sets such that $E \subseteq V \times V$, which means that the elements of E are 2-element subsets of V . The set V contains the *vertices* or *nodes* and the set E contains the *edges*. For a *directed graph* (or *digraph*) we construct E as a set of ordered pairs instead of a set of sets. Each ordered pair represents an edge starting at the node indicated by the first entry and directed to the node indicated by the second entry. An edge $e = (x, y)$ may simply be referred to as xy . The edges directed out from node v are denoted by $E(v)$ and the edges directed into v are denoted by $E^{-1}(v)$. $E(v)$ may be the empty set, a single edge, or a set of edges, and likewise for $E^{-1}(v)$. As an example,

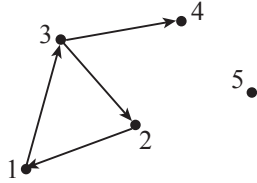


Fig. 4: Example directed graph.

for the directed graph shown in Fig. 4 we have

$$V = \{1, 2, 3, 4, 5\},$$

$$E = \{(2, 1), (3, 2), (1, 3), (3, 4)\}.$$

A *path* $P = (V, E)$ from x_0 to x_k in graph G is a subgraph of G with $V = \{x_0, x_1, \dots, x_k\}$ and $E = \{(x_0, x_1), (x_1, x_2), \dots, (x_{k-1}, x_k)\}$. Path P is a *cycle* if $x_0 = x_k$. A *reverse path* P_R in graph G is a path on R , where R is the reverse graph of G obtained by switching the orientation of every edge.

Let I be a nonempty set such that for each $i \in I$ there is a corresponding set A_i . The set of sets $\mathcal{A} =$

$\{A_i \mid i \in I\}$ is called an indexed family of sets with index i and indexing set I [24]. The union over this family of sets can be described in a few different ways:

$$\bigcup_{i \in I} A_i = \bigcup_{A \in \mathcal{A}} A = \{x \mid x \in A \text{ for some } A \in \mathcal{A}\}. \quad (3)$$

Lastly, the cardinality of a set B is the number of elements in B and is denoted as $|B|$.

3.1 Node and Edge Types

We categorize nodes and edges into distinct types in order to provide an intuitive approach to MDAO problem formulation. The three node types are

variable node: represents scalar or array data, inputs and outputs,

function node: represents the computation performed by analysis tools,

driver node: represents control logic capable of managing iterations (present only in a PSG),

and the three edge types are

connection edge: represents exchange of information external to analysis tools,

function edge: represents exchange of information internal to analysis tools,

driven edge: represents passing of information from a driver node to a variable node (present only in a PSG).

Figure 5 demonstrates the usage of these node and edge types via the Sellar problem. In this figure, function nodes are indicated by squares, variable nodes are indicated by circles, connection edges are indicated by dotted lines, and function edges are indicated by solid lines.

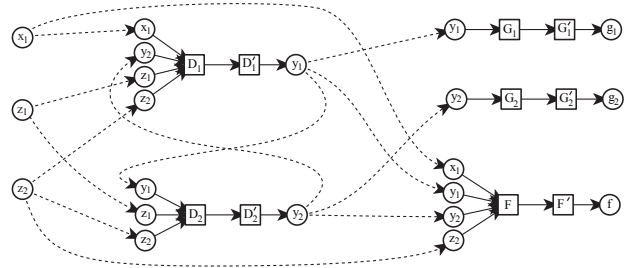


Fig. 5: Sellar problem represented as a graph.

A rule set is provided for the usage of these node and edge types to provide a structure to the graph-based representation. The driver node and the driven

edge are allowed only in PSGs, whereas the other node and edge types can be present in any of the three graph types, subject to the following restrictions:

1. A function node may have only one edge directed to or from another function node.
2. A function node may have only function edges directed in or out.
3. A function node must have at least one edge directed in and at least one edge directed out.
4. If a variable node has an outgoing function edge, then it may not have other outgoing edges.
5. If a variable node has an incoming function edge, then it may not have any additional incoming edges.

Alexandrov and Lewis’s REMS syntax includes only two node types (variable and function) and one edge type [19]. The present work adds one additional node type and two additional edge types to the syntax to allow descriptive graphs for all three phases of the design problem formulation process discussed in Sec. 2.3.

3.2 Analysis Blocks

Analysis tools take in a set of input variables and calculate the values for their respective outputs. We represent this process by a digraph called an *analysis block*; a notional analysis block is shown in Fig. 6. As indicated in this figure, analysis blocks comprise three sets of nodes representing the distinct local inputs, the analysis (computation), and the distinct local outputs. The local input and local output nodes are variable nodes, while the nodes representing the analysis are function nodes. All of the edges within the analysis block are function edges, and are considered fixed to the analysis block. This graph structure demonstrated by Fig. 6 satisfies the rules listed in Sec. 3.1. Conversely, the rules ensure that analysis tools are represented via this analysis block structure.

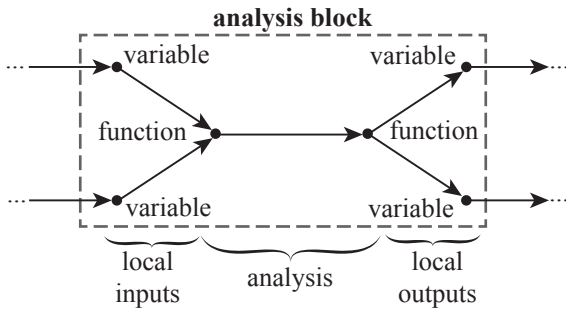


Fig. 6: Example analysis block with node types labeled.

The function edge connecting the two function nodes represents the necessary calculations to map the inputs to the outputs of the analysis. This edge also provides the opportunity to encode computational cost or other characteristics of the analysis code as a weight in a weighted graph formulation. Because all the edges within analysis blocks are fixed, the blocks themselves are fixed sub-graphs within the overall MDAO problem graph. The connectivity of nodes and edges in an analysis block cannot be altered for the purposes of MDAO problem formulation; however, analysis block sub-graphs can be added or removed from the MDAO problem graph as needed. Variable nodes in an analysis block can be distinguished as either an input or an output by the manner in which they are connected. As shown in Fig. 6, inputs are represented as variable nodes that have an outgoing edge into a function node, and outputs are represented as variable nodes that have an incoming edge from a function node.

3.3 Objectives, Constraints, and Inputs

Along with analysis tools, objectives, constraints, and inputs also need to be represented. In the case of objective functions, a single output value generated by an analysis block could be selected, but commonly, multiple output values from different analysis tools are aggregated together to form a composite objective function. Generally, both objective and constraint functions accept a set of inputs and map them to an output value of significance to the overall design problem.

The operations of implementing composite objective and constraint functions, although typically simple, are effectively identical to the task performed by an analysis block. A composite constraint or objective function can therefore be represented as an analysis block within the graph with its own input and output variable nodes. Although fundamentally no different than an analysis block, for clarity and convenience, it is useful to distinguish between analysis blocks corresponding to analysis codes and those that arise from the addition of objectives or constraints to the graph. Therefore, we use an *expression block* to represent an objective or constraint. These expression block graphs follow the same structure as analysis blocks presented in Sec. 3.2.

Finally, inputs to the problem formulation are represented in the graph by individual variable nodes with connection edges directed out to corresponding local inputs of analysis blocks, and they are referred to simply as *inputs*. These nodes serve to indicate that the variable nodes within analysis or expression blocks to which they are connected represent the same variable in the problem formulation.

