

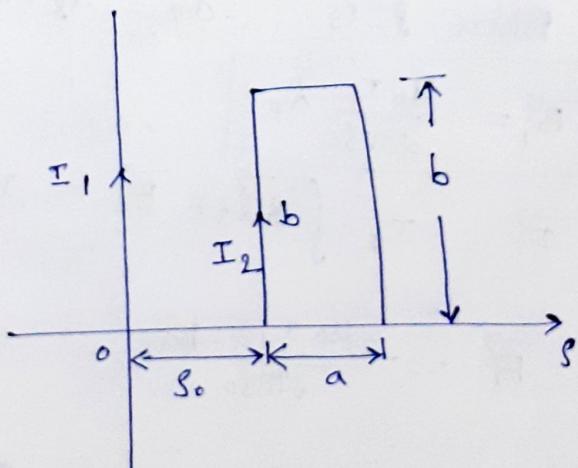
Conduction current: conduction current requires
a conductor (31)

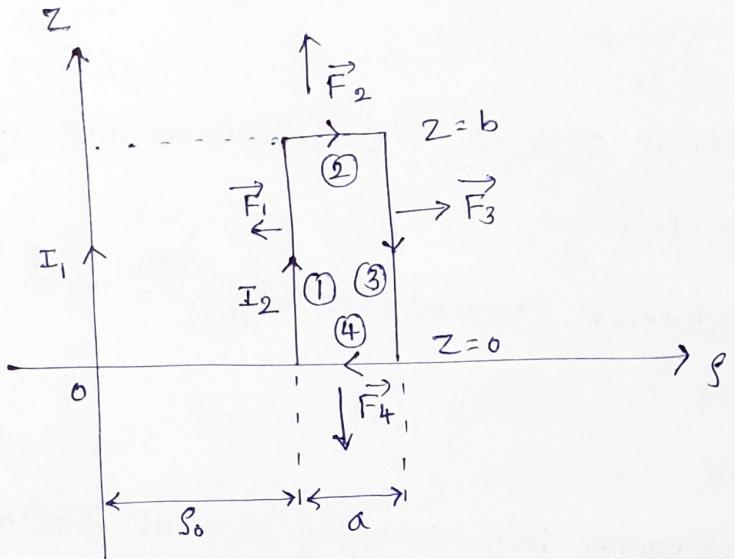
$$\text{conduction current density } \vec{J} = \sigma \vec{E}$$

- i) A rectangular loop carrying current I_2 is placed parallel to an infinitely long filamentary wire carrying current I_1 , as shown in figure. Show that the force experienced by the loop is given by

$$\vec{F} = - \frac{\mu_0 I_1 I_2 b}{2\pi} \left[\frac{1}{s_0} - \frac{1}{s_0 + a} \right] \hat{a}_N$$

Solution:





Let the force on the loop be

$$\vec{F}_L = \vec{F}_1 + \vec{F}_2 + \vec{F}_3 + \vec{F}_4$$

\vec{B}_1 = Magnetic flux density due to infinitely long conductor carrying current I_1

$$\vec{B}_1 = \mu_0 \vec{H}_1 = \frac{\text{Amperian loop}}{2\pi s_0} \hat{a}_\phi = \frac{\mu_0 I_1}{2\pi s_0} \hat{a}_\phi$$

$$\text{where } g = s_0 \quad \hat{a}_\phi = \hat{a}_\theta \times \hat{a}_\phi = \hat{a}_2 \times \hat{a}_s = \hat{a}_\phi$$

$$\boxed{\vec{B}_1 = \frac{\mu_0 I_1}{2\pi s_0} \hat{a}_\phi}$$

$$\vec{F}_1 = I_2 \int d\vec{l}_2 \times \vec{B}_1 = I_2 \int_{z=0}^{z=b} dz \hat{a}_2 \times \frac{\mu_0 I_1}{2\pi s_0} \hat{a}_\phi$$

$$\vec{F}_1 = - \frac{\mu_0 I_1 I_2 b \hat{a}_s}{2\pi s_0} \quad \begin{vmatrix} \hat{a}_s & \hat{a}_\phi & \hat{a}_2 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{vmatrix} = - \hat{a}_s$$

$$\vec{F}_3 = I_2 \int d\vec{l}_2 \times \vec{B}_1 = I_2 \int_{z=b}^0 dz \hat{a}_2 \times \frac{\mu_0 I_1}{2\pi(s_0+a)} \hat{a}_\phi$$

$$\vec{F}_3 = \frac{\mu_0 I_1 I_2 b}{2\pi(s_0+a)} \hat{a}_s$$

$$\vec{F}_2 = I_2 \int d\vec{l}_2 \times \vec{B}_1 \quad (33)$$

$$= I_2 \int ds \hat{a}_s \times \frac{\mu_0 I_1 \hat{a}_\phi}{2\pi s}$$

$$= \frac{\mu_0 I_1 I_2}{2\pi} \int_{s_0}^{s_0+a} \frac{1}{s} ds \hat{a}_z$$

$$\begin{vmatrix} \hat{a}_s & \hat{a}_\phi & \hat{a}_z \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{vmatrix} = \hat{a}_z$$

$$= \frac{\mu_0 I_1 I_2}{2\pi} \ln s \Big|_{s_0}^{s_0+a} \quad (\text{Parallel})$$

