## **Appendix C: Gear calculations**

In **Appendix B** the 100 rpm motor was selected. Its calculated properties are listed below:

The maximum motor

current:

$$I_{max} = 2.936 \; A$$

The maximum output torque:

$$T_{max} = 1.211 \ N \cdot m$$

The maximum output speed:

$$w_{max} = 11.367 \frac{rad}{s}$$

The maximum overload time to trip:

$$t_{max\_trip} = 3.091 \ s$$

In **Appendix A** the required bending moment to bend the pipe was determined to be the following:

Bending moment required to bend the pipe:

$$M_{required} \coloneqq 12.922 \ \textit{N} \cdot \textit{m}$$

Before selecting the gears, the required gear ratio needs to be determined. The required gear ratio will be determined using the required bending moment and the peak output torque of the motor.

Required gear ratio:

$$GR_{required} \coloneqq \frac{M_{required}}{T_{max}}$$

$$GR_{required} = 10.671$$

Therefore, the gear train ratio has to be equal to the required gear ratio taking into account all the efficiencies.

Through trial and error, and taking into account the shape of the model and the user requirements. Below is how the gear train is designed.

Gears	Driven by	Drives	On the same shaft as
12T spur gear	The motor	36T spur gear	-
36T spur gear	12T spur gear	-	24T bevel gear
24T bevel gear	-	24T bevel gear	36T spur gear
24T bevel gear	24T bevel gear	-	12T spur gear
12T spur gear	<del>-</del>	36T spur gear	24T bevel gear
36T spur gear	12T spur gear	-	24T spur gear
24T spur gear	1	48T spur gear	36T spur gear
48T spur gear	24T spur gear	-	-

Figure 2: Table summarising the gearbox design.

In the table above each gear is given its own colour to make it easy for the reader to follow. The table also shows which gears are driven, which gears drives and which gears are on the same shaft.

Using figure 1 and 2, the meshing gears can be shown in the table below.

	Meshing gears
Mesh 1	12T spur gear with 36T spur gear
Mesh 2	24T bevel gear with 24T bevel gear
Mesh 3	12T spur gear with 36T spur gear
Mesh 4	24T spur gear with 48T spur gear
Mesh 5	48T spur gear with 48T spur gear

Figure 3: Table showing meshing gears

Using the above table, the gear train efficiency can be calculated

$$\eta_{spur} = 1 - \mu \pi \left( \frac{1}{Z_1} + \frac{1}{Z_2} \right)$$

The above equation from the gearbox efficiency document will be used to calculate the efficiency between two meshing spur gears.

The same equation will be used to calculate the efficiency for bevel gears because the friction on bevel gears is very similar to spur gears.

Assuming that the gear that will be used is made up of Dry Acetal on Acetal plastic, the coefficient that will be used is 0.2.

Mesh 1 (12T spur gear with 36T spur gear):

$$\eta_{mesh\_1} \coloneqq 1 - 0.2 \cdot \boldsymbol{\pi} \cdot \left(\frac{1}{12} + \frac{1}{36}\right)$$

$$\eta_{mesh\_1}\!=\!0.93$$

Mesh 2 (24T bevel gear with 24T bevel gear):

$$\eta_{mesh_2} := 1 - 0.2 \cdot \pi \cdot \left(\frac{1}{24} + \frac{1}{24}\right)$$

$$\eta_{mesh\_2}\!=\!0.948$$

Mesh 3 (12T spur gear with 36T spur gear):

$$\eta_{mesh\_3} := 1 - 0.2 \cdot \pi \cdot \left(\frac{1}{12} + \frac{1}{36}\right)$$

$$\eta_{mesh\_3}\!=\!0.93$$

Mesh 4 (24T spur gear with 48T spur gear):

$$\eta_{mesh\_4} \coloneqq 1 - 0.2 \cdot \boldsymbol{\pi} \cdot \left(\frac{1}{24} + \frac{1}{48}\right)$$