Figure 7 demonstrates the use of inputs (black circles), analysis blocks (dotted boxes), and expression blocks (dashed boxes), for the Sellar problem graph.

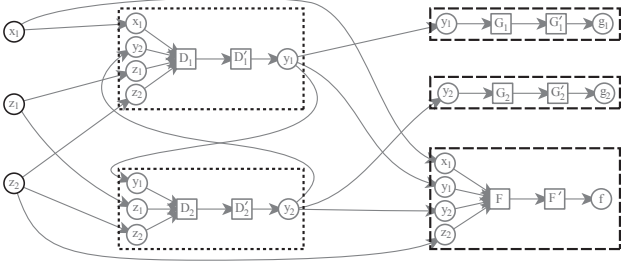


Fig. 7: Sellar problem graph indicating inputs (black circles), analysis blocks (dotted boxes), and expression blocks (dashed boxes).

3.4 Indegree and Outdegree Limits

To address the MDAO notion of design variables, we first introduce the concept of the degree of a node. In a digraph, *indegree* of a node is the number of edges directed in and is denoted as $\deg^-(v)$, and the *outdegree* is the number of edges directed out and it is denoted as $\deg^+(v)$ [23].

We may now define the *upper indegree limit*

$$\deg_u^-(v) : V \rightarrow \mathbb{N} \quad (4)$$

and the *lower indegree limit* as

$$\deg_l^-(v) : V \rightarrow \mathbb{N}. \quad (5)$$

These user-specified limits govern the number of connection edges that may be directed into a node for a valid graph; of course, the specification must satisfy $\deg_l^-(v) \leq \deg_u^-(v)$. For example, consider a variable node v with $\deg_u^-(v) = \deg_l^-(v) = 1$. In this case, v must have exactly one incoming connection edge or the graph is deemed an invalid problem formulation.

3.5 Driver Nodes and Driven Edges

Within this syntax, all iterative processes are represented with Driver nodes. The driver node shares some basic qualities with the model node. It can have incoming and outgoing function edges to and from variable nodes. For example, many optimizers take convergence tolerance as input and output iteration counts and final objective value. With respect to variable nodes

and function edges, drivers behave exactly the same as model nodes and are subject to the same rules governing their use in the graph. In this context, driver nodes can be part of driver blocks which behave just like analysis blocks.

Driven edges are the distinguishing characteristic associated with driver nodes and driver blocks. Driven edges don't follow the same rules as other edges. Driven edges will always connect a driver node to a variable node (in either direction), but they are not considered when counting the indegree or outdegree of the variable node. Hence a single variable node could have multiple incoming driven edges from different driver blocks, e.g. in a sequential optimization strategy, both drivers would at different times, pick values for the same variable. Figure 8 shows a notional example where a driver block represents an optimizer solving an unconstrained minimization problem.

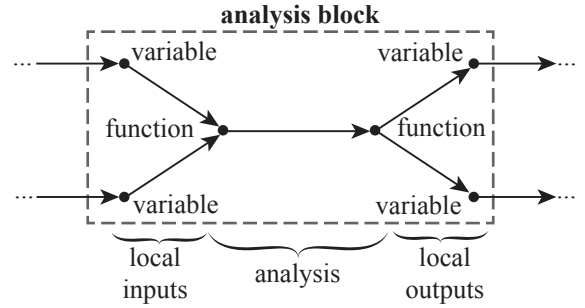


Fig. 8: Example driver block with node types labeled.

4 MDAO Constructs Derived from the Graph-Based Syntax

In Sec. 3, we presented the structure of the graph-based representation. We now discuss how these formalisms provide the remaining MDAO problem constructs identified in Sec. 2.3.

4.1 Design Variables, Holes, and Collisions

Design variables are input variables whose values are free to be changed by the designer or by an optimizer in an MDAO study. In the graph-based syntax, a node corresponds to a design variable if the indegree limits of the node are prescribed as zero.

If the indegree limits are violated by the number of incoming connection edges (the indegree of the node), then the graph is regarded as an invalid problem formulation. There are two classifications for these violations:

hole: The number of incoming edges is less than the lower indegree limit:

$$\deg^-(v) < \deg_l^-(v). \quad (6)$$

A hole represents a lack of information being supplied to the variable node. This implies that the analysis tool being represented by the analysis block would not be capable of producing outputs.

collision: The number of incoming edges is greater than the upper indegree limit:

$$\deg^-(v) > \deg_u^-(v). \quad (7)$$

A collision represents redundant information being supplied to the variable node from two or more sources. This conflict implies an ambiguity as to which information is to be used as an input for the analysis tool. In multifidelity problems (discussed subsequently), the upper indegree limit could be specified as $\deg_u^- > 2$, which implies that a collision is not noted in the case of multiple inputs.

The presence of holes and collisions in a graph represent conflicts that will give rise to an invalid problem formulation. The process of obtaining an FPG from an MCG will reveal these conflicts.

4.2 Coupling Between Analyses

In MDAO, coupling is the mutual dependence between two or more analysis tools and their respective outputs. In this graph-based syntax, coupling is described by the presence of a cycle between two or more analysis blocks. In the Sellar problem from Eq. 1 a mutual dependence between D_1 and D_2 exists through the variables y_1 and y_2 . The edges belonging to a cycle in the Sellar problem are highlighted in Fig. 9. These edges collectively form a closed path between analysis blocks D_1 and D_2 .

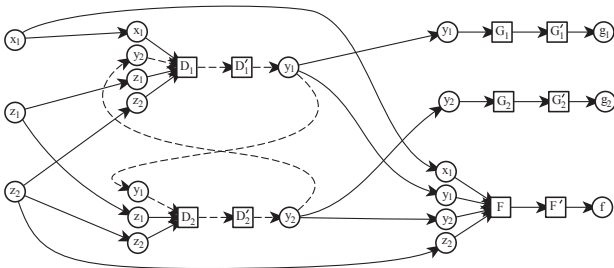


Fig. 9: Sellar problem graph with dashed edges indicating participation in a cycle.

Coupling cycles do not contain driver node or driven edgess since these are not allowed in the MCG or FPG

representations. Solvers, optimizers, and other iterative processes are not invovled in the coupling definition; however, one or more solvers will be required to build a valid PSG from a given FPG that includes cycles. Additionally, a coupling cycle has no inherent start or end point. It would be acceptable to select a node in the cycle as a starting point and proceed around the loop until the starting point is reached again. For the Sellar Problem, selecting D_1 as the starting point would yield a problem as given in Eq. 2. Larger problems can involve more complex cycles in their FPG, indicating more complex coupling between analyses. For example, a cycle can involve more than two analysis blocks. Multiple independent cycles could also exist, indicating independent coupling relationships. Cycles can also overlap, meaning that the same analysis blocks are involved in multiple different coupling cycles. All of these situations arise naturally as the size of problems grows, and managing this coupling may become difficult. In the present work, Sec. 6 demonstrates how building an FPG from an MCG provides an opportunity to identify and potentially reduce the number of cycles in a graph.

If many couplings are present, convergence rates can be improved by searching for an effective ordering for the execution of analyses. Rogers' DeMAID tool uses a genetic algorithm to find an ordering that minimizes the overall coupling of the system by separating independent cycles in the graph [14,15]. Rogers work focused on the matrix form of the DSM for ordering optimization. Lu and Martins more recently leveraged a weighted form of the DSM and used an iterative clustering approach to perform a similar task to DeMAID [22].