$$\vec{F}_2 = \frac{\mu_0 I_1 I_2}{2\pi} \ln \left[\frac{s_0+a}{s_0} \right] \hat{a}_z \quad (\text{Parallel})$$

$$\vec{F}_4 = I_2 \int d\vec{l}_2 \times \vec{B}_1$$

$$= I_2 \int ds \hat{a}_s \times \frac{\mu_0 I_1 \hat{a}_\phi}{2\pi s}$$

$$= \frac{\mu_0 I_1 I_2}{2\pi} \ln \left(\frac{s_0}{s_0+a} \right) \hat{a}_z$$

$$= - \frac{\mu_0 I_1 I_2}{2\pi} \ln \left(\frac{s_0+a}{s_0} \right) \hat{a}_z$$

$$\text{Total Force} \quad \therefore \vec{F}_d = \vec{F}_1 + \vec{F}_2 + \vec{F}_3 + \vec{F}_4$$

$$= \frac{\mu_0 I_1 I_2 b}{2\pi} \left[\frac{1}{s_0} - \frac{1}{s_0+a} \right] (-\hat{a}_s)$$

- ① A charged particle moves with a uniform velocity $4\hat{a}_x \text{ m/s}$ in a region where $\vec{E} = 20\hat{a}_y \text{ V/m}$ and $\vec{B} = B_0\hat{a}_z \text{ Td/m}^2$. Determine B_0 such that the velocity of the particle remains constant.

Solution:

If the particle moves with a constant velocity, it is implied that its acceleration is zero. In other words, the particle experiences no net force.

$$\vec{F} = m\vec{a} = m(0) \xrightarrow{\text{constant velocity}} \vec{F} = 0 \quad (1)$$

$$\vec{F} = Q(\vec{E} + \vec{v} \times \vec{B})$$

$$0 = Q(\vec{E} + 4\hat{a}_x \times B_0\hat{a}_z)$$

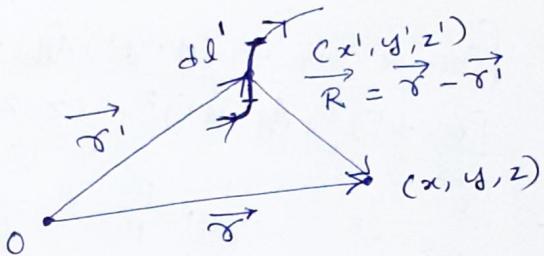
~~$$-Q\vec{E} = -Q4B_0\hat{a}_y$$~~

~~$$-Q \times 20\hat{a}_y = -Q4B_0\hat{a}_y$$~~

$$20 = 4B_0$$

$$B_0 = 5$$

Derivation of Biot-Savart's law and Ampere's law



Both Biot-Savart's law and Ampere's law may be derived by using the concept of magnetic vector potential.

$$\text{We know } \nabla \times \nabla \times \vec{A} = \nabla(\nabla \cdot \vec{A}) - \nabla^2 A$$

$$\text{consider } \vec{B} = \nabla \times \vec{A} = \nabla \times \oint_L \frac{\mu_0 I}{4\pi R} \vec{dl}'$$

$$\vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \nabla \times \frac{1}{R} \vec{dl}' \rightarrow (1)$$

We know from vector identity

$$\vec{F} \times \nabla f = f \nabla \times \vec{F} - \nabla \times f \vec{F}$$

$$\therefore \nabla \times f \vec{F} = f \nabla \times \vec{F} - \vec{F} \times \nabla f$$

$$\nabla \times \frac{1}{R} \vec{dl}' = \frac{1}{R} \nabla \times \vec{dl}' - \vec{dl}' \times \nabla \left(\frac{1}{R} \right) \rightarrow (2) \quad \text{where } \vec{F} = \vec{dl}'$$

using (2) in (1)

$$\vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \left[\frac{1}{R} \nabla \times \vec{dl}' - \vec{dl}' \times \nabla \left(\frac{1}{R} \right) \right] \rightarrow (3)$$

Since ∇ operator operates with respect (x, y, z) and \vec{dl}' is a function of (x', y', z')

$$\therefore \nabla \times \vec{dl}' = 0 \rightarrow (4)$$

$$|\vec{R}| = R = \left[(x - x')^2 + (y - y')^2 + (z - z')^2 \right]^{\frac{1}{2}}$$

$$\frac{1}{R} = \left[(x - x')^2 + (y - y')^2 + (z - z')^2 \right]^{-\frac{1}{2}} \quad (36)$$

$$\nabla \left(\frac{1}{R} \right) = \frac{\partial \frac{1}{R}}{\partial x} \hat{a}_x + \frac{\partial \frac{1}{R}}{\partial y} \hat{a}_y + \frac{\partial \frac{1}{R}}{\partial z} \hat{a}_z$$

$$\therefore \nabla \left(\frac{1}{R} \right) = - \frac{\left[(x - x') \hat{a}_x + (y - y') \hat{a}_y + (z - z') \hat{a}_z \right]}{\left[(x - x')^2 + (y - y')^2 + (z - z')^2 \right]^{\frac{3}{2}}}$$

$$\nabla \left(\frac{1}{R} \right) = - \frac{\vec{R}}{R^3} = - \frac{1}{R^2} \cdot \frac{\vec{R}}{R} = - \frac{1}{R^2} \hat{a}_R \rightarrow (5)$$

