EL2450 Hybrid and Embedded Control

Lecture 2: Models of sampled systems

- Sampling of continuous-time systems
- State-space and input-output models
- Poles and zeros

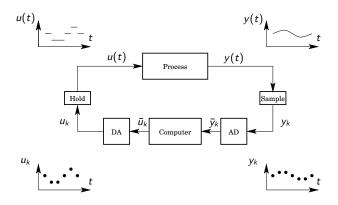
Today's Goal

You should be able to

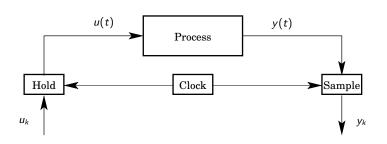
- Derive zero-order-hold sampling of systems (without and with delays in the loop)
- Relate SS and IO models
- Derive poles and zeros of discrete-time systems and relate them to their continuous-time counterparts

Computer-Controlled System

Consider the mapping from u_k to y_k :



Sampled Continuous-Time System



Process:

$$\dot{x}(t) = Ax(t) + Bu(t)$$
$$y(t) = Cx(t) + Du(t)$$

Sampling Continuous-Time System

For all $t \in [t_k, t_{k+1}]$

$$x(t) = e^{A(t-t_k)}x(t_k) + \int_{t_k}^t e^{A(t-\tau)}Bu(\tau)d\tau$$

$$= e^{A(t-t_k)}x(t_k) + \int_{t_k}^t e^{A(t-\tau)}d\tau Bu(t_k)$$

$$= e^{A(t-t_k)}x(t_k) + \int_0^{t-t_k} e^{As}dsBu(t_k),$$

$$\begin{split} x(t_{k+1}) &= \Phi(t_{k+1}, t_k) x(t_k) + \Gamma(t_{k+1}, t_k) u(t_k) \\ y(t_k) &= C x(t_k) + D u(t_k) \\ \Phi(t_{k+1}, t_k) &= e^{A(t_{k+1} - t_k)}, \quad \Gamma(t_{k+1}, t_k) = \int_0^{t_{k+1} - t_k} e^{As} ds B \end{split}$$

Note: Time-varying linear system

Uniform Sampling

Periodic sampling with h > 0 gives linear time-invariant system

$$x(kh + h) = \Phi x(kh) + \Gamma u(kh)$$
$$y(kh) = Cx(kh) + Du(kh)$$

where

$$\Phi = e^{Ah}, \quad \Gamma = \int_0^h e^{As} ds B$$

Example

Sampling the system

$$\dot{x} = ax + bu, \quad a \neq 0$$

gives

$$x(kh+h) = \Phi x(kh) + \Gamma u(kh)$$

with

$$\Phi=e^{ah}, \quad \Gamma=\int_0^h e^{as}dsb=rac{b}{a}(e^{ah}-1)$$

Discrete-Time Systems

Suppose now on (if not otherwise stated) that h = 1:

$$x(k+1) = \Phi x(k) + \Gamma u(k)$$
$$y(k) = Cx(k) + Du(k)$$

With initial condition x(0), the solution is

$$x(k) = \Phi x(k-1) + \Gamma u(k-1)$$

$$= \Phi^2 x(k-2) + \Phi \Gamma u(k-2) + \Gamma u(k-1) = \dots$$

$$= \Phi^k x(0) + \sum_{j=0}^{k-1} \Phi^{k-j-1} \Gamma u(j)$$

Discrete-Time Systems

With initial condition x(0), the solution is

$$x(k) = \Phi^{k}x(0) + \sum_{j=0}^{k-1} \Phi^{k-j-1}\Gamma u(j)$$

First part depends on x(0) and the second one on the input sequence. Solution properties related to eigenvalues of Φ , given by its *characteristic equation*

$$\det(\lambda I - \Phi) = 0$$

Changing Coordinates

T nonsingular matrix and z = Tx. Then

$$z(k+1) = \tilde{\Phi}z(k) + \tilde{\Gamma}u(k)$$
$$y(k) = \tilde{C}z(k) + \tilde{D}u(k)$$

with $\tilde{\Phi}=T\Phi T^{-1}, \tilde{\Gamma}=T\Gamma, \tilde{C}=CT^{-1}, \tilde{D}=D.$ Key result:

$$\det(\lambda I - \Phi) = \det(\lambda I - \tilde{\Phi})$$

Coordinates can be chosen to give simple forms to system equations (revise canonical and special forms from basic control course).

Example: Diagonal Form

 Φ has distinct eigenvalues $\lambda_1, \ldots, \lambda_n$. Then there exists a T such that

$$T\Phi T^{-1} = \begin{bmatrix} \lambda_1 & & 0 \\ & \ddots & \\ 0 & & \lambda_n \end{bmatrix}$$

Solution can be decoupled and has the form

$$z_i(k) = \lambda_i^k z_i(0) + \sum_{i=0}^{k-1} \lambda_i^{k-j-1} \beta_i u(j)$$

where $i = 1, \ldots, n$.