4.3 Multi-fidelity Problems

A multi-fidelity MDAO problem can be characterized by a formulation in which two or more different analyses each calculate the same data. Multi-fidelity is represented in a graph by a variable node having an indegree greater than one, which means that multiple connection edges are directed into it. When the upper indegree limit of a variable node is set above one, then the node is implied to allow multiple fidelity instances of the variable. When the lower indegree limit of a variable node is set above one, then multiple fidelity instances are required.

In a multi-fidelity problem, a given variable node may have multiple incoming edges without implying a collision as defined by Eq. 7. Figure 10 shows a modified version of the Sellar problem with a new analysis, D_0 , representing a low fidelity version of D_1 . In this modified version, the variable nodes with an upper indegree

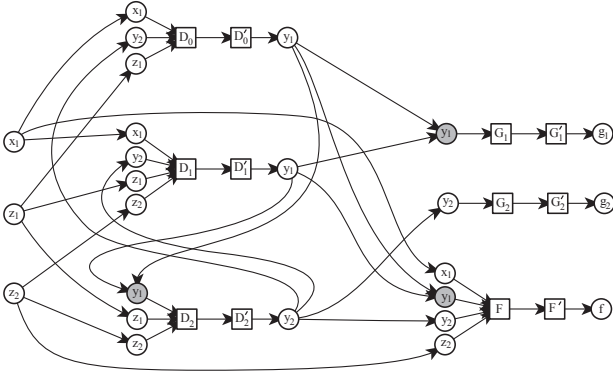


Fig. 10: Graph of the modified Sellar problem with multi-fidelity nodes highlighted in gray.

limit of two are highlighted in gray, and changing the upper indegree limits for the variable nodes representing y_1 in D_2 , F , and G_1 avoids a collision. In Sec. 5.3 we present an algorithm for locating conflicts within a given MCG such that a designer can make the necessary decisions about each one in turn.

Multi-fidelity problems are always characterized by graphs in which at least some of the variable nodes that have an $\deg_u^-(v) > 1$. These problems require special techniques for resolving the conflicting edges by introducing some mechanism to manage when each of the different fidelity analyses are run [25–27]. The specifics of this mechanism are not represented within an MCG or FPG. Instead, the multi-fidelity mechanism specifics would be represented as a driver in a PSG derived from a multi-fidelity FPG.

Table 1 summarizes the classification of a variable node as a hole, design variable, single valid input (nominal), collision, or multi-fidelity node.

Table 1: Variable Node Classification

$\deg_l^-(v)$	$\deg_u^-(v)$	$\deg^-(v)$	valid	classification
0	0	0	yes	design variable
0	0	1	yes	collision
0	1	0	yes	design variable
0	1	1	yes	single input
1	1	0	no	hole
1	1	1	yes	single input
1	1	> 1	no	collision
1	2	1	yes	supplied input
1	2	2	yes	multi-fidelity
2	2	< 2	no	hole
2	2	2	yes	multi-fidelity
2	2	> 2	no	collision

4.4 Iterative Control: Drivers

There are many iterative processes that are used to help solve MDAO problems such as solvers, optimizers, and Design of Experiment (DOE). Abstractly, even a human picking values guided by experience and trend could be viewed as an iterative process. These processes represent the control structures that govern how a design problem marches toward a solution but they do not fundamentally impact the definition of the problem to be solved. e.g. which optimizer you choose does not change the problem you are solving but will change the path you follow to solve it. Hence, as a rule, driver nodes and driven edges are excluded from both the MCG and FPG which deal exclusively with problem formulation. They only come into play with in the PSG where the issue of how to solve a specific problem is addressed. In fact, at least one driver block is required to be present in any PSG in order to select values for the design variables.

5 The MCG, FPG, and PSG

We now discuss how the graph-based syntax defined in Secs. 3 and 4 is used to represent an MDAO problem in its entirety. This discussion is based on the MCG and the FPG.

5.1 Maximal Connectivity Graph

For a specified MDAO problem, the maximal connectivity graph represents every analysis tool, objective, constraint, and input being considered, as well as every possible interconnection among them. The definition of the MCG is given via construction. To construct the maximal connectivity graph, we presume that a set of analysis tools, inputs, objectives, and constraints are provided. Each of the m analysis codes correspond to an index $i \in I_A$, $I_A = \{1, 2, \dots, m\}$, and are represented by an analysis block graph $G_{A_i} = (V_{A_i}, E_{A_i})$. Each of the n expression blocks correspond to an index $i \in I_E$, $I_E = \{1, 2, \dots, n\}$, and is represented by expression block graph $G_{E_i} = (V_{E_i}, E_{E_i})$. Finally, the inputs are represented as a set of variable nodes V_{in} . We presume that V_{in} , each G_{A_i} , and each G_{E_i} are given, and that any potential connection between variables is specified in the form of connection edges in the set $E_{M,con}$. One method for defining these connections is to use a constant variable naming convention.

We may then construct the maximal connectivity graph $M = (V_M, E_M)$. V_M is the union of the sets of

variable nodes from the inputs, analysis blocks, and expression blocks.

$$V_M = V_{\text{in}} \cup \left(\bigcup_{i \in I_A} V_{A_i} \right) \cup \left(\bigcup_{i \in I_E} V_{E_i} \right) \quad (8)$$

E_M is the union of all connection and fixed edges from the all the analysis blocks and expression blocks.

$$E_M = E_{M,\text{con}} \cup \left(\bigcup_{i \in I_A} E_{A_i} \right) \cup \left(\bigcup_{i \in I_E} E_{E_i} \right) \quad (9)$$

The MCG M is uniquely determined by the given set of analysis blocks, inputs, and expression blocks. In the cases where the set of inputs is not known a priori, the process of obtaining the FPG will reveal the required inputs, as discussed subsequently.

The nodes and edges in M can be partitioned in sets according to their type:

$$V_M = V_{M,\text{var}} \cup V_{M,\text{fun}}, \quad V_{M,\text{var}} \cap V_{M,\text{fun}} = \emptyset, \quad (10)$$

where $V_{M,\text{var}}$ and $V_{M,\text{mod}}$ are the sets of variable nodes and function nodes, respectively;

$$E_M = E_{M,\text{con}} \cup E_{M,\text{fun}}, \quad E_{M,\text{con}} \cap E_{M,\text{fun}} = \emptyset, \quad (11)$$

where $E_{M,\text{con}}$ and $E_{M,\text{fun}}$ are the sets of connection edges and function edges, respectively. These sets will be referenced in the process for obtaining an FPG.

5.2 Fundamental Problem Graph (FPG)

We now define the fundamental problem graph $F = (V_F, E_F)$ as a directed graph meeting the following conditions:

- (1) $F \subset M$ and $G_{E_i} \subset F \forall i \in I_E$
- (2) $\forall i \in I_A$, if $F \cap G_{A_i} \neq \emptyset$ then $G_{A_i} \subset F$
- (3) $\forall v \in V_F$ with $v \in V_{M,\text{var}}$ and $\deg_l^-(v) \leq \deg^-(v) \leq \deg_u^-(v)$
- (4) $\forall v \in V_F$ there exists a reverse path $P \subset R_F$ from x to v with $x \in V_{E_i}$

Condition (1) asserts that only the nodes and edges provided by the maximal connectivity graph can be used in the fundamental problem graph and that every expression block must be included. Condition (2) requires that analysis blocks must be included or excluded in their entirety. Condition (3) stipulates that the number of edges directed into each variable node must be within the lower and upper in-degree limits; if $\deg^-(v) < \deg_l^-(v)$ the node is the location of a *hole*, and if $\deg^-(v) > \deg_u^-(v)$ the node is the location of a *collision*. Lastly, condition (4) ensures that only the nodes that are used in the MDAO problem formulation

are included in the FPG by requiring that for every node a reverse path exists from at least one expression block to that node. The reverse graph R_F is obtained from F by simply switching the orientation of every edge in E_F .

