# **Summary | Statics**

## Introduction

# **Centroid / Centre of area**

The point where the area of a figure is assumed to be concentrated.

Located on the axes of symmetry.

### First moment of area

Measure of spatial distribution of a shape in relation to an axis.

About x-axis 
$$=\int_A y \, \mathrm{d}A = A ar{x}$$

About y-axis 
$$=\int_A x \, \mathrm{d} A = A ar{y}$$

Here:

- $ar{m{x}}$  Centroid's  $m{x}$  coordinate
- $ar{m{y}}$  Centroid's  $m{y}$  coordinate
- $oldsymbol{A}$  Total area

About an axis of symmetry, first moment of area is  $\boldsymbol{0}$ .

# Second moment of area

About x-axis 
$$=I_{xx}=I_x=\int_A y^2 \; \mathrm{d}A$$

About y-axis 
$$=I_{yy}=I_y=\int_A x^2 \; \mathrm{d}A$$

Always positive.

# The product of moment of area about x,y axes

$$I_{xy} = \int_A xy \ \mathrm{d}A$$

# The polar moment of area about z axis

$$I_{zz}=J_0=\int_A r^2 \;\mathrm{d}A=I_{xx}+I_{yy}$$

# **Radius of gyration**

$$ext{About x-axis} = r_x^2 = rac{I_{xx}}{A}$$

$$\text{About y-axis} = r_y^2 = \frac{I_{yy}}{A}$$

$$ext{About z-axis} = r_z^2 = rac{I_{zz}}{A}$$

# **Derived Formulas for Common Shapes**

| Shape                      | Description   |                   |
|----------------------------|---|-------------------|
| Rectangle or Parallelogram | Base $m{b}$ . Height $m{h}$ . About centroidal axis parallel to base. | $rac{bh^3}{12}$  |
| Triangle                   | Base $m{b}$ . Height $m{h}$ .<br>About base.                          | $rac{bh^3}{12}$  |
| Triangle                   | Base $m{b}$ . Height $m{h}$ . About centroidal axis parallel to base. | $\frac{bh^3}{36}$ |

| Shape  | Description                                      | $I_{xx}$            |
|--------|--|---------------------|
| Circle | Diameter $oldsymbol{d}$ . About centroidal axis. | $rac{\pi d^4}{64}$ |

# **Parallel Axis Theorem**

$$I_x = I_{x_1} + Aar{y}^2$$

$$I_y = I_{y_1} + Aar{x}^2$$

$$I_{xy}=I_{x_1y_1}+Aar{x}ar{y}$$

#### Here

- On LHS, the moments of area are about some  $\,x\,$  ,  $\,y\,$  axes.
- On RHS, the moments of area are about centroidal axes  $\,x_1\,$  ,  $\,y_1\,$  parallel to x, y.
- $ar{x}$  is the distance between x and  $x_2$  axes.
- $ar{y}$  is the distance between  $\,y\,$  and  $\,y_1\,$  axes.

### (i) Note

 $I_x$  is at a minimum when the axis is through the centroid. Same for  $I_y$ .

# **Perpendicular Axis Theorem**

$$I_{zz} = I_{xx} + I_{yy} = I_{mm} + I_{nn}$$

x, y, z are a set of axes. m, n, z are another set of axes.

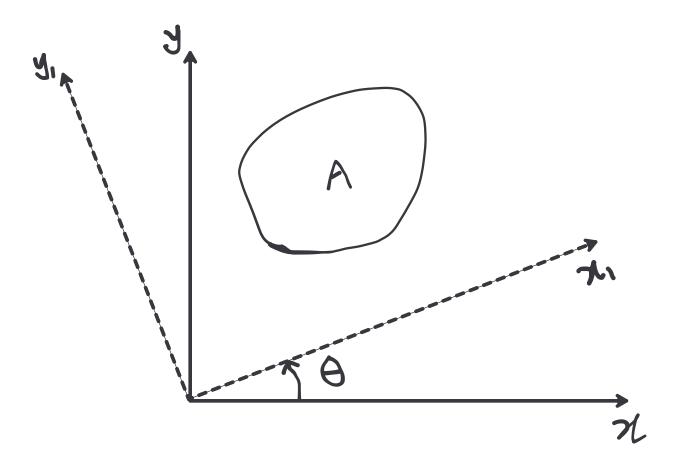
If  $I_{xx}$  is at maximum,  $I_{yy}$  will be at minimum.