Example: Jordan Form

 Φ has multiple eigenvalues, then generally not diagonalizable. There exists a T such that

$$T\Phi T^{-1} = \begin{bmatrix} L_{k_1}(\lambda_1) & 0 \\ & \ddots & \\ 0 & L_{k_r}(\lambda_r) \end{bmatrix}$$

where $k_1 + \ldots + k_r = n$ and L_k is a $k \times k$ matrix with

$$L_k(\lambda) = \begin{bmatrix} \lambda & 1 & 0 & \dots & 0 \\ 0 & \lambda & 1 & \dots & 0 \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & \lambda & 1 \\ 0 & \dots & 0 & 0 & \lambda \end{bmatrix}$$

Pulse Response

For linear time-invariant systems, input-output relation has the general form

$$y(k) = \sum_{m=0}^{k} h(k-m)u(m) + y_p(k)$$

where y_p relates to initial conditions. For zero initial conditions, h(k-m) gives the output at k of a unit pulse injected at m. It is called *pulse-response function* of the system.

Pulse Response

We can derive the pulse response from the state-space model

$$y(k) = C\Phi^{k}x(0) + \sum_{j=0}^{k-1} C\Phi^{k-j-1}\Gamma u(j) + Du(k)$$

Hence, the response to a unit pulse at k = 0 with x(0) = 0 is

$$h(k) = \begin{cases} 0, & k < 0 \\ D, & k = 0 \\ C\Phi^{k-1}\Gamma, & k > 0 \end{cases}$$

Pulse-Transfer Operator

Introduce forward- and backward- shift operator q: qx(k) = x(k+1), $q^{-1}x(k) = x(k-1)$. Then,

$$qx(k) = \Phi x(k) + \Gamma u(k)$$

Hence.

$$y(k) = Cx(k) + Du(k) = \underbrace{[C(qI - \Phi)^{-1}\Gamma + D]}_{H(q)} u(k)$$

H(q) is the *pulse-transfer operator*. h(k), H(q) are also coordinate transformation invariant.

Pulse-Transfer Function

Similarly, with z-transform, $X(z) = \sum_{k=0}^{\infty} x(k)z^{-k}$, we obtain

$$z(X(z)-x(0))=\Phi X(z)+\Gamma U(z)$$

SO

$$Y(z) = CX(z) + DU(z)$$

$$= \underbrace{[C(zI - \Phi)^{-1}\Gamma + D]}_{H(z)} U(z) + C(zI - \Phi)^{-1}zx(0)$$

 $H(z) = \mathcal{Z}\{h(k)\}$ and is called the *pulse-transfer function*.

Note: H(z) is equal to H(q) with q replaced by z. Still they are two different mathematical objects. (Why?)

State-Space and Input-Output Models

Consider a state-space system of order *n*:

$$x(k+1) = \Phi x(k) + \Gamma u(k)$$
$$y(k) = Cx(k) + Du(k)$$

Then,
$$y(k) = H(q)u(k) = \frac{B(q)}{A(q)}u(k)$$
, where

$$A(q) = q^{n} + a_1 q^{n-1} + \cdots + a_n, \quad B(q) = b_0 q^{n} + b_1 q^{n-1} + \cdots + b_n$$

or equivalently

$$y(k+n) + a_1y(k+n-1) + \cdots + a_ny(k)$$

= $b_0u(k+n) + b_1u(k+n-1) + \cdots + b_nu(k)$

Sampled Double Integrator

What is H(q) for a ZOH sampled $G(s) = 1/s^2$ with h = 1?

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$
$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} x$$

$$\Phi = e^{Ah} = I + A + A^2/2 + \dots = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$
$$\Gamma = \int_0^h \begin{bmatrix} s \\ 1 \end{bmatrix} ds = \begin{bmatrix} 1/2 \\ 1 \end{bmatrix}$$

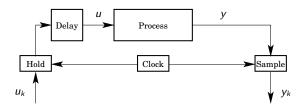
$$H(q) = C(qI - \Phi)^{-1}\Gamma = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} q-1 & -1 \\ 0 & q-1 \end{bmatrix}^{-1} \begin{bmatrix} 1/2 \\ 1 \end{bmatrix}$$

$$= \frac{q+1}{2(q-1)^2}$$

Note: Table 2 on page 22 in [WAA] gives $H(q) \stackrel{\text{ZOH samp}}{\longleftrightarrow} G(s)$