where $\hat{a}_R = \frac{\vec{R}}{R}$ = unit vector

using (4) and (5) $\vec{B} = \frac{\mu_0 I}{4\pi} \oint_{L'} \vec{dl}' \times \hat{a}_R$

in (3)

$$\vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \left[\nabla \times \vec{dl}' - \vec{dl}' \times \nabla \left(\frac{1}{R} \right) \right]$$

$$\vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \left[- \vec{dl}' \times \left(- \frac{\hat{a}_R}{R^2} \right) \right]$$

$$\vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \frac{\vec{dl}' \times \hat{a}_R}{R^2} \quad \text{or} \quad \vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \frac{\vec{dl}' \times \vec{R}}{R^3}$$

which is the Biot-Savart's law
if we drop prime in \vec{dl}' , it becomes \vec{dl}

$$\therefore \vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \frac{\vec{dl} \times \hat{a}_R}{R^2} \quad \text{or} \quad \vec{B} = \frac{\mu_0 I}{4\pi} \oint_L \frac{\vec{dl} \times \vec{R}}{R^3}$$

which is Biot-Savart's law

$$\nabla \times \vec{B} = \nabla \times \nabla \times \vec{A}$$

$$\nabla \times \vec{B} = \nabla (\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$$

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$\boxed{\nabla \cdot \vec{A} = 0}$ which is called coulomb's gauge

$$\nabla \times \vec{B} = \nabla (\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$$

$$\nabla \times \mu_0 \vec{H} = \nabla (\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$$

$$\nabla^2 \vec{A} = -\mu_0 \nabla \times \vec{H}$$

$$\boxed{\nabla^2 \vec{A} = -\mu_0 \vec{J}} \quad \text{where } \nabla \times \vec{H} = \vec{J}$$

$\nabla^2 \vec{A} = -\mu_0 \vec{J}$ is known as vector Poisson equation

$$\nabla^2 A_x = -\mu_0 J_x$$

$$\nabla^2 A_y = -\mu_0 J_y$$

$$\nabla^2 A_z = -\mu_0 J_z$$

which may be regarded as the scalar Poisson equations

$$\oint_L \vec{H} \cdot d\vec{l} = \int_S (\nabla \times \vec{A}) \cdot d\vec{s}$$

$$= \frac{1}{\mu_0} \int_S (\nabla \times \frac{\vec{B}}{\mu_0}) \cdot d\vec{s}$$

$$= \frac{1}{\mu_0} \int_S \nabla \times (\nabla \times \vec{A}) \cdot d\vec{s}$$

$$\nabla \times \nabla \times \vec{A} = -\nabla^2 \vec{A} = \mu_0 \vec{J}$$

$$= \frac{1}{\mu_0} \int_S \mu_0 \vec{J} \cdot d\vec{s}$$

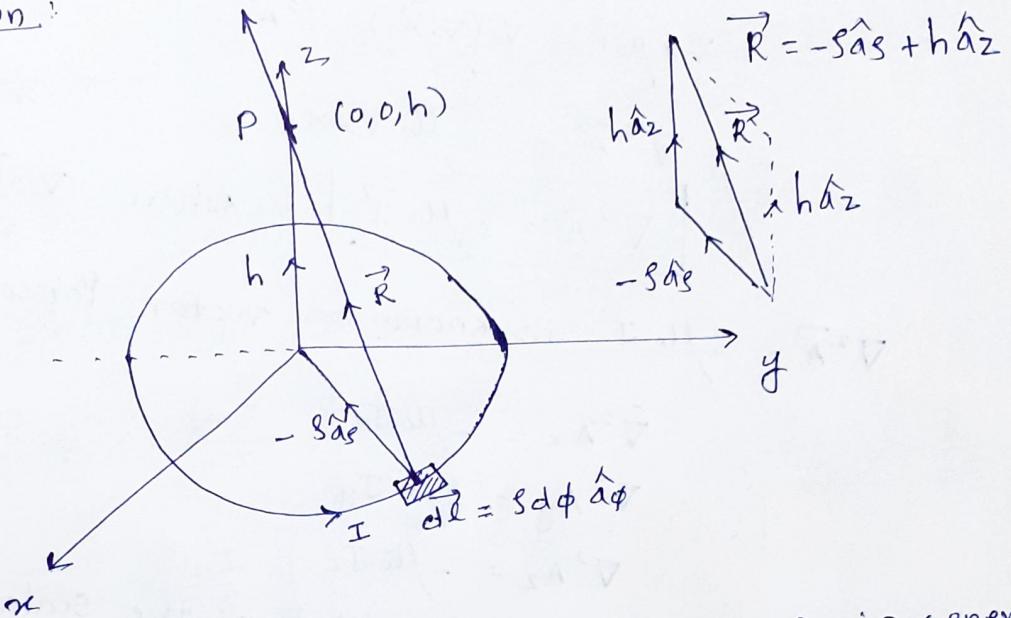
$$\oint_L \vec{H} \cdot d\vec{l} = \int_S \vec{J} \cdot d\vec{s} = I \quad \text{which is}$$

Ampere's circuit law

- 1) A circular loop located on $x^2 + y^2 = 9$, $z=0$ carries a direct current of 10A along \hat{a}_ϕ . Determine \vec{H} at $(0,0,4)$ and $(0,0,-4)$.