5.3 Algorithm for Obtaining the Fundamental Problem Graph from the MCG

In general, there may be zero, one, or many graphs that satisfy the FPG conditions in Sec. 5.2. Here, we describe an algorithm for obtaining an FPG from a given MCG by starting with the MCG and disconnecting connection edges until the FPG conditions are met. With this approach, the problem is reduced to deciding which connection edges to remove.

Step 1: Holes The first step is to detect holes and disconnect the first set of connection edges downstream of them, as indicated in Fig. 11.

To begin the process, an initial graph is created as a copy of the MCG

$$F_0 = M, \quad (12)$$

where $F_0 = (V_{F_0}, E_{F_0})$, and $C_{F_0,\text{con}}$ is the set of connection edges. The set of variable nodes that are holes is identified as

$$H = \{v \in V_{F_0} \mid v \in V_{M,\text{var}} \text{ and } \deg^-(v) < \deg_l^-(v)\}, \quad (13)$$

which is the set of variable nodes with fewer incoming edges than are allowed by the lower indegree limit. An updated set of edges is then created by removing the connection edges preceding or succeeding the analysis block:

$$E_{F_1} = E_{F_0} \setminus \{(x, y) \in E_{F_0,\text{con}} \mid x \in V_{A_i} \text{ or } y \in V_{A_i}, \text{ and } H \cap V_{A_i} \neq \emptyset\},$$

and the graph is updated as

$$F_1 = (V_{F_0}, E_{F_1}). \quad (14)$$

Because removing these edges can create new holes, this step must be repeated until no additional holes are found. If the hole identification step identifies a variable node in an expression block as hole, meaning $V_{E_i} \cap H \neq \emptyset$ for some $i \in I_E$, then the algorithm terminates because an FPG cannot be obtained.

If this step terminates without identifying a hole in an expression block, it is guaranteed that an FPG can be obtained because F_1 now satisfies all conditions from Sec. 5.2 except for (3), which requires

that no holes or collisions be present in the graph. Since the graph is free of holes, and collisions can always be resolved without producing a hole, (see Table 1), then it is guaranteed that an FPG can be obtained.

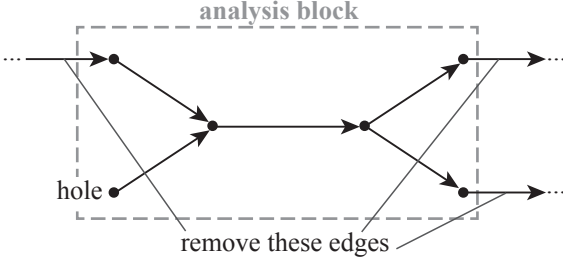


Fig. 11: Example variable node indicating a hole.

Step 2: Collisions The second step is to detect collisions and to disconnect precisely the number of connection edges required such that all collisions are resolved without introducing holes. The set of variable nodes at which collisions occur is

$$S_{\text{nodes}} = \{v \in V_{M,\text{var}} \mid \deg^-(v) > \deg_u^-(v)\}, \quad (15)$$

where the degree is now calculated with respect to F_1 . For each collision node we can construct a set containing the edges directed into the node. The set containing all of these sets is constructed as

$$S_{\text{edges}} = \{\{(x, y) \in E_M\} \mid y \in S_{\text{nodes}}\} \quad (16)$$

Let $J = \{1, 2, \dots, |S_{\text{edges}}|\}$ be an indexing set for S_{edges} such that each $S_{\text{edges},j}$ corresponds to a set in S_{edges} for $j \in J$. An example collision is shown in Fig. 12 to exemplify the definition of $S_{\text{edges},j}$. J also indexes S_{nodes} because there is a one-to-one correspondence between the elements in S_{nodes} and the elements in S_{edges} (which are sets). We may then construct sets of edges as

$$B_j = \{e_k \in S_{\text{edges},j} \mid k \in \{1, 2, \dots, K\} \\ \text{with } \deg_u^-(v_j) \leq K \leq \deg_u^-(v_j)\}, j \in J,$$

which means that each set B_j is constructed from the set $S_{\text{edges},j}$ by taking only as many edges as are allowed by the upper and lower indegree limits of v_j . The construction of each B_j corresponds to making a decision about which edges to include and which edges not to include. Let the new set of connection edges be denoted

$$E_{F_2,\text{con}} = \{e \in E_{F_1,\text{con}} \mid e \in B_j \text{ for some } j \in J\}. \quad (17)$$

The set of all edges is created by removing the connection edges not in $E_{F_2,\text{con}}$:

$$E_{F_2} = E_{F_0} \setminus (E_{M,\text{con}} \setminus E_{F_2,\text{con}}), \quad (18)$$

which gives

$$F_2 = (V_{F_0}, E_{F_2}). \quad (19)$$

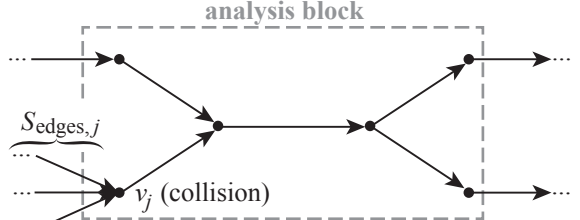


Fig. 12: Example variable node indicating a collision.

Step 3: Finalize The third and final step is to prune the graph to exclude any analysis blocks that became unneeded after the collisions were resolved. This is accomplished by first creating the reverse graph of F_2 , $R = (V_R, E_R)$, where

$$E_R = \{(x, y) \mid (y, x) \in E_{F_2}\}, V_R = V_{F_2} \quad (20)$$

Next, a new node b is added to V_R and edges directed from this node to each of the expression blocks are added:

$$\forall i \in I_E, \forall v \in V_{E_i}, \text{ if } \deg^-(v) = 0 \text{ then } (b, v) \in E_R. \quad (21)$$

The set of nodes that may be reached from b is then constructed as

$$U = \{v \in V_R \mid \exists P \text{ a path from } b \text{ to } v, P \subset R\}. \quad (22)$$

Because b is directed into only the expression blocks, any path from b necessarily provides a path from at least one expression block, which means the node is being used in the problem formulation.

The list of analysis blocks with at least one node in U is constructed as

$$I_F = \{i \in I_A \mid V_{A_i} \cap U \neq \emptyset\} \quad (23)$$

Any analysis block not in I_F should be removed from the graph because none of its outputs contribute to the problem. Inputs that are not being

used are also removed. The set of nodes to remove is then

$$N = (V_{\text{in}} \setminus U) \cup \left(\bigcup_{i \notin I_F} V_{A_i} \right), \quad (24)$$

and the new set of nodes is created as

$$V_F = V_{F_2} \setminus N. \quad (25)$$

Edges involving the removed nodes are also deleted as

$$E_F = E_{F_2} \setminus \{(x, y) \mid x \in N \text{ or } y \in N\}. \quad (26)$$

The fundamental problem graph is then

$$F = (V_F, E_F). \quad (27)$$

If desired, the set of connection edges can be extracted by considering only edges whose endpoints are not in the same analysis block:

$$E_{F,\text{con}} = \{(x, y) \in E_F \mid \sim (x \in V_{A_i} \text{ and } y \in V_{A_i} \text{ for some } i \in I_F)\}.$$

This algorithm will always provide an FPG if one exists. If an FPG does not exist, the implementation reveals the limiting factors that prevent a valid FPG from being achieved.

