

Exercise Problems — Part 2

(Due Date: Tuesday, 06.10.15, before the lecture. You can also put the solutions in the red box outside office FY277.)

1. Atmospheric Drag

(a) Check from a source of your choice what is the structure of the *upper* part of Earth's atmosphere. Describe briefly the different parts and altitude ranges. What densities are expected there, roughly?

(b) Derive the equation given in the lecture

$$\frac{de}{dt} = -\frac{C_d A \rho}{m} v (e + \cos f) .$$

for the slow evolution of the eccentricity under the influence of atmospheric drag.

(c) Solve the equation for the slow evolution of the semi-major axis

$$\frac{da}{dt} = -\frac{C_d A \rho}{m} \frac{a^2}{\mu} v^3$$

for the case of constant density ρ and $e = 0$.

2. Advanced: Slow evolution of the longitude of the ascending node

Show that the general evolution equation for the longitude of the ascending node reads

$$\frac{d\Omega}{dt} = \sqrt{\frac{a(1-e^2)}{\mu}} N \frac{\sin \varphi}{1+e \cos f} .$$

Hint: Use the relations given in the lecture and express the longitude of the ascending node in terms of components of the angular momentum vector as

$$\tan \Omega = -\frac{h_x}{h_y} .$$

Also, you must express the unit vectors normal to the orbital plane and in azimuthal direction, \vec{e}_N and \vec{e}_φ , respectively, in terms of Ω , i , and $\varphi = \varpi + f$ as

$$\vec{e}_N = \begin{pmatrix} \sin i \sin \Omega \\ -\sin i \cos \Omega \\ \cos i \end{pmatrix}, \quad \text{and} \quad \vec{e}_\varphi = \begin{pmatrix} -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi \\ -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi \\ \sin i \cos \varphi \end{pmatrix} .$$

Keep in mind that the angular momentum vector points in the direction of \vec{e}_N .

Exercise Problems Part 2

(1)

1. Atmospheric Drag

c) Exosphere — 700 km to 10,000 km
molecular or ballistic trajectories, no
collisions, practically

$$\rho \sim 10^{-14} \frac{\text{kg}}{\text{m}^3}$$

Thermosphere — 80 km to ~~700 km~~
or 1000 km
height depends on solar activity

80 - 500 km: the Ionosphere

Mesosphere — 50 km to 80 km, to high for spacecraft
to low for spacecraft

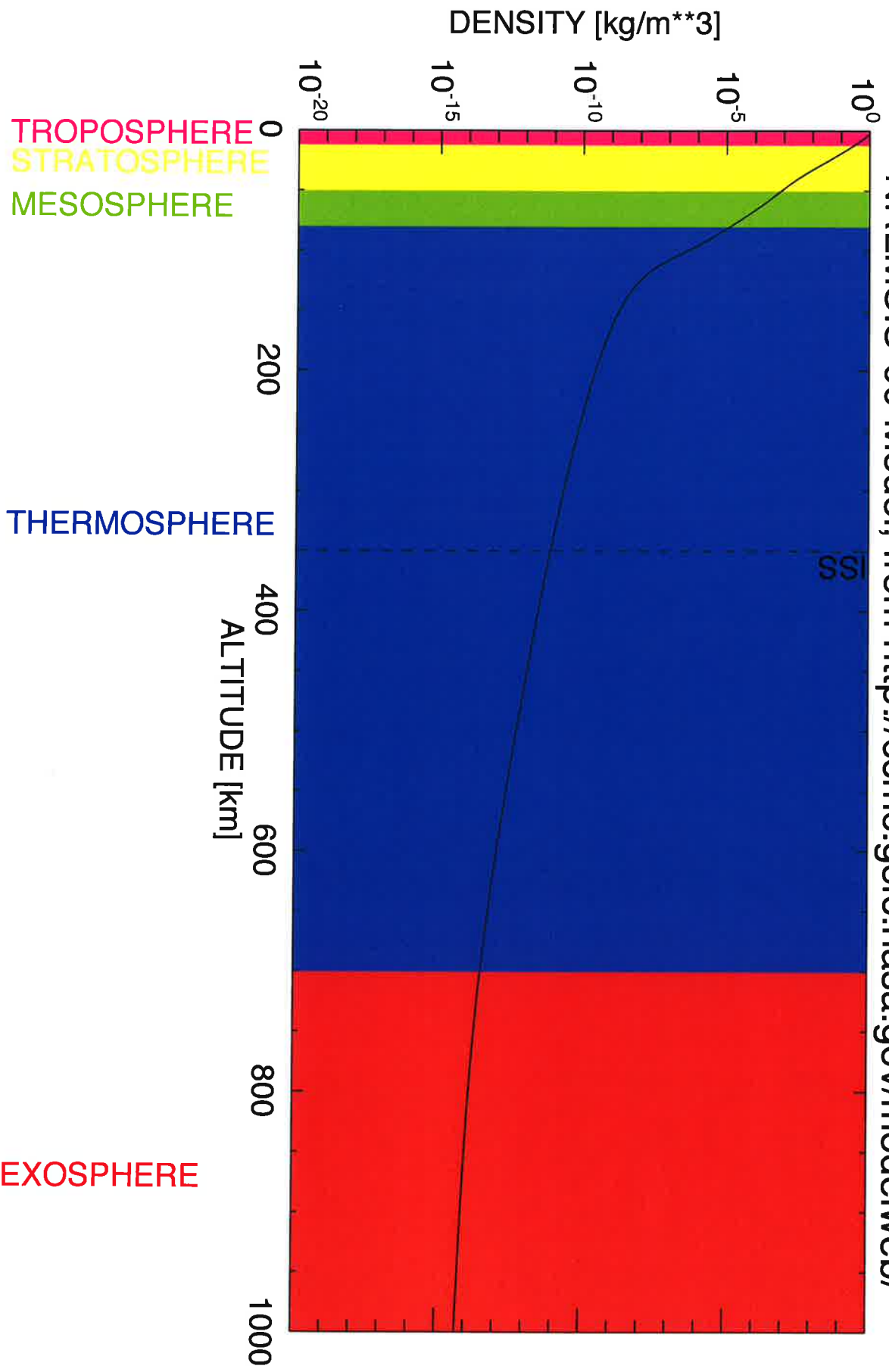
Stratosphere — 12 km to 50 km;