$$\eta_{mesh\_4}$$
 = 0.961

Mark 5 (40T annu annuith	
Mesh 5 (48T spur gear with 48T spur gear):	$\eta_{mesh\_5} \coloneqq 1 - 0.2 \cdot \pi \cdot \left(\frac{1}{48} + \frac{1}{48}\right)$
	$\eta_{mesh\_5}\!=\!0.974$
Now that the efficiency for all the be determined.	meshing gears is determined, the gear train efficiency can
Gear train efficiency:	$\eta_{gear\_train} \coloneqq \eta_{mesh\_1} \cdot \eta_{mesh\_2} \cdot \eta_{mesh\_3} \cdot \eta_{mesh\_4} \cdot \eta_{mesh\_5}$
	$\eta_{gear\_train}$ $=$ $0.767$
The gear ratio of the gearbox can gears.	be determined using figure 3, taking into only meshing
Gear 1 (12T spur gear with 36T spur gear):	$GR_1$ := $\frac{36}{12}$
	$GR_1 = 3$
Gear 2 (24T bevel gear with 24T bevel gear):	$GR_2$ := $\frac{24}{24}$
	$GR_2 \!=\! 1$
Gear 3 (12T spur gear with 36T spur gear):	$GR_3 \coloneqq \frac{36}{12}$
	$GR_3 = 3$

Gear 4 (24T spur gear with 48T spur gear):	$GR_4 \coloneqq \frac{48}{24}$
	$GR_4 = 2$
Gear 5 (48T spur gear with 48T spur gear):	$GR_5 \coloneqq \frac{48}{48}$
	$GR_5 \!=\! 1$
Now that the gear ratio for all the determined, taking into account the	meshing gears is determined, the gear train ratio can be ne efficiency.
Gear train ratio:	$GR_{gear\_train} \coloneqq GR_1 \boldsymbol{\cdot} GR_2 \boldsymbol{\cdot} GR_3 \boldsymbol{\cdot} GR_4 \boldsymbol{\cdot} GR_5 \boldsymbol{\cdot} \eta_{gear\_train}$
	$GR_{gear\_train} \!=\! 13.808$
The gear train ratio works out per is $GR_{required}\!=\!10.671$ .	fectly because it greater than the required gear ratio, which
Now the actual current, output tor calculated.	rque, output speed and trip time for the motor can be
Actual output motor torque:	$T_{actual} \coloneqq rac{M_{required}}{GR_{gear\_train}}$
	$T_{actual}$ = 0.936 $ extbf{ extit{N}} \cdot  extbf{ extit{m}}$
Output torque $[Nm]$ $T_{m} = I$	$I_m K_T r_g \eta_g - T_0$ $I_m = \text{motor current}$

Figure 4: Motor torque equation

The above equation is from the motor specification document, it will be used to calculate the

operating motor current. The motor specifica constant in the equation.	tion document also gives the values for the
Gearbox reduction ratio:	$r_g \coloneqq 156.8$
Gearbox efficiency:	$\eta_g\!\coloneqq\!0.7$
Static drag:	$T_0 \coloneqq 110 \cdot N \cdot mm$
Torque constant:	$K_T \coloneqq 4.1 \; N \cdot \frac{mm}{A}$
Armature resistance:	$R_a \coloneqq 1.87 \; \Omega$
Operating motor current:	$I_{actual} \coloneqq rac{T_{actual} - T_0}{K_T \! \cdot \! r_g \! \cdot \! \eta_g}$
	$I_{actual}\!=\!1.835~ extbf{ ex}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}$
Output speed $[rad/s]$ $\omega_{m} = \frac{V_{b} - I_{m}R_{a}}{K_{T}r_{g}}$	$V_b$ = supply voltage
Figure 5: Motor speed equation	
The above equation is from the motor specifi motor output speed.	cation document, it will be used to calculate the
Supply voltage to the motor calculated in Appendix B:	$V_{supply}$ := 12.8 $oldsymbol{V}$
Motor output speed:	$w_{actual} \coloneqq rac{V_{supply} \! - \! I_{actual} \! \cdot \! R_a}{K_T \! \cdot \! r_g}$
	$w_{actual}\!=\!14.573~rac{oldsymbol{rad}}{oldsymbol{s}}$
	/ T \_3.54

Overload time to trip:	$t_{actual\_trip} \coloneqq 14$	$0 \cdot \left(\frac{I_{actual}}{1 \cdot A}\right)$ $\cdot s$
	$t_{actual\_trip} {=}\ 16.$	322 s
	Dools on dition	

	Peak condition	Actual condition
Current [A]	2.936	1.847
Output speed [rad/s]	11.367	14.537
Output torque [Nm]	1.211	0.941
Trip time [s]	3.091	15.948

Figure 6: Comparing peak conditions and actual conditions

The table above the shows the difference when the motor is operating at its peak and at its actual point.

