

Evaluation and Quantification of Semi-Empirical Compressor Model Predictive Capabilities under Modulation and Extrapolation Scenarios

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Abstract

Testing and evaluation of select semi-empirical compressor models is carried out to quantify performance in modulation and extrapolation scenarios. Three representative models from literature are benchmarked against an artificial neural network (ANN) model and the industry standard AHRI model. A methodology for quantifying model performance, compared against experimental data, in extrapolation and modulation scenarios is developed. The different formulations are compared against high-fidelity performance data taken from either a hot-gas bypass load stand or a compressor calorimeter. Scroll, screw, reciprocating, and spool compressor technologies and four different refrigerants were used in the evaluation. In total, 327 data points were used during model testing. The mean absolute percentage error (MAPE) is calculated for each scenario and used to determine model performance against one another. Given a model predicts the compressor technology, the semi-empirical models yield MAPE's less than 5% for mass flow rate and power in modulation scenarios while performing at or below 8% MAPE in envelope extrapolation scenarios. They capture superheat extrapolation to below 6% MAPE for mass flow rate and power with the exception of one model performing at 18% MAPE in power prediction for one data set. The empirical formulations do not predict modulation behavior and showed varying performance at the extrapolation scenarios. Limitations with respect to model training data and overall performance are described. A model developed by Winandy et. al is identified as a starting point for a new semi-empirical model that can capture multiple compressor technologies while exhibiting good modulation and extrapolation capabilities.

Keywords: Semi-empirical compressor modeling, extrapolation, modulation, model evaluation

1. Introduction

In 2020 the residential sector used approximately 1.46 trillion kWh of electricity accounting for 39% of total retail sales in the United States. Heating ventilation, air conditioning, and refrigeration (HVAC&R) equipment consumed the largest percentage (37%) of energy within the sector, U.S. Energy Information Administration (2021). The compressor operating in a vapor compression cycle is the largest energy consumer in HVAC&R systems. Today compressor manufactures are challenged by regulatory changes aimed at mitigating climate change and global warming, while still meeting system efficiency requirements. Modeling compressor performance is a vital part in estimating overall system behavior.

Compressor models exist on a spectrum of black box (statistical correlations) to white box (distributed models). Black box models require little information about the machine itself, while

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white box models need detailed input information sometimes only known by the manufacturer.

Nomenclature

α	Work loss coefficient	[-]	W_{cal}	Polytropic process work rate	[kJ/min]
$a_1 - a_5$	Mass flow coefficients	[-]	W_{in}	Internal compression power	[W]
$B_1 - B_2$	Heat transfer loss coefficients	[-]	W_{loss}	Constant power loss	[W]
$b_1 - b_5$	Power coefficients	[-]	ANN	Artificial Neural Network	
$C_1 - C_{10}$	AHRI coefficients	[-]	C	Clearance factor	[-]
$c_1 - c_3$	Mass flow ratio coefficients	[-]	MAPE	Mean Absolute Percent Error	
$d_1 - d_5$	Power ratio coefficients	[-]	N	Rotational speed	[rev/min]
Q_{cyl}	Cylinder heat transfer	[kJ/min]	n	Polytropic exponent	[-]
T_d	Discharge dew point temp.	[C or F]	RPD	Piston displacement	[m ³ /min]
T_s	Suction dew point temp.	[C or F]	RPM	Revolutions per minute	[rev/min]
V_s	Swept volume	[m ³ /rev]			

Grey box or semi-empirical models aim to hit the middle ground between the two extremes. These models are computationally efficient to run and can be implemented into system simulations. When manufactures test their systems through simulation it is desired that a variety of operating conditions be predicted accurately. Additionally, part load conditions sometimes require the compressor to be operated at a different operational speed than full load conditions. These two situations present unique needs that a model must fulfil, that is, extrapolation and modulation capability. Semi-empirical models may have the potential of meeting these two needs.

This work aims to identify select semi-empirical compressor models from literature, quantify performance at extrapolation and modulation scenarios, and give insights into future model capable of predicting multiple compressor technologies in said scenarios. Li (2012b) gives a semi empirical method to calculate mass flow rate, shaft power, and discharge temperature using four different refrigerants and three types of variable speed compressors: reciprocating, scroll, and rotary. The author presents volumetric and isentropic efficiencies as second order functions of normalized speed, claiming the two may be independent of pressure ratio. For variable speed performance modeling, the method used a reference at a nominal frequencies to calculate volumetric flow rate at other speeds. The RMS error for the model is less than 3% for mass flow rate and compressor power, while the discharge temperature RMS error is 3K. Li (2012a) presented semi empirical model for hermetic scroll and reciprocating compressors with a focus on extrapolation. The model is able to capture mass flow rate, compressor power, and discharge temperature for reciprocating and scroll compressors with all the main parameters modeled within 5% relative error. Compressor data is taken from other literature sources and extrapolation performance is tabulated in the study. Conditions where the saturated suction temperature is 10°C or the saturated discharge temperature is 15°C away from experimental data used for parameter fitting showed good accuracy, 5%. Navarro et al. (2007) presents a phenomenological model for analyzing reciprocating compressors using propane. The compressor efficiency and volumetric efficiency is presented as a set of implicit equations. The model needs 10 empirical parameters, each claimed to have physical interpretation, to be curve

fitted. The computational time for fitting these parameters using a Monte Carlo method is lengthy. This model is supposed to be compatible with variable speed application. It reproduced compressor and volumetric efficiency with an error lower than 3% under a wide range of operating conditions. Corber et al. (2007) use the model presented by Navarro et al. (2007) to predict reciprocating compressor performance with R407C and propane as the refrigerants. The work used parameters fitted with propane to estimate performance with R407C. Results showed deviations of less than 5% for compressor efficiency in all tests except one. A phase change factor was adjusted in the model and results improved. Tello-Oquendo et al. (2019) presents a semi-empirical model based on Navarro et al. (2007)'s work to predict scroll compressor performance. The method is extended to capture vapor injection scroll compressors using R407C, where results obtained were $\pm 5\%$ for compressor and volumetric efficiency. The suction mass flow rate, injection mass flow rate, compressor power and discharge temperature were reported with deviations lower than $\pm 2\%$, $\pm 4\%$, $\pm 5\%$, and $\pm 4\text{K}$, respectively. Mackensen et al. (2002) presented a semi empirical model for reciprocating, screw, and scroll compressors. The mass flow model is based on the concept of a polytropic process and volumetric efficiency. The polytropic process model is also used to predict power consumption. An efficiency factor was found to be necessary for the model and it is based on the operating conditions. The model had a maximum average mean weighted error of 3.7%, 2.3%, and 0.6% for mass flow rate of the reciprocating, scroll, and screw, respectively. The model had problems with the power consumption estimates leading to an average mean weighted error of 8%, 7.6%, 6.4%, and 5% for the screw, scroll, open-drive reciprocating, and semi-hermetic reciprocating, respectively. Jahnig et al. (2000) presented a semi-empirical model for small hermetic reciprocating compressors used in household refrigerators. The model is based on volumetric efficiency and assumes a polytropic compression process. There are five parameters that must be determined by fitting experimental data. The authors find that the model extrapolates within 5% error with condensing and evaporating temperatures that extend measured data by 10°C . Shao et al. (2004) presents a map based modeling approach for variable speed rolling piston compressors. The authors conclude that the ratio of mass flow rate at a constant frequency to that at the basic frequency remain constant at different evaporating and condensing temperatures. This observation is then used to define a mass flow rate ratio which is expressed as a second order function of compressor frequencies. A power ratio is defined similarly. Validation is done by comparing the model to experimental data yielding the maximum error to be 3%, 5%, 8% and the relative error to be 2%, 3%, and 4% for the refrigerant mass flow rate, compressor power, and COP, respectively. Aprea and Renno (2008) presents the empirical method utilized in Shao et al. (2004) to represent the performance of a variable speed reciprocating compressor. Santos et al. (2019) presents a semi empirical compressor model for predicting the performance of a variable capacity crankshaft and a linear compressor for light refrigeration applications. Model validation was carried out where extrapolation and data set sensitivity were verified against experimental data for a single speed, variable speed, and linear variable-displacement reciprocating compressors. For single speed compressors, approximately 97% of the mass flow rate and 93% of the power consumption data presented errors within 10% thresholds. For variable speed compressors, more than 95% of the data points had absolute errors lower than 10% for both mass flow rate and power consumption. Negrão et al. (2011) presents a semi empirical compressor model to be used in transient simulation of a reciprocating compressor for household refrigeration appliances. The model is based on thermodynamic equations fitted to manufacturer data. The volumetric flow rate is assumed to be a linear function of pressure ratio and the power consumption is assumed to be a linear function of the mass flow rate times the isentropic work. The comparison of manufacturer data to the model results showed that 77% and 83% of mass flow rate and compressor power differences were within error bands of $\pm 5\%$. Popovic and Shapiro (1995) propose a compressor performance model with a semi-empirical formulation

