



Modellbildung und Simulation Kapitel 7: Systeme mit verteilten Parametern

Balázs Pritz pritz@kit.edu

Institut für Thermische Strömungsmaschinen Prof. Dr.-Ing. Hans-Jörg Bauer



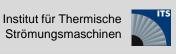


Saalübung



7. Systeme mit verteilten Parametern

7.2 Modellreduktion

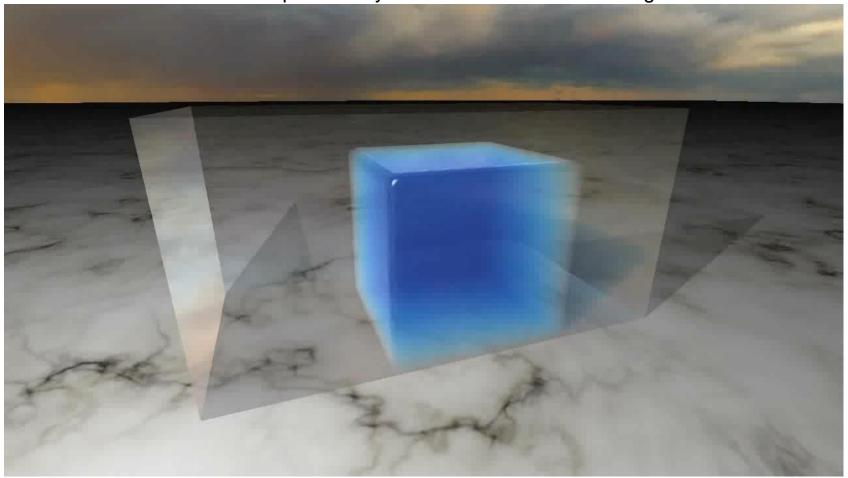


Modellreduktion – Mathematische Reduktion



NVIDIA PhysX - SPH (Smoothed Particle Hydrodynamics)

NVIDIA GF100 Fluids Demo https://www.youtube.com/watch?v=UYIPg8TEMmU







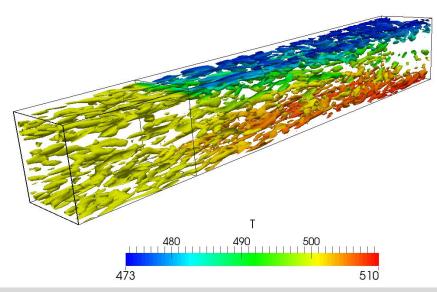
Einsatzgebiet:

Kanalströmung kommt in vielen technischen Bereichen vor, aber die ist für Modelluntersuchungen (vor allem für Turbulenzmodelle) auch ganz gut geeignet.

Als Ausgangspunkt dienen die dreidimensionale kompressible Navier-Stokes Gleichungen.

Die Vereinfachung des Modells durch den folgenden Annahmen wird ausführlich diskutiert:

- $3D \rightarrow 2D$
- Kompressibel → inkompressibel
- Instationär → stationär
- Turbulent → laminar
- Konstante Materialeigenschaften





Ausgang: 3D, instationär, kompressibel

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0$$

$$T_{ij} = \mu \left(\frac{\partial \rho u_i u_j}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} \right)$$

$$T_{ij} = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right)$$

$$\delta_{ij} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\frac{\partial \rho E}{\partial t} + \frac{\partial \rho u_i E}{\partial x_i} = \frac{\partial (q_i - p u_i)}{\partial x_i} + \frac{\partial u_i T_{ij}}{\partial x_i} + u_i g_i$$

$$q_i = \lambda \frac{\partial T}{\partial x_i}$$
 $E = \frac{1}{2}u_iu_i + e$ $e = \frac{p}{\rho(\gamma - 1)} = c_vT$ $p = \rho RT$