Now the torque and forces experienced by each gear can calculated. The efficiencies for all the meshing gears are calculated.

## Gear 1

Gear 1 is a spur gear driven by the motor through a shaft.

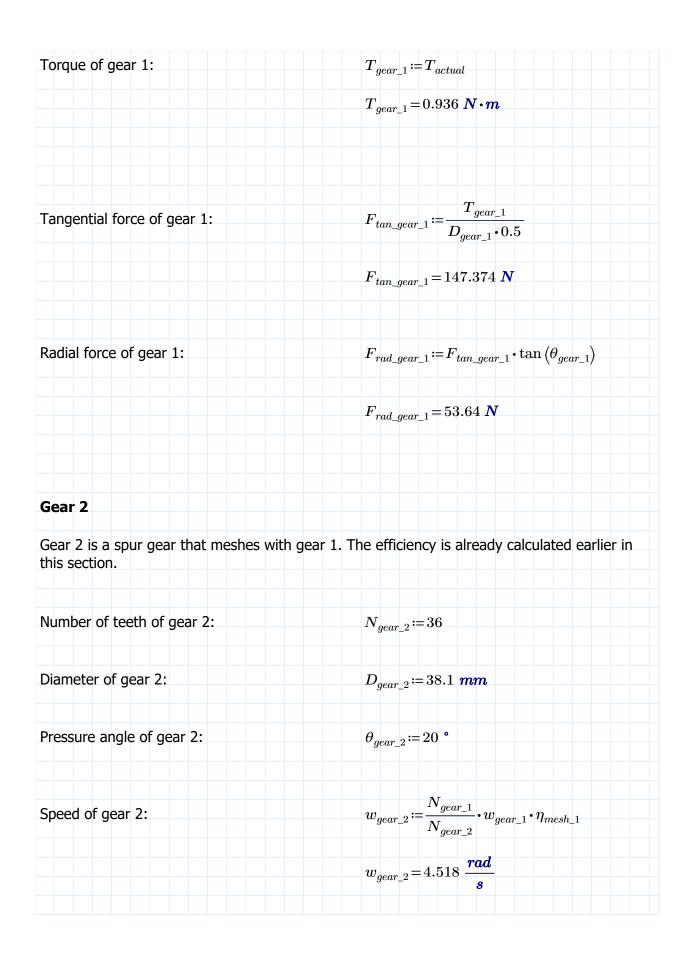
Number of teeth of gear 1:  $N_{gear\_1} \coloneqq 12$ 