(38)

Solution:



- (a) case(i): Let point of interest $P(0,0,4)$ in general it is taken as $(0,0,h)$

$$\vec{d}H = \frac{I \vec{dl} \times \vec{R}}{4\pi R^3}, \text{ now } \vec{dl} = s d\phi \hat{a}_\phi$$

$$\vec{R} = s(-\hat{a}_s) + h\hat{a}_z \Rightarrow R = |\vec{R}| = \sqrt{s^2 + h^2}$$

$$\vec{dl} \times \vec{R} = \begin{vmatrix} \hat{a}_s & \hat{a}_\phi & \hat{a}_z \\ 0 & s d\phi & 0 \\ -s & 0 & h \end{vmatrix} = \hat{a}_s [s h d\phi] - \hat{a}_\phi [0] + \hat{a}_z (s^2 d\phi)$$

$$= h s d\phi \hat{a}_s + s^2 d\phi \hat{a}_z$$

Due to symmetry the contribution along \hat{a}_s components add up to zero. Because the radial components produced by the current element pairs are separated by 180° . Hence they cancel.

$$\vec{dH} = \frac{\vec{I} \vec{dl} \times \vec{R}}{4\pi R^3} = \frac{\vec{I} s^2 d\phi \hat{a}_z}{4\pi (\sqrt{s^2 + h^2})^3}$$

(39)

$$x^2 + y^2 = s^2, \text{ given } x^2 + y^2 = 9 \Rightarrow s = 3$$

$$P(0, 0, 4) \therefore h = 4$$

$$\vec{H} = \int_{\phi=0}^{2\pi} \frac{\vec{I} s^2 d\phi \hat{a}_z}{4\pi (\sqrt{s^2 + h^2})^3} = \frac{\vec{I} s^2 2\pi \hat{a}_z}{4\pi (\sqrt{s^2 + h^2})^3}$$

$$\vec{H} = \frac{\vec{I} s^2 \hat{a}_z}{2 (\sqrt{s^2 + h^2})^3} = \frac{(10)(3^2)(\hat{a}_z)}{2 (\sqrt{3^2 + 4^2})^3} = 0.36 \hat{a}_z$$

(b) case (ii) At $(0, 0, -4)$

$$\vec{dH} = \frac{\vec{I} \vec{dl} \times \vec{R}}{4\pi R^3}$$

$$\vec{dl} = s d\phi \hat{a}_\phi$$

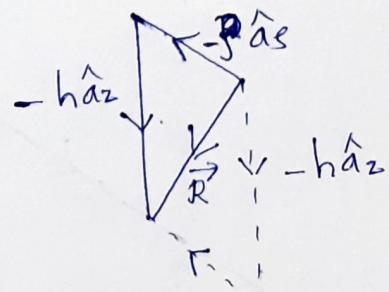
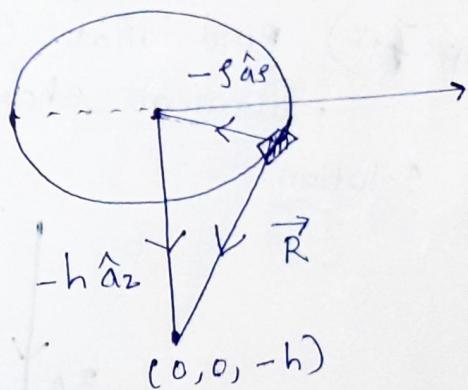
$$\vec{R} = -s \hat{a}_s - h \hat{a}_z$$

$$\vec{H} = \int_{\phi=0}^{2\pi} \frac{\vec{I} s^2 d\phi \hat{a}_z}{4\pi (s^2 + h^2)^{3/2}}$$

$$\vec{H} = \frac{\pm s^2 2\pi \hat{a}_z}{4\pi (s^2 + h^2)^{3/2}}$$

$$s = 3, h = -4, I = 10$$

$$\vec{H} = 0.36 \hat{a}_z$$



$$\vec{dl} = s d\phi \hat{a}_\phi \vec{R} = -s \hat{a}_s - h \hat{a}_z$$

$$\vec{dl} \times \vec{R} = \begin{vmatrix} \hat{a}_s & \hat{a}_\phi & \hat{a}_z \\ 0 & s d\phi & 0 \\ -s & 0 & -h \end{vmatrix}$$

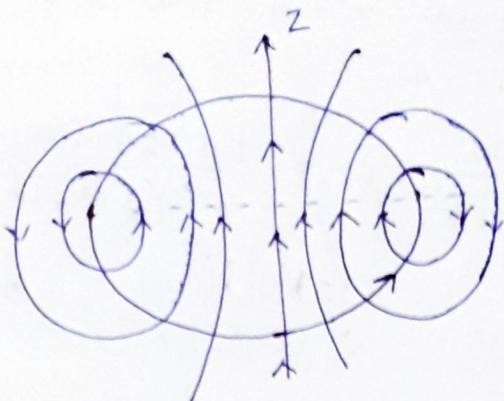
$$= \hat{a}_s (-h s d\phi) - \hat{a}_\phi (0)$$