5.4 Suggested Process for Applying the FPG Algorithm

Section 5.3 provided an algorithm for obtaining an FPG from the given MCG. The algorithm can be applied as part of a broader process in which the designer changes the problem formulation or the supplied analysis tools to attempt to obtain an FPG. The following steps detail the suggested procedure for obtaining an FPG:

- (A) Begin with a set of inputs, analysis tools, objectives, and constraints.
- (B) Build the MCG as described in Sec. 5.1.
- (C) Set indegree limits for variable nodes representing local inputs as described in Sec. 3.4 and Table 1.
- (D) Run the FPG algorithm described in Sec. 5.3. If a valid FPG is unattainable:
 - (a) Change the MCG by adding analysis blocks and/or inputs, which means identifying new analysis tools to include in a potential MDAO workflow.
 - (b) Change indegree limits (see Table 1).
- (E) Repeat from step (A) until an FPG is obtained.

This process illustrates how the algorithm for obtaining a valid FPG can be applied. However, the process also serves to illustrate how a designer may revisit the MCG after an FPG has already been produced. For example, if a designer desires to change an input to be multifidelity, new analysis blocks can be added to the original MCG, the indegree limits can be modified accordingly, and the algorithm can be applied again.

5.5 Problem Solution Graph

Once a suitable FPG has been obtained the issue of how to structure a solution strategy can be addressed. Similar to the way an MCG can be manipulated into a FPG, an FPG can be further manipulated into a PSG. To get from an MCG to an FPG you eliminated analysis blocks and connection edges to reduce the problem to something solvable, but to get from an FPG to a PSG you add in driver blocks, driven edges to describe the structure of the solution strategy being applied to the problem. For example, Figure 13 shows the PSG that solves the Sellar problem with an MDF solution strategy. There are two driver blocks in this PSG, one for the solver that ensures compatibility and another for the optimizer that picks the design variables.

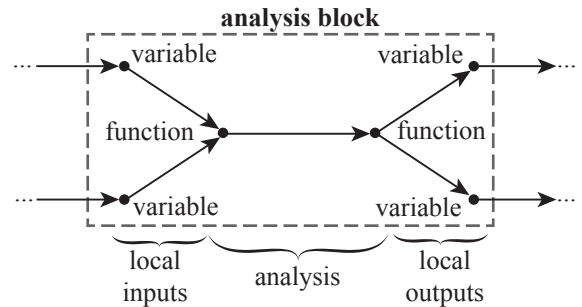


Fig. 13: Example PSG for solving the Sellar problem with MDF strategy

The PSG in figure 13 can be compared to the XDSDM for the same situation in Fig. 2. While the two diagrams contain much of the same information there is a significant difference. The PSG describes the data passing that happens between the drivers and the rest of the problem, but it does not describe when that data passing will occur (the execution order of the blocks). In the proposed graph syntax edges describe the passing of data between one node and another, but they do not define when that communication happens.

XDSDM diagrams do contain information about data passing as well as when that data should be passed.

XDSM essentially represents two related, but independent graphs simultaneously. This is accomplished by including two distinct sets of edges, one for data connections and a second indicating execution sequence. As seen in Fig. 2 data connections are bold-gray edges and execution connections are numbered-black edges. The execution edges, the back edges, in XDSM represent an additional graph that follows a completely different set of rules and behaviors from the data connections graph. On the other hand the data described by the gray edges, the data passing information, is equivalent to the information in the PSG. XDSM presents this information in a more compact and human readable manner by aggregating groups of related variables into combined nodes. The more verbose form presented in a PSG is less human readable, but more easily machine readable as a consequence of a more consistent structure.

6 Example Problem

This section presents an example problem to demonstrate the process of obtaining the FPG and the advantages of doing so. The example task is to create an FPG for the conceptual sizing of a single-aisle subsonic transport aircraft using a set of analysis tools with objectives including performance and gross weight for a required mission. The full set of analysis codes available for use is provided in Table 2. Each analysis tool

Table 2: Analysis tools for subsonic transport sizing

analysis tool	description
VSP	parametric vehicle geometry
PDCYL	wing and fuselage weight estimation
NPSS	engine sizing and performance
VORLAX	vortex lattice method aerodynamics
PMARC	low-order panel method aerodynamics
WATE	engine weight estimation
FLOPSa	mission performance
	engine sizing and weight estimation
FLOPSb	mission performance only

contributes individual disciplinary analysis capability, but the outputs of the tools are not mutually exclusive. For example, VORLAX and PMARC are both aerodynamics codes that predict induced drag but with different levels of fidelity. The Flight Optimization System (FLOPS) is included twice to represent two different configurations corresponding to different uses. FLOPSa denotes FLOPS implemented to execute both mission performance and engine analysis, while FLOPSb indicates FLOPS implemented to execute only mission

performance analysis. This representation is useful for “supercodes” that are capable of being implemented in different ways and with different sets of inputs and outputs. The enumeration of these analysis tools and objectives concludes step (A) in Sec. 5.4.

Step (B) is the production of the MCG. In this example, the MCG is formed by using a consistent variable naming convention and then connecting all variables with the same name with connection edges. Table 3 presents the full list of variables in the leftmost column and indicates whether the variable is an input or an output of each analysis tool. Some variables, such as geometry and performance, represent groups of variables that are passed as arrays or other data structures due to their similarity. This bundling of variables is not fundamental and does not limit the generality of this example; rather, it simplifies the presentation.

In this example, the MCG M is formed in four steps:

1. An analysis block is created for each analysis code using the information in each column of Table 3. Each analysis block is formed by first creating variable nodes for each input and adding directed edges into a single function node. A function edge is created from this function node into a second function node, which is then directed into variable nodes corresponding to each output. A sample analysis block is shown for analysis code FLOPSa in Fig. 14.

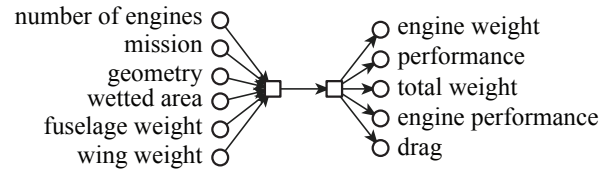


Fig. 14: Sample analysis block for analysis code FLOPSa using Table 3

2. Expression blocks are created to represent the objectives for performance and total weight.
3. A variable node is created to represent the geometry variable as an input. Any inputs incorrectly omitted will be identified in step (D).
4. Connection edges are created that connect each variable node to every other variable node representing variables with the same name. The direction is determined by whether the variable node has an edge directed into or out of a function node, i.e. whether it is a local input or a local output.

The resulting MCG is shown in Fig. 15. Cycles are shown as dashed lines. FPGs formed from this MCG may or may not retain these cycles, depending on user choices.