Diameter of gear 1:  $D_{gear\_1} = 12.7 \ \textit{mm}$ 

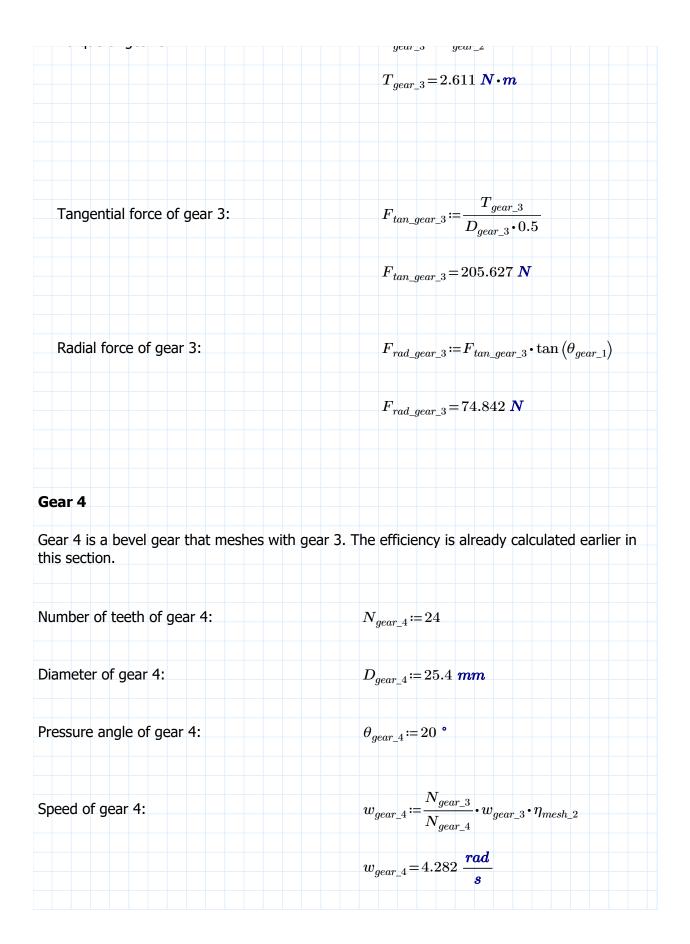
Pressure angle of gear 1:  $\theta_{gear\_1} \coloneqq 20$  °