$$+ \hat{a}_z (s^2 d\phi)$$

$\Rightarrow \hat{a}_s$ component cancel due to symmetry

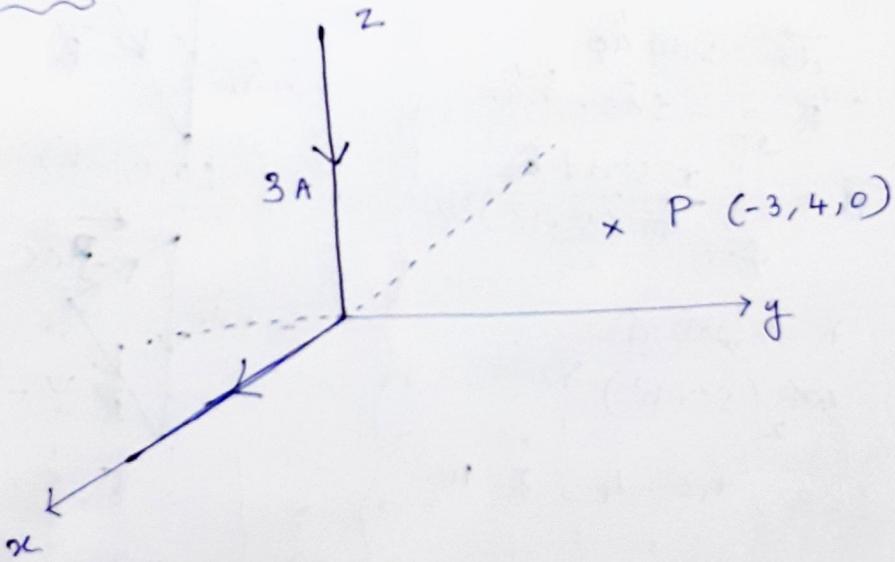
The flux lines due to current loop

(40)



Example 2) Find \vec{H} at $(-3, 4, 0)$ due to current filament shown in figure.

Solution:

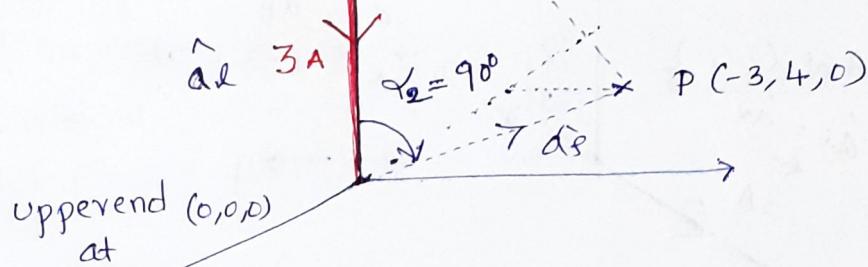


In the given problem point $P(-3, 4, 0)$ is in xy -plane $\vec{H} = \vec{H}_1 + \vec{H}_2$

\vec{H}_1 = Magnetic field intensity at 'P' due to the portion of the filament along x -axis

\vec{H}_2 = Magnetic field intensity at 'P' due to the portion of the filament along z -axis

Lower end (0, 0, 10)
at



(41)

We know $\vec{H}_2 = \frac{\mathcal{I}}{4\pi s} [\cos \alpha_2 - \cos \alpha_1] \hat{a}_\phi$

$$\hat{a}_\phi = \hat{a}_z \times \hat{a}_s$$

$$\alpha_2 = 90^\circ \quad \alpha_1 = 180^\circ$$

$$\hat{a}_z = -\hat{a}_z \quad \hat{a}_s = -\frac{3\hat{a}_x + 4\hat{a}_y + 0\hat{a}_z}{\sqrt{3^2 + 4^2}}$$

$$\hat{a}_s = -\frac{3}{5}\hat{a}_x + \frac{4}{5}\hat{a}_y + 0\hat{a}_z$$

$$\mathcal{I} = 3 \quad s = \sqrt{3^2 + 4^2} = 5$$

$$\vec{H}_2 = \frac{3}{4\pi(5)} [\cos 90^\circ - \cos 180^\circ] \hat{a}_\phi$$

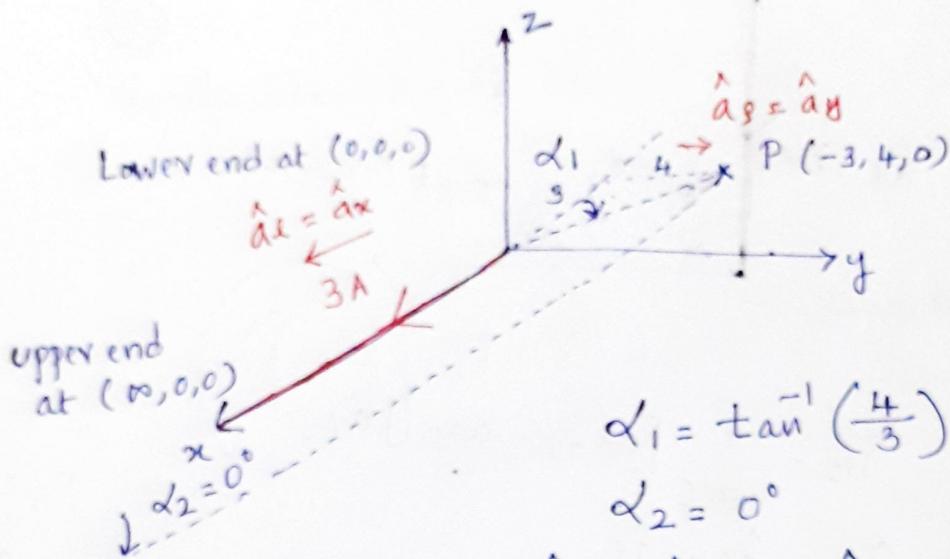
$$\begin{aligned} \hat{a}_\phi &= \hat{a}_z \times \hat{a}_s \\ &= (-\hat{a}_z) \times \left(-\frac{3}{5}\hat{a}_x + \frac{4}{5}\hat{a}_y\right) = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0 & 0 & -1 \\ -\frac{3}{5} & \frac{4}{5} & 0 \end{vmatrix} \end{aligned}$$