Ausgeschrieben

$$\vec{u} = \begin{pmatrix} u \\ v \\ w \end{pmatrix} \qquad \vec{x} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} + \frac{\partial \rho w}{\partial z} = 0$$

$$\frac{\partial \rho u}{\partial t} + \frac{\partial \rho u u}{\partial x} + \frac{\partial \rho u v}{\partial y} + \frac{\partial \rho u w}{\partial z} = -\frac{\partial p}{\partial x} + \frac{\partial T_{xx}}{\partial x} + \frac{\partial T_{xy}}{\partial y} + \frac{\partial T_{xz}}{\partial z} + g_x$$

$$\frac{\partial T_{xx}}{\partial x} = \frac{\partial}{\partial x} \mu \left(2 \frac{\partial u}{\partial x} - \frac{2}{3} \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) \right)$$
$$\frac{\partial T_{xy}}{\partial y} = \frac{\partial}{\partial y} \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right)$$
$$\frac{\partial T_{xz}}{\partial z} = \frac{\partial}{\partial z} \mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right)$$



Ausgeschrieben

$$\vec{u} = \begin{pmatrix} u \\ v \\ w \end{pmatrix} \qquad \vec{x} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} + \frac{\partial \rho w}{\partial z} = 0$$

$$\frac{\partial \rho u}{\partial t} + \frac{\partial \rho u u}{\partial x} + \frac{\partial \rho u v}{\partial y} + \frac{\partial \rho u w}{\partial z} = -\frac{\partial p}{\partial x} + \frac{\partial T_{xx}}{\partial x} + \frac{\partial T_{xy}}{\partial y} + \frac{\partial T_{xz}}{\partial z} + g_x$$

$$\frac{\partial \phi}{\partial x} = \frac{\phi_i - \phi_{i-1}}{x_i - x_{i-1}}$$
Anzahl der mathematischen Operationen

$$\frac{\partial T_{xx}}{\partial x} = \frac{\partial}{\partial x} \mu \left(2 \frac{\partial u}{\partial x} - \frac{2}{3} \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) \right)$$
$$\frac{\partial T_{xy}}{\partial y} = \frac{\partial}{\partial y} \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right)$$
$$\frac{\partial T_{xz}}{\partial z} = \frac{\partial}{\partial z} \mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right)$$



Ausgeschrieben

$$\vec{u} = \begin{pmatrix} u \\ v \\ w \end{pmatrix} \qquad \vec{x} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} + \frac{\partial \rho w}{\partial z} = 0 \qquad \Sigma \ \mathbf{11}$$

$$\frac{\partial \rho u}{\partial t} + \frac{\partial \rho u u}{\partial x} + \frac{\partial \rho u v}{\partial y} + \frac{\partial \rho u w}{\partial z} = -\frac{\partial p}{\partial x} + \frac{\partial T_{xx}}{\partial x} + \frac{\partial T_{xy}}{\partial y} + \frac{\partial T_{xz}}{\partial z} + g_x \qquad \Sigma 67$$
2+3
2+3
2+3
3
21
11

$$\frac{\partial \phi}{\partial x} = \frac{\phi_i - \phi_{i-1}}{x_i - x_{i-1}}$$
 3

$$\frac{\partial T_{xx}}{\partial x} = \frac{\partial}{\partial x} \mu \left(2 \frac{\partial u}{\partial x} - \frac{2}{3} \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) \right) \qquad \Sigma 21$$

$$\frac{\partial T_{xy}}{\partial y} = \frac{\partial}{\partial y} \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \qquad \Sigma 11$$

$$\frac{\partial T_{xz}}{\partial z} = \frac{\partial}{\partial z} \mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \qquad \Sigma 11$$



- Vereinfachungen
 - Inkompressibel

$$\rho = \text{konst.} \Rightarrow \partial \rho = 0$$

Isotherm

$$\mu = \text{konst.}$$

$$(\mu \neq f(T), \rho \neq f(T))$$

2D

$$\frac{\partial}{\partial z} = 0$$

Stationär

$$\frac{\partial}{\partial t} = 0$$

Voll entwickelt

$$\frac{\partial}{\partial x} = 0$$



K

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} + \frac{\partial \rho w}{\partial z} = 0$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$\frac{\partial v}{\partial y} = 0$$

inkompressibel

2D

voll entwickelt

RB an Wänden

$$v = 0$$



- E
 - \blacksquare inkomp. \Rightarrow wird entkopelt
 - p muss mit Hilfe einer Poisson-Gleichung iterativ gesucht werden...