Speed of gear 1:  $w_{gear\_1} \coloneqq w_{actual}$ 

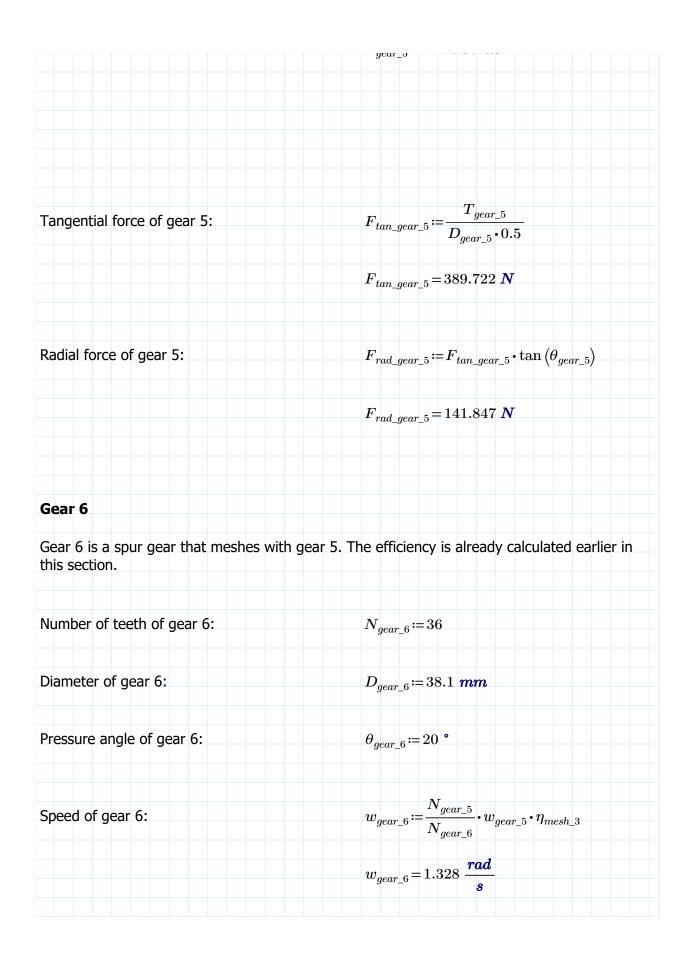
 $w_{gear\_1} = 14.573 \frac{rad}{s}$ 



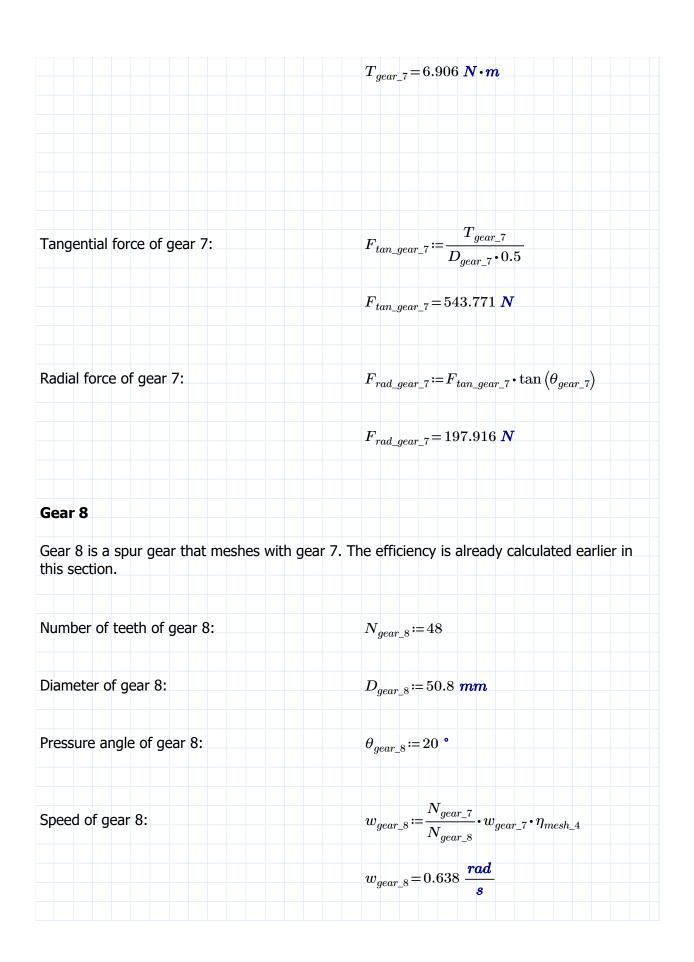
Torque of gear 2:	$T_{gear\_2} \coloneqq rac{N_{gear\_2}}{N_{gear\_1}} { extbf{ iny }} T_{gear\_1} { extbf{ iny }} \eta_{mesh\_1}$
	$T_{gear\_2} \!=\! 2.611~ extbf{ extbf{N}} \! \cdot \!  extbf{m}$
Tangential force of gear 2:	$F_{tan\_gear\_2}\!\coloneqq\!rac{T_{gear\_2}}{D_{gear\_2}\!\cdot\!0.5}$
	$F_{tan\_gear\_2}\!=\!137.085~ extbf{ extit{N}}$
Radial force of gear 2:	$\boldsymbol{F}_{rad\_gear\_2} \!\coloneqq\! \boldsymbol{F}_{tan\_gear\_2} \!\cdot\! \tan \left(\boldsymbol{\theta}_{gear\_2}\right)$
	$F_{rad\_gear\_2}\!=\!49.895~ extbf{ extf{ extbf{ extf{ extbf{ ex}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}$
Gear 3	
Gear 3 is a bevel gear and is on the	shaft as gear 2.
Number of teeth of gear 3:	$N_{gear\_3}\!\coloneqq\!24$
Diameter of gear 3:	$D_{gear\_3}\!\coloneqq\!25.4$ $m{mm}$
Pressure angle of gear 3:	$ heta_{gear\_3}\!\coloneqq\!20$ °
Speed of gear 3:	$w_{gear\_3} \coloneqq w_{gear\_2}$
	$w_{gear\_3}\!=\!4.518rac{oldsymbol{rad}}{oldsymbol{s}}$
Torque of gear 3:	$T_{\text{corn}} \circ := T_{\text{corn}} \circ$