# **Transformation Law**

The 2 sets of axes must share the origin.

### (i) Note

Don't have to memorize this. Will be given on exams, if required.



$$I_{x_1x_1} = rac{I_{xx}+I_{yy}}{2} + \left(rac{I_{xx}-I_{yy}}{2}
ight)\cos2 heta - I_{xy}\sin2 heta$$

$$I_{y_1y_1} = rac{I_{xx}+I_{yy}}{2} - \left(rac{I_{xx}-I_{yy}}{2}
ight)\cos2 heta + I_{xy}\sin2 heta$$

$$I_{x_1y_1} = \left(rac{I_{xx}-I_{yy}}{2}
ight)\sin 2 heta + I_{xy}\cos 2 heta$$

# **Principal Axes**

The product of moment of area is  $\mathbf{0}$  about principal axes.

$$I_{xy}=0$$

There will be 2 directions of principal axes which are perpendicular to each other.

# Principal second moments of area

Second moments about the principal axes.

About principal axes second moments of area will be at minimum and maximum.

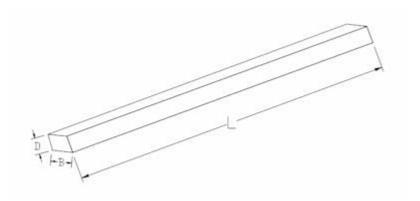
# **Centroidal principal axes**

Principal axes through the centroid.

(i) Note

Any axis of symmetry is a centroidal principal axis

## **Beams**



- long ( L>>B,D )
- · axis of the beam is straight
- · constant cross-section throughout its length

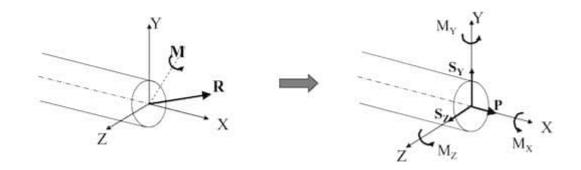
# Classified by supporting conditions

First 3 are the mandatory ones in s1.

u.d.l means uniformly distributed load.

| Туре                      | Image  |
|---------------------------|--|
| Simply supported beam     | $W_1$ $W_2$  |
| Cantilevered beam         | u.d.l. W   |
| Overhanging beam          | $\frac{\mathbf{w}_1}{\mathbf{w}_2}$                  |
| Propped cantilevered beam | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| Continuous beam           | $W_1$ $W_2$ $u.d.l.$                                 |
| Fixed beam                | J mm ↓   |

### At a section



- $oldsymbol{\cdot}$  P Normal force / Axial force
- $S_y, S_y$  Shear forces along y and z axis
- ullet  $M_x$  Twisting moment / Torque
- $M_y, M_z$  Bending moments about  $\, y \,$  and  $\, z \,$  axis

## **Degress of freedom**

A plane member have 3 degrees of freedom. Any of the 3 can be restrained.

- Displacement in  $oldsymbol{x}$  -direction
- Displacement in  $oldsymbol{y}$  -direction
- Rotation about z-direction

#### SFD & BMD

## Sign convention

- · Bending moment
  - Hogging (curves upwards in the middle) is (+) ve
  - Sagging (curves downwards in the middle) is (-) ve
- Shear force
  - Clockwise shear is (+) ve.
  - Counterclockwise shear is (-) ve.

### **Pure bending**

A member is in pure bending when shear force is  $\boldsymbol{0}$  and bending moment is a constant.

#### **Point of Contraflexure**

The point about which bending moment is 0.