Table 3: Analysis code input and output description

variable	analysis code							
	VSP	PDCYL	NPSS	VORLAX	PMARC	WATE	FLOPSa	FLOPSb
geometry	in	in		in	in	in	in	in
number of engines			in				in	in
mission							in	in
fuselage weight		out					in	in
wing weight		out					in	in
engine weight						out	out	in
wetted area	out						in	in
inviscid drag				out	out			in
drag			in				out	out
engine performance			out			in	out	in
performance							out	out
total weight		in					out	out

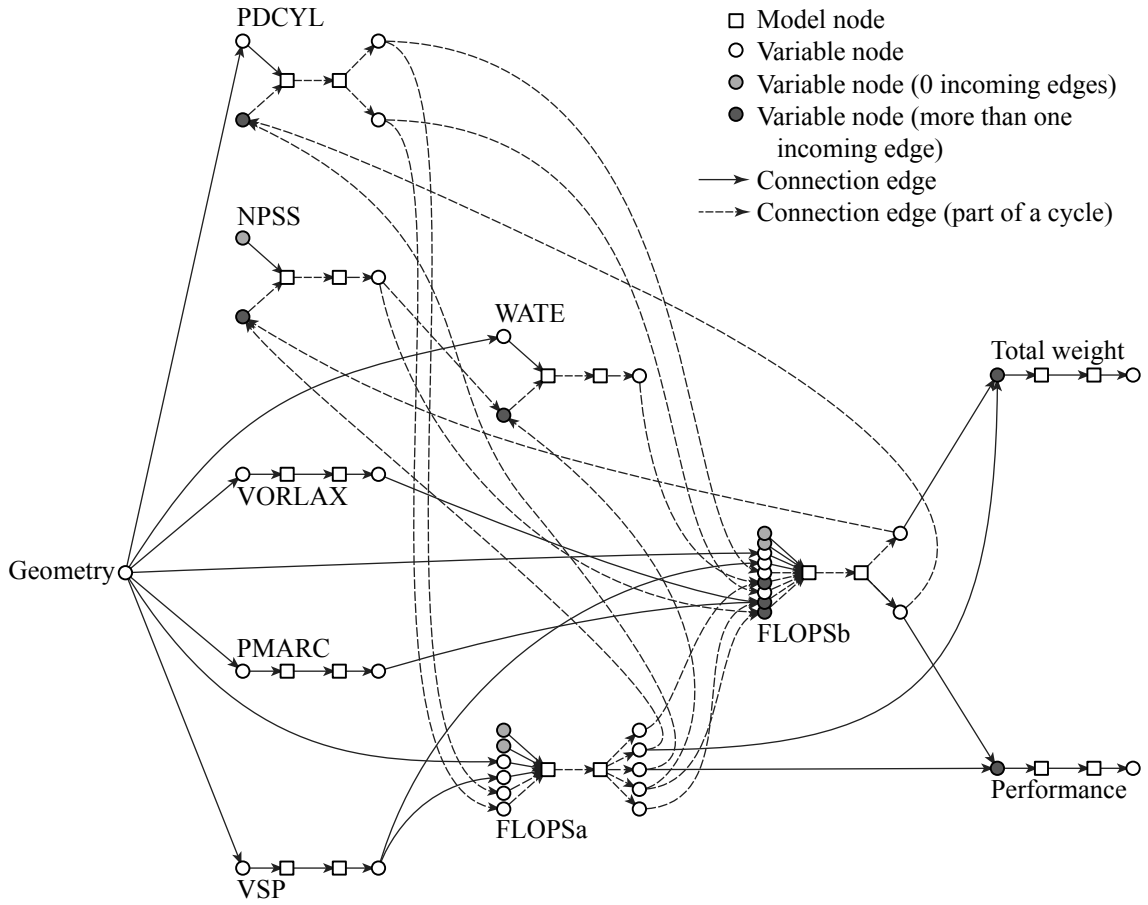


Fig. 15: Maximal connectivity graph for the subsonic transport example problem

To implement step (C) in Sec. 5.4, the indegree of every variable node is set to unity to reflect a single fidelity analysis for which the design variables have not yet been selected.

Step (D) now proceeds by executing the FPG algorithm. An FPG cannot be obtained because the variable nodes representing the number of engines are holes

for NPSS, FLOPSa, and FLOPSb, and the variable nodes representing the mission definition are holes for FLOPSa and FLOPSb. These holes are propagated upstream by the FPG algorithm and create holes in the objectives, thereby preventing a valid FPG.

Step (D)(a) begins to resolve this conflict by creating an input for the number of engines. In this exam-

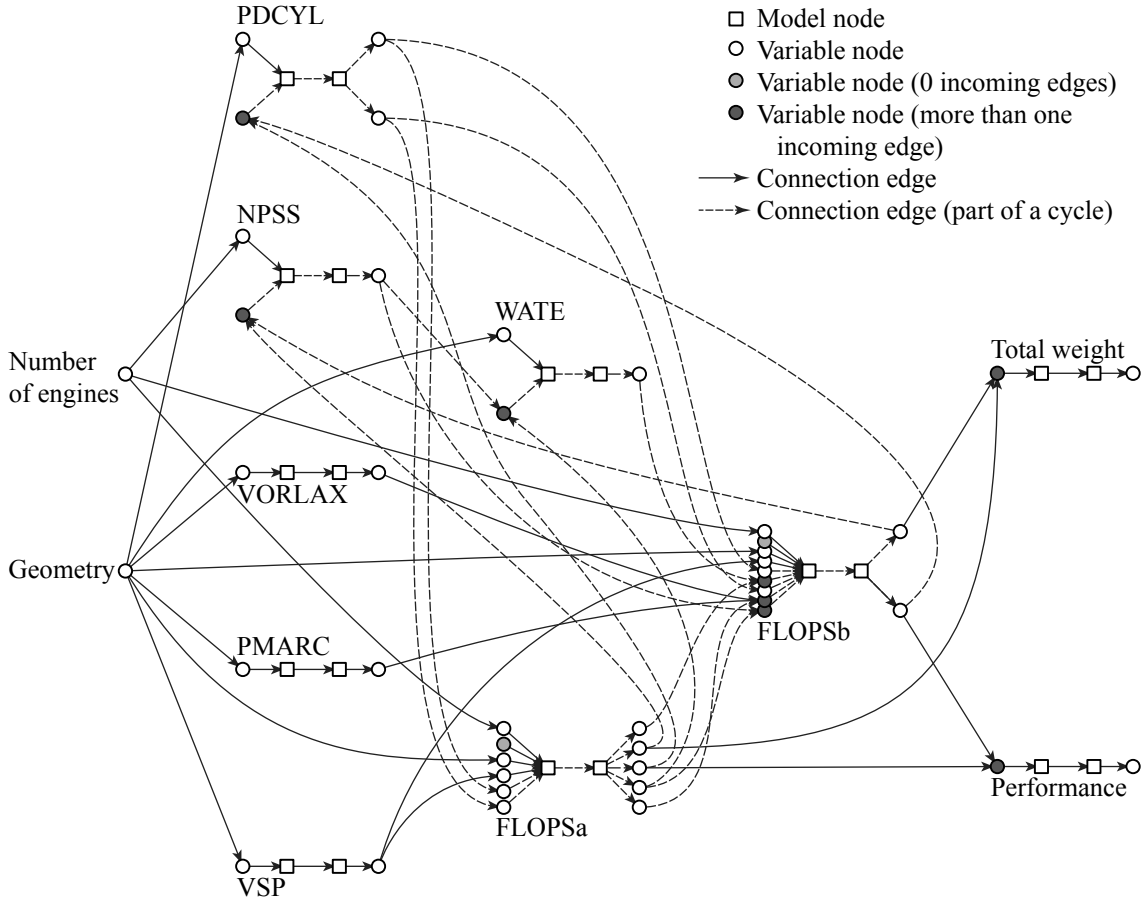


Fig. 16: The updated MCG with a new input.

ple, the number of engines was not originally included as an input to demonstrate how the process can reveal the need to select a variable as an input. Step (D)(b) then reduces the lower and upper indegree limits for the variable node representing the mission definition to zero, implying that these nodes must be specified as design variables (see Table 1). The new MCG is shown in Fig. 16.

