

Driver assistance system design A

Observers

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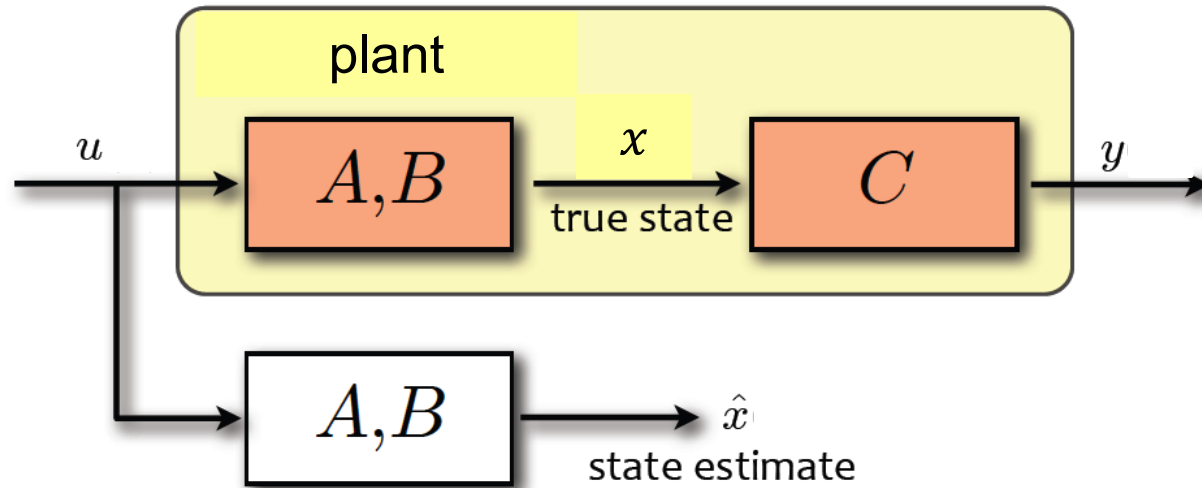
Dip. Elettronica e Telecomunicazioni

Observer design – Introduction

- In most practical situations, **the state** of the system to control (plant P) **cannot be measured**, and thus full state feedback cannot be performed.
- In these situations, the state can be estimated by an **observer**.
- Two possible options:
 - open-loop observer.
 - closed-loop observer.

Observer design – Open-loop observer

- A **copy (or a model) of the plant** is used as the observer.



System A, B : $\dot{x} = Ax + Bu$

Observer A, B : $\dot{\hat{x}} = A\hat{x} + Bu$

C : gain matrix

$D = 0$ (only in the figure)

Observer design – Open-loop observer: Estimation error dynamics

- Plant: $\dot{x} = Ax + Bu$
 $y = Cx + Du$

Observer: $\dot{\hat{x}} = A\hat{x} + Bu$

Estimation error: $e = x - \hat{x}$

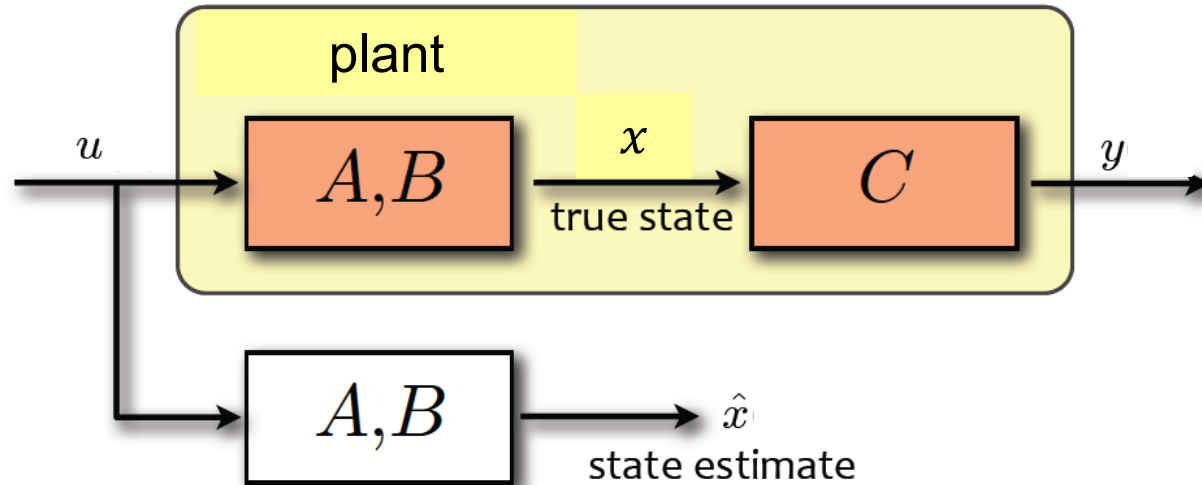
- Dynamics of the estimation error:

$$\dot{e} = Ae$$

← does not depend on u

← can be unstable

Observer design – Open-loop observer



- Drawbacks:
 - divergent estimation error if the plant is unstable;
 - less accurate estimate;
 - no noise attenuation.

Observer design – Closes-loop observer: basic idea

- Plant:

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du.$$

- Observer:

$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - \hat{y})$$

$$\hat{y} = C\hat{x} + Du$$

The idea is to **improve** the estimate \hat{x} by using the measured y . The matrix L has to be suitably designed (as discussed later).

- Combining the above equations:


$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - C\hat{x} - Du)$$

$$\dot{\hat{x}} = (A - LC)\hat{x} + Ly + (B - LD)u.$$

The latter equation is the so-called **Luenberger observer**.

Observer design – Closes-loop observer: Estimation error dynamics

- Plant: $\dot{x} = Ax + Bu$
 $y = Cx + Du$

Observer: $\dot{\hat{x}} = (A - LC)\hat{x} + Ly + (B - LD)u$  Luenberger observer

Estimation error: $e = x - \hat{x}$

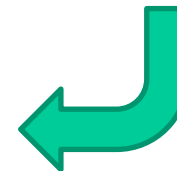
- Dynamics of the estimation error:

$$\dot{e} = (A - LC)e$$

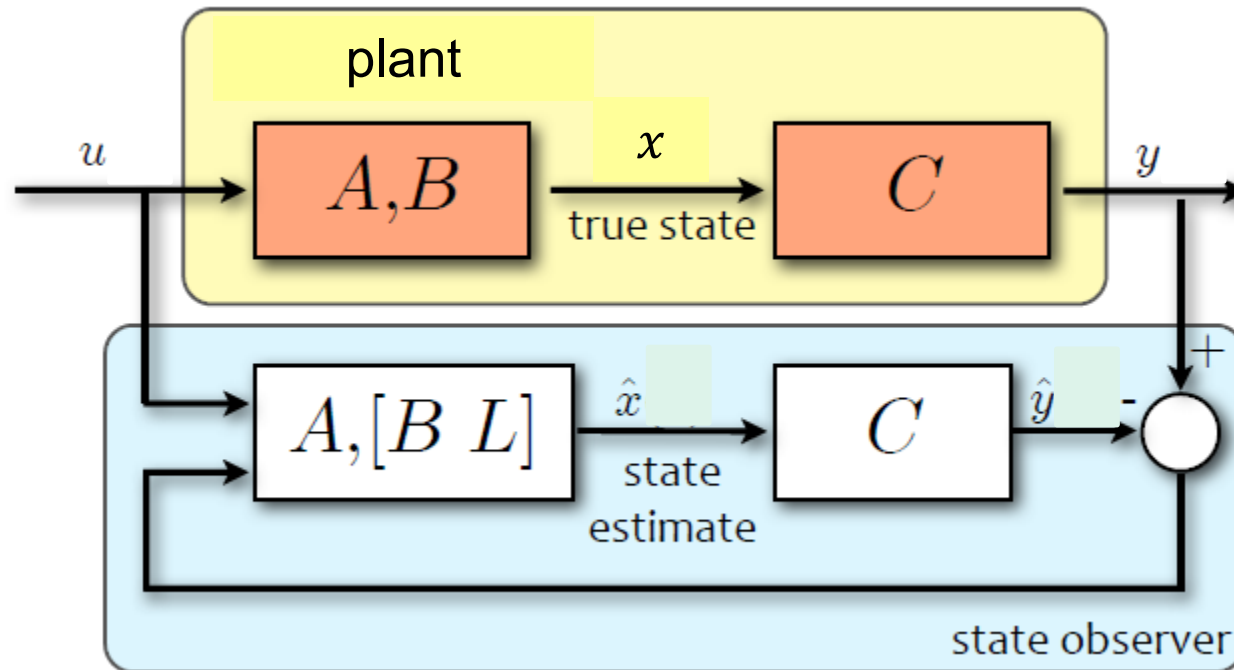
← does not depend on u

← L is chosen to stabilize the error dynamics

$$\lim_{t \rightarrow \infty} \hat{x}(t) = x(t)$$

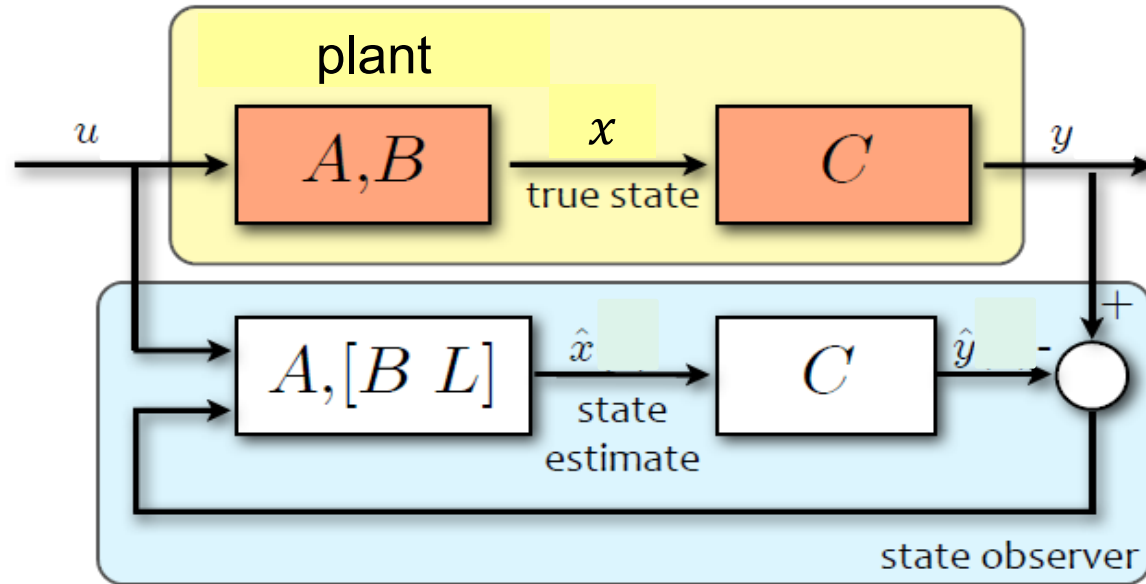


Observer design – Closed-loop observer

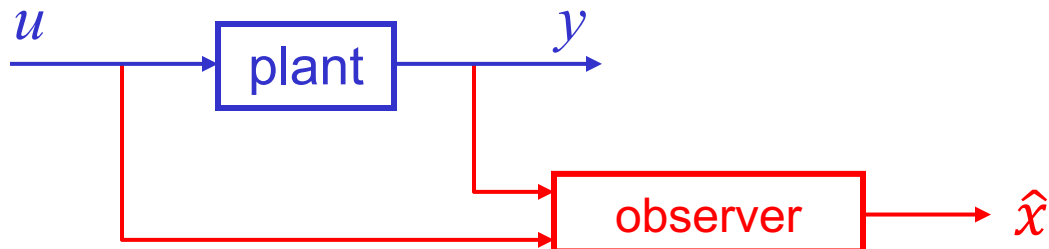


- The estimation is **corrected** at each time t by means of a **feedback from the estimation error**.