Sampling System with Time-Delay

Delayed actuation with fixed delay $au \in (0,h)$



Then, $\dot{x}(t) = Ax(t) + Bu(t - \tau)$. u(t) changes at $kh + \tau$, so

$$x(kh + h) = e^{Ah}x(kh) + \int_{kh}^{kh+h} e^{A(kh+h-s)}Bu(s-\tau)ds$$

$$= e^{Ah}x(kh) + \int_{kh}^{kh+\tau} e^{A(kh+h-s)}ds Bu(kh-h) + \int_{kh+\tau}^{kh+h} e^{A(kh+h-s)}ds Bu(kh)$$

$$\begin{split} x(kh+h) &= \Phi x(kh) + \Gamma_0 u(kh) + \Gamma_1 u(kh-h) \\ \Phi &= e^{Ah}, \quad \Gamma_0 = \int_0^{h-\tau} e^{As} ds B \\ \Gamma_1 &= e^{A(h-\tau)} \int_0^{\tau} e^{As} ds B \end{split}$$

Hence.

$$\begin{bmatrix} x(kh+h) \\ u(kh) \end{bmatrix} = \begin{bmatrix} \Phi & \Gamma_1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x(kh) \\ u(kh-h) \end{bmatrix} + \begin{bmatrix} \Gamma_0 \\ I \end{bmatrix} u(kh)$$

Note: Still LTI system, but of one order higher

Sampling System with Larger Time-Delay

What if the delay τ is larger than h? Then, the previous approach still works, but needs a modification: **Example** Suppose $\tau \in (h, 2h)$. Then,

$$\begin{bmatrix} x(kh+h) \\ u(kh-h) \\ u(kh) \end{bmatrix} = \begin{bmatrix} \Phi & \Gamma_1 & \Gamma_0 \\ 0 & 0 & I \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x(kh) \\ u(kh-2h) \\ u(kh-h) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ I \end{bmatrix} u(kh)$$

for suitable Γ_1 , Γ_0

Frequency Response

Recall that the frequency response of a continuous-time system G(s) is given by $G(i\omega)$ for $\omega \in [0,\infty)$.

The frequency response of a sampled-data system H(z) is given by $H(e^{i\omega h})$ for $\omega h \in [0, \pi]$.

Note that for H(z) it suffices to study ω up to ω_N .

Poles and Zeros

- Poles are the zeros of A(z)
- Zeros are the zeros of B(z)

Equivalently

- Poles are the eigenvalues of Φ
- Zeros are $z \in \mathbf{C}$ such that $\det \begin{bmatrix} zI \Phi & -\Gamma \\ C & D \end{bmatrix} = 0$

Physical interpretation:

Pole in p gives $mode p^k$ in time response Zero in a gives blocking of inputs a^k

Example: Blocking Zeros

y(k+1) - ay(k) = u(k+1) - bu(k), 0 < a < 1 < b, corresponds to

$$Y(z) = H(z)U(z) = \frac{z-b}{z-a}U(z)$$

 $u(k) = b^k$ gives

$$Y(z) = \frac{z}{z-a} \stackrel{\mathcal{Z}^{-1}}{\to} y(k) = a^k$$

Hence, $y(k) \to 0$ and does not depend on u(k). The zero of H(z) in b thus blocks the input $u(k) = b^k$.

Blocking Zeros

Consider

$$x(k+1) = \Phi x(k) + \Gamma u(k)$$
$$y(k) = Cx(k) + Du(k)$$

A zero in a means blocking of inputs a^k . Then for the system above, the input a^k gives zero output for z=a such that $\det \begin{bmatrix} zI - \Phi & -\Gamma \\ C & D \end{bmatrix} = 0.$

Pole Locations of Sampled System

Suppose

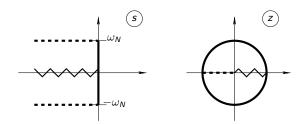
$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$

has poles $\lambda_i(A)$, i = 1, ..., n. Then,

$$x(kh + h) = \Phi x(kh) + \Gamma u(kh)$$
$$y(kh) = Cx(kh) + Du(kh)$$

has poles $\exp(\lambda_i(A)h)$. Follows from $\Phi = \exp(Ah)$.

Pole Mapping Through $z = \exp(sh)$



The mapping $s \mapsto \exp(sh)$ is not invertible. Several points of the *s*-plane are mapped into the *z*-plane.

The pole z = 0 has no counterpart in s-plane.

The left half plane of the *s*-domain is mapped into the unit disc of the *z*-plane. What might this imply?

Zero Locations of Sampled System

Zeros in s-domain is not easily mapped to z-domain.

Example:

$$G(s) = \frac{1}{s^2}$$
 is sampled into $H(q) = \frac{q+1}{2(q-1)^2}$.

G(s) has no zero, but H(q) has zero in z=-1.

The sampling procedure gives more zeros.

Next Lecture

Analysis of sampled control

- Stability
- Reachability and observability
- Observers
- State and output feedback