utilizing extensive data collected from an air-conditioning installation at a US university. The model is derived for reciprocating compressors and an expressed purpose is to reduce the amount of data required to completely characterize compressor performance using alternate refrigerants. The postulated model needs 8 input values. The mass flow rate and required power are the two parameters characterized by this model. Two compressors, 8 different working fluids, and 122 total data points are used for validation. The model demonstrates 8% relative error in mass flow and 6% relative error in the power requirement for the entire data set. Winandy et al. (2002a) presented a detailed experimental analysis of an open-type reciprocating compressor. Based on the experimental results, a simplified steady state model was proposed. A fictitious isothermal wall is assumed to transfer heat and work throughout the suction to discharge process. Seven parameter are needed to calculate mass flow rate and exhaust temperature: swept volume, clearance factor, two throttling parameters, and three heat transfer coefficients. The model needs two parameters to calculate compressor shaft power and a power coefficients. The relative error on the mass flow rate varies between -6.6% and 6.6%, while the shaft power varies between -7% and 3%. The absolute error on the exhaust temperature was reported as -3 K to 6 K. Winandy et al. (2002b) presented a semi-empirical based on Winandy et al. (2002a) for scroll compressor modeling. Relative error on mass flow rate varied from -3.5% to 2.5%, and the shaft power varied between -2.5% and 3%. The absolute error on the discharge temperature varies between -2.5 and 5 K. Winandy and Lebrun (2002) adapted the model by Winandy et al. (2002b) to characterize a vapor and liquid injected scroll compressor. The authors tested three compressors; one without injection, one with vapor injection, and one with liquid injection. Corrections were made to the model to account for the two additional flow phenomena when injection occurs. Simulation resulted in a mass flow rate relative error of -4.5% to 4% for all tests except 5 runs that were using liquid injection at low flow rates. Relative error for shaft power was -4.5 to 4.5%. The absolute error on discharge temperature varied between -5 to 5 K. Cuevas and Lebrun (2009) studied a variable speed scroll compressor. The semi empirical modeling method was adapted from Winandy et al. (2002a). Parameters for the model are developed at 50Hz, then used to simulate performance at other frequencies. Simulation resulted in average error of -0.5 K for exhaust temperature, +3 g/s for mass flow rate, and -24 W for electrical input power. Cuevas et al. (2010) then utilize a constant speed scroll compressor for experimental analysis at operating conditions extending beyond nominal ranges. The study again uses the model proposed by Winandy et al. (2002a) to simulate the compressor performance with average errors for exahust temperature, mass flow rate, and power consumption of 0.0K, 0.001kg/s, and -0.129kW, respectively. The authors state that adding additional isothermal walls may increase model accuracy. Dardenne et al. (2015) presents a semi empirical model of a variable speed scroll compressor with vapor injection. The authors modify the model presented by Winandy et al. (2002a) and propose 10 parameters needed to calculate mass flow rate, compressor power, injection mass flow rate, and discharge temperature. The method adds ‘virtual compressors’ to the Winandy model. These further break down the compression and injection processes. The model shows decent accuracy since 89% to 98% of the calculated data is within $\pm 5\%$, $\pm 10\%$, and $\pm 5\text{K}$ for mass flow, compressor power, and discharge temperature respectively. Giuffrida (2016) studied an open drive screw compressor by presenting a semi-empirical model based on Winandy et al. (2002b) that uses eight parameters to predict mass flow, shaft power, discharge temperature, volumetric and compressor efficiency, and ambient heat losses. The mass flow rate and shaft power is predicted within an error of 3% and 2.44% respectively. The authors tested the model prediction capability with two other compressors using tuned parameters from an initial compressor run. Results were adequate with mass flow rate and shaft power error, taken as absolute value, always less than 3% and 5%, respectively. James et al. (2016) presents a semi empirical modeling method for an oil flooded scroll compressor with liquid injection. The authors utilize and extend the model presented by Winandy et al. (2002b).

Fourteen parameters need to be identified for the model to calculate mass flow, compressor power, and discharge temperature. Once identified, the model predicts around 90% of the discharge temperature data within $\pm 3\%$. The mass flow rate is predicted within $\pm 3\%$ relative error and the power consumption is within $\pm 2\%$ relative error. Molinaroli et al. (2017) presents a semi empirical model for hermetic rolling piston compressors based on models used by Dardenne et al. (2015); Giuffrida (2016); Li (2012b), Li (2012a); and Winandy et al. (2002a). The method accounts for re-expansion and leakage which is an improvement to the models before mentioned. Data from four different hermetic rolling piston compressors are used in validation. Eight parameters are needed to calculate mass flow rate and compressor power. The results were that 96% of the calculated mass flow rate was within $\pm 5\%$ of data and 97% of the calculated compressor power was within $\pm 5\%$.

2. Model Selection

The literature survey was done to find representative models for evaluation under modulation and extrapolation scenarios. The search focused on semi-empirical formulations exhibiting good accuracy, 5%, a minimum number of inputs, simplified analysis techniques, and low computation costs. The Winandy et al. (2002b) model is found often in the literature surveyed. Its been modified to 3 different compressor technologies; open type reciprocating Winandy et al. (2002a), scroll Winandy et al. (2002b), and hermetic rolling piston Molinaroli et al. (2017). Additionally, its been adapted to vapor and liquid injected and oil flooded scroll compressors (Winandy and Lebrun (2002), James et al. (2016)). The Popovic and Shapiro (1995) model is a legacy model that captures the thermodynamics and some physics present in a positive displacement reciprocating machine. This formulation seems promising and is selected as a candidate for future model development. The Shao et al. (2004) model is a more empirical model chose for evaluation. This model exhibited good accuracy and modulation capabilities therefore it is has been chosen as a candidate for testing.