Troposphere — 0 km to 12 km

contains about 80% of mass of the atmosphere

c2)

NRLMSIS-00 Model, from <http://ccmc.gsfc.nasa.gov/modelweb/>



(3)

(15) Lecture:

$$\frac{de}{dt} = \sqrt{\frac{a(1-e^2)}{a}} \left[R \sin f + T \cos f + \frac{T}{e} \left(1 - \frac{r}{a} \right) \right]$$

radial component of force

azimuthal component of force

For atmospheric drag (lecture):

$$R = - \frac{C_d A \rho}{2m} v \frac{h}{a(1-e^2)} e \sin f$$

$$T = - \frac{C_d A \rho}{2m} v \frac{h}{r}$$

$$\Rightarrow \frac{de}{dt} = \sqrt{\frac{a(1-e^2)}{a}} \left[- \frac{C_d A \rho}{2m} v \frac{h}{a(1-e^2)} \left\{ e \sin^2 f + \cos f (1 + e \cos f) + \frac{1}{e} \left(1 - \frac{1-e^2}{1+e \cos f} \right) \right\} \right]$$

$$= - \frac{C_d A \rho}{2m} v \left\{ e \sin^2 f + \cos f + e \cos^2 f + \frac{1}{e} (4e \cos f - 1 + e^2) \right\}$$

$= \cos f + e$

$$= - \frac{C_d A \rho}{2m} v \left\{ e + \cos f + \cos f + e \right\}$$

$$= - \frac{C_d A \rho}{m} v (e + \cos f)$$

(4)

$$(c) \frac{da}{dt} = - \frac{c \Gamma A P}{m} \frac{a^2}{\mu} v^3$$

$$P = \text{const}; e = 0$$

$$\Rightarrow v = \Omega a = \sqrt{\frac{\mu}{a}}$$

$$\Rightarrow \frac{da}{dt} = - \frac{c \Gamma A P}{m} \frac{a^2}{\mu} \left(\frac{\mu}{a} \right)^{3/2}$$

$$= - \frac{c \Gamma A P}{m} \sqrt{a \mu}$$

$$\text{let } a = x \cdot a_0$$

\uparrow characteristic scale

(e.g. initial semi-major axis)

$$t = \tau \cdot \theta$$

\uparrow characteristic timescale

$$\Rightarrow \frac{a_0}{\theta} \frac{dx}{d\tau} = - \frac{c \Gamma A P}{m} \cancel{a_0^2} \sqrt{a_0 \mu} \sqrt{x}$$

$$\frac{dx}{d\tau} = - \theta \frac{c \Gamma A P}{m} \sqrt{\frac{\mu}{a_0}} \sqrt{x}$$

$$\underbrace{\hspace{1cm}}_{\text{choose } \theta = \frac{c \Gamma A P}{m} \sqrt{\frac{\mu}{a_0}}}$$

$$\Rightarrow \boxed{\frac{dx}{d\tau} = - \sqrt{x}}$$

$$\frac{dx}{\sqrt{x}} = -d\tau$$

(5)