$$= \hat{a}_x \left(\frac{4}{5}\right) - \hat{a}_y \left(-\frac{3}{5}\right) + \hat{a}_z (0) = 0.8\hat{a}_x + 0.6\hat{a}_y$$

$$\vec{H}_2 = \frac{3}{4\pi(5)} [0 - (-1)] [0.8\hat{a}_x + 0.6\hat{a}_y]$$

$$\vec{H}_2 = 38.1971 \times 10^{-3} \hat{a}_x + 28.6478 \times 10^{-3} \hat{a}_y$$

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$$\alpha_1 = \tan^{-1} \left(\frac{4}{3} \right) = 53.13^\circ$$

$$\alpha_2 = 0^\circ$$

$$\hat{a}_l = \hat{a}_x \quad \hat{a}_s = \frac{4 \hat{a}_y}{\sqrt{4^2}} = \hat{a}_y$$

$$\vec{H}_1 = \frac{I}{4\pi S} \left[\cos \alpha_2 - \cos \alpha_1 \right] \hat{a}_\phi$$

$$\vec{H}_1 = \frac{3}{4\pi(4)} \left[\cos 0^\circ - \cos 53.13^\circ \right] \hat{a}_z$$

$$\vec{H}_1 = \frac{3}{4\pi(4)} [1 - 0.6] \hat{a}_z$$

$$\vec{H}_1 = 23.8732 \times 10^{-3} \hat{a}_z$$

$$\vec{H}_1 = \underline{23.8732 \times 10^{-3} \hat{a}_z} \quad \vec{H}_2 = \underline{38.1971 \times 10^{-3} \hat{a}_x} + \underline{28.6478 \times 10^{-3} \hat{a}_y}$$

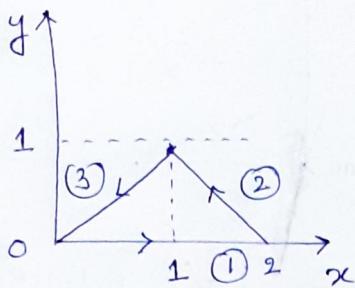
$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

$$\vec{H} = \underline{23.8732 \times 10^{-3} \hat{a}_z} + \underline{38.1971 \times 10^{-3} \hat{a}_x} + \underline{28.6478 \times 10^{-3} \hat{a}_y}$$

$$\vec{H} = \underline{38.1971 \times 10^{-3} \hat{a}_x} + \underline{28.6478 \times 10^{-3} \hat{a}_y} + \underline{23.8732 \times 10^{-3} \hat{a}_z} \text{ A/m}$$

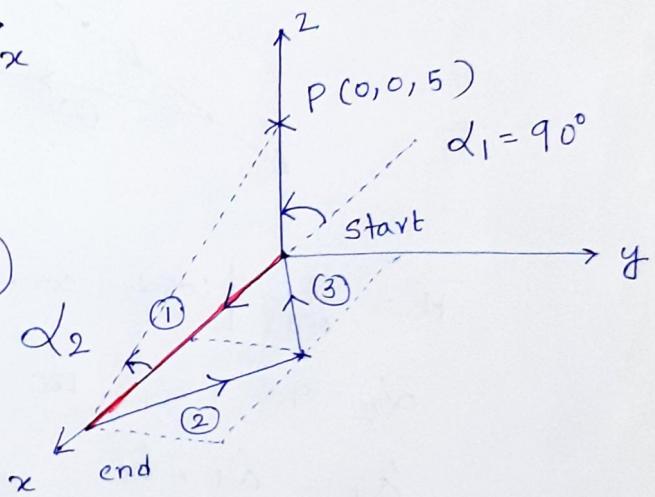
(43)

- 7.1) The conducting loop triangular loop shown in figure carries a current of 10A. Find \vec{H} at (0,0,5) due to side ① of the loop.