2.1. Baseline Models

2.1.1. AHRI Model

The AHRI model, coming from AHRI (2020), is a mathematically simple third order curve fit to 10 data points. The mass flow rate and power are fitted separately as a function of evaporating and condensing temperatures. This results in two equations for performance prediction. The method is very accurate with respect to the data it is fitted to. The computational burden is minimal making it a good option for system simulators. It's used extensively in the HVAC&R industry for system level modeling, therefore it is used as a baseline for comparison in the present study.

$$X = C_1 + C_2T_s + C_3T_d + C_4T_s^2 + C_5T_sT_d + C_6T_d^2 + C_7T_s^3 + C_8T_s^2T_d + C_9T_sT_d^2 + C_{10}T_d^3 \quad (1)$$

Where X is the power input or mass flow rate, T_s and T_d are the suction and discharge dewpoint temperatures, respectively, and C_1 - C_{10} are coefficients determined from least squares regression.

2.1.2. Artificial Neural Network Model

The ANN modeling approach provides an additional model for testing performance prediction in extrapolation and modulation scenarios. The ANN formulation is black box in nature and comprises of nodes and layers that take numerical inputs. Each node has a weight and bias that is tuned to performance data via an optimization algorithm. The main tool used for developing these models was the open source Tensorflow package developed by the Google Brain team. The Python programming language, *Python.org* (2020), was used to codify models. A compact architecture

was utilized for simplicity and reduced model training time. Hyperparameters considered during model development include: number of layers, number of nodes, optimizer, activation function, loss function, learning rate, training epochs, and callbacks. The table below shows some main hyperparameters selected for the modeling effort.

Parameter	Value
Machine Learning Package	Tensorflow 2.5.0
No. of Inputs	3
No. of Outputs	2
No. of Layers	1
No. of Nodes	8
Activation Function	Rectified Linear
Optimizer	Adam & Adamax

Table 1: Important parameters used during ANN model development

The loss function was selected as the Mean Squared Error (MSE) for most data sets with the exception of the scroll and screw compressor data sets where the Mean Absolute Percentage Error (MAPE) and Mean Absolute Error (MAE) were used. The necessity of different loss functions stems from the ANN having difficulty training to a certain data set with a chosen hyperparameter selection. Changing the loss function resulted in the optimizer successfully minimizing the loss to an acceptable level.

2.2. Models from Literature

2.2.1. The Shao Model

The Shao Model from Shao et al. (2004) is a black box model that utilizes performance data at different operational frequencies. The equations for mass flow and power are second order functions of evaporation and condensing temperatures. They need six coefficients tuned to data. The variable speed data is used to fit a second order function to mass flow rate and power ratio. These ratios relate the mass flow and power at the base frequency to performance at different frequencies.

Parameter	Equation to be fitted
Mass Flow Rate	$a_1T_c^2 + a_2T_c + a_3T_cT_e + a_4T_e^2 + a_5T_e + a_6$
Mass Flow Rate Ratio	$c_1(f - f^*) + c_2(f - f^*) + c_3$
Power	$b_1T_c^2 + b_2T_c + b_3T_cT_e + b_4T_e^2 + b_5T_e + b_6$
Power Ratio	$d_1(f - f^*) + d_2(f - f^*) + d_3$

Table 2: Formulations that need tuning in the Shao Model formulation.

2.2.2. The Popovic and Shapiro Model

The Popovic and Shapiro model from Popovic and Shapiro (1995) is a semi-empirical compressor model derived to predict reciprocating compressor performance. The model utilizes a volumetric efficiency foundation for mass flow rate. A clearance factor, taken as an unknown, is defined and used

in the aforementioned efficiency calculation. The authors identify the importance of suction pressure drop on mass flow rate and for simplicity set the magnitude of suction and discharge pressure drops equal. The model utilizes a compression power requirement equal to the thermodynamic work rate of a polytropic process. It splits the compressor three control volumes, a compressor control volume, and two internal control volumes, the motor and the cylinder. A heat balance is applied to these volumes and a parameter defined as the heat transfer loss coefficient is related back to the compressor overall efficiency. It is fitted as a function of cylinder heat transfer and used in the overall compressor energy requirement. Table 3 below shows the final equations used in calculation of mass flow rate and power.

Parameter	Equation
Mass Flow Rate	$\frac{RPD * RPM}{v_{suc}} (1 + C - C(\frac{p_{dis}}{p_{suc}})^{\frac{1}{n}})$
Power	$\frac{\dot{m}(h_{out} - h_{in}) - \dot{W}_{cal}(B_1 + B_2\dot{Q}_{cyl})}{1 - (B_1 + B_2\dot{Q}_{cyl})}$

Table 3: Popovic and Shapiro model mass flow rate and power formulations.

The work achieves 8% and 6% relative errors for mass flow rate and power respectively. The postulated model needs eight inputs which include: refrigerant inlet state, refrigerant outlet pressure, pressure drops, clearance volume, motor speed, piston displacement, a polytropic exponent estimate, and lastly an estimate of the heat transfer loss coefficient.

2.2.3. The Winandy Model

The Winandy model presented by Winandy et al. (2002b) is a semi-empirical compressor model that was derived to predict the performance of scroll compressors. The model utilizes an isothermal envelope that heats up suction gas, cools the discharge gas, absorbs electro-mechanical power losses, and exchanges heat with the ambient. The compression process is broken into two steps and modeled as isentropic up to the adapted pressure, then adiabatic at constant volume to the discharge pressure. The mass flow rate is predicted utilizing a swept volume that is considered an unknown in the formulation. Heat transfer coefficients are taken as unknowns and tuned to experimental data. The shaft power calculation follows the ASHRAE Toolkit, Bourdhouxhe et al. (1994), and is the sum of the compression power term, constant electro-mechanical loss term, and electro-mechanical losses proportional to the compression power. Table 4 shows the final formulations for mass flow rate and power prediction.

The authors proposed model takes four parameters to predict mass flow rate; the swept volume, and the suction, discharge, and ambient heat transfer coefficients. The power formulation take three parameters to calculate electric power; built in volume ratio, constant power loss term, and the power coefficient. The authors achieve relative errors between -3.5% and 2.5% for mass flow rate and relative errors spanning -2.5% and 3% for power estimation.

2.3. Model Implementation

These models represent legacy formulations identified by this work. All models were codified into the Python programming language except the Winandy formulation, which was coded into

Parameter	Equation
Mass Flow Rate	$\frac{NV_s}{v_{suc}}$
Power	$W_{in} + W_{loss} + \alpha W_{in}$

Table 4: Winandy model mass flow rate and power formulations.

Engineering Equation Solver (EES) Klien and Alvarado (2000).

3. Data for Model Testing

Data needed to train parameters and coefficients in the semi-empirical and empirical formulations is desired to be of high fidelity. The Popovic and Shapiro model was derived using data that is not often provided by manufacturers, discharge temperature. To this end, measured compressor data from either a hot-gas-bypass compressor load stand or a compressor calorimeter was sought. High fidelity data, collected to a stated standard was found and used in the present study.

Performance data for four different compressor technologies; scroll, screw, reciprocating, and spool compressors are used. The first three compressor types represent the most common technologies used in commercial and residential heating and cooling equipment today. The fourth technology, spool compressors, represent a novel compression technology that is still in the design optimization phase of development. Data sets from the above mentioned compressors provide a span of technologies that models will need to capture. Additionally, operational data for four different refrigerants is used to ensure a model is not strictly limited to a certain refrigerant. The refrigerants are R134a, R401A, R1234ze(E), and R32. A total of 327 data points have been collected and used in the present work.