$$\Rightarrow 2 d\sqrt{x} = -d\tau$$

$$\Rightarrow d\left(\sqrt{x} + \frac{\tau}{2}\right) = 0$$

$$\Rightarrow \sqrt{x} + \frac{\tau}{2} = \text{const}$$

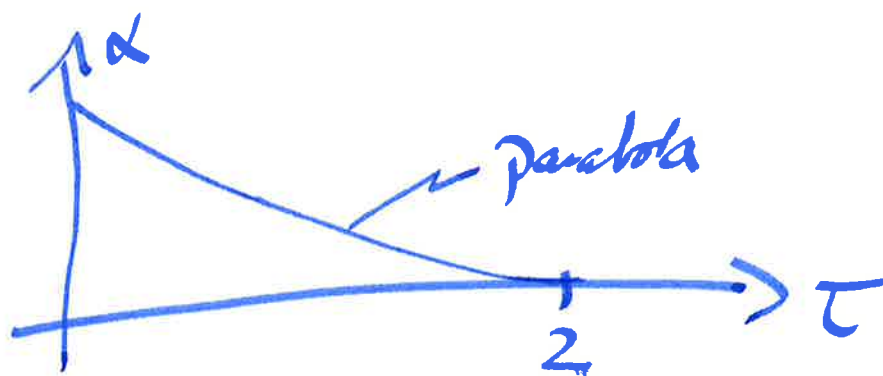
$$\equiv \sqrt{x_0} = \sqrt{x(\tau=0)} \stackrel{\uparrow}{=} 1$$

if we take $a_0 = a(t=0)$

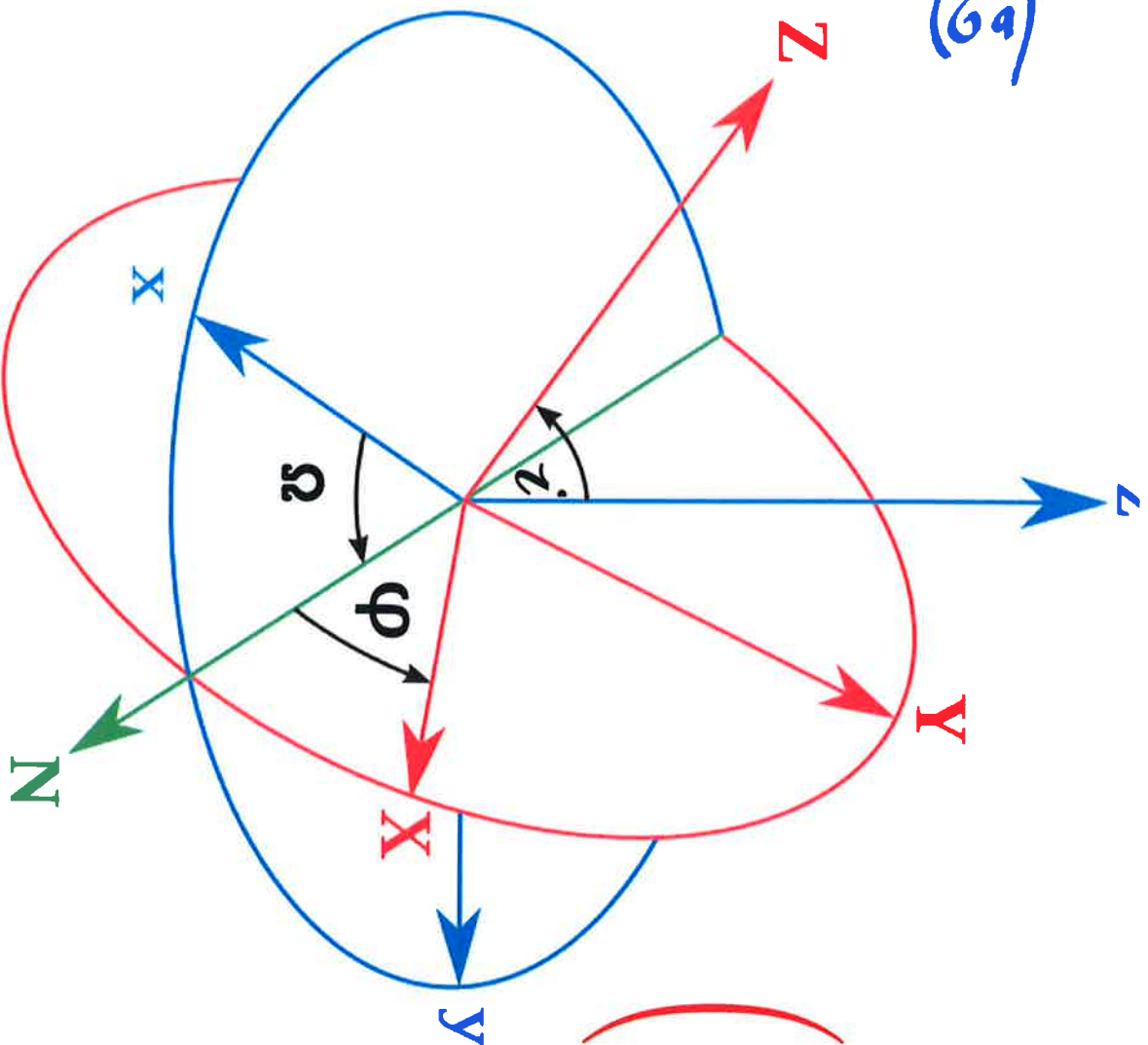
$$\Rightarrow x = \left(1 - \frac{\tau}{2}\right)^2$$