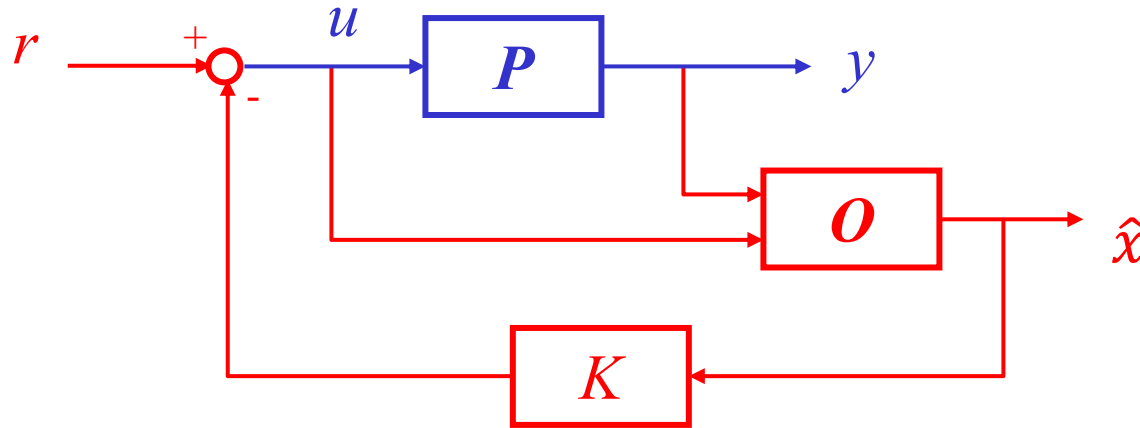
Observer design – Closed-loop observer



- A closed-loop **observer** is a dynamic system with
 - input: (u, y)
 - output: an **estimate** \hat{x} of the system state



Observer design – Feedback control from the estimated state



- The eigenvalues of the observer O (of $A-LC$) should be stable and placed in such a way that $\text{Re}[\text{eig}(A-LC)] \ll \text{Re}[\text{eig}(A-BK)]$,
 - with **not too large (in absolute value) real part**, in order to avoid amplification of high-frequency noises and numerical problems.
- **Matlab:** $L = \text{acker}(A', C', \text{Po_des})'$; (**place**)
 Po_des = vector with the **desired observer eigenvalues**.

- The eigenvalues of $A-LC$ can be arbitrarily placed **if and only if** (A, C) is **completely observable**.

Observer design – Separation principle

Theorem (separation principle). The eigenvalues of the closed-loop system are $\text{eig}(A - BK) \cup \text{eig}(A - LC)$.

Proof. Consider the closed-loop system with $r = 0$.

The state of the closed-loop system is given by $\begin{bmatrix} x \\ \hat{x} \end{bmatrix}$ or, equivalently, by $\begin{bmatrix} x \\ e \end{bmatrix} = \begin{bmatrix} x \\ x - \hat{x} \end{bmatrix}$.

First, we have that $\dot{x} = Ax + Bu$, $u = -K\hat{x}$.