3.1. High Fidelity Data Collection

Data sets came from measured data that was collected at Oklahoma State University’s (OSU) 10-80 ton hot-gas-bypass compressor load stand and from a 3 ton compressor calorimeter at the Heat Exchanger Advanced Testing Facility at Oak Ridge National Laboratory. The data collected at OSU is labeled ‘In House Data’. The data collected at Oak Ridge was motivated by an initiative at AHRI called the Low-GWP Alternative Refrigerants Evaluation Program (AREP). Details of the data can be found in Table 5. Tests were conducted according to ASHRAE Standard 23.1, except AREP Report #59, which didn’t state a collection standard. Scroll and reciprocating performance data was collected at the Oak Ridge facility while the spool and screw compressor performance originated from OSU’s facility.

3.2. Data Sets

Five total data sets were collected and used for model testing in this work. Two data sets from a 40 ton spool compressor were utilized. One set was collected with R-134a and other used R-1234ze(E) as the working fluid. The 2 ton scroll compressor data set used in this study had R-410A as the working fluid. The 2.5 ton reciprocating compressor data set utilized R-32 as its working fluid. And finally, the 75 ton screw compressor data set used R-134a as the working fluid during testing.

Compressor Type	Capacity	Refrigerant	Data Point	Collection Standard	Reference	Splits
Spool	40 tons	R-134a	58	ASHRAE 23.1	In House Data	4
Spool	40 tons	R-1234ze(E)	44	ASHRAE 23.1	In House Data	4
Scroll	2.5 tons	R-401A	196	ASHRAE 23.1	AREP #11	4
Screw	75 tons	R-134a	13	ASHRAE 23.1	In House Data	2
Reciprocating	2 tons	R-32	16	Not Mentioned	AREP #59	2

Table 5: Information on the data sets collected.

Each data set was collected in bulk and had to be split into subsets for model capability testing. Data was split into subsets in order to form a training data set to train model parameters with. Other subsets of data are used to test model capabilities at extrapolation and modulation scenarios. A constant speed and constant superheat data subset was selected from a full data set as the baseline. Model training data and extrapolation testing data points were selected as a subset of the baseline data set. Data sets that contained variable speed or variable superheat data points were split into variable speed sets and variable superheat sets to test model performance.

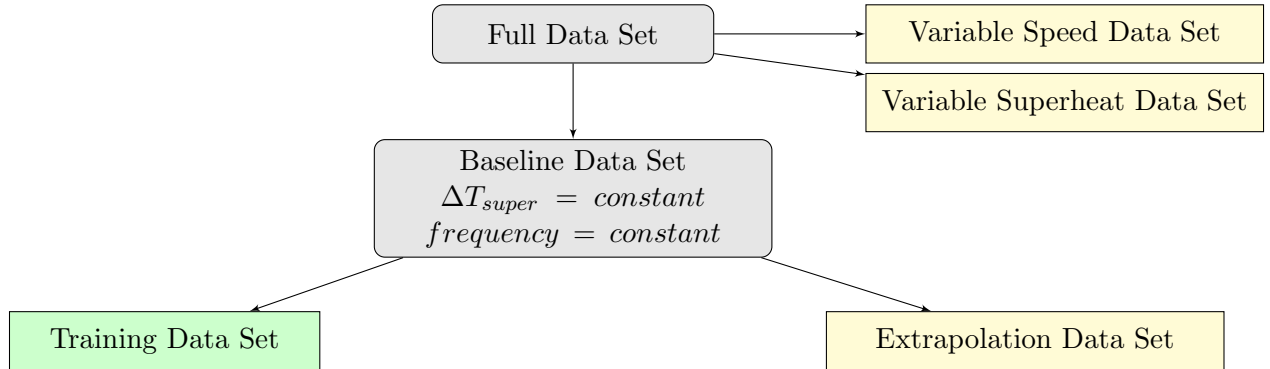


Figure 1: Flowchart showing an overview of semi-empirical model testing and data splits

4. Model Testing Methodology

Model testing begins with defining a baseline data set from which a training data set is used to train model parameters. Ten data points were selected to train the models. Motivation for this number of training points stems from the fact that the AHRI model needs ten data points for tuning its ten regression coefficients. The training data set is selected at points interior to the most extreme envelope conditions present within a data set. This allows for an extrapolation data set to be defined such that all or most points in the extrapolation set are outside the training bounds of the baseline data set.

4.1. Modulation

Modulation or variable speed testing consisted of running the models at operating speeds differing from that in the training data set. This gives an estimate of a models capability of capturing variable speed operation. The MAPE is used to quantify model performance.

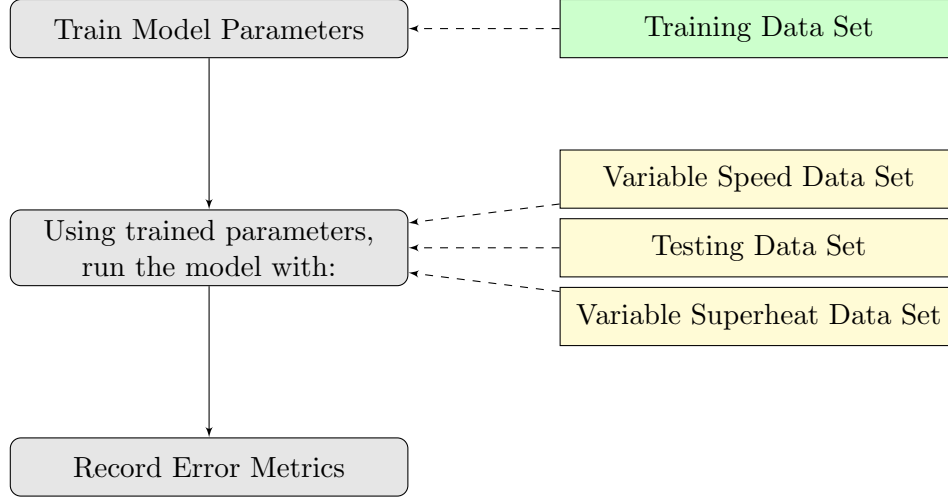


Figure 2: Flowchart showing an overview of semi-empirical model testing and data splits

4.2. Extrapolation

Extrapolation performance quantification in this work consists of running a model at conditions outside of its training data. There are two extrapolation scenario defined: envelope extrapolation and superheat extrapolation. Modulation scenarios could be included in this definition of extrapolation, however, the authors have included modulation testing separately.

4.2.1. Envelope Extrapolation

Envelope extrapolation is tested by running a model at data points outside the envelope conditions in which a model is trained. Data points were plotted as evaporating temperature verses condensing temperature and a training envelope was determined. Envelope extrapolation points are defined as points outside this envelope. These data points directly test a models capability of predicting performance outside training bounds.

4.2.2. Superheat Extrapolation

Superheat extrapolation is tested by running a model at data points with a different superheat than that of its training data. Constant superheat data is used for model training therefore evaluating model performance at conditions different than that of the training data will indicate a models capability at superheat extrapolation.