$$a = a_0 \left(1 - \frac{1}{2} \frac{t}{\theta}\right)^2$$

$$a = a_0 \left[1 - \frac{1}{2} \frac{GAS}{m} \sqrt{\frac{m}{a_0}} t\right]^2$$



(6a)



xyz - inertial frame

XYZ - cartesian frame

with XY = orbit

plane

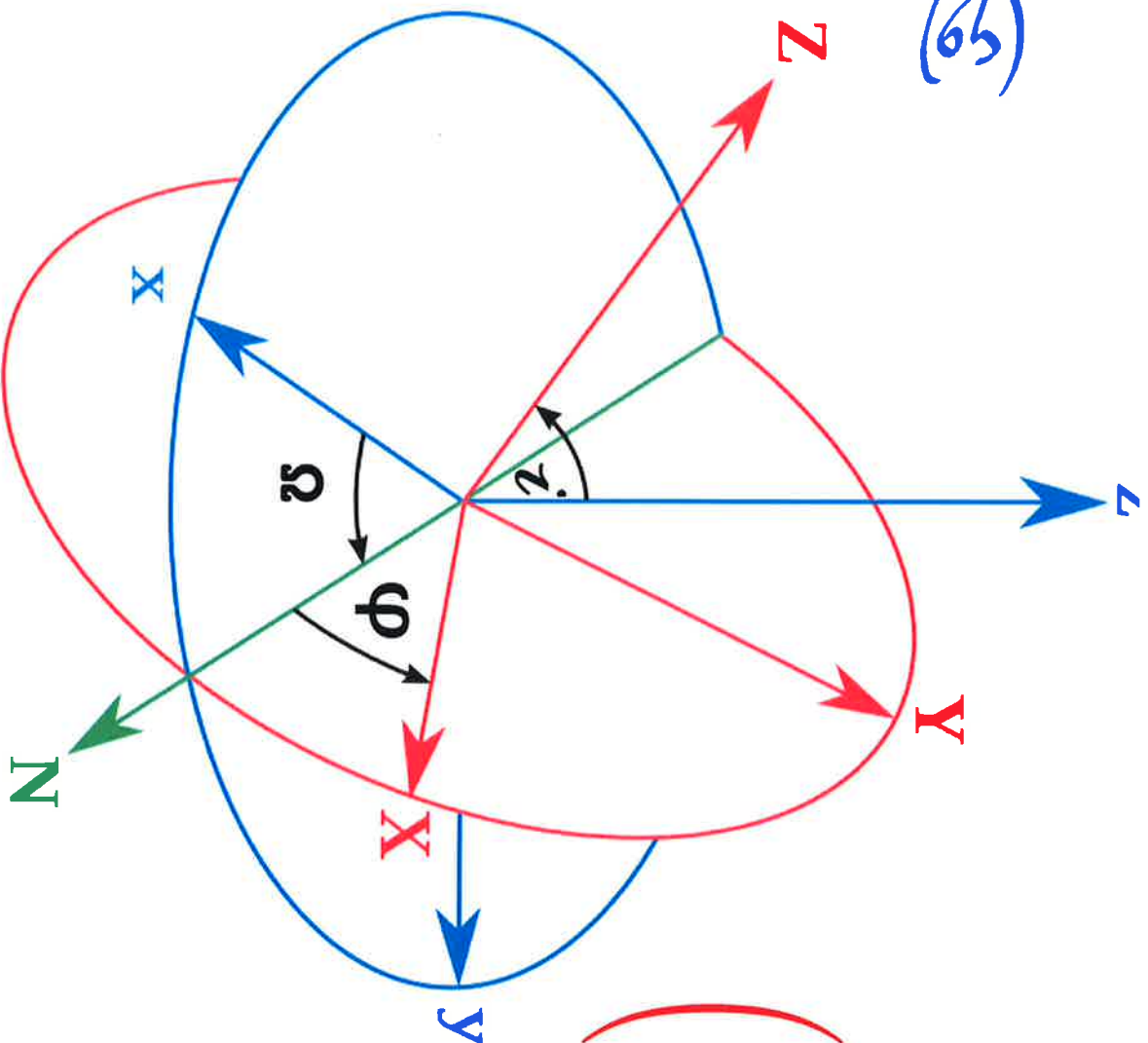
$$\begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = B C D \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$D = \begin{pmatrix} \cos \Omega & \sin \Omega & 0 \\ -\sin \Omega & \cos \Omega & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$C = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos i & \sin i \\ 0 & -\sin i & \cos i \end{pmatrix}$$