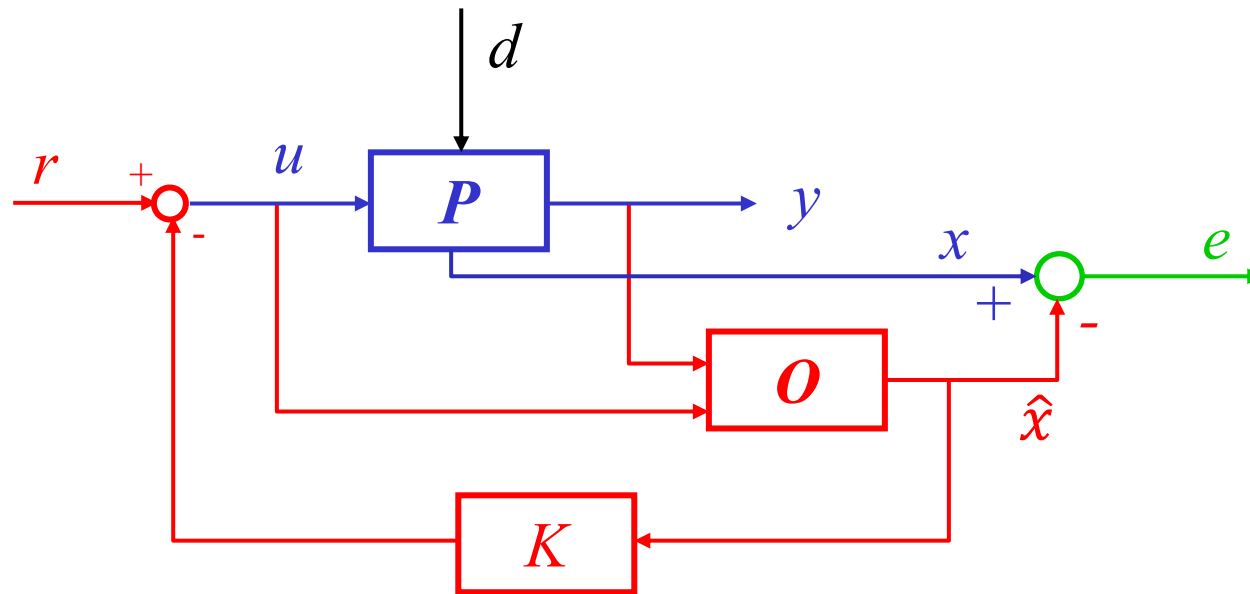
Then, $\dot{x} = Ax - BK\hat{x} = Ax - BK(x - e) = (A - BK)x + BKe$.

Second, we have that $\dot{\hat{x}} = (A - LC)\hat{x} + Ly + Bu$, $y = Cx$.

Then, $\dot{e} = (A - LC)e$.

It follows that $\begin{bmatrix} \dot{x} \\ \dot{e} \end{bmatrix} = \begin{bmatrix} A - BK & BK \\ 0 & A - LC \end{bmatrix} \begin{bmatrix} x \\ e \end{bmatrix}$. ■

Observer design – Estimation error dynamics



- In the **presence of noise**:

$$\dot{e} = (A - LC)e + w$$

where w accounts for the disturbance d .

If $A-LC$ is asymptotically stable and the disturbance is bounded, then **$x - \hat{x}$ is bounded**.

Observer design– Kalman-Bucy filter

- Plant: $\dot{x} = Ax + Bu + B_d d_a$
 $y = Cx + d_y$

$$d = \begin{bmatrix} d_a \\ d_y \end{bmatrix}$$

- Steady-state **Kalman-Bucy filter**:

$$\dot{\hat{x}}(t) = (A - LC)\hat{x}(t) + Ly(t) + Bu(t)$$

- The KB filter is a particular case of Luenberger observer, where L is designed to obtain an **optimal filter**:
 - the KB filter is optimal in the sense that it **minimizes the estimation error variance** for white Gaussian disturbances.
- Problem: the KB filter may not be fast enough when the estimated state is used for feedback control → **robustness problems**.