5. Results

The five models were tested at modulation and extrapolation scenarios following the methodology outlined in Section 4. The Winandy model failed to predict reciprocating compressor data while the Popovic and Shapiro model did not predict scroll compressor data. The semi-empirical models do extrapolate and capture modulation given the model predicts the data. The AHRI model does not extrapolate or capture modulation adequately. The ANN model does extrapolate to a reasonable level, however it does not predict variable speed performance. The Shao model captures extrapolation and modulation to a reasonable level, but requires variable speed data in its training data pool. The Shao model was derived for capturing variable speed performance, therefore it is not unreasonable to expect it to perform well in modulation testing.

5.1. Modulation Scenarios

5.1.1. Mass Flow Rate

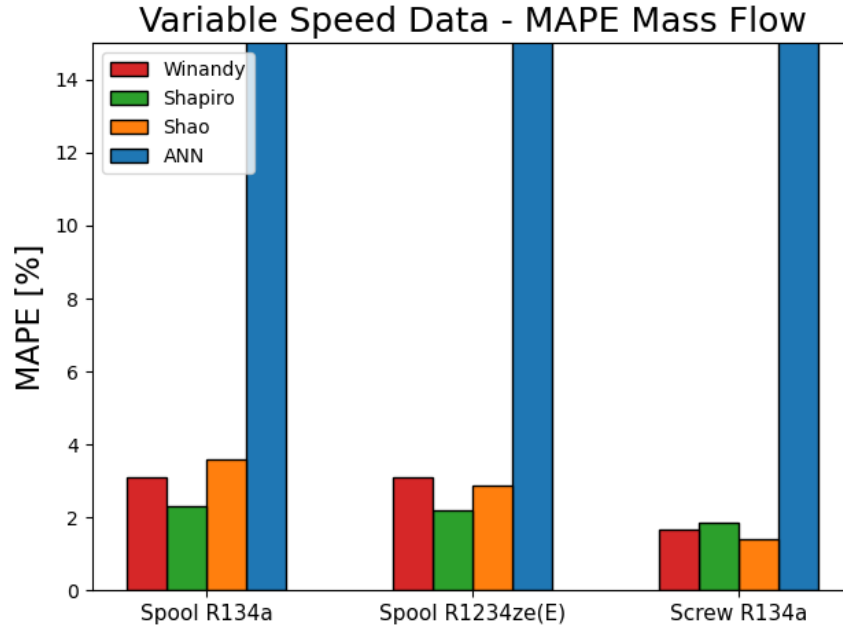


Figure 3: Showing mass flow rate results under modulation testing. (Errors for ANN Spool R134a, ANN Spool R1234ze(E), and ANN Screw R134a are: 19.9%, 19.6%, 25.2% respectively.)

The testing results for modulation situations show the Winandy, Popovic and Shapiro, and the Shao model capture mass flow rate at MAPE's less than 5%. This provides good indication that the a fore mentioned models could be used to predict mass flow rate at conditions outside the bounds of their training data. The ANN model produced errors around 20% and performs poorly when tested at modulation scenarios. The errors achieved for the AHRI model are not shown on the modulation bar plot since the screw compressor data did have ten data points at constant superheat and speed to train the model's coefficients. The errors achieved for spool compressor mass flow rate using R134a and R1234ze(E) when running the AHRI model were 20.7% and 20.3%, respectively.

5.1.2. Power Results

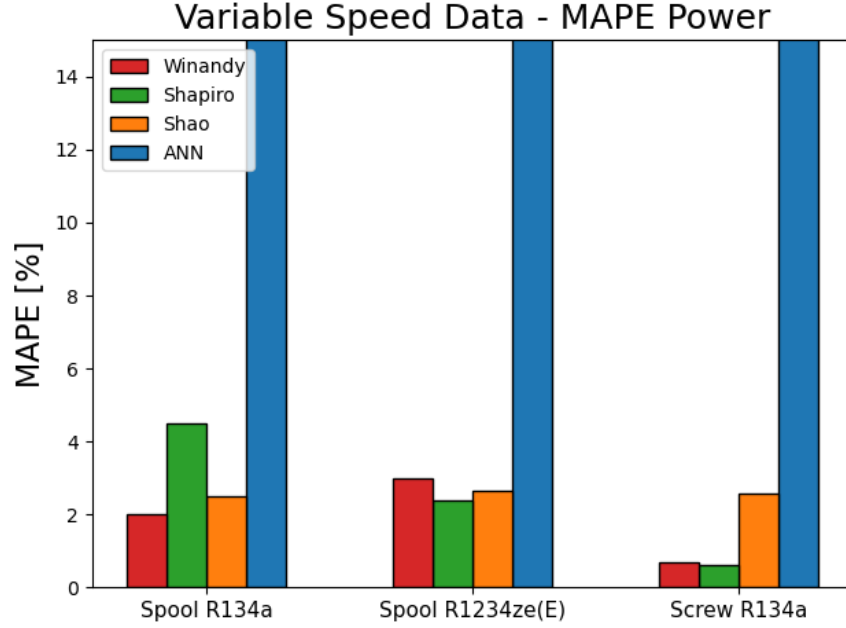


Figure 4: Power results under modulation testing. (Errors for ANN Spool R134a, ANN Spool R1234ze(E), and ANN Screw R134a are: 19.1%, 20.4%, 20.6% respectively).

The results for power prediction under modulation scenarios were similar to that of mass flow rate. The Winandy, Popovic and Shapiro, and Shao model performed under 5% MAPE. The ANN model again performs at MAPE's around 20% for power prediction when tested at modulation scenarios. Similar to the mass flow rate plots, the AHRI model is not shown on the graph for power prediction. The errors achieved for power prediction using the AHRI model and tested with the spool compressor using R134a and R1234ze(E) were 20.2% and 21.4%, respectfully.

5.2. Extrapolation Scenarios

5.2.1. Mass Flow Rate Results

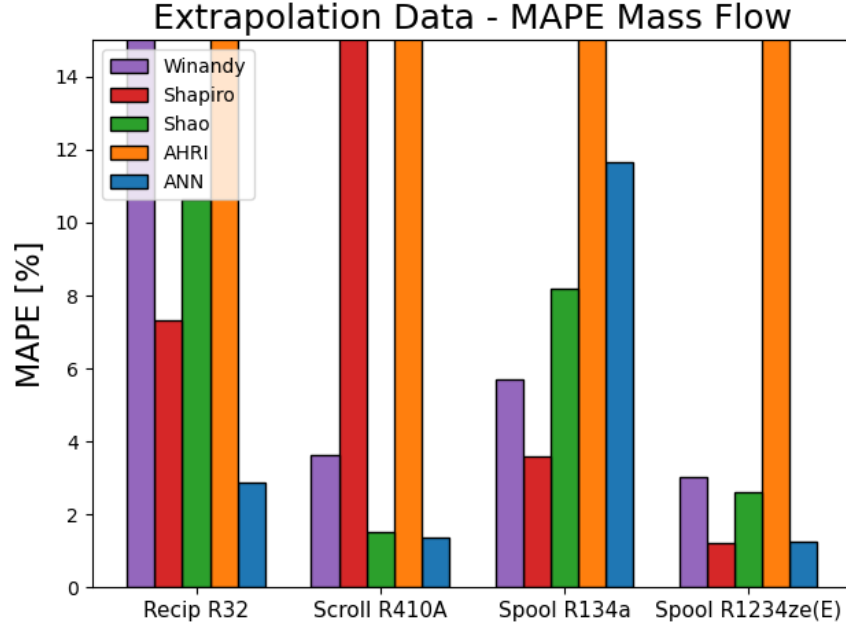


Figure 5: Mass flow rate results at extrapolation scenarios for all models.