$$B = \begin{pmatrix} \cos \varphi & \sin \varphi & 0 \\ -\sin \varphi & \cos \varphi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

(65)

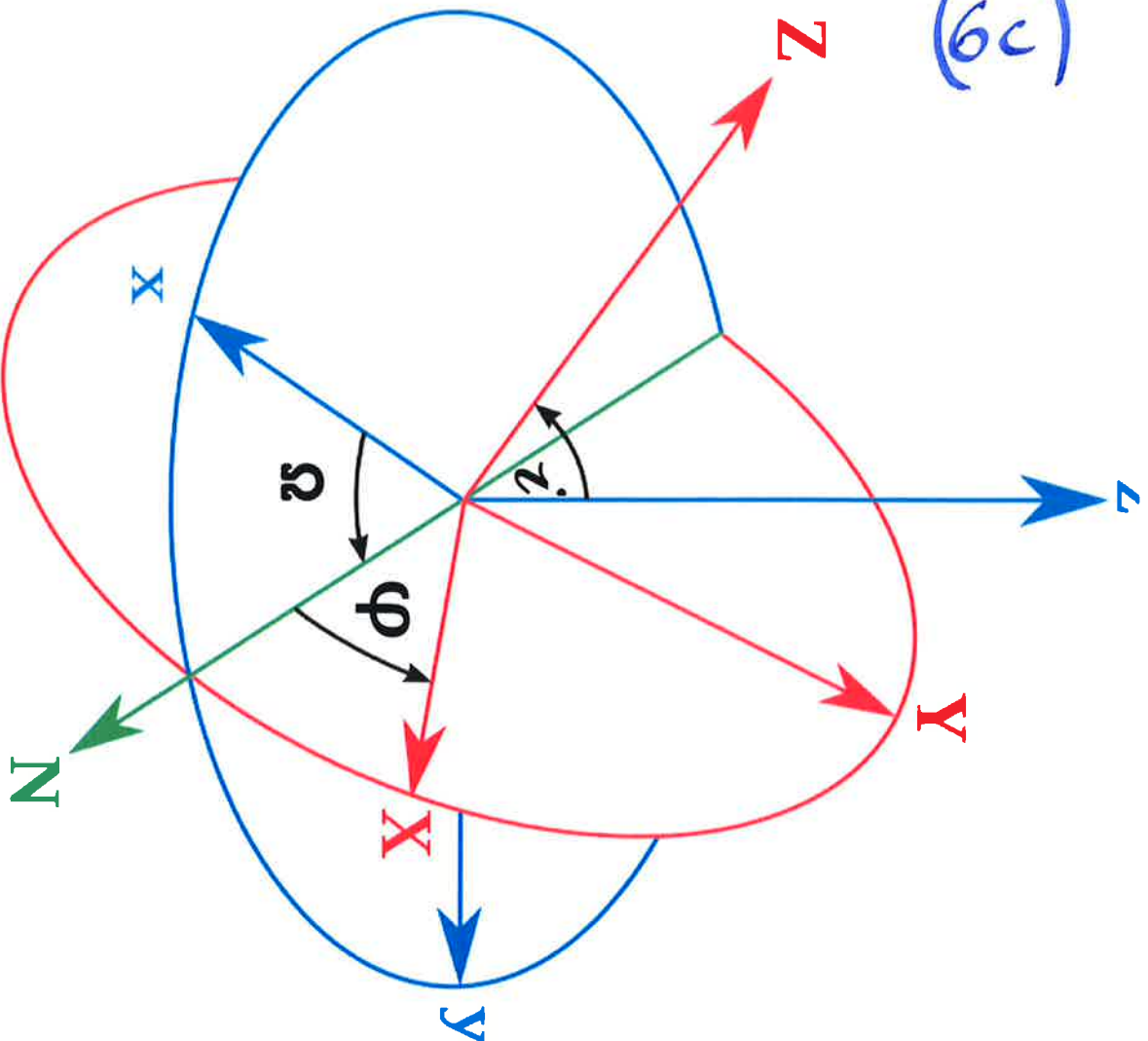


xyz - inertial frame
XYZ - cartesian frame
with XY = orbit plane

$$\begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = BCD \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$BCD = \begin{pmatrix} \cos \varphi \cos \Omega - \cos i \sin \Omega \sin \varphi & \cos \varphi \sin \Omega + \cos i \cos \Omega \sin \varphi & \sin i \sin \varphi \\ -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi & -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi & \sin i \cos \varphi \\ \sin i \sin \Omega & -\sin i \cos \Omega & \cos i \end{pmatrix}$$