$$\alpha_2 = \tan^{-1}\left(-\frac{5}{2}\right)$$

$$\alpha_2 = 68.19^\circ$$



$$\vec{H} = \frac{I}{4\pi\sigma} [\cos \alpha_2 - \cos \alpha_1] \hat{a}_\phi$$

$$\hat{a}_\phi = \hat{a}_x \times \hat{a}_y$$

$$\hat{a}_x = \hat{a}_x$$

$$I = 10$$

$$\hat{a}_y = \hat{a}_z$$

$$\sigma = 5$$

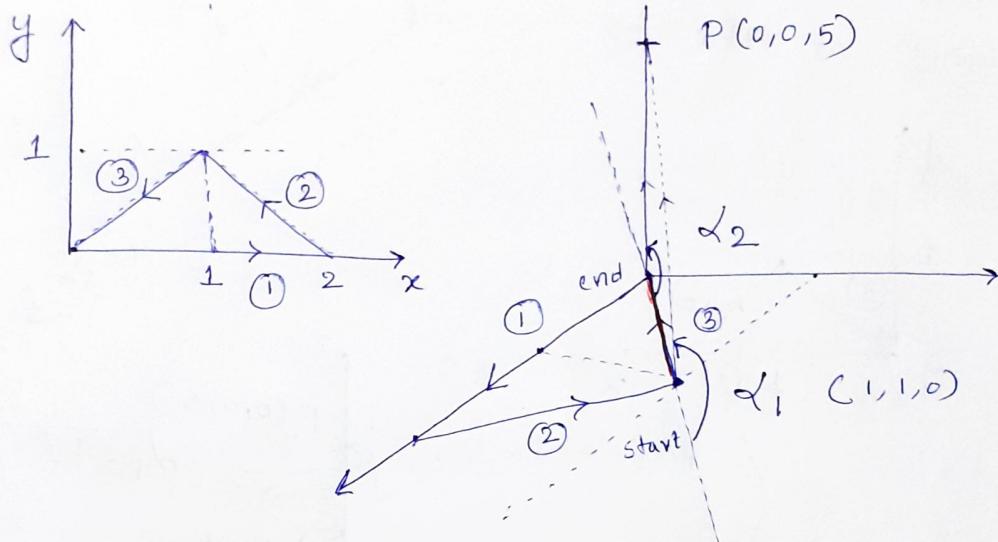
$$\vec{H} = \frac{10}{4\pi(5)} [\cos 68.19^\circ - \cos 90^\circ] (\hat{a}_x \times \hat{a}_z)$$

$$\vec{H} = -59.108 \times 10^{-3} \hat{a}_y \text{ A/m}$$

Practice Exercise 7.1

- 7.1) The conducting triangular loop shown in figure carries a current of 10A. Find \vec{H} at $(0,0,5)$ due to side ③ of the loop

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$$\vec{H} = \frac{I}{4\pi S} [\cos \alpha_2 - \cos \alpha_1] \hat{a}_\phi$$

$$\alpha_2 = 90^\circ \quad \alpha_1 = 180 - \tan^{-1}\left(\frac{5}{\sqrt{2}}\right) = 180^\circ - \tan^{-1}(3.535) \\ = 180^\circ - 74.20^\circ \\ = 105.8^\circ$$

$$\hat{a}_\phi = \hat{a}_z \times \hat{a}_s$$

$$\hat{a}_z = -\frac{\hat{a}_x - \hat{a}_y + 0}{\sqrt{2}} \quad \hat{a}_s = \hat{a}_z$$

$$\hat{a}_z \times \hat{a}_s = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ -\frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 0 \\ 0 & 0 & 1 \end{vmatrix}$$

$$= \hat{a}_x \left(-\frac{1}{\sqrt{2}}\right) - \hat{a}_y \left(-\frac{1}{\sqrt{2}}\right) + \hat{a}_z (0)$$

$$= -\frac{1}{\sqrt{2}} \hat{a}_x + \frac{1}{\sqrt{2}} \hat{a}_y$$

$$\oint = 5$$

(45)

$$\begin{aligned}
 \vec{H} &= \frac{10}{4\pi(5)} \left[\cos 90^\circ - \cos(105.8) \right] \left[-\frac{1}{\sqrt{2}} \hat{a}_x + \frac{1}{\sqrt{2}} \hat{a}_y \right] \\
 &= \frac{10}{4\pi(5)} \left[0 - (-0.2722) \right] \left[-\frac{1}{\sqrt{2}} \hat{a}_x + \frac{1}{\sqrt{2}} \hat{a}_y \right] \\
 &= \frac{10}{4\pi 5} \left[0.2722 \right] \left[-\frac{1}{\sqrt{2}} \hat{a}_x + \frac{1}{\sqrt{2}} \hat{a}_y \right] \\
 &= \underline{-30.628 \times 10^{-3} \hat{a}_x} + \underline{30.628 \times 10^{-3} \hat{a}_y} \text{ A/m}
 \end{aligned}$$

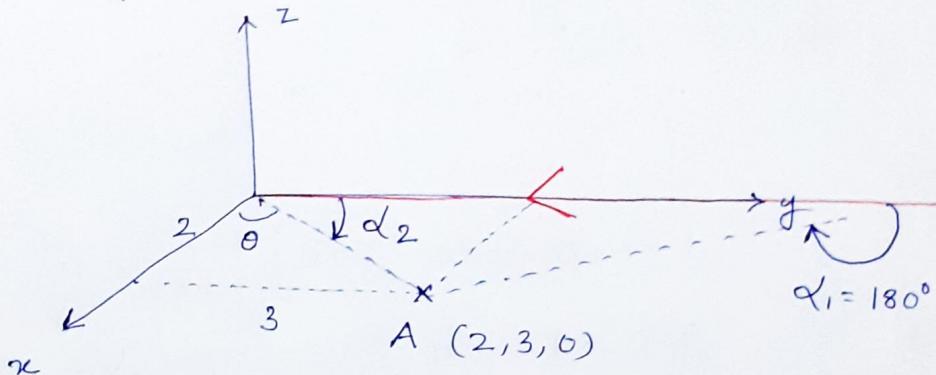
Practice Exercise 7.2

(4b)

- ① The positive y-axis (semi-infinite line with respect to the origin) carries a filamentary current $2A$ in the $-\hat{a}_y$ direction. Assume it is part of a large circuit. Find \vec{H} at