Observer design– Kalman-Bucy filter

- Plant: $\dot{x} = Ax + Bu + B_d d_a$
 $y = Cx + d_y$ $d = \begin{bmatrix} d_a \\ d_y \end{bmatrix}$

- Steady-state **Kalman-Bucy filter**:

$$\dot{\hat{x}}(t) = (A - LC)\hat{x}(t) + Ly(t) + Bu(t) \quad \leftarrow \text{KB observer}$$

$$L = AP_d C^T R_d^{-1}$$

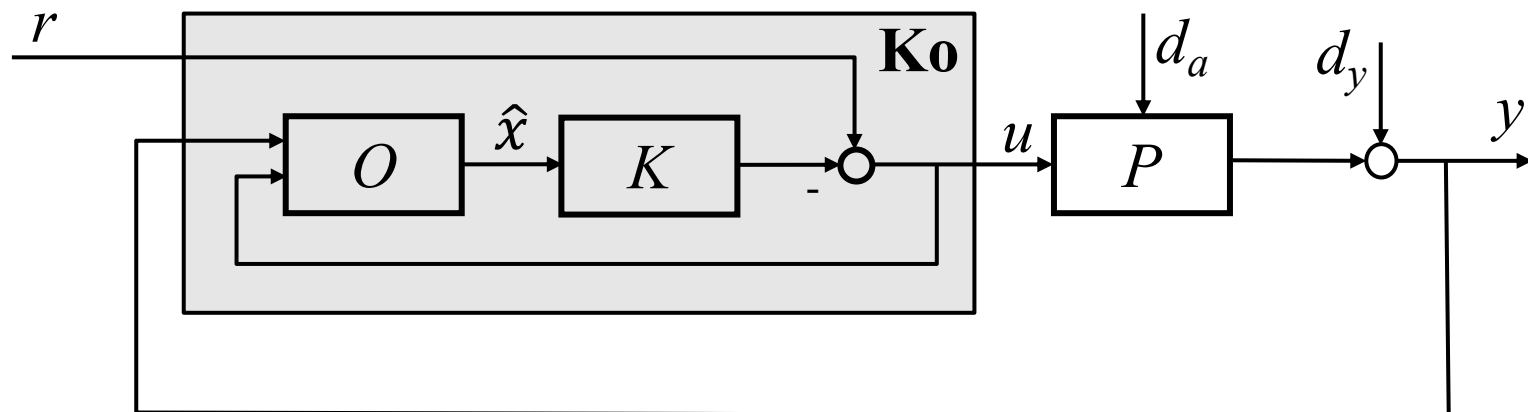
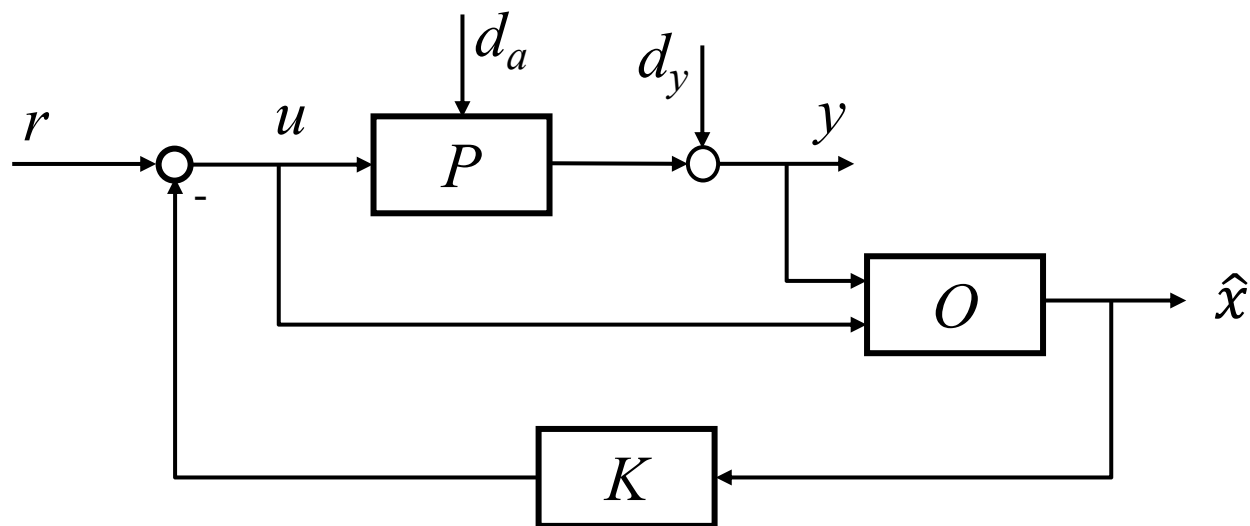
$$AP_d + P_d A^T + Q_d - P_d C^T R_d^{-1} C P_d = 0 \quad \leftarrow \text{Algebraic Riccati Equation}$$