(6c)

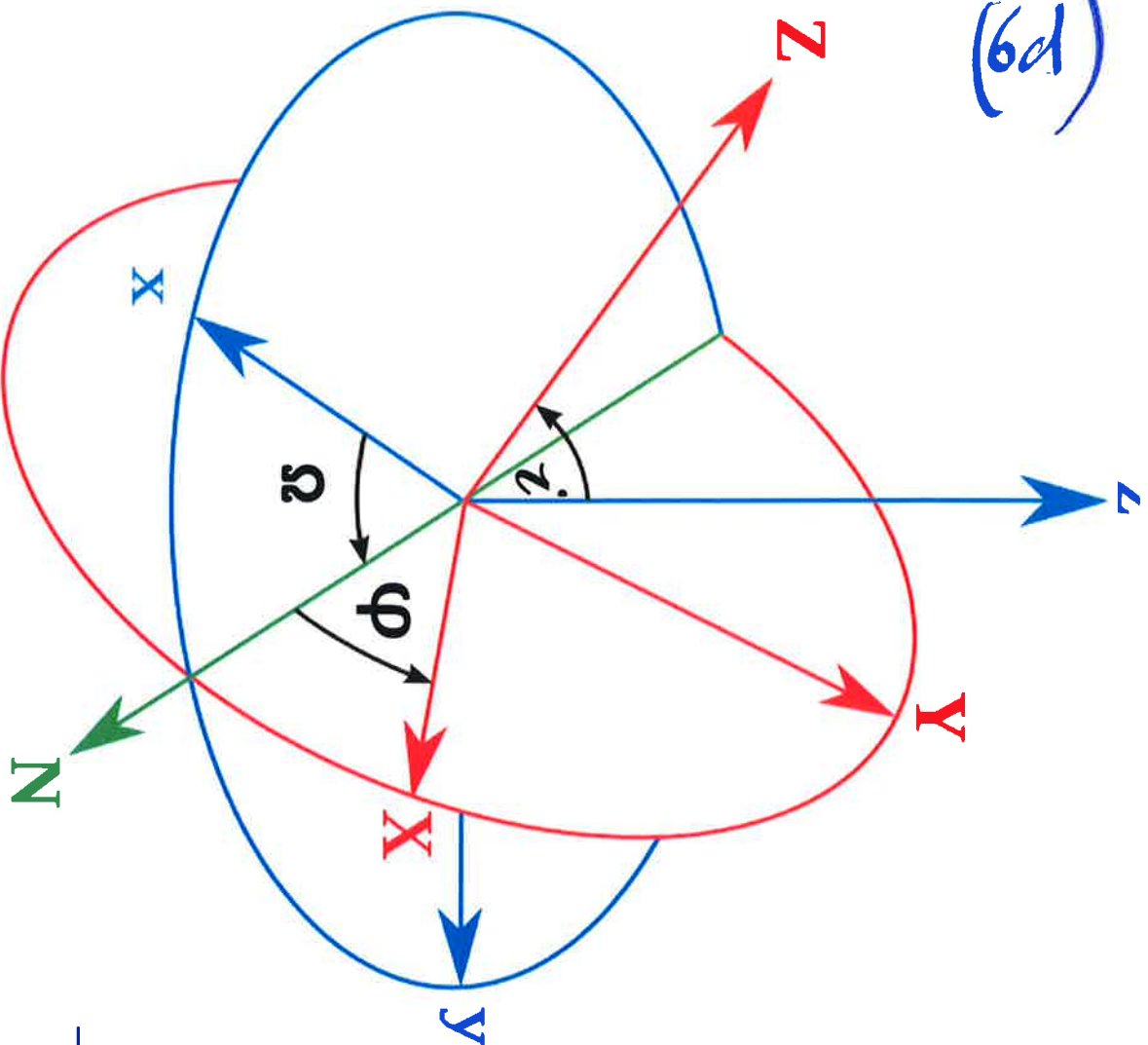


xyz - inertial frame
XYZ - cartesian frame
with XY = orbit plane

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = (BCD)^{-1} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

$$(BCD)^{-1} = \begin{pmatrix} \cos \varphi \cos \Omega - \cos i \sin \Omega \sin \varphi & -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi & \sin i \sin \Omega \\ \cos \varphi \sin \Omega + \cos i \cos \Omega \sin \varphi & -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi & -\sin i \cos \Omega \\ \sin i \sin \varphi & \sin i \cos \varphi & \cos i \end{pmatrix}$$