Data Set	Model MAPE - Mass Flow				
	Winandy	Popovic & Shapiro	Shao	AHRI	ANN
Recip. R32	23.3%	7.3%	10.7%	45.1%	2.9%
Scroll R410A	3.6%	19.3%	1.5%	6.4e+5%	1.4%
Spool R134a	5.7%	3.6%	8.2%	6.0e+6%	11.9%
Spool R1234ze(E)	3.0%	1.2%	2.6%	3.5e+6%	1.3%

Table 6: Mass flow rate MAPE's under extrapolation scenarios.

Results show that mass flow rate extrapolation is captured by the semi-empirical models, given that they do predict the compressor technology. The Winandy model performs below 6% MAPE for the scroll and spool compressor technologies. The model extrapolated with two different refrigerant data sets for the spool compressor. The model did not capture reciprocating compressor performance. The Popovic and Shapiro model extrapolated below 8% MAPE for the compressor technologies that it predicted. This model however, did not capture scroll compressor technology but performed better at extrapolating spool compressor data than reciprocating data, the latter of which the model was derived initially to predict. The ANN model extrapolated below 3% MAPE except in the case of the spool compressor utilizing R134a. The Shao model performed well when ran with scroll and the spool R1234ze(E) data, however extrapolation errors rose to 8.2% and 10.7% MAPE for the reciprocating and spool R134a data respectively. The AHRI model did not perform adequately when extrapolating as can be seen by the errors rising from 45.% to 6.0e+6.

5.2.2. Power Results

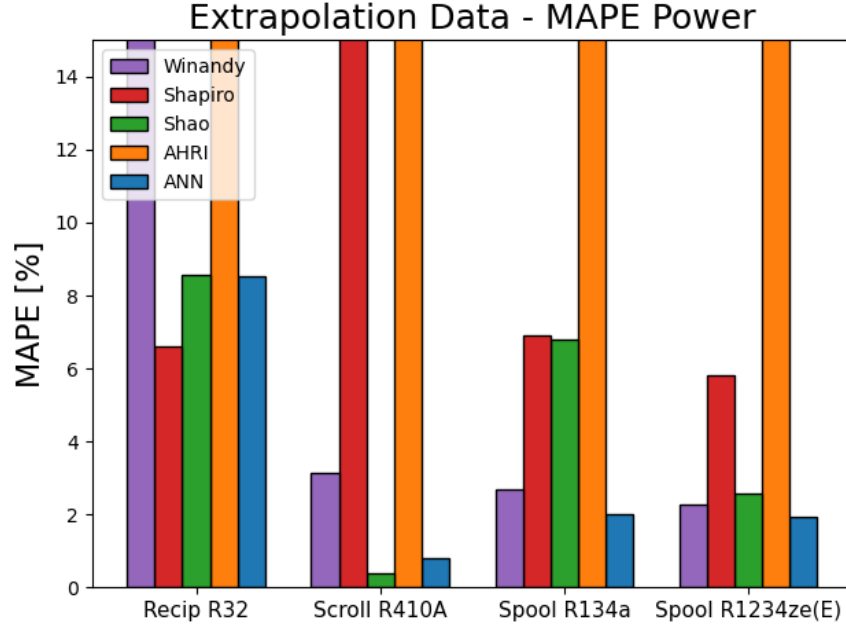


Figure 6: Power results under extrapolation testing for all models.

Data Set	Model MAPE - Power				
	Winandy	Popovic & Shapiro	Shao	AHRI	ANN
Recip. R32	16.4%	6.6%	8.6%	27.5%	8.5%
Scroll R410A	3.1%	3.4e+3%	0.4%	9.0e+5%	0.8%
Spool R134a	2.7%	6.9%	6.8%	6.7e+6%	1.9%
Spool R1234ze(E)	2.3%	5.8%	2.6%	6.3e+4%	1.9%

Table 7: Power MAPE's for extrapolation scenarios.

Since the mass flow rate results are used in the power prediction for the Winandy and Popovic and Shapiro models, it can be expected that when either model doesn't predict the mass flow rate adequately, the power formulation will suffer. This is the case for the Winandy model predicting reciprocating compressor power requirements and the Shapiro and Popovic model predicting scroll compressor power requirements under envelope extrapolation scenarios. When the Winandy model predicts the compressor technology, it extrapolates below 4% MAPE. The Popovic and Shapiro model extrapolates below 7% MAPE. The Shao model extrapolated below 9% MAPE for all cases while the ANN model performed under 2% MAPE for cases except that of the reciprocating data in which it performed at 8.5% MAPE. The AHRI model did not extrapolate adequately. It produced errors between 27.5% and 6.7e+6% MAPE.

5.3. Variable Superheat Scenarios

5.3.1. Mass Flow Rate Results

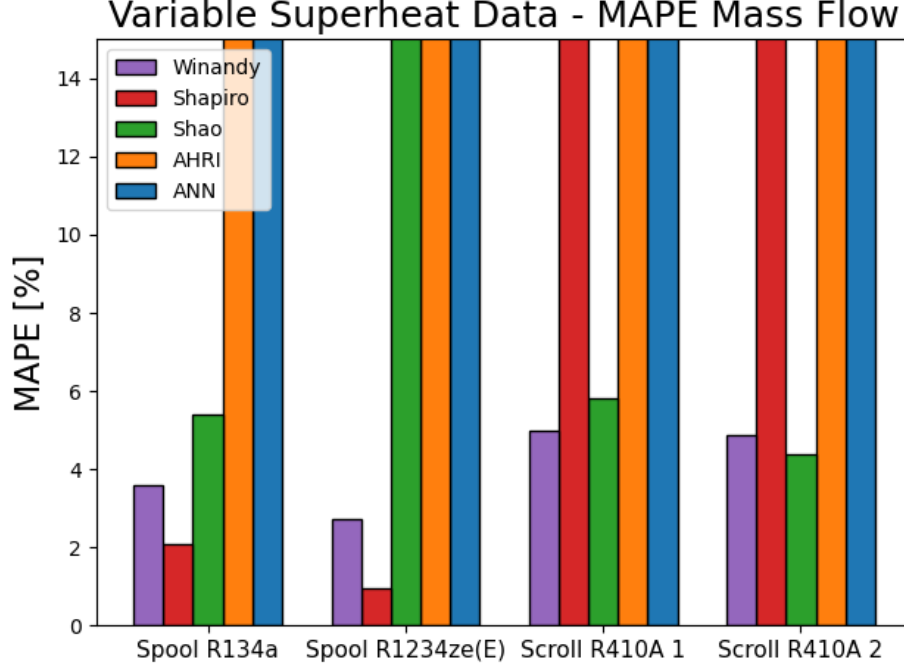


Figure 7: Mass flow rate results under variable superheat testing.

Data Set	Model MAPE - Mass Flow Rate				
	Winandy	Popovic & Shapiro	Shao	AHRI	ANN
Spool R134a	3.6%	2.1%	5.4%	2.9e+5%	25.5%
Spool R1234ze(E)	2.7%	1.0%	42.2%	6.0e+7%	20.9%
Scroll R410A 1	5.0%	20.1%	5.8%	6.6e+5%	21.2%
Scroll R410A 2	4.9%	19.3%	4.4%	6.6e+5%	18.6%

Table 8: Mass flow rate results for variable superheat scenarios.