I, 3D

$$\frac{\partial \rho u}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_i} = -\frac{\partial p}{\partial x_i} + \frac{\partial T_{ij}}{\partial x_i} + g_i$$

stationär, inkomp.

$$\frac{\partial \rho u}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial T_{ij}}{\partial x_j} + g_i \qquad \frac{\partial T_{ij}}{\partial x_i} = \frac{\partial}{\partial x_i} \mu \left(\frac{\partial u_i}{\partial x_i} + \frac{\partial u_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right)$$

isotherm, inkomp.

$$\frac{\partial T_{ij}}{\partial x_{j}} = \mu \frac{\partial}{\partial x_{j}} \left(\frac{\partial u_{i}}{\partial x_{j}} + \frac{\partial u_{j}}{\partial x_{i}} \right)$$

$$= \mu \left(\frac{\partial}{\partial x_{j}} \left(\frac{\partial u_{i}}{\partial x_{j}} \right) + \frac{\partial}{\partial x_{j}} \left(\frac{\partial u_{j}}{\partial x_{i}} \right) \right)$$

$$= \mu \left(\frac{\partial}{\partial x_{j}} \left(\frac{\partial u_{i}}{\partial x_{j}} \right) + \frac{\partial}{\partial x_{i}} \left(\frac{\partial u_{j}}{\partial x_{j}} \right) \right)$$

$$\frac{\partial^{2} u_{i}}{\partial x_{j}} \left(\frac{\partial u_{i}}{\partial x_{j}} \right)$$
Kont.







$$\rho\left(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right) = -\frac{\partial p}{\partial x} + \mu\frac{\partial^2 u}{\partial x_j^2}$$
 voll entwickelt \times Kont.

$$0 = -\frac{\partial p}{\partial x} + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$$

$$\downarrow \qquad \qquad \qquad \qquad \bigvee$$
voll entwickelt

$$\frac{\partial^2 u}{\partial y^2} = \frac{1}{\mu} \frac{\partial p}{\partial x}$$

$$\rho\left(u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y}\right) = -\frac{\partial p}{\partial y} + \mu \frac{\partial^2 v}{\partial x_j^2}$$

$$\downarrow \qquad \downarrow \qquad \downarrow \qquad \downarrow$$

$$\swarrow \qquad \bigvee \qquad \bigvee \qquad \mathsf{Kont.}$$

$$0 = -\frac{\partial p}{\partial y} + \mu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right)$$

$$\downarrow \qquad \qquad \downarrow$$

$$\frac{\partial p}{\partial y} = 0$$





Integration:

$$\frac{\partial u}{\partial y} = \frac{1}{\mu} \frac{\partial p}{\partial x} y + C_1$$

$$u(y) = \frac{1}{\mu} \frac{\partial p}{\partial x} \frac{y^2}{2} + C_1 y + C_2$$

Randbedingungen:

$$u(0) = 0 \qquad \Rightarrow C_2 = 0$$

$$\Rightarrow C_2 = 0$$

$$u(h) = U$$

$$u(y) = \frac{1}{2\mu} \frac{\partial p}{\partial x} y^2 + \left(\frac{U}{h} - \frac{1}{2\mu} \frac{\partial p}{\partial x} h \right) y$$

$$U = \frac{1}{2\mu} \frac{\partial p}{\partial x} h^2 + C_1 h$$

$$C_1 = \frac{U}{h} - \frac{1}{2\mu} \frac{\partial p}{\partial x} h$$

$$u(y) = \frac{1}{2\mu} \frac{\partial p}{\partial x} [y^2 - hy] + \frac{U}{h} y$$



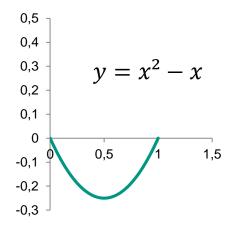
$$u(y) = \frac{1}{2\mu} \frac{\partial p}{\partial x} [y^2 - hy] + \frac{U}{h} y$$

Couette

$$\frac{\partial p}{\partial x} = 0 \implies u(y) = \frac{U}{h}y$$

Poiseuille

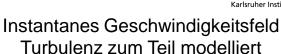
$$U = 0 \implies u(y) = \frac{1}{2\mu} \frac{\partial p}{\partial x} [y^2 - hy]$$