Although an FPG may now be obtained, this process has not provided a method to decide which edges to retain when resolving a collision, and these decisions will likely determine which analysis tools are included in the FPG. These decisions are left to the discretion of the designer in the context of the specific implementation. However, the graph-based approach presented in this paper enables standard graph algorithms to be employed to automate these decisions based on considerations of metrics related to the graph or other data related to the analysis. An example is a metric to obtain an FPG with the fewest possible number of cycles. In this example, the FPG with the fewest cycles is shown in Fig. 17, in which the edges belonging to a cycle are

indicated by dashed lines. For this example problem, the cycles were detected using the implementation of Johnson's algorithm [28] in the Python package NetworkX. There are two cycles which arise from each local output from PDCYL being directed into FLOPSa and then back into PDCYL.

Similar alternatives would be to minimize the number of analysis blocks involved in cycles, counting multiplicity, or to minimize the length of the longest cycle (called the *circumference* of the graph). It is beyond the scope of this work to explore efficient methods for finding the FPGs meeting these criteria. However, as discussed by Gabow [29], graph algorithms typically scale well with the size of the graph. This suggests that the computation cost of finding an FPG should be small even for large problems.

Alternatively, it may be desirable to resolve collisions by preferentially choosing analysis tools with favorable properties, such as higher accuracy or minimal run time, whenever possible. One method to implement an FPG in this paradigm is to use a ranking system. Each analysis block is assigned a value by the designer

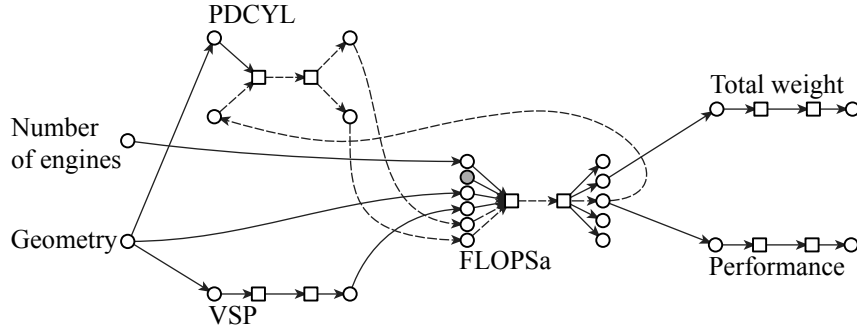


Fig. 17: FPG with the fewest number of cycles.

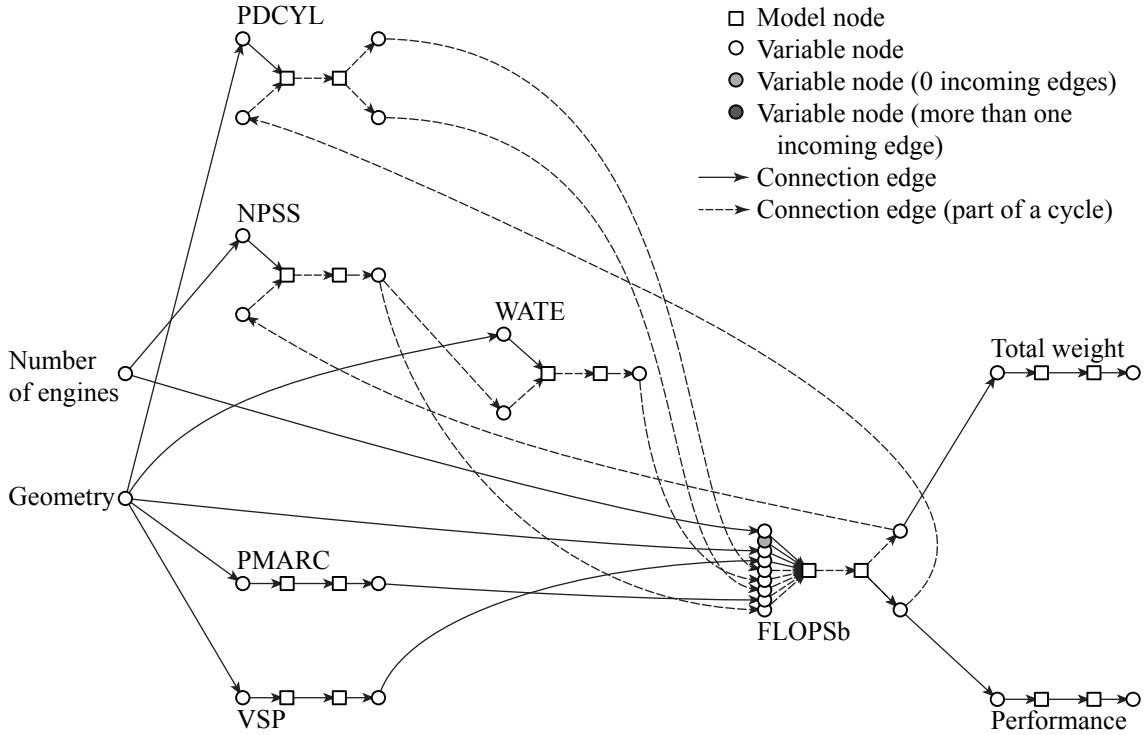


Fig. 18: FPG obtained using a ranking system.

describing how desirable it is for this block to be present in the FPG. The connection edges directed out of each analysis block are then assigned a weight equal to the value assigned to the analysis block. Finally, each collision is resolved by selecting the edges with the highest weights. For the current example problem, consider the rankings for each analysis code given in Table 4. The resulting FPG has four cycles and is shown in Fig. 18.

Finally, consider a case in which the induced drag input into FLOPSb is a multi-fidelity input, meaning that multiple analysis codes calculate the same variable. This multi-fidelity formulation is implemented by setting the upper indegree limit for this node as two and then repeating the (automated) process. In this case,

Table 4: Example ranking of importance

analysis code	rank
VSP	5
PDCYL	5
NPSS	4
PMARC	4
FLOPSb	4
VORLAX	3
WATE	3
FLOPSa	2

both VORLAX and PMARC are retained, resulting in an FPG that omits only FLOPSa.

Conclusions

In this paper, we have presented an approach for describing MDAO problems with constructs and syntax from graph theory. Our graph description shares similarities to other approaches such as REMS, Ψ , FDT, DSM, and XDMS, but it provides new constructs tailored to algorithmic analysis and manipulation. The proposed syntax has applications in early phases of MDAO problem formulation, especially for problems with large numbers of variables and analyses. In particular, we introduce the concepts of the Maximally Connected Graph (MCG) and the Fundamental Problem Graph (FPG).

The MCG addresses the question, "Given a set of analysis tools, what are all of the variable interconnections between them that could be established?" The MCG provides a structured formalism to identify *holes* and *collisions* in interconnections between the set of analysis tools. In order to achieve a valid problem formulation, all of the holes and collisions must be resolved. We present an algorithm to perform this resolution which guarantees that you will find an FPG if one exists. In some cases this algorithm still relies on some input from the designers to make decisions. One benefit of a graph theoretic approach is the standard algorithms which can be used to inform the user's decisions, such as cycle detection, minimum spanning trees, and shortest path algorithms.