Ⓐ A (2, 3, 0) Ⓠ B (3, 12, -4)

- ⓐ Field point A (2, 3, 0)



$$\alpha_1 = 180^\circ \quad \alpha_2 = 90 - \tan^{-1}\left(\frac{3}{2}\right)$$

$$\alpha_2 = 90 - 56.30^\circ = 33.7^\circ$$

$$f = 2$$

$$\hat{a}_e = -\hat{a}_y \quad \hat{a}_s = \hat{a}_x$$

$$\hat{a}_\phi = \hat{a}_x \times \hat{a}_s = -\hat{a}_y \times \hat{a}_x = \hat{a}_z$$

$$H = \frac{I}{4\pi S} [\cos \alpha_2 - \cos \alpha_1] (\hat{a}_e \times \hat{a}_s) \hat{a}_\phi = \hat{a}_z \quad (1)$$

$$\begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0 & -1 & 0 \\ 1 & 0 & 0 \end{vmatrix}$$

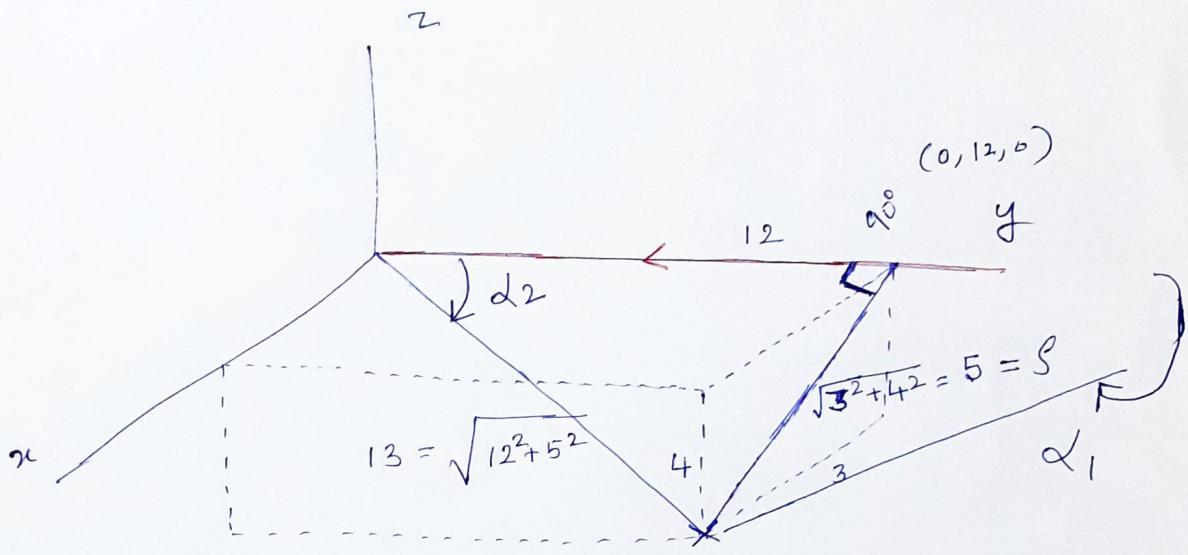
$$= \frac{\cancel{I}}{4\pi S} [\cos 33.7^\circ - \cos 180^\circ] \hat{a}_z$$

$$= \frac{1}{4\pi} [0.8319 + 1] \hat{a}_z = 0.1457 \hat{a}_z$$

$$= 145.7 \times 10^{-3} \hat{a}_z \text{ A/m}$$

(6) Field point B (3, 12, -4)

(47)



$$B(3, 12, -4) \quad \alpha_1 = 180^\circ$$

$$\cos \alpha_2 = \frac{12}{13} \quad \text{or} \quad \alpha_2 = 22.62^\circ$$

$$\text{or} \quad \alpha_2 = \tan^{-1}\left(\frac{5}{12}\right) = 22.62^\circ$$

$$s = \sqrt{3^2 + 4^2} = 5$$

$$\hat{\alpha}_x = -\hat{a}_y \quad \hat{\alpha}_s = \frac{3\hat{a}_x + 0\hat{a}_y - 4\hat{a}_z}{\sqrt{3^2 + 4^2}}$$

$$\hat{\alpha}_x = -\hat{a}_y \quad \hat{\alpha}_s = 0.6\hat{a}_x - 0.8\hat{a}_z$$

$$\hat{\alpha}_x \times \hat{\alpha}_s = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ 0 & -1 & 0 \\ 0.6 & 0 & -0.8 \end{vmatrix} = \hat{a}_x (0.8) + \hat{a}_z (0.6)$$

$$\vec{H} = \frac{I}{4\pi s} [\cos \alpha_2 - \cos \alpha_1] (\hat{a}_x (0.8) + \hat{a}_z (0.6))$$

$$= \frac{2}{4\pi (5)} [\cos 22.62^\circ - \cos 180^\circ] [0.8\hat{a}_x + 0.6\hat{a}_z]$$

$$= -\frac{2}{4\pi 5} [0.9230 - (-1)] [0.8\hat{a}_x + 0.6\hat{a}_z]$$

$$= \underline{48.96 \times 10^{-3} \hat{a}_x} + \underline{36.72 \times 10^{-3} \hat{a}_z} \text{ A/m}$$