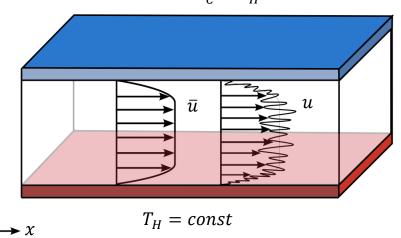


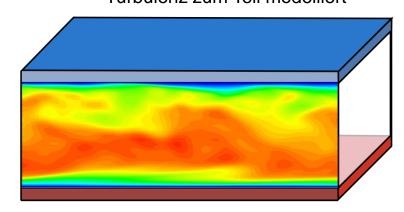
Turbulente Kanalströmung





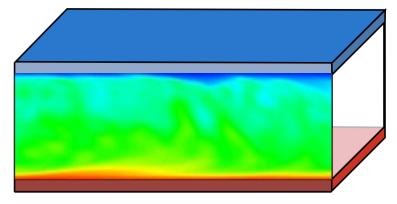


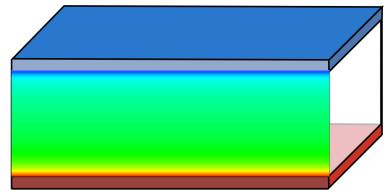




Turbulenz zum Teil modelliert

Turbulenz vollständig modelliert





Instantanes Temperaturfeld

RANS – Temperaturfeld (Reynolds-averaged Navier-Stokes)

Turbulente Kanalströmung



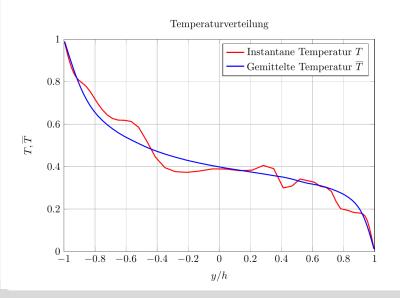
Impulsgleichungen (inkompressibel):

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial p}{\partial x_i} + v \frac{\partial^2 u_i}{\partial dx_j^2}$$

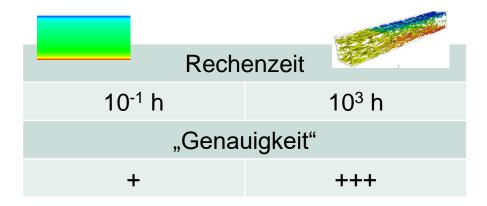
Reynolds-Zerlegung:

$$u_i = \overline{u_i} + u_i'$$

Reynoldsgemittelte Impulsgleichung (inkompressibel):



$$\frac{\partial \overline{u_i}}{\partial t} + \overline{u_j} \frac{\partial \overline{u_i}}{\partial x_j} + \frac{\partial \left(\overline{u_i' u_j'}\right)}{\partial x_j} = -\frac{1}{\rho} \frac{\partial \overline{p}}{\partial x_i} + \nu \frac{\partial^2 \overline{u_i}}{\partial dx_i^2}$$



Zylinderumströmung



2D, stationär

2D, instationär

3D, instationär

Re=2.5e5

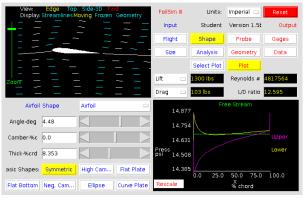
Quelle: cfd.solvcon.net

Rechenzeit			
10 ⁻¹ h	10 ⁰ h	10 ⁶ h	
"Genauigkeit"			
+	++	+++	

Profilumströmung

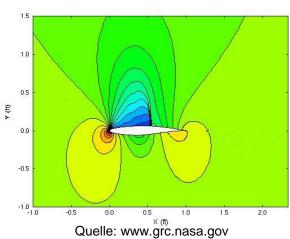


FoilSim (Euler, inkomp., 2D, stationär)