The mass flow rate for variable superheat scenarios is best predicted by the Winandy model. The Shapiro and Popovic model performs well for the compressor technology it does predict, it performs under 2.5% MAPE for the spool data sets. The Shao model predicts mass flow under 6% for all cases except the spool compressor data set using R1234ze(E). As can be seen from the bar chart and table, the AHRI model does not predict mass flow rate at variable superheat condition adequately. There exists a superheat correction factor for the model, however it is not applied in the present study. The ANN model predicts mass flow rate at a MAPE above 20% for all situations and yielded inadequate results.

5.3.2. Power Results

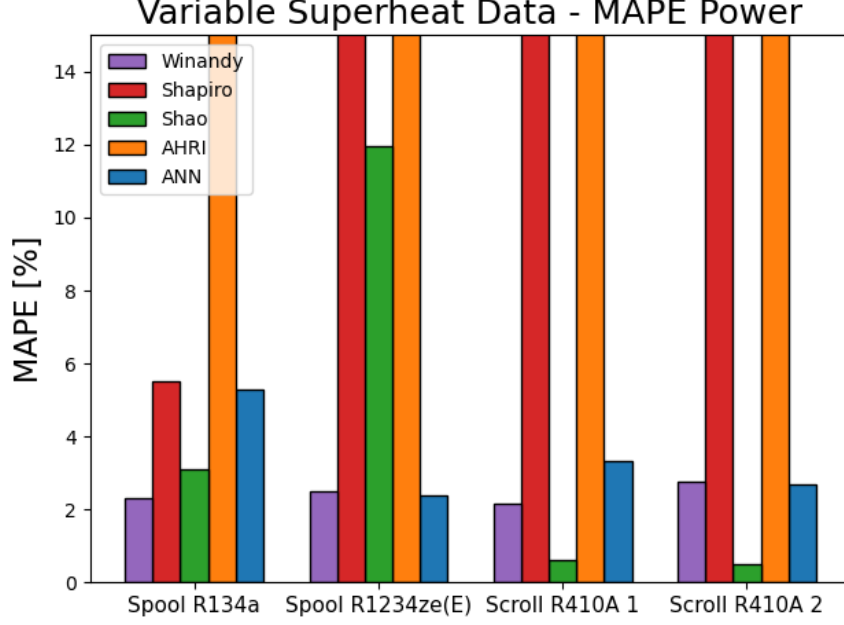


Figure 8: Power results under variable superheat testing.

Data Set	Model MAPE - Power				
	Winandy	Popovic & Shapiro	Shao	AHRI	ANN
Spool R134a	2.3%	5.5%	3.1%	5.8e+5%	5.3%
Spool R1234ze(E)	2.5%	2.4%	11.9%	1.6e+6%	2.4%
Scroll R410A 1	2.2%	232%	0.6%	9.2e+5%	3.3%
Scroll R410A 2	2.8%	372%	0.5%	9.0e+5%	2.7%

Table 9: Power results for variable superheat scenarios.

Power results show that the Winandy model performed best at predicting variable superheat power consumption. The model performed below 3% MAPE for all data sets. The Shapiro and Popovic model performed under 6% MAPE for the technologies it predicted. The errors resulting from the scroll power prediction were above 200% MAPE. The Shao model performed well at power prediction for the data sets resulting in MAPE's under 3.5% except for the spool data set using R1234ze(E), where it yielded 11.1% MAPE. The AHRI model did not perform adequately and gave errors above 5.8e5%. The ANN model performed better at power prediction than mass flow rate prediction for variable superheat scenarios. The model gave MAPE's below 5.5% for all data sets it was tested with.

6. Discussion

The semi-empirical models (Winandy model and Popovic and Shapiro model) performed adequately in extrapolation and modulation scenarios. Given that the model predicted the compressor technology, the highest MAPE for mass flow rate came from the Shapiro and Popovic model at

7.3%. For power prediction the same model recorded the highest error, which was 6.9%. The more empirical Shao model gave promising results for mass flow rate and power prediction in modulation scenarios, however, mixed results were achieved in extrapolation testing where resulting MAPE's ranged from 0.4% to 42.2%. The AHRI formulation performed the worst in modulation and extrapolation scenarios. Results show that the model should not be used in modulation scenarios or beyond the bounds of its' training data. The ANN model has performed poorly in modulation scenarios where errors above 19% were recorded in all data sets. In extrapolation scenarios, results were mixed with MAPE's between 0.8% and 25.5%.

From these results some conclusions can be made regarding the performance of the semi-empirical and empirical models.

- The Winandy model, as tested, will capture extrapolation and modulation in scroll, screw, and spool compressors
- The Winandy model outperforms the Shapiro and Popovic model when compared head to head
- The ANN model cannot predict performance during compressor modulation, given a constant speed training data set
- The Shao model, even though empirical in nature, will capture modulation scenarios
- The AHRI model will not predict compressor performance under modulation or extrapolation scenarios

6.1. Model Capabilities

The semi-empirical models yielded more consistent performance at extrapolation and modulation scenarios than the empirical models. The Shao model performed best at modulation scenarios, however as previously mentioned, the model uses variable speed data for training parameters. It does not account for a compression process and only takes data to fit coefficients. Similarly, the ANN and AHRI formulations only require data for tuning parameters. The Winandy model attempts to account for phenomena occurring in the suction line, discharge line, and compression chamber via the isentropic compression assumption and the suction and discharge heat transfer assumptions. The Shapiro and Popovic model does not account for suction and discharge gas heating, but it does model the compression process as polytropic and assumes suction and discharge pressure drops. These two models incorporate more physics into their formulations and are thought to be a good foundation for future model development.

6.1.1. Model Limitations

The five models tested in this work have limitations due to either training data or performance prediction. The training data for a model should require minimal operating conditions and no detailed information derived from comprehensive measurements of the compressor. To this end, the Shao and the Popovic and Shapiro models training data is a limiting factor. Shao requires operating conditions at three different operational speeds to adequately fit the power and mass flow ratios. The Shapiro and Popovic model requires discharge temperature measurements to fit the polytropic exponent to pressure ratio. Limitations in performance prediction are exhibited by each model. The Winandy model did not capture reciprocating compressor performance and the Shapiro and Popovic model did not capture scroll compressor performance. Other models exhibited limitations during specific testing scenarios. The ANN model did not predict compressor behavior during modulation testing. The AHRI model exhibited large errors throughout testing.

6.2. Future Model Development

Future work based on the results presented herein will be developing a compressor model to capture multiple compressor technologies and adequately capture modulation and extrapolation. The model will be tested subject to the same methodology as used here. The Winandy model offered good results during testing of the compressors that it predicted. With its performance here and the body of literature showing modifications, it is selected as the basis for future model development.

7. Conclusions

The present work studied the extrapolation and modulation capabilities of select semi-empirical compressor models. Data sets selected for model testing were of high fidelity to ensure model prediction is accurate to measured data instead of manufacture published data. Data sets were split to enable training model parameters at constant conditions then test model with data outside that of the training data. Four different data sets were identified and used: the training data set, envelope extrapolation data set, variable superheat data set, and variable speed data set. Models were trained using the training data set then tested at the others to record performance. Based on the results, the semi-empirical models outperform the empirical models when considering all aspects desired by the author. These were: limited training data, low computational cost, and accurate performance at extrapolation and modulation scenarios. The model proposed by Winandy et al. (2002a) is chosen as a formulation with promising attributes for future model development. As cited in the literature survey, this formulation has been modified to capture a range of technologies and will be the basis for a new model desired to capture multiple compressor technologies and exhibit strong extrapolation and modulation capabilities.

