

## RW Control Devices

- ❖ First let us develop a feedback control law for a spacecraft with N reaction wheels with general orientation.

EOM:

$$[I_{RW}]\dot{\boldsymbol{\omega}} = -\boldsymbol{\omega} \times [I_{RW}]\boldsymbol{\omega} - \boldsymbol{\omega} \times [G_S]\mathbf{h}_s - [G_S]\mathbf{u}_s + \mathbf{L}$$

With

$$\mathbf{h}_s = \begin{pmatrix} \vdots \\ J_{s_i}(\omega_{s_i} + \Omega_i) \\ \vdots \end{pmatrix}$$

Inertial Matrix:

$$[I_{RW}] = [I_s] + \sum_{i=1}^N (J_{t_i} \hat{\mathbf{g}}_{t_i} \hat{\mathbf{g}}_{t_i}^T + J_{g_i} \hat{\mathbf{g}}_{g_i} \hat{\mathbf{g}}_{g_i}^T)$$

The RW motor control torque vector is:

$$\mathbf{u}_s = \begin{pmatrix} \vdots \\ J_{s_i}(\dot{\Omega} + \hat{\mathbf{g}}_{s_i}^T \dot{\boldsymbol{\omega}}) \\ \vdots \end{pmatrix}$$

- ❖ **Spacecraft Tracking Errors:**

$\boldsymbol{\sigma}$ : MRP vector of body frame relative to reference frame

$\delta\boldsymbol{\omega} = \boldsymbol{\omega} - \boldsymbol{\omega}_r$ : Body angular velocity tracking error vector

- *Lyapunov Function:*

$$V(\boldsymbol{\sigma}, \delta\boldsymbol{\omega}) = \frac{1}{2} \delta\boldsymbol{\omega}^T [I_{RW}] \delta\boldsymbol{\omega} + 2K \ln(1 + \boldsymbol{\sigma}^T \boldsymbol{\sigma})$$

Components taken in  
the  $B$  frame

- Let's set the Lyapunov Rate to:

$$\dot{V} = -\delta\omega[P]\delta\omega \leq 0$$



$$[I_{RW}] \frac{B_d}{dt}(\delta\omega) + K\sigma + [P]\delta\omega = 0$$

Close-loop dynamics



$$[G_s]\mathbf{u}_s = \frac{K\sigma + [P]\delta\omega - [\tilde{\omega}]([I_{RW}]\omega + [G_s]\mathbf{h}_s) - [I_{RW}](\dot{\omega}_r - \omega \times \omega_r) + L}{L_r}$$

- Control condition:

$$[G_s]\mathbf{u}_s = L_r$$

Case 1: 3 RWs aligned with principal axes of spacecraft.

$$\mathbf{u}_s = L_r$$

Case 2:  $N$  RWs aligned generally.

$$\mathbf{u}_s = [G_s]^T([G_s][G_s]^T)^{-1}L_r$$

Minimum-norm inverse

Energy rate:

$$\dot{T} = \omega^T L + \sum_{i=1}^N \Omega_i u_{s_i}$$

Work/energy principle