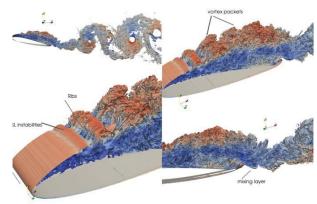


Quelle: www.grc.nasa.gov

NS, 2D, stationär



NS, 3D, instationär

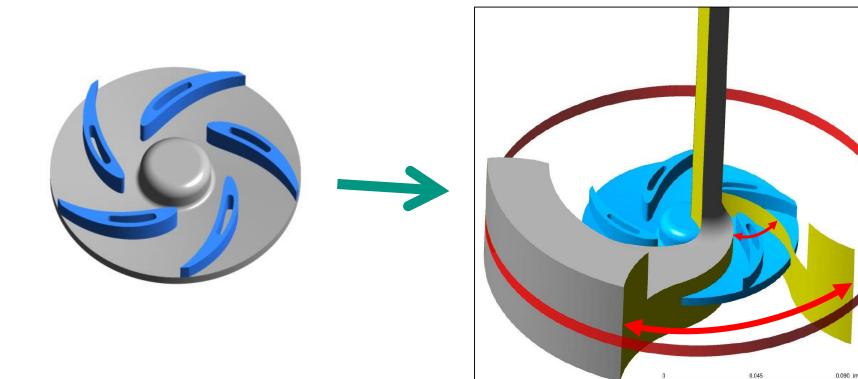


Quelle: www.cttc.upc.edu

Rechenzeit			
10 ⁻⁵ h	10 ⁰ h	10 ⁶ h	
"Genauigkeit"			
+	++	+++	

Geometrische Vereinfachung - Periodizität

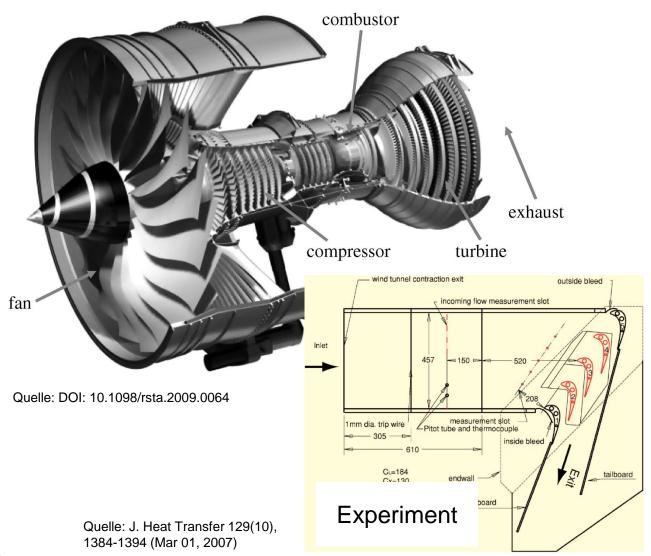


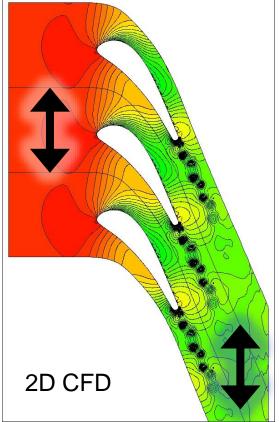




Geometrische Vereinfachung - Periodizität



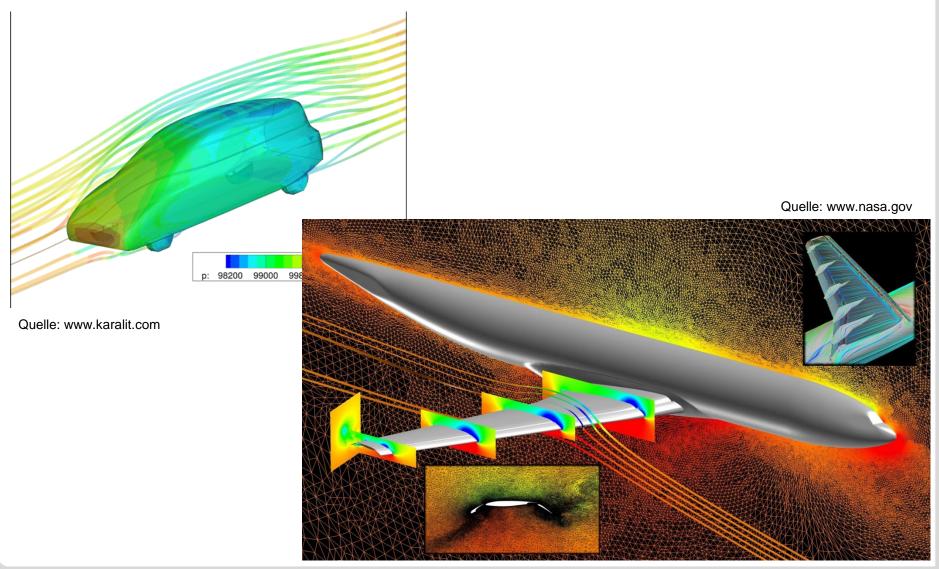






Geometrische Vereinfachung – Symmetrie, ...