Torque of gear 4:	$T_{gear\_4} \coloneqq rac{N_{gear\_4}}{N_{gear\_3}} ullet T_{gear\_3} ullet \eta_{mesh\_2}$
	$T_{gear\_4}\!=\!2.475~ extbf{ extbf{N}}\!\cdot\! extbf{m}$
Tangential force of gear 4:	$egin{aligned} F_{tan\_gear\_4} \coloneqq & rac{T_{gear\_4}}{D_{gear\_4} \cdot 0.5} \end{aligned}$
	$F_{tan\_gear\_4} \!=\! 194.861~  extbf{ extit{N}}$
Radial force of gear 4:	$F_{rad\_gear\_4} \coloneqq F_{tan\_gear\_4} \cdot  an\left( heta_{gear\_4} ight)$
	$F_{rad\_gear\_4}\!=\!70.924~ extbf{ extf{ extbf{ extbf{ extbf{ extbf{ extbf{ extbf{ extf{ extbf{ ex}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}$
Gear 5	
Gear 5 is a spur gear and it's on the sl	haft as gear 4.
Number of teeth of gear 5:	$N_{gear\_5}$ := $12$
Diameter of gear 5:	$D_{gear\_5} \coloneqq 12.7$ $m{mm}$
Pressure angle of gear 5:	$ heta_{gear\_5}\!\coloneqq\!20$ °
Speed of gear 5:	$w_{gear\_5}\!\coloneqq\!w_{gear\_4}$
	$w_{gear\_5}\!=\!4.282rac{oldsymbol{rad}}{oldsymbol{s}}$
Torque of gear 5:	$T_{gear\_5}\!\coloneqq\!T_{gear\_4}$
	$T_{\text{con}} = 2.475  N \cdot m$



Torque of gear 6:	$T_{gear\_6} \coloneqq rac{N_{gear\_6}}{N_{gear\_5}} ullet T_{gear\_5} ullet \eta_{mesh\_3}$
	$T_{gear\_6}\!=\!6.906~ extbf{ extbf{N}}\!\cdot\! extbf{m}$
Tangential force of gear 6:	$egin{aligned} F_{tan\_gear\_6} \coloneqq & rac{T_{gear\_6}}{D_{gear\_6} \cdot 0.5} \end{aligned}$
	$F_{tan\_gear\_6}\!=\!362.514~ extbf{ ex}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}$
Radial force of gear 6:	$egin{aligned} F_{rad\_gear\_6} \coloneqq F_{tan\_gear\_6} \cdot  an\left( heta_{gear\_6} ight) \end{aligned}$
	$F_{rad\_gear\_6}$ = 131.944 $N$
Gear 7	
Gear 7 is a spur gear and it's on the s	haft as gear 6.
Number of teeth of gear 7:	$N_{gear\_7}\!\coloneqq\!24$
Diameter of gear 7:	$D_{gear\_7} \coloneqq 25.4 \; m{mm}$
Pressure angle of gear 7:	$ heta_{gear\_7}\!\coloneqq\!20$ °
Speed of gear 7:	$w_{gear\_7}\!\coloneqq\!w_{gear\_6}$
	$w_{gear\_7}\!=\!1.328rac{rad}{s}$
Torque of gear 7:	$T_{gear\_7} \coloneqq T_{gear\_6}$



Torque of gear 8:	$T_{gear\_8}\!\coloneqq\!rac{N_{gear\_8}}{N_{gear\_7}}\!ullet\!T_{gear\_7}\!ullet\!\eta_{mesh\_4}$
	$T_{gear\_8}\!=\!13.269~ extbf{ extbf{N}}\!\cdot\! extbf{m}$
Tangential force of gear 8:	$F_{tan\_gear\_8} \coloneqq rac{T_{gear\_8}}{D_{gear\_8} \cdot 0.5}$
	$F_{tan\_gear\_8}\!=\!522.417~N$
Radial force of gear 8:	$egin{aligned} F_{rad\_gear\_8} \coloneqq F_{tan\_gear\_8} \cdot  an\left( heta_{gear\_8} ight) \end{aligned}$
	$F_{rad\_gear\_8}\!=\!190.144~ extbf{ extf{ extbf{ extf{ extbf{ ex}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}}$
Gear 9	
Gear 9 is a spur gear that meshes with gethis section.	ear 8. The efficiency is already calculated earlier in
Number of teeth of gear 8:	$N_{gear\_9}\!\coloneqq\!48$
Diameter of gear 8:	$D_{gear\_9}$ := $50.8$ $mm$
Pressure angle of gear 8:	$ heta_{gear\_9} \coloneqq 20$ °
Speed of gear 8:	$w_{gear\_9} \coloneqq rac{N_{gear\_8}}{N_{gear\_9}} { extbf{\cdot}} w_{gear\_8} { extbf{\cdot}} \eta_{mesh\_5}$
	$w_{gear\_9}$ = 0.621 $\frac{rad}{s}$