The FPG is a graph that describes a data connection structure corresponding to an MDAO problem formulation free of collisions and holes. An FPG is the result of user choices to fill holes and resolve collisions in the initial MCG. Typically, many different FPGs could be attained from a given MCG, depending on the user choices. The number of possible FPGs that can be attained by selecting different design variables or introducing additional analysis tools to fill holes and/or resolve collisions can be viewed as a measure of the freedom available to the user in implementing the available analysis tools to formulate valid MDAO problems. In Sec. 6, we provide an example application of formulating multiple FPGs from an MCG for a commercial aircraft design problem.

For simple problems with few analysis tools and variables, the formulation of a valid problem description is straightforward. However, MDAO problems continue to grow in scale and complexity. As the numbers of analysis tools and variables have increased, it has become increasingly challenging and time consuming for engineering teams to determine how the multiple analysis tools can be interconnected to produce valid problem formulations, to know when other tools must be intro-

duced, and to determine the number of free variables in the problem that can or should be varied by the designer or an optimizer. The graph formalism presented in this paper is intended to offer value in this context of increasing problem complexity by providing a formal approach to programatically identify and resolve missing and redundant data in order to create valid MDAO problem formulations.

References

1. Cramer, E. J., Dennis, Jr., J. E., Frank, P. D., Lewis, R. M., and Shubin, G. R., "Problem Formulation for Multidisciplinary Optimization," *SIAM Journal on Optimization*, Vol. 4, No. 4, November 1994, pp. 754–776.
2. Sobieszczanski-Sobieski, J. and Haftka, R. T., "Multidisciplinary Aerospace Design Optimization: Survey of Recent Developments," *Structural Optimization*, Vol. 14, 1998, pp. 1–23.
3. de Weck, O., Agte, J., Sobieszczanski-Sobieski, J., Arendsen, P., Morris, A., and Spieck, M., "State-of-the-art and future trends in multidisciplinary design optimization," *48th AIAA/ASME/ASCE/AHS/ASC Structures, Structural Dynamics, and Materials Conference, 23 - 26 April 2007, Honolulu, Hawaii*, 2007.
4. Dean, S. R. H., Doherty, J. J., and Wallace, T. R., "MDO-Based Concept Modelling and the Impact of Fuel Systems on Wing Design," *47th AIAA Aerospace Sciences Meeting Including The New Horizons Forum and Aerospace Exposition Orlando, Florida, 5 - 8 January*, 2009.
5. Gavel, H., Ölvander, J., and Krus, P., "Optimal Conceptual Design of Aircraft Fuel Transfer Systems," *Journal of Aircraft*, Vol. 43, No. 5, 2006, pp. 1334–1340.
6. Antoine, N. E. and Kroo, I. M., "Aircraft Optimization for Minimal Environmental Impact," *Journal of Aircraft*, Vol. 41, No. 4, 2004, pp. 790–797.
7. Rallabhandi, S. K. and Mavris, D. N., "Aircraft Geometry Design and Optimization for Sonic Boom Reduction," *Journal of Aircraft*, Vol. 44, No. 1, 2007, pp. 35–47.
8. Kirby, M. R. and Mavris, D. N., "The Environmental Design Space," *26th International Congress of the Aeronautical Sciences*, 2008.
9. Gray, J., Moore, K. T., Hearn, T. A., and Naylor, B. A., "A Standard Platform for Testing and Comparison of MDAO Architectures," *8th AIAA Multidisciplinary Design Optimization Specialist Conference (MDO)*, Honolulu, Hawaii, 2012, pp. 1–26.
10. Sellar, R., Batill, S., and Renaud, J., "Response surface based, concurrent subspace optimization for multidisciplinary system design," *34th AIAA Aerospace Sciences Meeting and Exhibit*, Citeseer, Reno, NV, Jan. 1996.
11. Tedford, N. P. and Martins, J. R. R. a., "Benchmarking multidisciplinary design optimization algorithms," *Optimization and Engineering*, Vol. 11, No. 1, March 2009, pp. 159–183.
12. Gray, J., Moore, K. T., Hearn, T. A., and Naylor, B. A., "A Standard Platform for Testing and Comparison of MDAO Architectures," *AIAA Journal*, Vol. in press, 2013.
13. Steward, D. V., "The Design Structure System: A Method for Managing the Design of Complex Systems," *IEEE Transactions on Engineering Management*, Vol. EM-28, No. 3, 1981, pp. 71–74.
14. Rogers, J., McCulley, C., and Bloebaum, C., *Integrating a genetic algorithm into a knowledge-based system for ordering*

- complex design processes*, NASA Technical Memorandum, Hampton Virginia, 1996.
15. Rogers, J., "DeMAID/GA-an enhanced design managers aid for intelligent decomposition (genetic algorithms)," *the Proceedings of the 6th AIAA/USAF/NASA/ISSMO Symposium on Multidisciplinary Analysis and Optimization*, AIAA-96-4157-CP, 1996, pp. 1497–1504.
 16. Wagner, T. C. and Papalambros, P. Y., "A general framework for decomposition analysis in optimal design," *Advances in Design Automation*, Vol. 2, 1993, pp. 315–325.
 17. Michelena, N. F. and Papalambros, P. Y., "A Hypergraph Framework for Optimal Model-Based Decomposition of Design Problems," *Mechanical Engineering*, Vol. 8, No. 2, 1997, pp. 173–196.
 18. Allison, J., *Optimal partitioning and coordination decisions in decomposition-based design optimization*, Ph.D. thesis, University of Michigan, 2008.
 19. Alexandrov, N. and Lewis, R., "Reconfigurability in MDO Problem Synthesis, Part 1 and Part 2," Tech. rep., Papers AIAA-2004-4307 and AIAA-2004-4308, 2004.
 20. Lambe, A. B. and Martins, J. R. R. A., "Extensions to the Design Structure Matrix for the Description of Multidisciplinary Design, Analysis, and Optimization Processes," *Structural and Multidisciplinary Optimization*, 2012.
 21. Martins, J. R. R. A. and Lambe, A. B., "Multidisciplinary Design Optimization: Survey of Architectures," *AIAA Journal*, 2012, pp. 1–46.
 22. Lu, Z. and Martins, J., "Graph Partitioning-Based Coordination Methods for Large-Scale Multidisciplinary Design Optimization Problems," *ISSMO Multidisciplinary Analysis Optimization Conference*, No. September, Indianapolis, Indiana, 2012, pp. 1–13.
 23. Diestel, R., *Graph Theory*, Springer, 2010.
 24. Smith, D., Eggen, M., and Andre, R. S., *A Transition to Advanced Mathematics*, Brooks/Cole Pub Co, 2006.
 25. March, A. and Willcox, K., "Provably Convergent Multifidelity Optimization Algorithm Not Requiring High-Fidelity Derivatives," *AIAA journal*, Vol. 50, No. 5, 2012, pp. 1079–1089.
 26. Alexandrov, N. M., Lewis, R. M., Gumbert, C. R., Green, L. L., and Newman, P. A., "Approximation and model management in aerodynamic optimization with variable-fidelity models," *Journal of Aircraft*, Vol. 38, No. 6, 2001, pp. 1093–1101.
 27. Huang, D., Allen, T. T., Notz, W. I., and Miller, R. A., "Sequential kriging optimization using multiple-fidelity evaluations," *Structural and Multidisciplinary Optimization*, Vol. 32, No. 5, 2006, pp. 369–382.
 28. Johnson, D. B., "Finding all the elementary circuits of a directed graph," *SIAM Journal on Computing*, Vol. 4, No. 1, March 1975, pp. 77–84.
 29. Gabow, H. N., "Scaling algorithms for network problems," *Journal of Computer and System Sciences*, Vol. 31, No. 2, 1985, pp. 148–168.