## Distributed load, shear force & bending moment

Suppose a beam is under a distributed load of w=f(x) per unit length.

$$\frac{\mathrm{d}S}{\mathrm{d}x} = -w$$

$$rac{\mathrm{d}M}{\mathrm{d}x} = -S \ \wedge \ rac{\mathrm{d}^2M}{\mathrm{d}x^2} = w$$

### **Deflection of a beam**

Suppose a simply supported beam is applied a load of  $oldsymbol{W}$  at mid-span.

$$S_{
m max} = rac{WL}{4I} ~\wedge ~D_{
m max} = rac{WL^3}{48EI}$$

Here:

- $S_{
  m max}$  Maximum stress
- $D_{
  m max}$  Deflection
- $oldsymbol{\cdot}$   $oldsymbol{W}$  Load
- $oldsymbol{L}$  Span length
- $oldsymbol{\cdot}$   $oldsymbol{E}$  Young's modulus
- $oldsymbol{\cdot}$  I Second moment of cross-sectional area

# **Principle of Superposition**

A beam with multiple loads can be split into multiple systems each with a single load. Reason for doing so is the ease of calculations.

Values will be the sum of each system's corresponding value.

# **Structural Elements**

### 3 types:

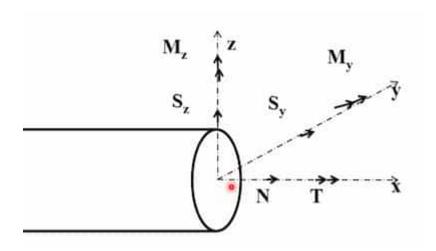
- Bars (1D)
- Plates and Shells (2D)
- Blocks (3D)

Bar elements are only focused for s1.

# **Pin Joint**

Doesn't exert a moment. Free rotations are allowed. When only pin joints are used, bars will have only axial forces.

#### **Bars**



#### Here

- $\it N$  Axial force
- $S_x, S_y$  Shear force
- $M_x$

## **Types of bars**

## **Axially loaded**

Generally in trusses, **pin joints** are considered.

- Predominant tension Ties
- Predominant compression Struts

#### **Flexural**

• Predominant bending - beams

#### **Torsional**

• Predominant torque - shafts

### **Trusses**

Also known as Ties-Struts model.

### **Definition**

An assembly of members used to span long distances. Idealized as

- Connected by **frictionless** pin joints at their ends
- Developing axial forces

# **Types**

2 types:

- Plane truss (2D)
- Space truss (3D)

A truss requires 3 external reactions for equilibrium.

Predominant force is axial force.

# **Advantages of truss**

- High span
- Material efficiency

## **Triangulation**

To create a truss:

- Start with a triangle (3 bars and 3 joints)
- Add 2 more bars and 1 joint repeatedly

This type of truss is a **simple truss**.

## Simple (Closed) Truss

When a truss is only made of bars and joints.

### **Open Truss**

When a truss is pinned directly to a foundation. It has 1 member & 2 free joints less than a closed truss.

## Stability of trusses

When a truss is:

• unstable: it's called a mechanism

stable: it's called a structure

#### Stable truss

When the shape cannot be altered, the structure is **internally stable**.

#### Stable & determinate (simply stiff)

**Determinate** means internal forces can be determined by laws of statics alone.

#### Stable & indeterminate

**Indeterminate** means laws of statics alone are not sufficient to determine forces; relative stiffness of members will influence the solution (Indeterminate trusses are safer).

#### **Unstable truss**

When the shape can be altered, the truss is called a mechanism.

# Necessary condition for being simply stiff

(i) Note

These are necessary (but not sufficient) conditions.

#### Here:

- m Number of members (bars)
- $m{j}$  Number of joints

### For a 2D simple (closed) truss

- $oldsymbol{\cdot} m < 2j-3$  truss is unstable
- $oldsymbol{\cdot} \quad m=2j-3$  truss is determinate if stable
- m>2j-3 truss is indeterminate if stable

## For a 2D open truss

- $oldsymbol{\cdot} m < 2j$  truss is unstable
- m=2j truss is determinate if stable
- m>2j truss is indeterminate if stable

# For a 3D simple (closed) truss

$$m = 3j - 6$$

# For a 3D open truss

$$m=3j$$

# **Analysis of Trusses**

Deviations from the ideal in real trusses.