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References

- AHRI (2020), ‘ANSI/AHRI standard 540:2020 standard for performance rating of positive displacement refrigerant compressors and compressor units’, *Air Conditioning and Refrigeration Institute Arlington, VA, USA*.
- URL:** [https://www.ahrinet.org/App_Content/ahri/files/STANDARDS/AHRI/AHRI_Standard_540_\(I-P_and_SI\)_2020_Standard_for_Performance_Rating_of_Positive_Displacement_Refrigerant_Compressors_and_Compressor_Units.pdf](https://www.ahrinet.org/App_Content/ahri/files/STANDARDS/AHRI/AHRI_Standard_540_(I-P_and_SI)_2020_Standard_for_Performance_Rating_of_Positive_Displacement_Refrigerant_Compressors_and_Compressor_Units.pdf)
- Aprea, C. and Renno, C. (2008), ‘Experimental model of a variable capacity compressor’, *Archives of Thermodynamics* **33**(4), 29–37.
- Bourdhouxhe, J.-P., Grodent, M., Lebrun, J., Saavedra, C. and Silva, K. (1994), ‘A toolkit for primary hvac system energy calculation—part 2: reciprocating chiller models’, *ASHRAE Transactions* **100**, 774–786.
- Corber, J. M., Navarro, E. and Urchuegui, J. F. (2007), ‘Performance analysis of a series of hermetic reciprocating compressors working with R290 (propane) and R407C ’ rie de compresseurs a ‘ piston Analyse de la performance d ’ une se ’ tiques fonctionnant au R290 (propane) et au R407C herme’, *International Journal of Refrigeration* **30**, 1244–1253.
- Cuevas, C. and Lebrun, J. (2009), ‘Testing and modelling of a variable speed scroll compressor’, *Applied Thermal Engineering* **29**(2-3), 469–478.
- URL:** <http://dx.doi.org/10.1016/j.applthermaleng.2008.03.016>
- Cuevas, C., Lebrun, J., Lemort, V. and Winandy, E. (2010), ‘Characterization of a scroll compressor under extended operating conditions’, *Applied Thermal Engineering* **30**(6-7), 605–615.
- URL:** <http://dx.doi.org/10.1016/j.applthermaleng.2009.11.005>
- Dardenne, L., Fraccari, E., Maggioni, A., Molinaroli, L., Proserpio, L. and Winandy, E. (2015), ‘Semi-empirical modelling of a variable speed scroll compressor with vapour injection’, *International Journal of Refrigeration* **54**, 76–87.
- URL:** <http://dx.doi.org/10.1016/j.ijrefrig.2015.03.004>
- Giuffrida, A. (2016), ‘A semi-empirical method for assessing the performance of an open-drive screw refrigeration compressor’, *Applied Thermal Engineering* **93**, 813–823.
- URL:** <http://dx.doi.org/10.1016/j.applthermaleng.2015.10.023>
- Jahnig, D. I., Reindl, D. T. and Klein, S. A. (2000), ‘Semi-empirical method for representing domestic refrigerator/freezer compressor calorimeter test data’, *ASHRAE Transactions* **106**(January).
- James, N. A., Braun, J. E., Groll, E. A. and Horton, W. T. (2016), ‘Semi-empirical modeling and analysis of oil flooded R410A scroll compressors with liquid injection for use in vapor compression systems’, *International Journal of Refrigeration* **66**, 50–63.
- URL:** <http://dx.doi.org/10.1016/j.ijrefrig.2015.12.011>
- Klien, S. and Alvarado, F. (2000), ‘EES-engineering equation solver’.
- URL:** <https://www.fchartsoftware.com/ees/>
- Li, W. (2012a), ‘Simplified steady-state modeling for hermetic compressors with focus on extrapolation’, *International Journal of Refrigeration* **35**(6), 1722–1733.
- URL:** <http://dx.doi.org/10.1016/j.ijrefrig.2012.03.008>

- Li, W. (2012b), ‘Simplified steady-state modeling for variable speed compressor’.
URL: <http://dx.doi.org/10.1016/j.applthermaleng.2012.08.041>
- Mackensen, A., Klein, S. A. and Reindl, D. T. (2002), ‘Characterization of Refrigeration System Compressor Performance’, *International Refrigeration and Air Conditioning Conference* p. Paper 567.
URL: <https://docs.lib.purdue.edu/iracc/567/>
- Molinaroli, L., Joppolo, C. M. and De Antonellis, S. (2017), ‘A semi-empirical model for hermetic rolling piston compressors’, *International Journal of Refrigeration* **79**, 226–237.
URL: <http://dx.doi.org/10.1016/j.ijrefrig.2017.04.015>
- Navarro, E., Granryd, E., Urchueguía, J. F. and Corberán, J. M. (2007), ‘A phenomenological model for analyzing reciprocating compressors’, *International Journal of Refrigeration* **30**(7), 1254–1265.
- Negrão, C. O., Erthal, R. H., Andrade, D. E. and Silva, L. W. D. (2011), ‘A semi-empirical model for the unsteady-state simulation of reciprocating compressors for household refrigeration applications’, *Applied Thermal Engineering* **31**(6-7), 1114–1124.
URL: <http://dx.doi.org/10.1016/j.applthermaleng.2010.12.006>
- Popovic, P. and Shapiro, H. N. (1995), Semi-empirical method for modeling a reciprocating compressor in refrigeration systems, in ‘ASHRAE Transactions’, Vol. 101, ASHRAE, pp. 367–382.
- Python.org (2020), <https://www.python.org/>.
- Santos, G. Z., Ronzoni, A. F. and Hermes, C. J. (2019), ‘Performance characterization of small variable-capacity reciprocating compressors using a minimal dataset’, *International Journal of Refrigeration* **107**, 191–201.
URL: <https://doi.org/10.1016/j.ijrefrig.2019.07.014>
- Shao, S., Shi, W., Li, X. and Chen, H. (2004), ‘Performance representation of variable-speed compressor for inverter air conditioners based on experimental data’, *International Journal of Refrigeration* **27**(8), 805–815.
- Tello-Oquendo, F. M., Navarro-Peris, E., Barceló-Ruescas, F. and González-Maciá, J. (2019), ‘Semi-empirical model of scroll compressors and its extension to describe vapor-injection compressors. Model description and experimental validation’, *International Journal of Refrigeration* **106**, 308–326.
URL: <https://doi.org/10.1016/j.ijrefrig.2019.06.031>
- U.S. Energy Information Administration (2021), ‘Electricity Explained, use of electricity’.
URL: <https://www.eia.gov/energyexplained/electricity/use-of-electricity.php>
- Winandy, E. L. and Lebrun, J. (2002), ‘Scroll compressors using gas and liquid injection: Experimental analysis and modelling’, *International Journal of Refrigeration* **25**(8), 1143–1156.
- Winandy, E., Saavedra O, C. and Lebrun, J. (2002a), ‘Simplified modelling of an open-type reciprocating compressor’, *International Journal of Thermal Sciences* **41**(2), 183–192.
- Winandy, E., Saavedra O, C. S. and Lebrun, J. (2002b), ‘Experimental analysis and simplified modelling of a hermetic scroll refrigeration compressor’, *Applied Thermal Engineering* **22**(2), 107–120.