Q_d and R_d are the covariance matrices of d_a and d_y .

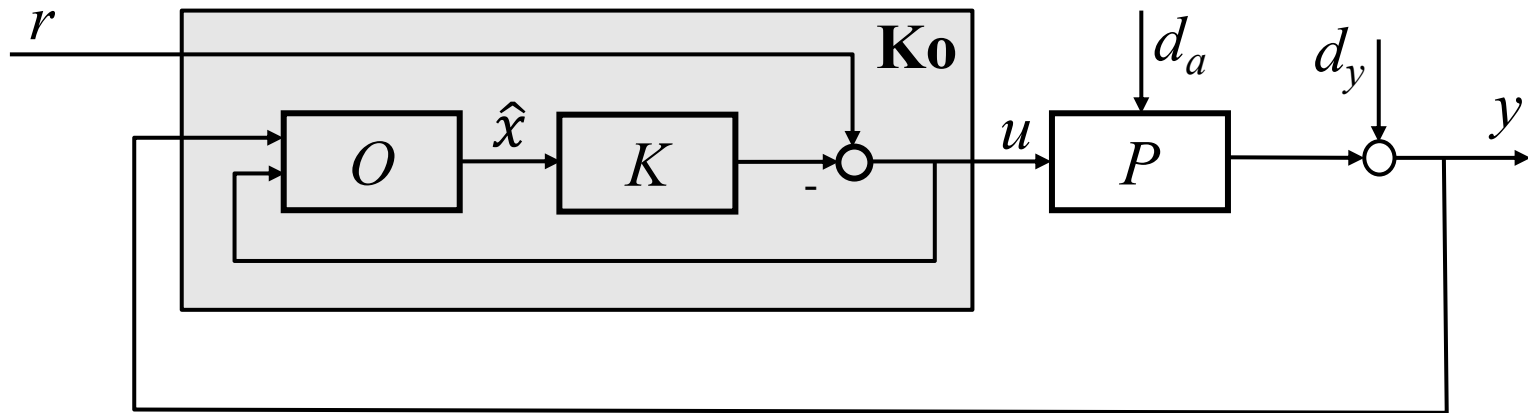
- The Kalman-Bucy filter can be designed using **Matlab**:

```
P = ss(A, [B Bd], C, [D zeros(ny,1)]);  
[O,L] = kalman(P,Qd,Rd);
```

Observer design – Overall controller



Observer design – Overall controller



$$\mathbf{K_o} : \begin{cases} \dot{\hat{x}}(t) = (A - BK - LC) \hat{x}(t) + Br(t) + Ly(t) \\ u(t) = -K\hat{x}(t) + r(t) \end{cases}$$

- The overall controller is defined in **Matlab** as

```
Ak = A-B*K-L*C;  
Bk = [B L];  
Ck = -K;  
Dk = [1 0];  
Ko = ss(Ak,Bk,Ck,Dk);
```