- Loads are not applied only at joints; hence there is bending in members
- Joints are not perfectly pinned, so moments can be developed at joints

## **Method of Joints**

### **Principle**

Since the truss is in equilibrium, each pin joint must also be in equilibrium.



#### (i) Note

2 equilibrium equations can be written at each joint - vertical & horizontal.

#### Sign convention

Forces acting on each joint is marked. Tensile forces are positive. Compressive forces are negative.

#### Method

- Find external reactions using equilibrium equations for the entire truss.
- Start with a joint with only 2 unknown joint forces.
- Mark the forces (consider all forces are tensile) acting on the joint.
- Find the unknown forces at the selected joint, using 2 equilibrium equations for the joint.
- Go to all other joints in turn and find forces in all the members.

#### **Special cases**

| Case | Description                                    |  |
|------|--|--|
| D B  | $F_{ m AX} = F_{ m XB}, F_{ m DX} = F_{ m XC}$ |  |

| Case      | Description                               |
|-----------|---|
| D $B$ $C$ | $F_{ m P}=F_{ m XB}, F_{ m DX}=F_{ m XC}$ |
| C B       | $F_{ m XB}=0, F_{ m DX}=F_{XC}$           |
| X (d)     | $F_{ m DX} = F_{ m XC}$                   |
| C (e)     | $F_{ m DX} = F_{ m XC} = 0$               |

### **Method of Sections**

### **Principle**

Since the truss is in equilibrium, each of its section must be in stable equilibrium.

#### **Method**

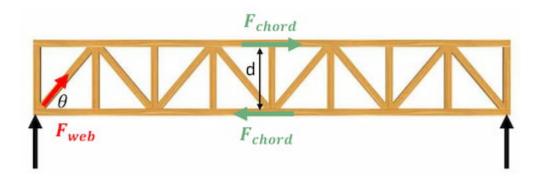
- Decide on which member's internal force must be calculated.
- Cut the truss through 3 or less members including the target member.
- Internal forces in cut members become external forces. Can be represented as tensile forces.
- Use equilibrium equations for RHS or LHS section to find the internal forces.

# **Beam Analogy (Approximate) method**

In this method, the internal forces are found assuming the elongated truss is a beam.

### (i) For a simply supported beam

- Maximum bending moment is at mid-span:  $M_{
  m max}=rac{wL^2}{8}$
- Maximum shear force is at the supports:  $rac{wL}{2}$



#### Here:

- Chord members horizontal members
- Web members diagonal members
- d truss depth

In the truss,

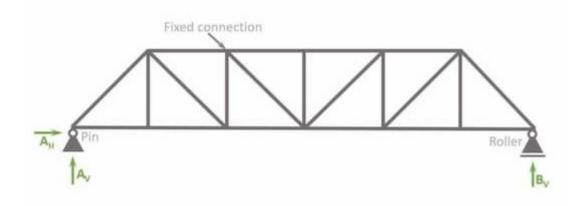
• Bending moment is carried by chord members.

Bending moment = 
$$F_{\mathrm{chord}} \times d$$

• Shear force is carried by vertical component of web member force

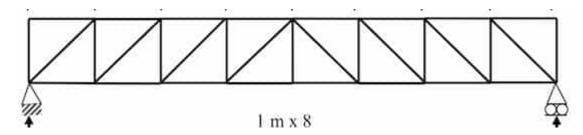
### (i) Pratt & Howe type trusses

**Pratt type truss** is shown below.



Internal force in web members are tensile.

**Howe type truss** is a shown below.



Internal force in web members are compressive.

Usually **Pratt type** is cost-efficient. To make sure a howe type truss is strong enough like pratt type, web members must be shorter and thicker.

# **Indeterminate Trusses**

When a truss is indeterminate, one or more compatibility equations (related to truss deformation) must be used.

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