(6d)



xyz - inertial frame
XYZ - cartesian frame
with XY = orbit plane

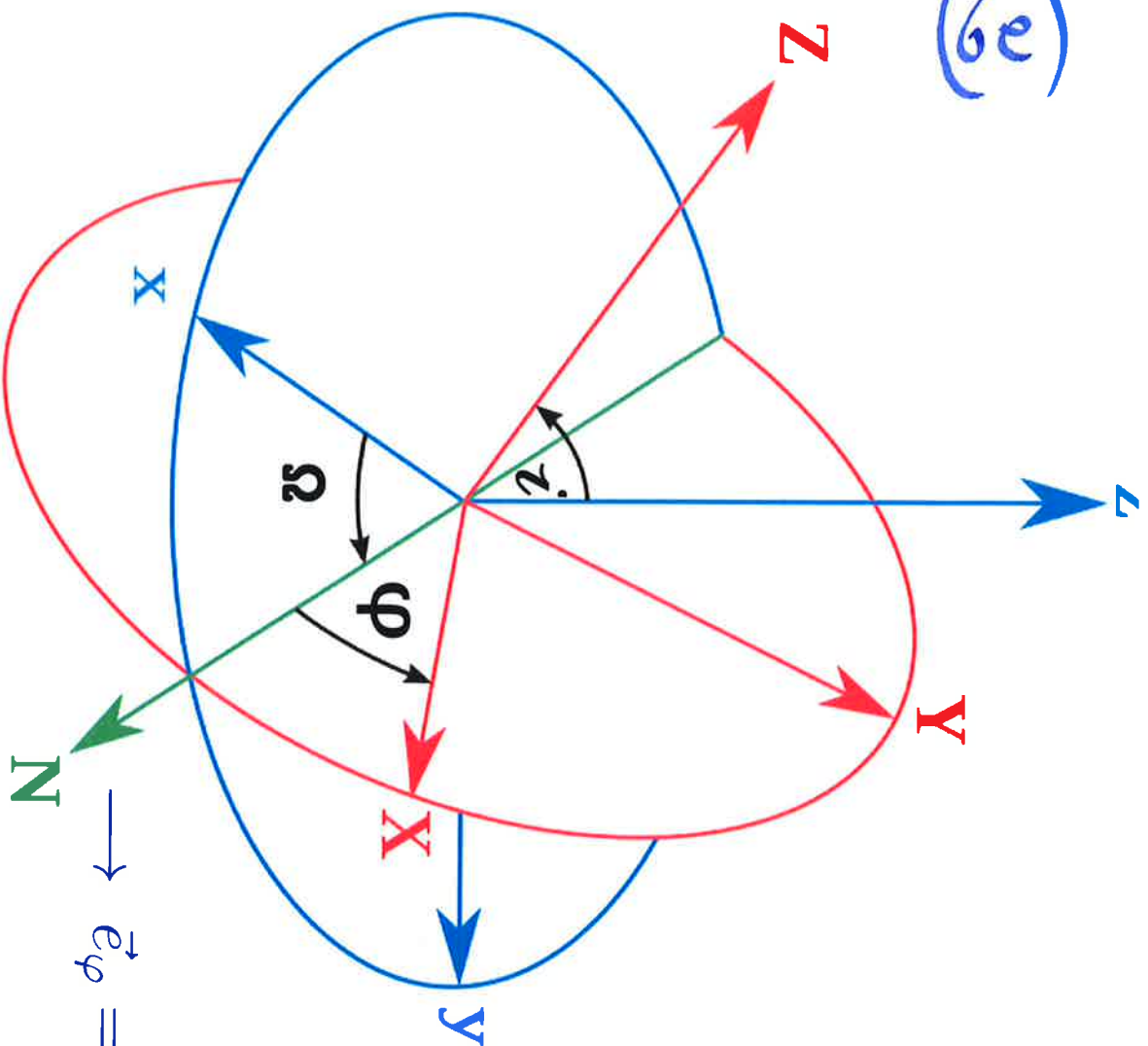
$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = (BCD)^{-1} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

$$\vec{e}_N = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

$$\rightarrow \vec{e}_N = \begin{pmatrix} \sin i \sin \Omega \\ -\sin i \cos \Omega \\ \cos i \end{pmatrix}$$

$$(BCD)^{-1} = \begin{pmatrix} \cos \varphi \cos \Omega - \cos i \sin \Omega \sin \varphi & -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi & \sin i \sin \Omega \\ \cos \varphi \sin \Omega + \cos i \cos \Omega \sin \varphi & -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi & -\sin i \cos \Omega \\ \sin i \sin \varphi & \sin i \cos \varphi & \cos i \end{pmatrix}$$