Modellreduktion am Beispiel eines Radialventilators



- Was sieht man in der Animation?
 - Größe des Strömungsgebietes
 - Auflösung
 - Was passiert an der Wand?
 - Zusätzliche Modelle für die Strömung.
 - Zeitliche Abläufe



Xflow - Radialventilator



- https://www.youtube.com/watch?v=BnShaho5eQY&list=UUYMvQ8kW8 WoKjtl99jUNa1Q
- Veröffentlicht am 16.09.2014
- In this CFD-project of an industrial fan the rotation of the impeller geometry was easily modeled in detail and with real motion laws. The XFlow's particle-based approach avoids any compromises in the modeling of moving parts considering the highest fidelity Wall-Modeled Large Eddy Simulation (WMLES) approach to the turbulence modeling. The accuracy and the pressure increase was predicted with only 0.9% error by XFlow compared to measurements from the test bench.

Xflow - Radialventilator

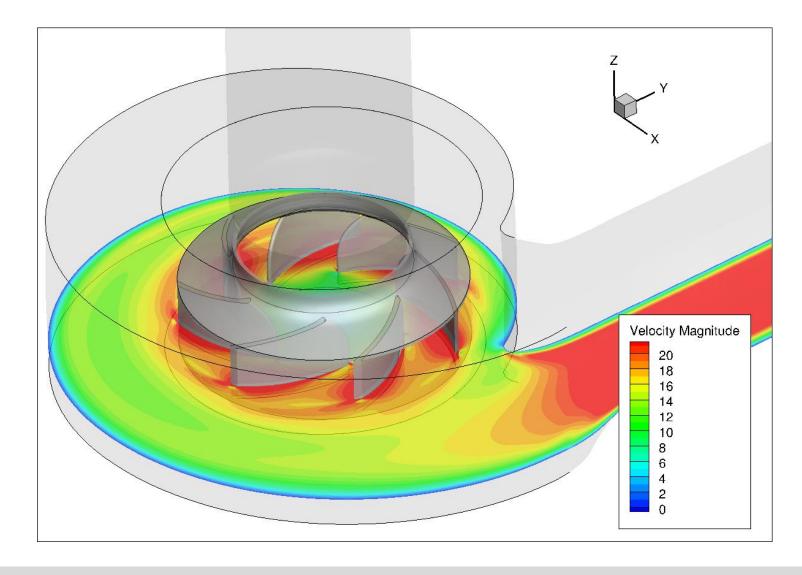






Radialventilator – Wand aufgelöst

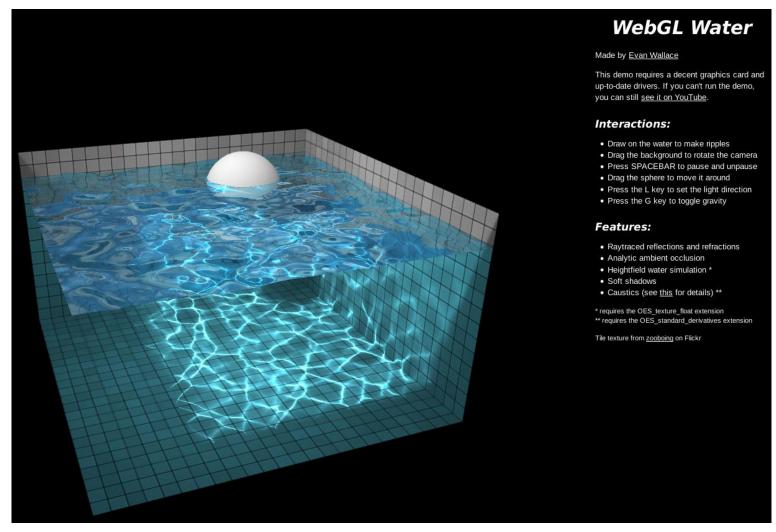






Was wird hier modelliert?





Quelle: madebyevan.com/webgl-water/