Forque of g	ear 8:		T	$N_{gear\_9} \coloneqq rac{N_{gear\_}}{N_{gear\_}}$	$\frac{9}{8} {m \cdot} T_{gear\_8} {m \cdot} \eta_m$	$nesh\_5$
			7	$T_{gear\_9} = 12.922$	$N \cdot m$	
Γangential f	orce of gear	8:	F	$t_{tan\_gear\_9} \coloneqq rac{1}{D_g}$	$T_{gear\_9} = 0.5$	
			F	$T_{tan\_gear\_9} = 508$	3.74 <b>N</b>	
Radial force	of gear 8:		F	$F_{rad\_gear\_9} \coloneqq F_{ta}$	$_{m\_gear\_9}$ • $ an$ ((	$ heta_{gear\_9} ig)$
			F	$T_{rad\_gear\_9} = 185$	5.166 <b>N</b>	
	Maximum	Experience	Maximum	Experience	Experience	Rotational
	Maximum Torque [Nm]	Experience d Torque [Nm]	Maximum tangential force [N]	Experience d tangential force [N]	Experience d radial force [N]	Rotational speed [rad/s]
Gear 1 [12T]	Torque	d Torque	tangential	d tangential	d radial	speed
Gear 1 [12T] Gear 2 [36T]	Torque [Nm]	d Torque [Nm]	tangential force [N]	d tangential force [N]	d radial force [N]	speed [rad/s]
	Torque [Nm]	d Torque [Nm] 0.941	tangential force [N] 450	d tangential force [N] 148.228	d radial force [N] 53.95	speed [rad/s]
Gear 2 [36т]	Torque [Nm]	d Torque [Nm] 0.941 2.627	tangential force [N] 450 700	d tangential force [N] 148.228 137.879	d radial force [N] 53.95 50.184	speed [rad/s] 14.537 4.508
Gear 2 [36T] Gear 3 [24T]	Torque [Nm]  3  3.4	d Torque [Nm] 0.941 2.627	tangential force [N]  450  700  300	d tangential force [N]  148.228  137.879  206.819	d radial force [N] 53.95 50.184 75.276	speed [rad/s] 14.537 4.508
Gear 2 [36T] Gear 3 [24T] Gear 4 [24T]	Torque [Nm]  3  3.4  3	d Torque [Nm] 0.941 2.627 2.627 2.489	tangential force [N]  450  700  300  300	d tangential force [N]  148.228  137.879  206.819  195.99	d radial force [N] 53.95 50.184 75.276 71.335	speed [rad/s] 14.537 4.508 4.508
Gear 2 [36T] Gear 3 [24T] Gear 4 [24T] Gear 5 [12T]	Torque [Nm]  3  3.4  3  3  3	d Torque [Nm] 0.941 2.627 2.627 2.489 2.489	tangential force [N]  450  700  300  300  450	d tangential force [N]  148.228  137.879  206.819  195.99  391.98	d radial force [N]  53.95  50.184  75.276  71.335  142.669	speed [rad/s] 14.537 4.508 4.508 4.272 4.272
Gear 2 [36T] Gear 3 [24T] Gear 4 [24T] Gear 5 [12T] Gear 6 [36T]	Torque [Nm]  3  3.4  3  3.4  3  3.4	d Torque [Nm] 0.941 2.627 2.627 2.489 2.489 6.946	tangential force [N]  450  700  300  450  700	d tangential force [N]  148.228  137.879  206.819  195.99  391.98  364	d radial force [N]  53.95  50.184  75.276  71.335  142.669  132.709	speed [rad/s]  14.537  4.508  4.508  4.272  4.272  1.324

igur	e 6	: Su	ımma	ry c	of ge	ar c	alc	ulat	ior	าร																	
he a neir	abc ex	ve l perie	nighlig encing	ghts g is	whi mor	ch g e th	gea an	rs r the	nus to	st b rqu	e s ie it	upp t ca	or in v	t in vith	red	d, tl ind.	his	is	bed	cau	se	the	to	rqu	e t	hat	
iear iear iear	6 ( 7 ( 8 (	(36T (24T (48T	oove t spur spur spur spur	gea gea	ar) ar) ar)	e fol	low	ring	mı	ust	be	su	ppc	orte	ed:												