(6e)



xyz - inertial frame
XYZ - cartesian frame
with XY = orbit plane

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix} = (BCD)^{-1} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

$$\vec{e}_\varphi = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$\vec{N} \rightarrow \vec{e}_\varphi = \begin{pmatrix} -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi \\ -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi \\ \sin i \cos \varphi \end{pmatrix}$$

$$(BCD)^{-1} = \begin{pmatrix} \cos \varphi \cos \Omega - \cos i \sin \Omega \sin \varphi & -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi & \sin i \sin \Omega \\ \cos \varphi \sin \Omega + \cos i \cos \Omega \sin \varphi & -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi & -\sin i \cos \Omega \\ \sin i \sin \varphi & \sin i \cos \varphi & \cos i \end{pmatrix}$$

(2) To show: $\frac{dR}{dt} = \sqrt{\frac{a(1-e^2)}{u}} N \frac{\sin \phi}{1+e \cos \phi}$

(6) 4

starting from $\frac{d\mathbf{h}}{dt} = r(\mathbf{T} \mathbf{e}_N - N \mathbf{e}_f)$

unit vector
tangent to the orbit
direction
unit vector normal to
the plane: $\mathbf{h} = h \mathbf{e}_N$

and $\tan \Omega = -\frac{h_x}{h_y}$

$\Rightarrow \frac{d}{dt} \tan \Omega = -\frac{d}{dt} \frac{h_x}{h_y}$

$\Rightarrow \frac{1}{\cos^2 \Omega} \frac{d\Omega}{dt} = -\frac{\frac{dh_x}{dt} h_y - h_x \frac{dh_y}{dt}}{h_y^2}$

$\frac{d}{dt} \tan \Omega = \frac{d}{dt} \frac{\sin \Omega}{\cos \Omega}$
 $= \frac{\cos \Omega \cos \Omega + \sin \Omega \sin \Omega}{\cos^2 \Omega} \frac{d\Omega}{dt}$
 $= \frac{1}{\cos^2 \Omega} \frac{d\Omega}{dt}$

$\Rightarrow \boxed{\frac{d\Omega}{dt} = \frac{h_x \frac{dh_y}{dt} - h_y \frac{dh_x}{dt}}{h_y^2} \cos^2 \Omega}$

(7)

from $\frac{d\tilde{h}}{dt} = r (\tilde{T}_v - N \tilde{e}_\varphi)$

we have

$$\frac{dh_x}{dt} = r (\tilde{T}_v^x - N e_\varphi^x)$$

x-components of these vectors

$$\frac{dh_y}{dt} = r (\tilde{T}_v^y - N e_\varphi^y)$$

and $h_x = h e_v^x$; $h_y = h e_v^y$; from $\tilde{h} = h \tilde{e}_v$

$$\Rightarrow \frac{d\Omega}{dt} = \frac{\omega^2 \Omega}{h^2 (e_v^y)^2} \left[h e_v^x r (\tilde{T}_v^y - N e_\varphi^y) - h e_v^y r (\tilde{T}_v^x - N e_\varphi^x) \right]$$

these cancel

$$= \frac{\omega^2 \Omega}{h (e_v^y)^2} r N [e_v^y e_\varphi^x - e_v^x e_\varphi^y]$$

(8)

$$e_N^y = -\sin i \cos \Omega ; e_N^x = \sin i \sin \Omega$$

$$e_\varphi^x = -\sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi$$

$$e_\varphi^y = -\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi$$

$$\Rightarrow \frac{d\Omega}{dt} = \frac{\cancel{\cos^2 \Omega}}{h \sin^2 i \cancel{\cos^2 \Omega}} rN \left[\cancel{\sin i} \left(\cancel{\cos \Omega} \right) - \sin \varphi \cos \Omega - \cos i \sin \Omega \cos \varphi \right] \\ - \sin \Omega \left(-\sin \varphi \sin \Omega + \cos i \cos \Omega \cos \varphi \right) \right]$$

$$= \frac{1}{h \sin i} \left\{ + \cos^2 \Omega \sin \varphi + \sin^2 \Omega \sin \varphi \right\} rN$$

$$= \frac{rN}{h \sin i} \sin \varphi ; r = \frac{a(1-e^2)}{1+e \cos \varphi} ; h = \sqrt{\mu a(1-e^2)}$$

$$\Rightarrow \left| \frac{d\Omega}{dt} = \sqrt{\frac{a(1-e^2)}{\mu}} N \frac{\sin \varphi}{1+e \cos \varphi} \right|$$